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54 **Production of chloro-s-triazine triones and their use in cleansing or bleaching compositions.**

57 Chloro-s-triazine triones are used as a source of chlorine in cleansing and bleaching compositions. The usual method for the production of chloro-s-triazine triones comprises reacting cyanuric acid, an alkali metal hydroxide and chlorine in an aqueous reaction mixture from which the chloro-s-triazine trione crystallizes forming a slurry which is then filtered. The filtration characteristics of the slurry and the storage stability of the product are both affected by the form in which the chloro-s-triazine trione crystallizes from the aqueous reaction mixture, and improvements on prior art procedures are desirable. According to the present invention the reaction is carried out in the presence of a crystal modifier which is a disulfonic acid of an alkylated diphenyloxide wherein the alkyl group contains from 8 to 14 carbon atoms or a corresponding alkali metal disulfonate. A product having enhanced crystal properties and improved storage stability is obtained.

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PRODUCTION OF CHLORO-s-TRIAZINE TRIONES

The present invention relates to an improved process for manufacturing chloro-s-triazine triones which are sometimes referred to as chlorocyanuric acids or chloro-isocyanuric acids. More specifically, this invention

5. pertains to a method for preparing chloro-s-triazine triones, particularly trichloro-s-triazine trione, having enhanced crystal properties.

The preparation of chloro-s-triazine triones such as trichloro-s-triazine trione or dichloro-s-triazine trione
10. is well known in the prior art.

- One method for producing chloro-s-triazine trione is described in U.S. Patent No. 2,969,360. In this process, cyanuric acid is fed along with aqueous alkali metal hydroxide (in molar ratio of about one mole of alkali
15. metal hydroxide per atom of chlorine to be attached) and chlorine to an aqueous reaction zone which is maintained at a pH in the vicinity of 3.5. The feed ingredients are added in essentially stoichiometric proportions. The crude chloro-s-triazine trione precipitates from the
20. solution forming a slurry. The slurry is continually or periodically filtered to separate the crystalline product from the mother liquor and the crystalline product is dried.

- Prior art processes for producing chloro-s-triazine
25. trione have been beset with numerous difficulties attributable to deficient particles size. For example,

considerable variations in the rate of production have been experienced in the manufacture of trichloro-s-triazine trione due to difficulties in water removal which result in a slushy feed to the dryer. When very

5. wet or slushy product material reaches the dryer it may become necessary to reduce the production rate or to shut down the unit to avoid packaging wet trichloro-s-triazine trione. The primary cause for this problem is believed to be the very fine particle size produced

10. in the process.

The patent literature reports other problems attributable to small particle size such as those relating to product separation (filtration, washing and drying as well as those relating to handling of the final dusty

15. product. Furthermore, it is thought that the crystal properties of the chloro-s-triazine triones have substantial influence on the retention of bleaching strength in formulations containing such triones. Thus, particle size and particle clarity are believed to be important for

20. superior bleach stability.

It has been proposed heretofore in U.S. Patent No. 3,120,522 that chloro-s-triazine trione crystals having increased size can be produced by adding to the reaction mixture from which these crystals are formed, from 50 to

25. 1,000 ppm of a chlorinated hydrocarbon containing 1 to 6 carbon atoms and having not more than one hydrogen atom in its molecule.

It has further been proposed in U.S. Patent No. 3,453,274 that the crystal size of chloro-s-triazine

30. triones may be increased by adding, as a surface active agent, an alkali metal alkyl sulfate or an alkali metal alkylarylsulfonate wherein the aryl portion is phenyl or naphthyl, to the reaction mixture while maintaining a pH between 1.0 to 4.5.

35. U.S. Patent No. 3,941,784, teaches the crystal promotion of chloro-s-triazine trione by adding to the reaction mixture a small amount of polyoxyethylene,

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polyoxypropylene, or polyoxyethylene-polyoxypropylene copolymers.

In accordance with the present invention, chloro-s-triazine triones, in particular dichloro-s-triazine trione, 5. trichloro-s-triazine trione and mixtures thereof, having enhanced crystal properties and exhibiting outstanding stability when formulated with other chemicals in bleaching products, are obtained by the use of certain crystal modifiers during the manufacture of chloro-s-triazine triones. These 10. crystal modifiers are alkylated diphenyloxide disulfonic acids wherein the alkyl group contains from 8 to 14 carbon atoms, or their alkali metal salts. In these compounds, the sulphonic groups are attached to carbon atoms of the diphenyloxide nucleus.

15. It is preferred to add the crystal modifier to the reaction mixture in the form of the alkali metal disulfonate rather than in the acid form. The preferred alkali metal is sodium.

The mechanism by which the crystal modifiers used in 20. this invention achieve superior bleach stability in the product is not fully understood. However, as indicated above, one of the factors involved is believed to be the crystalline form of the product and the mechanism is therefore regarded as one of crystal modification and the additive is referred 25. to herein as a "crystal modifier".

Examples of crystal modifiers which can be used in the process of the invention are sodium octyl diphenyloxide disulfonate; sodium nonyl diphenyloxide disulfonate; sodium n-decyl diphenyloxide disulfonate; potassium n-decyl 30. diphenyloxide disulfonate; sodium dodecyl diphenyloxide disulfonate; octyl diphenyloxide disulfonic acid; dodecyl diphenyloxide disulfonic acid; sodium tridecyl diphenyloxide disulfonate; and potassium tetradecyl diphenyloxide disulfonate. A preferred crystal modifier for use herein is 35. sodium dodecyl diphenyloxide disulfonate. This disulfonate is commercially available. It can be obtained in liquid form as a 45-50% by weight concentrate, for example, from Dow Chemical Company under

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the trade name "Dowfax 2A1".

The preferred concentration of the crystal modifier used in the process of the present invention is 20 to 500 parts per million (ppm) by weight based on the reactor contents. Improvements can be achieved with these crystal modifiers at higher or lower concentrations, however. Most preferred are concentrations of from 100 to 300 ppm by weight based on the reactor contents.

A preferred procedure for the production of trichloro-s-triazine trione by the process of the invention, comprises mixing a slurry of substantially pure cyanuric acid with alkali metal hydroxide (e.g., sodium or potassium hydroxide, preferably the former), to prepare an aqueous solution in which the alkali metal hydroxide to cyanuric acid molar ratio is about 3:1. The solution is then fed continuously to a reactor to which chlorine and the crystal modifier are also fed continuously, while maintaining the temperature of the reactor contents at about 25°C. with a pH of about 3.5. Although the pH can vary between about 1.0 and 4.5, the range of 3.0 to 4.5 is preferable. The crystal modifier feed rate is adjusted to maintain the desired concentration of the crystal modifier in the reactor.

The product (trichloro-s-triazine trione) is withdrawn from the reaction as a slurry, then filtered, dried and packaged. When produced in this manner, the particles of trichloro-s-triazine trione are single, clear crystals of suitable size and structural integrity to exhibit outstanding bleach stability when formulated with other chemicals in bleaching and scouring compositions.

In certain circumstances it may be advantageous, in the above-described procedure, for the reactor to contain initially a small volume of water having at least a portion of the crystal modifier charge in solution.

It may also be desirable to introduce certain antifoaming agents during a continuous manufacturing process in order to offset any tendencies of the crystal modifiers

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to generate foam.

For certain applications, dichloro-s-triazine trione is the desired end product instead of trichloro-s-triazine trione. The former can be prepared in a manner similar to 5. that described above except that the feed solution can be prepared by mixing a cyanuric acid slurry with an alkali metal hydroxide to produce a solution having a hydroxide to cyanuric acid mole ratio of about 2.1:1. Chlorine is typically introduced at a rate sufficient to maintain a pH 10. in the range 2.1 to 2.3.

In drying the product of the process of the present invention, control of the drying conditions as for the drying of conventionally-produced chloro-s-triazine triones should be exercised. It is known, for example, that 15. trichloro-s-triazine trione exhibits a significant temperature dependence during the drying step. Desirably, trichloro-s-triazine trione should not be dried at temperatures which will cause the particles to exceed about 130°C.

20. An abrupt absorption of heat into the trichloro-s-triazine trione particle is usually observed when the particle temperature during the drying step is allowed to exceed about 130°C. The phenomenon associated with this temperature is sometimes referred to as "phase change".

25. Exceeding 130°C. particle temperature during drying of trichloro-s-triazine trione is generally accompanied by a reduced density of the dried particle after cooling. Furthermore, the reduced density of the particle after cooling is characterized by extension of the lattice in 30. the crystalline structure of the particle. It is therefore desirable to conduct the drying step associated with the process of this invention in a manner which maintains particle temperature during drying between about 80°C. and about 120°C., preferably about 95°C. to about 105°C.

35. The invention is illustrated by Example 3 of the following Examples. Examples 1 and 2 are comparative Examples. Parts and percentages are by weight unless

otherwise specified.

EXAMPLE 1

This Example illustrates a conventional preparation of trichloro-s-triazine trione wherein no crystal modifier or promoter is employed. A feed solution was prepared by mixing a cyanuric acid slurry with sodium hydroxide to produce a solution containing 7.6% cyanuric acid with a mole ratio of sodium hydroxide to cyanuric acid of 3.2:1. The chlorination reaction was provided for by a jacketed 10.1.4 litre glass reactor equipped with a stirrer, side arm for product overflow, subsurface feed tube and a fritted glass sparger. Starting with water in the reactor, feed solution was introduced through the feed tube at about 40 ml. per minute and chlorine was introduced through the 15. sparger at about 5.5 grams per minute. The pH was controlled in the range 3.5 to 3.8 by adjusting the chlorine feed rate, and the reaction temperature was controlled between 22° and 27°C. by circulating ice water through the reactor jacket. The product slurry, which overflowed the side arm, was 20. filtered to separate the crystalline product from the mother liquor, giving a filter cake containing 10 to 12% by weight free moisture, and was then dried in an oven at about 100°C. (The product was observed to settle slowly from the slurry).

EXAMPLE 2

25. This Example was conducted in a manner identical to that of Example 1 except for the presence of a crystal promoter within the scope of aforementioned U.S. Patent No. 3,941,784. The promoter employed was a polyoxyethylene-polyoxypropylene copolymer identified as 30. "Pluronic L-62" and available from BASF-Wyandotte Corporation. A feed solution identical to that of Example 1 was prepared. A chlorination was conducted as described in Example 1 except that 200 ppm (based upon the reactor contents) of polyoxyethylene-polyoxypropylene 35. copolymer was introduced to the reaction mixture. Part of this 200 ppm promoter addition was admitted to the initial reactor water charge and part was admitted to the feed

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solution. The resulting product in this case was observed to settle rapidly and was filtered to 4-5% free moisture.

EXAMPLE 3

This Example illustrates the preparation of tri-chloro 5.-s-triazine trione with the aid of a crystal modifier in accordance with the present invention. Example 3 was conducted in a manner identical to that of Example 1 except for the addition of 200 ppm, based upon the reactor contents, of sodium dodecyl-diphenyloxide disulfonate (as a 45% 10. concentrate in a liquid vehicle) to the reaction vessel. The resulting trichloro-s-triazine trione product exhibited outstanding clarity in the single clear crystals which were produced.

EXAMPLE 4

15. Dichloro-s-triazine trione can be prepared by a procedure similar to that of Example 3 using a feed solution prepared by mixing a cyanuric acid slurry with sodium hydroxide to produce a solution containing about 9.8% of cyanuric acid and having a sodium hydroxide to cyanuric acid mole ratio of 20. about 2.1:1, and introducing chlorine at about 7.1 grams per minute to maintain a pH in the range 2.1 to about 2.3.

EXAMPLE 5

In this comparative Example, trichloro-s-triazine trione was prepared by a procedure similar to that of 25. Example 3, but using 200 ppm of a sodium (C₁₄ alkyl)benzene sulfonate, an example of the alkali metal alkylarylsulfonates disclosed in U.S. Patent 3,453,274, instead of sodium dodecyl diphenyloxide disulfonate.

Particle size comparisons were made on the respective 30. dried products from Examples 1, 2, 3 and 5 above. In a first test on the products of Examples 1, 2 and 3, apparent particle size, on a relative basis, was ascertained by observing the cumulative weight percent of product retained on a screen having a predetermined number of meshes per unit 35. length.

The unmodified, unpromoted product of Example 1 exhibited the smallest apparent particle size. The product

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of Example 2, although exhibiting an apparent size greater than that of Example 3 in screen measurements, is suspected of undergoing size attrition during certain conditions of handling in compounding operations sometimes employed to formulate cleansing and bleaching compositions referred to hereafter. Moreover, it will be seen from the chlorine stability testing described below that apparent particle size is not the sole factor determining stability.

In a second test, the relative particle sizes of the dried products of Examples 3 and 5 were determined using a screen having a mesh aperture of 0.074 mm. 95 percent of the product of Example 3 was retained on the screen, whereas only 62 percent of the product of Example 5 was retained, showing that the product made according to the process of the invention had a significantly lower percentage of particles smaller than 0.074 mm.

Bleach stability of cleansing compositions containing chloro-s-triazine triones is customarily determined by measuring the percentage of available chlorine remaining in the cleansing composition following a predetermined number of days exposure of the composition to ambient conditions. One such aging test calls for the placement of the cleansing composition in half-filled canisters and exposing the canisters to air at 80°F. (26.7°C.) and 80% relative humidity with both open and closed tops on the canisters.

Chlorine stability results with the product of Example 1 were substandard and unacceptable for commercial cleansing compositions. The following Table compares the chlorine stability of the products of Example 2 and Example 3. It will be seen that the single clear crystal of the product of Example 3, although of smaller apparent particle size than that of Example 2 according to screen measurements, is nonetheless a superior product from the standpoint of chlorine stability. The data in the Table were obtained following the typical aging test described above, using open top canisters, using typical cleansing formulations containing 80-85 percent of an abrasive and 0.5-1 percent

of the trichloro-s-triazine trione, the balance being an alkaline builder.

5.	Formulation Exposure (days)	Available Chlorine Remaining (%)	
		Example 2	Example 3
10.	8	78	82
	10	69	79
	12	61	77
	14	54	74
	16	47	72
	18	40	70

From these results, it can be seen that the use of sodium dodecyl diphenyloxide disulfonate according to the process of the invention contributes significantly to available chlorine stability of the product.

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CLAIMS

1. A process for the production of dichloro-s-triazine trione, trichloro-s-triazine trione or a mixture thereof by the reaction of cyanuric acid with an alkali metal hydroxide and chlorine in an aqueous reaction mixture containing a substance ("crystal modifier") which improves the form of the chloro-s-triazine trione product which precipitates from the reaction mixture, and recovering the chloro-s-triazine trione product from the reaction mixture, characterized in that the crystal modifier is an alkali metal disulfonate of an alkylated diphenyloxide wherein the alkyl group contains from 8 to 14 carbon atoms, or an alkylated diphenyloxide disulfonic acid wherein the alkyl group contains from 8 to 14 carbon atoms.
2. A process according to Claim 1 characterized in that the crystal modifier concentration in the aqueous reaction mixture is from 20 to 500 parts per million by weight.
3. A process according to Claim 2 characterized in that the crystal modifier concentration in the aqueous reaction mixture is from 100 to 300 parts per million by weight.
4. A process according to any of Claims 1 to 3 characterized in that the crystal modifier is a sodium disulfonate of a said alkylated diphenyloxide.
5. A process according to any of Claims 1 to 3 characterized in that the crystal modifier is sodium dodecyl diphenyloxide disulfonate, sodium n-decyl diphenyloxide disulfonate, or dodecyl diphenyloxide disulfonic acid.

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6. A cleansing or bleaching composition containing a chloro-s-triazine trione characterized in that the chloro-s-triazine trione is dichloro-s-triazine trione, trichloro-s-triazine trione or a mixture thereof that has been
5. produced by a process according to any of Claims 1 to 5.



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DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
D, A	US - A - 3 453 274 (J.M. MURRIN et al.) * Claim 1 *	1	C 07 D 251/36 D 06 L 3/06
			TECHNICAL FIELDS SEARCHED (Int. Cl.)
			C 07 D 251/36
			CATEGORY OF CITED DOCUMENTS
			X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
			&: member of the same patent family, BAD ORIGINAL corresponding document