

(12)

**EUROPEAN PATENT APPLICATION**

(21) Application number: **80106677.0**

(51) Int. Cl.<sup>3</sup>: **H 01 P 5/02**  
**H 01 P 7/08**

(22) Date of filing: **31.10.80**

(30) Priority: **05.11.79 IT 6914879**

(43) Date of publication of application:  
**13.05.81 Bulletin 81/19**

(84) Designated Contracting States:  
**DE FR GB NL**

(71) Applicant: **CSELT Centro Studi e Laboratori  
Telecomunicazioni S.p.A.  
Via Guglielmo Reiss Romoli, 274  
I-10148 Turin(IT)**

(72) Inventor: **Scudellari, Antonio  
Via Don Minzoni, 99  
Ravenna(IT)**

(74) Representative: **Riederer Freiherr von Paar zu Schönau,  
Anton  
Müllerstrasse 31  
D-8000 München 5(DE)**

(54) **Stub for matching microstrip circuits.**

(57) Introduction of a minimum redundancy into a microstrip stub for microwave circuits allowing reversibility of adjustment, always operating in the same manner, that is by only removing or by only adding conductive material.

**EP 0 028 403 A1**

./...

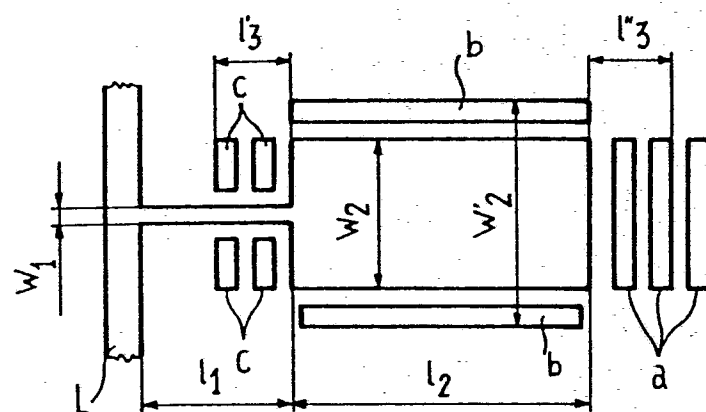


Fig.1

Stub for Matching Microstrip Circuits

1           The present invention relates to microwave circuits implemented by the so called microstrip technology and more particularly it concerns a stub for adjusting microstrip circuits.

          One of the fields in which microstrip stubs can be used is  
5 the measurements of characteristics of the active components.

          In fact to obtain the complete description of an active microwave device often it is not enough to effect on it just the measurement of the known diffusion parameters  $S$ , whose determination requires no adjustment.

10           In a number of cases it is necessary to connect at the input and at the output of the active device apparatuses able to introduce arbitrary variations in the impedances they present at the active device.

          This is valid for instance in the case of noise-figure measurement at the variation in the input impedance or in case of optimum  
15 input-output impedances measurement to check the operation of a power device of non-linear type.

          It would be of course preferable to effect such variations directly on the microstrip circuits containing the active device; but this is not convenient due to the typical irreversibility of microstrip  
20 matching devices.

- 2 -

1           In fact once the adjustment circuit has been modified, values prior to the adjustment cannot be recovered.

          This difficulty is generally overcome by means of coaxial cable matching devices, provided that the transition from microstrip  
5 to coaxial-cable has taken place.

          The inconvenience of the measurement method effected by means of coaxial matching devices resides in that a dismembering must be effected of component holder to measure the unknown impedance.

          A further field in which microstrip stubs are generally used  
10 is the implementation of amplifiers, oscillators, mixers and others. For these devices direct adjustment is generally required of the matching networks, stubs enclosed, to compensate for the unavoidable parameter losses characterizing the active components (as commercially available) and to compensate for possible parasitic parameters of passive  
15 circuitry.

          Such adjustment is critical when the active components must be pushed beyond their threshold of power dissipation; certain load impedances, in fact where imprudently varied can give rise to a breaking of the active components to which they are connected. These dangers  
20 are often present in microstrip circuit embodiments as the known stubs, not being of reversible type, must be precalibrated with values in excess so as to allow the progressive approximation for reduction to required operation conditions.

          In fact operating on a microstrip in the microwave range  
25 (bands X, K<sub>u</sub>, etc. ....), the usually method used for the circuit adjustment consists in removing the conductive material forming the microstrip; said removal is generally obtained through a laser beam, as the required precision in the adjustment is very high.

          Otherwise many active power components require for conjugated matching a very low impedance, but they do not tolerate short  
30 circuit conditions.

- 3 -

1           Operating by laser removing technique, the main inconvenience is that of acting only by removing the material without any recovery, if the removal was too severe.

          Obviously, the determination of the optimal condition can  
5 be obtained only by verifying worse performances beyond that condition.

          That is why it is necessary to dispose of microstrip stubs of the reversible type, that is such as to allow easy scanning about the optimal condition.

          Otherwise, in the superior microwave range, this revers-  
10 ibility cannot simply be obtained by adding other material after the removal of conductive material, since: above all the precision that could be achieved by adding further material would be poor, besides a much varied structure would result with respect to the original one with subsequent increased losses; finally such corrective material addition, necessarily requiring manual intervention, would not allow the automatic  
15 calibration process.

          Operating always in microstrip in the lower microwave range (bands L, C) an adjustment method alternative to the one previously described of laser removal, is the one of providing while  
20 planning a certain number of areolae of conductive material at the edges of metalized strips of microstrip and duly connecting a certain number to the main strip to the attainment of the required conditions.

          In this case due to the rather low frequencies these connections do not present serious problems.

25           From the literature it is not clear how the reversibility can be obtained by utilizing said areolae method.

          These and other problems of the present invention will be solved by a method devised to obtain the reversibility in stub microstrip adjustment modalities, that by introducing minimum redundancy in the  
30 stub topology allows this reversibility and optimal operation conditions to be obtained, operating always in the same direction, that is by the

1 only removal of conductive material, for instance by means of laser,  
or by the only addition of conductive material by means of areolae meth-  
od.

Another characteristic of the present invention resides in  
5 the fact that said slight added redundancy can be positively utilized by  
interpreting the stubs realized in that way as elements of abroad band  
matching network or by sending a polarization through a choke connect-  
ed to a short-circuit section of the stub.

It is a particular object of the present invention a stub for  
10 the adjustment of microstrip circuits consisting of two cascaded lines,  
the second of which having a length comprised between  $1/4$  and  $1/2$  of  
the used wavelength.

These and other characteristics of the present invention  
will become clearer from the following description thereof of a partic-  
15 ular embodiment of the same, taken by way of example and not in a lim-  
iting sense in connection with the annexed drawings in which.

- Fig. 1 is the most general version of a symmetrical reversible stub  
of the type with metalization addition (method of areolae);
- Fig. 2 is the equivalent scheme of the stub depicted in Fig. 1;
- 20 - Fig. 3 is a particular asymmetrical case of the reversible symme-  
trical stub depicted in Fig. 1 in which there are just two series of  
aereolae, one for carrying out the lengthening and the other one  
the short ening;
- Fig. 4 is the complementary version of the stub of Fig. 3 as the short-  
25 enning and the lengthening operations are effected not by addition but  
by removal of conductive material;
- Fig. 5 is, analogously to Fig. 4, the complementary version of the  
stub of Fig. 1;
- Fig. 6 represents an intermediate adjusting method between the one  
30 depicted in Fig. 1 and that of Fig. 5.

Fig. 1 shows the typical form of a symmetrical reversible  
stub; it consists of two cascaded lines, the first, connected to main line

- 5 -

1 L, has high characteristic impedance, and the second, left in open circuit, has low characteristic impedance.

References  $w_1, l_1$  denote respectively the width and the length of the first line prior to adjustment; references  $w_2, l_2$  denote  
5 respectively the analogous values of the second line prior to adjustment.

Reference  $l''_3$  denotes the lengthening of the second line at the open end; reference  $l'_3$  denotes the lengthening of the second line at the end of the connection with the first line, that then corresponds also  
10 to a shortening of the first line.

Reference  $w'_2$  denotes the widening of the microstrip relating to the second line.

References a, b, c denote some areolae placed in advance while planning the microstrip in suitable number and size, to carry out  
15 the required adjustments.

In the equivalent circuit of Fig. 2 reference  $Y_0$  denotes the characteristic admittance of the main line L of Fig. 1.

References  $Y_1, l_1$  denote the characteristic admittance and the length of the first line  $w_1, l_1$  prior to adjustment; references  $Y_2, l_2$  denote the analogous values of the second line  $w_2, l_2$  always before  
20 adjustment.

In Fig. 3 references L,  $l_1, l_2, l'_3, l''_3, w_1, w_2$  denote the same values as in Fig. 1.

Reference a denotes the same areolae as in Fig. 1; reference  
25 c' denotes the areolae that correspond, in the asymmetric version, to those denoted by a in the symmetric version of Fig. 1.

In Fig. 4 references L,  $l_1, l_2, w_1, w_2$  denote the same values as in Fig. 1.

References  $l'_4, l''_4$  denote areas of conductive material that  
30 can be partially or totally removed to realize the wanted adjustments.

In Fig. 5 the ordinary configuration of the microstrip is the same as in Fig. 1; the dotted lines denoted by d, e, f, represent areas

1 of conductive material that can be removed while adjusting.

References  $l_1$ ,  $l_2$ ,  $w_1$ ,  $w_2$  denote the same values as in  
in Fig. 1.

In Fig. 6 references a, b, c denote the same areolae as in  
5 Fig. 1, but this time during the planning they have not been plotted  
outside of (as they have in Fig. 1), but they have been plotted inside the  
original configuration of the microstrip and have been subsequently  
covered with conductive material (dotted zone) easy to remove, for  
instance by a sharpened stylus. References  $l_1$ ,  $l_2$ ,  $w_1$ ,  $w_2$  denote the  
10 same values as in Fig. 1.

With reference to the annexed drawings, the function will  
be now described of the adjusting method of the stub, object of the in-  
vention.

With reference to the generalized version with metalizing  
15 addition in Fig. 1, the initial equivalent circuit is the one of Fig. 2.

By adding to a second line ( $l_2$ ,  $w_2$ ) areolae of type a, length  
 $l_2$  is increased by an entity that, for instance, in case the two first  
areolae of type a were incorporated is equal to  $l''_3$ , i. e. passing from  
length  $l_2$ , to  $l_2 + l''_3$ .

20 By adding to second line ( $l_2$ ,  $w_2$ ) some areolae of type b,  
width  $w_2$  increases; in case for instance both areolae b represented in  
Fig. 1 were incorporated one would pass from width  $w_2$  to  $w'_2$ : charac-  
teristic admittance  $Y_2$  of Fig. 2 increases accordingly.

By adding to the second line ( $l_2$ ,  $w_2$ ) areolae of type c,  
25 length  $l_2$  increases, for instance in the case depicted in Fig. 1, by  $l'_3$   
and  $l_1$  diminishes by the same value.

Let us consider now the known expression of the input ad-  
mittance B, normalized with respect to  $Y_0$

$$jB = j\left(\frac{Y_1}{Y_0}\right) \frac{\tan \beta l_1 + \left(\frac{Y_2}{Y_1}\right) \tan \beta l_2}{1 - \left(\frac{Y_2}{Y_1}\right) \tan \beta l_1 \cdot \tan \beta l_2} \quad (1)$$

30 in which  $\beta$  is the phase constant, considered as equal, in the two mi-

1 crostrip lines. The expression (1) is for instance reported in "Founda-  
 tion for Microwave Engineering" by R. Collin, Chapter 5. New York  
 Mc Graw - Hill, 1966.

From (1) it derives that when  $l_2$  increases (for instance by  
 5  $l'_3$ ),  $B$  increases; but if  $\tan \beta l_2 < 0$  (that is if  $\frac{\lambda}{4} < l_2 < \frac{\lambda}{2}$ , being  $\lambda$   
 the microstrip wavelength),  $B$  decreases when  $Y_2$  increases or when  
 $l_2$  increases, for instance by  $l'_3$  (and correspondingly  $l_1$  decreases by  
 the same value).

Consequently, while connecting areolae of type a there is  
 10 an increase in electric length (as it happens in case of a single line  
 stub), incorporating areolae of type a and b everything works as if the  
 stub electric length decreased.

The same reversibility property is present if the remov-  
 ement operation of conductive material was taken into consideration  
 15 instead of area conglobation.

In fact, by considering (1) again it can be seen from Fig. 5  
 that when the conductive material is removed from side d (that is when  
 $l_2$  decreases)  $B$  decreases, but if  $\tan \beta l_2 < 0$   $B$  increases when  $Y_2$   
 decreases (removement of material from side e) or  $l_2$  decreases to the  
 20 advantage of  $l_1$  (removement of material from side f).

As a consequence a single transmission line in open circuit  
 used in shunt (that is a stub) can be converted into a reversible line  
 (that is into a line that can be lengthened or shortened by the same  
 method of adjustment no matter whether it consists of the addition or  
 25 of the removement of conductive material) if said line is replaced by  
 the cascaded connection of two different transmission lines, the second  
 of which has a length  $l_2$  comprised between  $\lambda/4$  and  $\lambda/2$   
 ( $\lambda/4 < l_2 < \lambda/2$ ); the length  $l_1$  of the first line is free and depends  
 on the initial value positive or negative of  $B$  that is to be realized.

30 The operating modalities of the stub of Fig. 6 are strictly  
 analogous to those of Fig. 5; however in this case while designing the  
 microstrip, initial areolae a, b, c, are to be prearranged (as in Fig. 1)

1 that must be covered with conductive material of the soft type that is  
easy to remove.

It has to be specified that the diagrams with areolae (Fig. 1,  
3 and 6) are particularly suitable for not too high frequencies ( $\leq 3$  GHz);  
5 while diagrams of Figures 1, 4 and 5 are necessary in case of high  
frequencies ( $> 3$  GHz).

The methodology described here is based on the replace-  
ment of a single line by a cascade of two lines and then by the introduc-  
tion of a redundancy.

10 Such redundancy can be usefully employed also, to send the  
polarization to active devices or to match loads on wide band.

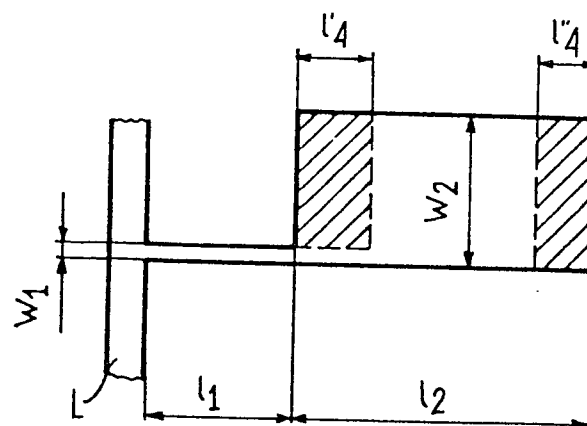
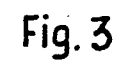
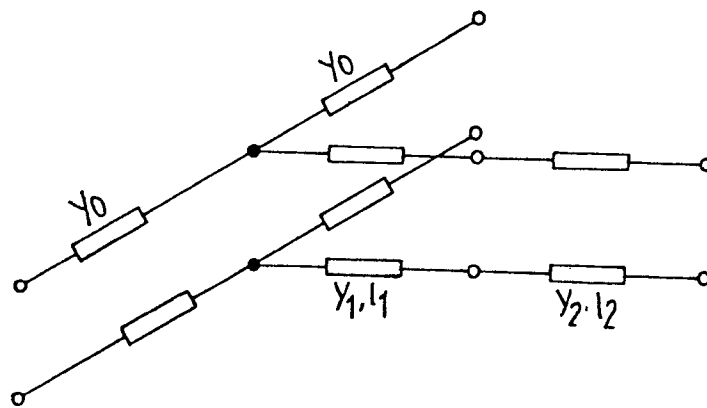
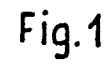
It is enough to note that the second line ( $l_2, w_2$ ) is a line  
with low characteristic impedance and has a length comprised between  
 $\lambda/4$  and  $\lambda/2$ . Therefore an intermediate position exists (correspond-  
15 ing to  $\lambda/4$ ) in which a short circuit at radio frequency is present with  
broad band due to the low impedance characteristic of the line.

This short circuit section can be utilized to insert a choke  
to send polarization voltage.

- 9 -

1 What we claim is:

1. Stub for matching microstrip circuits, characterized in that it consists of two cascaded lines, the second ( $l_2$ ,  $w_2$ ) of which has a length comprised between  $1/4$  and  $1/2$  of the used wavelength.
- 5 2. Stub according to claim 1 characterized in that the only addition of conductive material at suitable points of said sub causes both the increase and the decrease of the admittance (B) characteristic of the line; said increase or said decrease in the admittance exclusively depending on the point of the stub to which the conduc-  
10 tive material is added.
3. Stub as in claim 1, characterized in that the only removal of conductive material at suitable points of said stub causes both the increase and the decrease in the characteristic admittance (B) of the line; said increase or said decrease in the admittance depend-  
15 ing only on the point of the stub from which the conductive material is removed.
4. Transmission stub for matching microstrip circuits, the whole as described in the text and depicted in the annexed drawings.



2/2

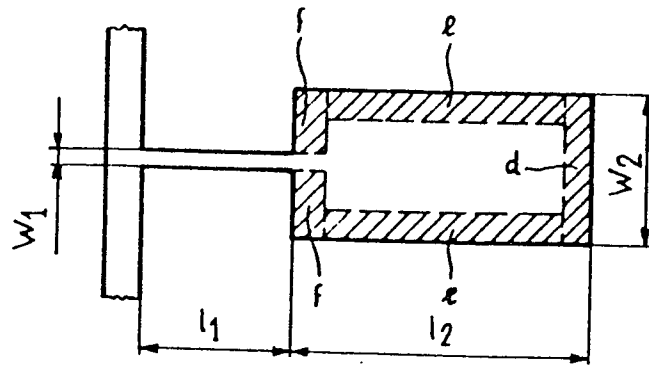


Fig. 5

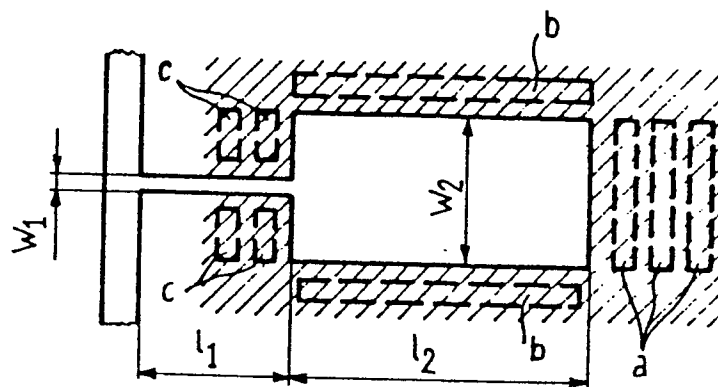


Fig. 6



DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	US - A - 4 070 639 (J.T. NEMIT et al.)  * column 4, line 47 to column 5, line 9; figures 1A and 3 *  --	1,4	H 01 P 5/02 7/08
	FR - A - 1 212 982 (C.S.F.)  * the whole document *  --	1,4	
	US - A - 4 105 959 (V. STACHEJKO)  * column 3, lines 39 to 49; figure 1 *  --	1,4	TECHNICAL FIELDS SEARCHED (Int. Cl. 3) H 01 P 1/20 5/00 7/08
	US - A - 3 417 352 (M.J. WALLER)  * abstract; column 3, lines 15 to 29; figures 1 and 4 *  --	1,4	
	US - A - 2 819 452 (M. ARDITI et al.)  * the whole document *  --	2-4	
	US - A - 2 820 206 (M. ARDITI et al.)  * column 4, lines 4 to 28; figures 7,8 and 9 *  --	2-4	CATEGORY OF CITED DOCUMENTS X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
	US - A - 4 157 517 (T.F. KNEISEL et al.)  * the whole document *  --	2-4	
	./.		
The present search report has been drawn up for all claims			&: member of the same patent family, corresponding document
Place of search The Hague	Date of completion of the search 11-02-1981	Examiner LAUGEL	



DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
A	<p><u>DE - A - 2 310 371</u> (LICENTIA PATENT- VERWALTUNGS- GmbH)</p> <p>* the whole document *</p> <p>--</p>	1-4	
A	<p>IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES, vol. MTT- 19, no. 7, July 1971 NEW YORK (US) M. CAULTON et al.: "Status of Lumped Elements in Microwave Integrated Circuits - Present and Future" pages 588 to 599</p> <p>* the whole document *</p> <p>-----</p>	1-4	TECHNICAL FIELDS SEARCHED (Int. Cl. 3)