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EUROPEAN PATENT APPLICATION

21 Application number: 78300834.5

51 Int. Cl.²: **H 01 R 7/00**
H 05 B 7/103

22 Date of filing: 15.12.78

30 Priority: 16.05.78 GB 1996078
16.11.78 GB 4476178

43 Date of publication of application:
28.11.79 Bulletin 79/24

84 Designated Contracting States:
CH DE FR GB IT SE

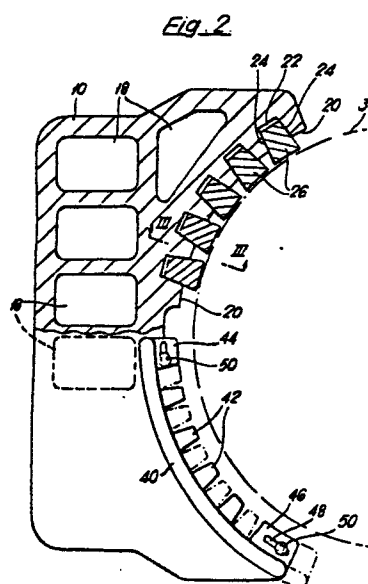
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54 Electrical contact assembly.

57 An electrical contact assembly between two conducting elements disposed face to face comprises wedge-shaped graphite inserts (26) located in similarly shaped grooves (22) in one of the faces (20). One end of each insert (26) lies short of the end of the groove (22) and the other end is proud of the face (20), so as to make good electrical contact with the other face (34) when the two faces (20, 34) are pressed together. The invention achieves good electrical contact and conduction of current in applications where this has proved difficult in the past. Particular examples are clamps for graphite electrodes and connections to steel billets used as electrodes in an electro slag refining process.



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"Electrical Contact Assembly"

The present invention relates to contact assemblies and seeks to provide a contact assembly which will give an adequate electrical contact between two conducting elements disposed in face to face relationship and which will permit satisfactory passage of electricity
5 and heat without demanding impracticably fine tolerances in manufacture of the various parts.

There are various applications in which electrical currents must be passed between two opposed faces which
10 are clamped together or biassed towards each other by spring force or gravity or the like, a particular and important example being the feeding of electrical current to an electrode.

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Clamps for cylindrical graphite electrodes, such as are used on an electric arc furnace, are normally made from cast or wrought copper and often include passages for water cooling.

5 In recent years, and in order to reduce the consumption of the graphite electrode, a technique has been developed of coating the graphite with aluminium and a large number of electric arc furnaces have been converted to use the aluminium coated type of electrodes. This
10 has produced the result that, whereas previously a direct copper contact was satisfactory between the clamp and the electrode, a different system had to be devised for the aluminium coated electrode, because it is impracticable to make contact between copper and aluminium, particular
15 in hot conditions.

For this reason the present practice is to provide the electrode clamp with two graphite pads to give the required electrical contact between the clamp and the coating of the electrode.

20 This has given rise to disadvantages in that the large surface areas of both the curved and the flat face demand a high degree of dimensional and angular accuracy which is vital in order to achieve good electrical and thermal transfers. In practice it is found that the tolerances of the various parts cannot be kept within such
25 strict limits as to ensure good contact surfaces. Furthermore, it is difficult to ensure dirt is not trapped

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between the copper and the graphite insert. This in turn results in a poor transfer of heat and in arcing, and this in turn damages the copper electrode clamp.

Another type of connection is to be found in the
5 electro slag refining process, where the electrode is constituted by a steel billet. Electric current is fed to this billet through a stainless steel pad which is welded onto the top of a stainless steel bar which in turn is welded to the top of the billet. The stainless
10 steel pad is supported on a fork which carries the weight of the assembly and through which the vertical height can be controlled so that an arc is maintained on the bottom of the electrode.

At the present time, in order to connect one phase
15 of the electrical supply to each of the three billets representing the three electrodes, a copper stub clamp is used which is shaped to form two-line contacts with the top face of the stainless steel pad and which is mechanically loaded with approximately nine tons to
20 maintain the necessary electrical contact between the copper stub clamp and the steel pad and also to retain the pad securely on the fork. Owing to the relatively low conductivity of stainless steel, it is often found that when a large current is applied between the line-
25 contacts of the stub clamp and the surface of the stainless steel pad, there is local over-heating and subsequent damage to the contact faces.

The present invention, inter alia, enables a more efficient system for electrical supply to both these different types of electrode.

According to the present invention we provide a
5 contact assembly capable of passing large electrical currents, the assembly comprising two conducting elements disposed face to face, a plurality of insert-receiving grooves in one of the faces, each groove having opposed side walls which converge away from the face, a plurality
10 of wedge-shaped graphite inserts in the grooves, each insert being shaped to fit between the convergent walls of a groove, leaving one end of the insert spaced from the end of the groove and the other end of the insert proud of the said one face, the said other end of the
15 insert being of a shape to make electrical contact with the other of the faces, and means whereby the two conducting elements press towards each other giving good electrical contact between the graphite inserts and the
20 two conducting elements and thereby a path for the electrical current from one conducting element to the other through the graphite inserts.

It is preferred that at least four carbon inserts be used. The wedge angle between the side walls of the grooves and of the graphite inserts should be such as to
25 give sufficiently firm pressure between the graphite inserts and the sides of the groove on the one hand and the said other of the faces on the other hand to provide

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adequate electrical contact between these parts, whilst permitting slight movement of the inserts under pressure to take up any inaccuracies in the said other of the faces.

The invention will now be described in further
5 detail with reference to the accompanying drawings, wherein:

Fig. 1 is a perspective view of an electrode clamp for a cylindrical graphite electrode as at present employed;

Fig. 2 is a plan view, the top half in section, of one form of clamp for a graphite electrode incorporating
10 a contact assembly according to the present invention;

Fig. 3 is a section on the line III-III of Fig. 2;

Fig. 4 is a side view and end view of one of the graphite inserts of the clamp;

Fig. 5 is a side view of the upper end of the
15 support and contact for an electrode billet for the electroslag refining process, showing the electrical connection thereto, being a contact assembly according to the present invention; and

Fig. 6 is a plan view thereof.

20 Fig. 1 shows a clamp of known type consisting of a copper cast body 10 provided with a bus tube connection 16 and having conduits 17 to lead water to and from water-cooling passages, which are not shown in this figure but may be the same as those illustrated in Fig. 2. Two
25 graphite pads 12 are held by top and bottom retaining plates 14 and lie within machined recesses in the body 10.

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The rear face of each of the graphite pads 12 is plane, whereas the front face is curved to the radius equivalent to the radius of the electrode which is to be clamped and the two graphite pads when in position having a common
5 axis for the radii of the curved surfaces.

The clamps illustrated are used with a clamping band to grip the cylindrical graphite electrodes; in other forms of construction more than one clamp may be arranged around the electrode with a suitable mechanism
10 to cause the clamp segments to grip the electrode. However, as previously explained, trouble has been caused through high resistance contact, arcing and poor heat transference from the electrode.

Figs. 2 and 3 show an electrode clamp according to
15 the present invention. The body 10 of the clamp is made from cast copper with the usual bus tube connection 16 and is provided with water passages 18, the construction of which will be well-known to those skilled in the art.

The body 10 is formed with ten longitudinal, vertical grooves 22 in its cylindrical electrode clamping face
20 20. The side walls 24 of each groove are planar and form between them a small included angle so that each groove is a wedge-shaped recess. In each recess is placed a graphite insert 26, as shown in the upper part of Fig.2. Each
25 insert, seen in detail in Fig. 4, is similarly wedge-shaped to the grooves 22 with side faces 28 having the

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same included angle as the side walls 24 of the groove. The rear face 30 can be planar and the front face 32 given a curved surface of the same radius as the outer surface of an electrode which is to be clamped. An outline of part of such an electrode is shown in broken lines at 34 in Fig. 2. The ends 36 of the inserts are chamfered, so that the inserts can be held in position by a bottom retainer 38 made of non-magnetic steel and upper aluminium bronze retainers 40.

10 When the clamp is to be used for clamping an electrode, the inserts 26 are comparatively loosely wedged in the wedge-shaped grooves 22. When clamping pressure is applied between the clamp shown in Fig. 2 and a clamping band on the other side which is not illustrated, the
15 clamping pressure between the clamp and the electrode forces the inserts 26 into their respective grooves and creates good electrical contact on the one hand between the electrode and the inserts and between the inserts and the clamp.

20 The function of the bottom and top retainers 38 and 40 is of course to hold the inserts in position before clamping pressure is applied. As seen in Fig. 2 there are two top clamps 40, each comprising an aluminium bronze member which is cast with four inwardly directed fingers
25 42 and two inwardly directed flanges 44,46 at the ends, these flanges having slots 48 which enable the retainer to be held in position under spring loading from headed bolts 50 screwed into the clamp body 10.

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Of the five graphite inserts 26 which are retained by each retainer 40, four of the inserts are held by the fingers 42 and one by the end flange 46. When it is desired to remove one of the inserts, it is only necessary
5 to slide the upper retainer so that the fingers 42 on the one hand and the flange 46 on the other hand move away from the top of the respective inserts, after which the insert can be removed by inserting a suitable instrument behind it, i.e. between the rear of the insert and the
10 end of the groove, and wedging the insert outwards.

The included wedge angle between the side walls 24 of the grooves 22 and the side faces 28 of the inserts 26 should be sufficiently high to ensure the adequate contact which is required and sufficiently low to permit
15 the slight movement which is necessary when the clamping is effected. In theory the optimum angle might well differ as between the grooves which are nearer the centre of the clamp and those which are nearer the two ends, since any movement of the clamp towards the electrode will
20 cause greater movement of the central insert than those at the ends. On the other hand, it would be a disadvantage of having different wedge angles that the inserts would not be interchangeable from one groove to another. At present we prefer to have the same angle for each of the
25 grooves and an included angle of 14° has been found to be satisfactory with one particular grade of graphite.

As can be seen from Fig. 2, the effect of the wedge-shaped inserts is to provide a large contact surface with the electrode where the larger front faces 32 of the inserts contact the outer periphery of the electrode. It
5 can be readily seen that the clamp which is shown in the drawings could be made with a smaller number of larger inserts or a larger number of smaller inserts. Where there are a large number of inserts it may even be found unnecessary to form the front surfaces with a cylindrical
10 surface.

Fig. 5 shows the upper end 52 of a stainless steel bar which is welded to the top of the steel billet (not shown) which becomes an electrode in the electro slag refining process. To the upper end of the stainless steel
15 bar 52 is welded a stainless steel pad 54 which is 50 mm in height, 356 mm in length and 240 mm in breadth. Four wedge-shaped grooves 58 are located lengthwise through the upper face 56 of the bar 54 and in each of these grooves is a wedge-shaped insert 60. As with the arrangement of
20 Figs. 2 to 4, the inserts 60 have their lower end spaced from the end of the groove and the upper end proud of the face 56 as seen in Fig. 5. In this case the electric supply is from a stub clamp the underface of which is flat (this stub clamp being indicated as 62 in chain lines in
25 the drawings) and in consequence the upper end of each insert 60 presents a flat face to register with the flat bottom face of the stub clamp. When pressure is applied

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to the stub clamp in order to weigh it down onto the pad
54, good electrical contact is made with the inserts 60;
if any of these are initially standing proud of the others,
the effect of the clamping pressure is to push it down
5 into its groove so as to level out the top surfaces to
the level of the lower face of the stub clamp whilst
maintaining excellent electrical contact both with the
stub clamp and with the pad 54.

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CLAIMS :

1. A contact assembly capable of passing large electric currents between two conducting elements disposed face to face characterized by a plurality of insert-receiving grooves in one of the faces, each
5 groove having opposed side walls which converge away from the face, a plurality of wedge-shaped graphite inserts in the grooves, each insert being shaped to fit between the convergent walls of a groove, leaving one end of the insert spaced from the end of the groove
10 and the other end of the insert proud of the said one face, the said other end of the insert being of a shape to make electrical contact with the other of the faces, and means whereby the two conducting elements press towards each other giving good electrical contact
15 between the graphite inserts and the two conducting elements and thereby a path for the electrical current from one conducting element to the other through the graphite inserts.

2. A contact assembly according to claim 1 having
20 at least four graphite inserts.

3. A contact assembly according to claim 1 or claim 2 wherein the wedge angle between the side walls of the grooves is such as to give sufficiently firm pressure between the graphite inserts and the sides of
25 the groove on the one hand and the said other of the faces on the other hand to provide adequate electrical

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contact between these parts, whilst permitting slight movement of the inserts under pressure to take up any inaccuracies in the said other of the faces.

4. A contact assembly according to claim 3 wherein
5 the said wedge angle is approximately 14° .

5. A contact assembly according to any one of the preceding claims wherein the two conducting elements are the curved body of a clamp and the rounded surface of an electrode held by the clamp.

10 6. A contact assembly according to claim 6 wherein the electrode is a cylindrical graphite electrode.

7. A contact assembly according to claim 6 wherein the graphite is coated with aluminium.

15 8. A contact assembly according to any one of claims 1 to 4 wherein the two conducting elements are a contacting element attached to a steel billet forming an electrode and a clamp biased towards said contacting element.

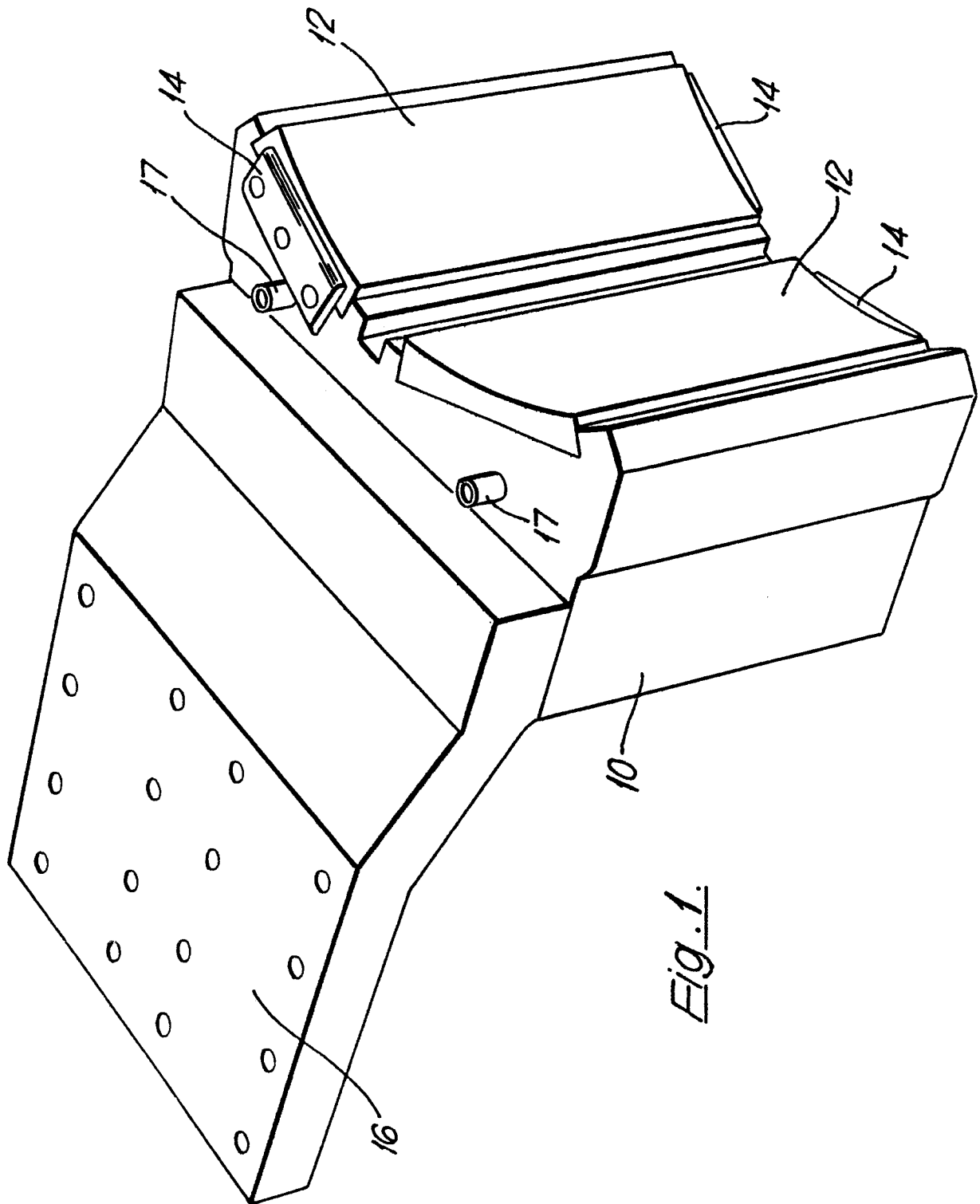
*Fig. 1.*

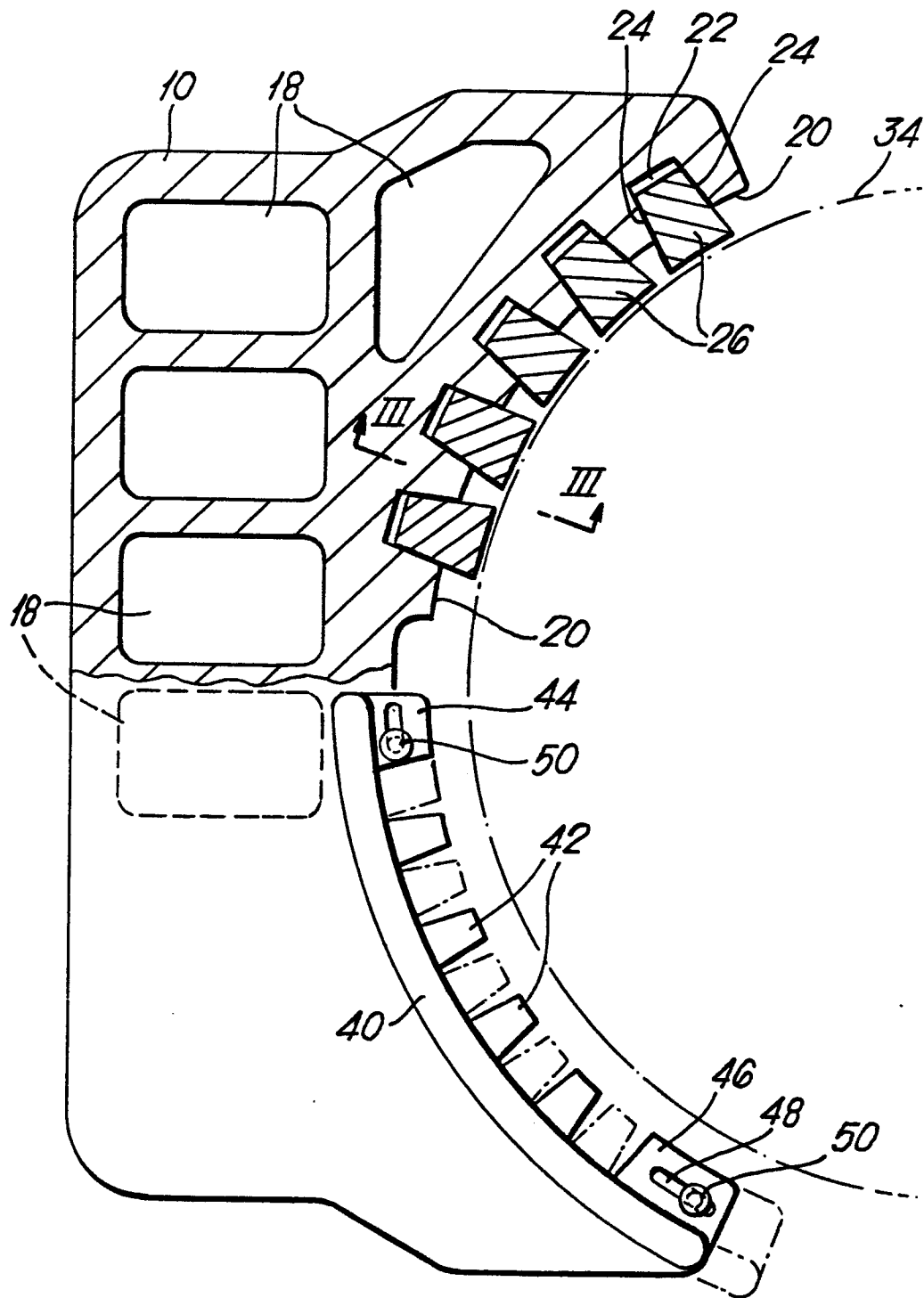
Fig. 2.

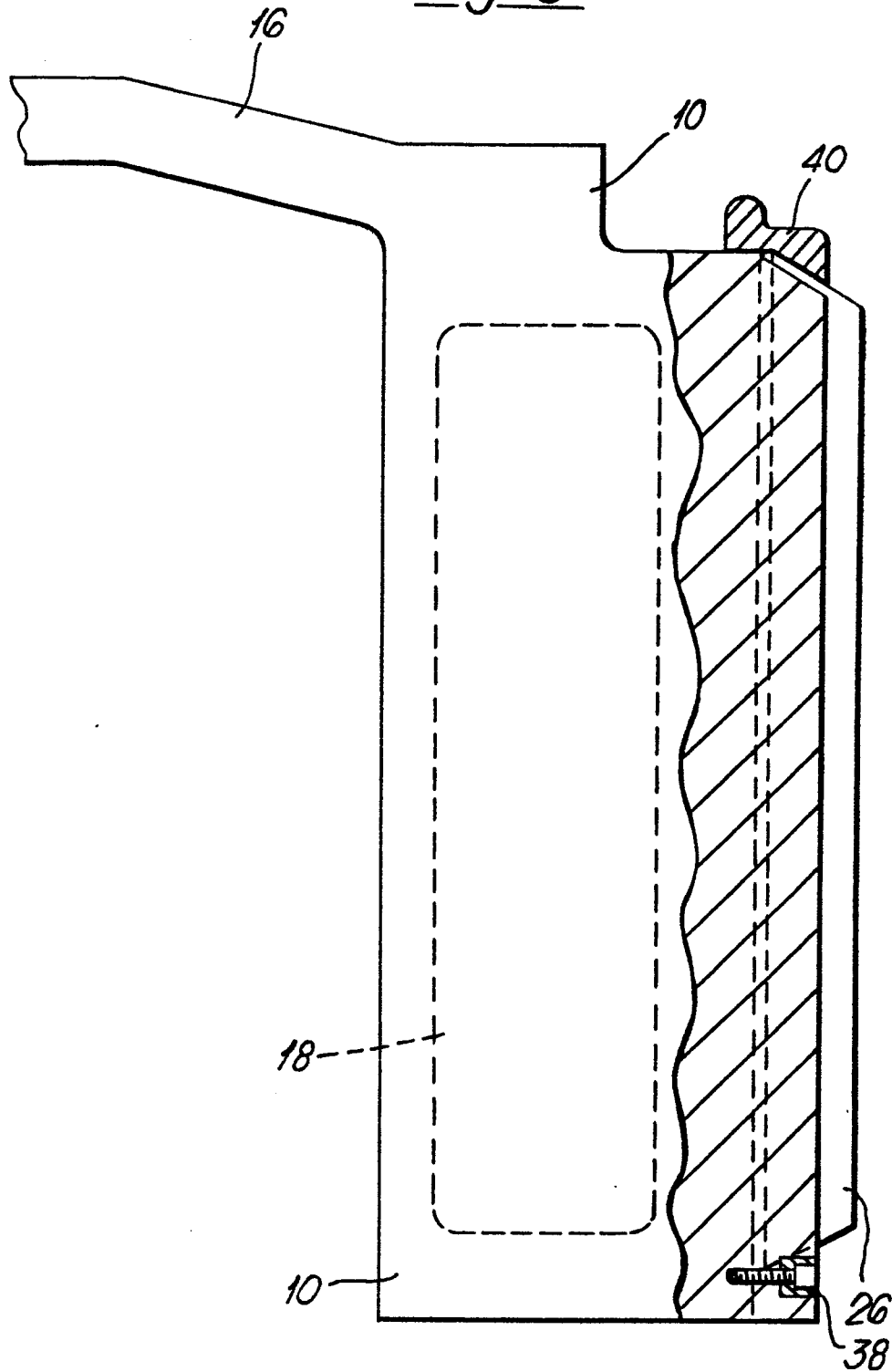
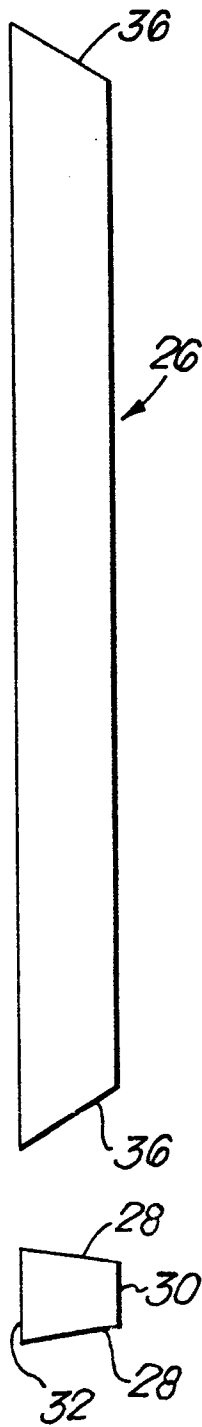
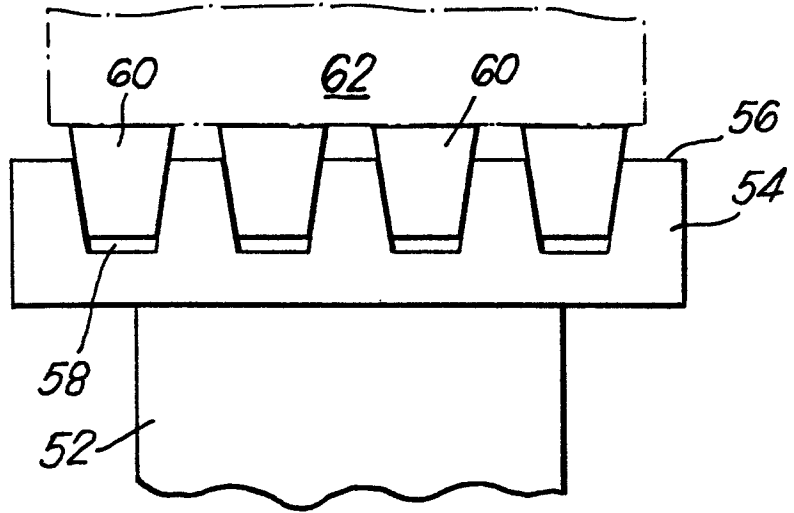
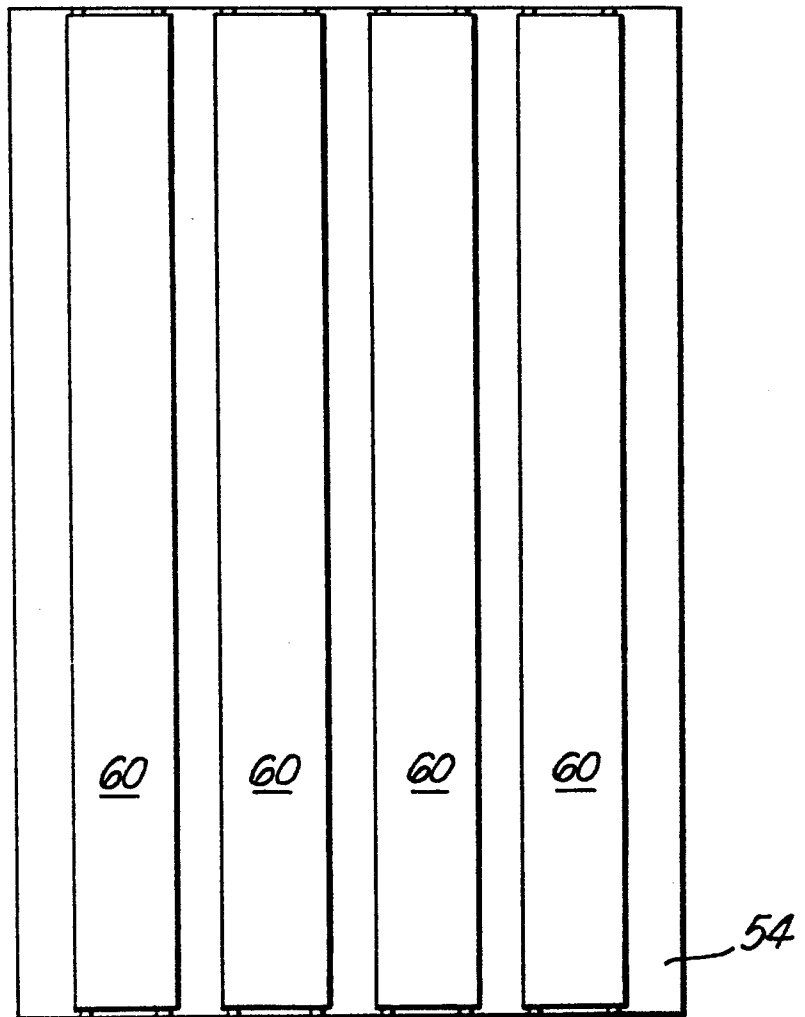
Fig. 3.

Fig. 4.*Fig. 5.**Fig. 6.*



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EUROPEAN SEARCH REPORT

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Application number

EP 78 30 0834

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. ²)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	<p><u>DE - C - 545 793</u> (DET NORSKE AKTIESELSKAB FOR ELEKTROKEMISK INDUSTRI)</p> <p>* Page 2 *</p> <p>---</p> <p><u>DE - A - 1 758 294</u> (VALTSHEV)</p> <p>* Pages 1-8 *</p> <p>---</p> <p><u>DE - C - 429 619</u> (SIEMENS)</p> <p>* Page 2, lines 89-112; figure 5 *</p> <p>---</p> <p><u>US - A - 2 834 824</u> (OHIO FERRO-ALLOYS)</p> <p>* Column 3, lines 12-75; column 4; column 5, lines 1-25 *</p> <p>---</p> <p><u>GB - A - 693 068</u> (A.G. STICKSTOFF-DUENGER)</p> <p>* Page 1, lines 9-94; page 2; page 3, lines 1-68 *</p> <p>---</p> <p><u>CH - A - 99 868</u> (FRIDERICH)</p> <p>* Page 2, left-hand column, paragraphs 4-6; right-hand column *</p> <p>---</p> <p><u>MACHINE DESIGN</u>, vol. 36, no. 9, April 9, 1964, Cleveland, Ohio, USA, L.F. SIMBECK et al. "7 methods ./. "</p>	<p>1,5,6</p> <p>1,5-7</p> <p>1,3</p> <p>1</p> <p>1</p> <p>1</p>	<p>H 01 R 7/00 H 05 B 7/103</p> <p>TECHNICAL FIELDS SEARCHED (Int.Cl.²)</p> <p>H 01 R 7/00 9/00 11/00 39/26 39/39 H 05 B 7/10 7/101 7/103 7/105</p> <p>CATEGORY OF CITED DOCUMENTS</p> <p>X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons</p> <p>&: member of the same patent family, corresponding document</p>
<p><input checked="" type="checkbox"/> The present search report has been drawn up for all claims</p>			
Place of search		Date of completion of the search	Examiner
The Hague		21-02-1979	LOMMEL



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Application number
EP 78 30 0834

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DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	for fastening carbon and graphite parts", pages 147-150 * Page 147; page 148, left-hand column, paragraphs 1-4 *		
			TECHNICAL FIELDS SEARCHED (Int. Cl.)