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54 Refrigeration system with clearance seal and discrete braking element.

57 In a refrigeration system such as a split Stirling system, fluid seals associated with the reciprocating displacer are virtually dragless clearance seals (53, 50). Movement of the displacer relative to the pressure variations in the working volume of gas is retarded by a discrete braking element (60, 62). Because it is not necessary that the brake providing any sealing action, the brake can be designed for greater durability and less dependence on ambient and operating temperatures. Similarly, the clearance seal (53, 59) can be formed of elements having low thermal expansion such that the seal is not temperature dependent. In the primary embodiments the braking element (60, 62) is a split friction brake.

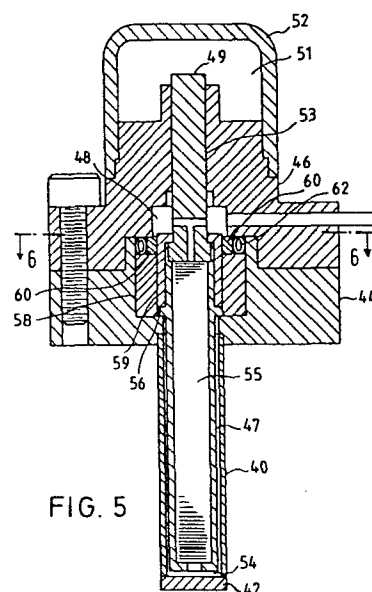


FIG. 5

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REFRIGERATION SYSTEM WITH CLEARANCE SEAL AND DIS-
CRETE BRAKING ELEMENT

Description

Field of the Invention

5 This invention relates to a refrigeration system and in particular to one in which a reciprocating displacer is driven by a pressure differential across that displacer such as a split Stirling cryogenic refrigerator.

10 Background Art

 A conventional split Stirling refrigeration system is shown in Figs. 1-4. This system includes a reciprocating compressor 14 and a cold finger 16. The piston 17 of the compressor provides a sinusoidal
15 pressure variation in a pressurized refrigeration gas such as helium. The pressure variation in a head space 18 is transmitted through a supply line 20 to the cold finger 16.

 The usual split Stirling system includes an
20 electric motor driven compressor. A modification of that system is the split Vuilleumier. In that system a thermal compressor is used. This invention is applicable to both of those refrigerators as well as others.

25 Within the housing of the cold finger 16 a cylindrical displacer 26 is free to move in a reciprocating motion to change the volumes of a warm space 22 and a cold space 24 within the cold finger. The displacer 26 contains a regenerative heat ex-
30 changer 28 comprised of several hundred fine-mesh metal screen discs stacked to form a cylindrical matrix. Other regenerators, such as those with

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stacked balls, are also known. Helium is free to flow through the regenerator between the warm space 22 and the cold space 24. As will be discussed below, a piston element 30 extends upwardly from the
5 main body of the displacer 26 into a gas spring volume 32 at the warm end of the cold finger.

The refrigeration system of Figs. 1-4 can be seen as including two isolated volumes of pressurized gas. A working volume of gas comprises the gas in
10 the space 18 at the end of the compressor, the gas in the supply line 20, and the gas in the spaces 22 and 24 and in the regenerator 28 of the cold finger 16. The second volume of gas is the gas spring volume 32 which is sealed from the working
15 volume by a piston seal 34 surrounding the drive piston 30.

Operation of the conventional split Stirling refrigeration system will now be described. At the point in the cycle shown in Fig. 1, the displacer
20 26 is at the cold end of the cold finger 16 and the compressor is compressing the gas in the working volume. This compressing movement of the compressor piston 17 causes the pressure in the working volume to rise from a minimum pressure to a maximum
25 pressure and this warms the working volume of gas. The pressure in the gas spring volume 32 is stabilized at a level between the minimum and maximum pressure levels of the working volume. Thus, at some point the increasing pressure in the
30 working volume creates a sufficient pressure difference across the drive piston 30 to overcome the

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friction of displacer seal 36 and drive seal 34. The piston and displacer then move rapidly upward to the position of Fig. 2. With this movement of the displacer, high-pressure working gas at about
5 ambient temperature is forced through the regenerator 28 into the cold space 24. The regenerator absorbs heat from the flowing pressurized gas and thereby reduces the temperature.

With the sinusoidal drive from a crank shaft
10 mechanism, the compressor piston 17 now begins to expand the working volume as shown in Fig. 3. With expansion, the high pressure helium in the cold space 24 is cooled even further. It is this cooling in the cold space 24 which provides the
15 refrigeration for maintaining a temperature gradient of over 200°K over the length of the regenerator.

At some point in the expanding movement of the piston 17, the pressure in the working volume drops sufficiently below that in the gas spring volume 32
20 for the gas pressure differential across the piston portion 30 to overcome seal friction. The displacer 26 is then driven downward to the position of Fig. 4, which is also the starting position of Fig. 1. The cooled gas in the cold space 24 is thus
25 driven through the regenerator to extract heat from the regenerator.

It is understood that the phase relationship between the working volume pressure and the displacer movement is determined by the braking force of the
30 seals on the displacer. For example, if those seals provided very low friction, the displacer would

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move from the lower position of Fig. 1 to the upper position of Fig. 2 as the working volume pressure increased past the pressure in the spring volume 32. Because the spring volume is at a
5 pressure about midway between the minimum and the maximum values of the working volume pressure, movement of the displacer would take place during the midstroke of the compressor piston 17. This would result in compression of a substantial
10 amount of gas in the cold end 24 of the cold finger, and because compression of gas warms that gas this would be an undesirable result.

To increase the efficiency of the system, upward movement of the displacer is retarded until
15 the compressor piston 17 is near the end of a stroke as shown in Figs. 1 and 2. In that way, substantially all of the gas is compressed and thus warmed in the warm end 22 of the cold finger, and that warmed gas is then merely displaced through
20 the regenerator 28 as the displacer moves upward. Thus, the gas then contained in the large volume 24 at the cold end is as cold as possible before expansion for further cooling of that gas. Similarly, it is preferred that as much gas as possible be
25 expanded in the cold end of the cold finger prior to being displaced by the displacer 26 to the warm end. Again, the movement of the displacer must be retarded relative to the pressure changes in the working volume.

30 In prior systems, the seals 34 and 36 are precisely designed and fabricated to provide a predetermined amount of loading to the displacer

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and thus retard the displacer movement by an optimum amount. A major problem of split Stirling systems is that with wear of the seals the braking action of those seals varies. As the braking action becomes
5 less the displacer movement is advanced in phase and the efficiency of the refrigerator is decreased. Also, braking action can be dependent on the direction of the pressure differential across the seal.

10 A primary object of the present invention is to provide sealing between the working volume and spring volume as well as consistent loading of the displacer even over long periods of use of the refrigerator.

15 In addition to the problem of wear of the seals, the refrigerator is often subjected to different environments. For example, a refrigerator may be stored at extremely high temperature and be called on to provide efficient cryogenic refrigeration. On
20 the other hand, the refrigerator may be subject to very cold environments. The sealing action and friction of the seals is generally very dependent on temperature.

A further object of this invention is to provide
25 sealing and braking action with minimum temperature dependence.

A problem common to all helium refrigerators is that, with wear, particles from worn seals contaminate the helium refrigerant. Those contaminants result in a significant degradation of performance and
30 shorten the operating life of the refrigerator.

A further object of this invention is to provide a refrigeration system having a longer life than prior systems due to lesser wear to dynamic
35 seals in the system.

Summary of the Invention

In a refrigerator such as a split Stirling refrigerator, the fluid seal between the working volume and spring volume is a virtually dragless clearance seal which does not retard movement of the displacer. The braking action for retarding movement of the displacer with pressure changes is provided by a separate braking element which applies a predetermined load to the displacer. Because the sealing and braking functions are separated, the brake can be designed for optimum loading of the displacer over an extended temperature range and over an extended life of the refrigerator without concern for providing sealing action. In fact, by equalizing the pressure across the braking element, changes in loading due to pressure differentials across the braking element are avoided. Also, the braking element may be isolated from the working volume so that debris generated with wear of the braking element does not contaminate the working volume. The clearance seal does not generate any detrimental contamination of the refrigerant.

In the preferred embodiment of the invention, the clearance seal is formed of hard ceramic material of low thermal expansion. Preferably, the clearance seal is at least 5 millimeters in length and the clearance between the seal element is no greater than about .005 millimeters.

The preferred braking elements are friction brakes which are noncontinuous about the periphery of the displacer. In one form the brake comprises spring biased brake shoes and in another form the brake is a split ring.

Brief Description of the Drawings

The foregoing and other objects, features and advantages of the invention will be apparent from the following more particular description of

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preferred embodiments of the invention, as illustrated in the accompanying drawings in which like reference characters refer to the same parts throughout the different views. The drawings are not necessarily to scale, emphasis instead being placed upon illustrating the principles of the invention.

Figs. 1-4 illustrate the operation of a prior art split Stirling refrigerator;

Fig. 5 is an elevational sectional view of a split Stirling refrigerator embodying the present invention;

Fig. 6 is a cross-sectional view of the refrigerator of Fig. 5 taken along line 6-6;

Fig. 7 is an elevational sectional view of an alternative embodiment of the invention;

Fig. 8 is a cross-sectional view of the braking element of the embodiment of Fig. 7 taken along line 8-8;

Description of Preferred Embodiments of the Invention

As shown in Figs. 5 and 6, a refrigerator includes a cylinder 40 having an end cap 42 and extending from a base plate 44. A working chamber head 46 is mounted to the plate 44 and has a warm portion 48 of the working chamber formed therein. A fluid line 50 extends from that working volume to a compressor as described with respect to the prior art.

A piston element 49 extends upwardly from the main body of a displacer 47. The piston 49 extends through the warm portion 48 of the working volume and through the head 46 to a spring volume 51. The spring volume is formed by the head 46 and a cap 52.

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The cylinder 40, plate 44, head 46 and cap 52 form a housing in which the displacer 47 reciprocates.

In accordance with this invention, the piston 49 is fabricated with a very close clearance fit to the head 46. The sealing between the warm volume and the spring volume 51 is thus provided by a clearance seal 53. With temperature stable material the seal is not greatly affected by variations in ambient temperature. With hard, smooth, abrasion resistant material, the clearance seal provides virtually dragless sealing action and long wear. The hardness of the clearance seal surfaces should be at least 60 on the Rockwell C scale and is preferably over 70 on the C scale. The abrasion resistance should be such that the wear rate of the two close fitting moving parts is less than about one microinch per hour. With respect to smoothness, the finish should be better than 16 microinches.

The clearance seal elements, piston 49 and head 46 are made of ceramic, hardened steel, or other hard, abrasion resistant material. Ceramic materials are particularly suited for use in forming the clearance seal because ceramic does not suffer from the problem of galling, a welding action, that might result from the use of metal clearance seal surfaces. Ceramics include compounds of any of the metals or metal-like materials in groups II, III and IV of the periodic table combined with a non-metal, typically oxygen, nitrogen, sulfur, carbon, boron or silicon. Ceramics are characterized by being hard and abrasion resistant. Examples of such ceramics are aluminum oxide (alumina), beryllium oxide (beryllia), titanium dioxide, titanium diboride, boron carbide, silicon nitride and pyrolytic graphite. Other substances

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may be added to a ceramic to improve its characteristics. Alumina is a preferred material. Although the piston and cylinder need not be solid ceramic, at least a bulk layer of ceramic should be provided on each of the piston and cylinder at the clearance seal to assure that these elements display the bulk characteristics of the ceramic.

In the usual application of this invention, the pressure differentials experienced between the working volume and the spring volume 51 are in the order of 75 pounds per square inch. To provide adequate sealing between the two volumes the clearance seal 53 should be about 5 millimeters long and a clearance between the head 46 and piston 49 should be no greater than about 0.005 millimeters.

A fluid seal is also provided between the warm portion of the working volume 48 and a cold portion 54 of the working volume to assure that all gas displaced by displacer 47 passes through the regenerator 55. This latter seal is formed of an inner ceramic ring 56 fixed to the displacer and an outer ceramic ring 58 fixed to the plate 44. As with the clearance seal 53, the elements of this clearance seal 59 are machined to extremely close tolerances to provide virtually dragless sealing action.

In order to retard movement of the displacer relative to pressure variations in the working volume a discrete braking element 60 is provided. As shown in Fig. 6, the braking element is comprised of three brake shoes 60A, 60B and 60C spring biased toward the ring 56 by a coiled garter spring 62. The slits 64 between the braking shoes equalize the pressure across the braking element. Thus, the loading on the displacer is not dependent on pressure. Also, in the event of any wear of the brake shoes 60,

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the spaces 64 allow for inward movement of the brake shoes so that a near constant loading of the displacer can be maintained by the spring 62. Even that wear is minimized because, there being no requirement that the brake shoes provide for fluid sealing, those shoes can be of hard, durable material.

In the embodiment of Figs. 7 and 8, a cylinder 70 extends from a plate 72 as before. Also, a head 74 is mounted to the plate 72 and supports a cap 76. The spring volume 78 and warm portion of the working volume 80 are thus formed as before. In this embodiment, however, a piston element 82 which serves as one element of a clearance seal 84 also serves as an element of a clearance seal 86 between the warm and cold portions of the working volume. The head 74 and a ceramic ring 88 form the outer elements of the clearance seals. Loading of the displacer to retard its movement is provided by a split ring friction brake shown in Fig. 8. Split ring 90 has a hard, inner thermoplastic coating 92 which serves as the single brake shoe. The split 94 in the split ring allows for equalization of fluid pressure across the brake.

In each embodiment shown, the braking element is positioned in the working volume. To minimize contamination of the refrigerant in the working volume, the braking element can be positioned in the spring volume 51 or 78. As a result, the working volume is exposed only to the clearance seals which are virtually without wear, and the braking element is isolated from the working volume by a clearance seal.

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In each of the above embodiments the seals around the displacer and piston are both clearance seals. This is ideal because the clearance seals are virtually dragless and are not subject to the wear of conventional lip seals. Also, the clearance seal about the piston assures equal leakage in each direction past the piston and thus assures a constant pressure in the spring volume.

While the invention has been particularly shown and described with reference to preferred embodiments thereof, it will be understood by those skilled in the art that various changes in form and details may be made therein without departing from the spirit and scope of the invention as described by the appended claims. For example, the invention has been illustrated by preferred friction brake embodiments. But the displacer retarding force might be applied by means of a magnetic coupling or the like. Friction brakes have the advantage of extracting work from the system.

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CLAIMS

1 1. In a refrigerator having a displacer which
2 reciprocates in a housing, there being a
3 working volume of gas and a spring volume of
4 gas in contact with opposing end surfaces
5 of the displacer and separated by a fluid
6 seal surrounding the displacer, the displacer
7 being driven by pressure differentials between
8 the working volume and the spring volume with
9 the phase relationship between the pressure
10 differential and the displacer movement being
11 determined by a braking force on the displacer,
12 characterized by:

13 all fluid seals between the
14 displacer and housing being
15 virtually dragless clearance
16 seals, there being additional
17 means provided for loading the
18 displacer to retard movement of
19 the displacer.

1 2. In a refrigerator having a displacer which
2 reciprocates in a housing, there being a work-
3 ing volume of gas and a spring volume of gas
4 in contact with opposing end surfaces of the
5 displacer and separated by a fluid seal surround-
6 ing the displacer, the displacer being driven
7 by pressure differentials between the working
8 volume and the spring volume with the phase
9 relationship between the pressure differential
10 and the displacer movement being determined by
11 a braking force on the displacer, the improve-
12 ment of:

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- 1 a clearance seal between the
2 working volume and the spring
3 volume to provide virtually
4 dragless fluid sealing; and
5 a discrete brake for applying
6 a predetermined load to the dis-
7 placer and thus retarding movement
8 of the displacer, the brake allow-
9 ing for equalization of fluid
10 pressure thereacross.
13. The improvement in a refrigerator as claimed in
2 Claim 2 wherein cooperating clearance seal ele-
3 ments are of a hard material of low thermal
4 expansion.
14. The improvement in a refrigerator as claimed in
2 Claim 3 wherein the clearance seal elements are
3 formed of ceramic.
15. The improvement in a refrigerator as claimed in
2 Claim 3 wherein the clearance seal is at least 5
3 millimeters in length and the clearance between
4 the seal element is no greater than about 0.005
 millimeters.
16. An improvement in a refrigerator as claimed in
2 Claim 2 wherein the brake is a friction brake
3 which is noncontinuous about the periphery of
4 the displacer.

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- 1 7. An improvement in a refrigerator as claimed in
2 Claim 6 wherein the friction brake comprises at
3 least two brake shoes pressed against the dis-
4 placer.
- 1 8. An improvement in a refrigerator as claimed in
2 Claim 7 wherein the brake shoes are pressed
3 against the displacer by a spring element sur-
4 rounding the displacer and shoes.
- 1 9. An improvement in a refrigerator as claimed in
2 Claim 6 wherein the friction brake is a split
3 ring.
- 1 10. An improvement in a refrigerator as claimed in
2 Claim 2 further comprising a clearance seal
3 around the displacer between portions of the
4 working volume at opposite ends of the displacer.
- 1 11. An improvement in a refrigerator as claimed in
2 Claim 10 wherein the friction brake is positioned
3 adjacent the clearance seal between the end por-
4 tions of the working volume.
- 1 12. An improvement in a refrigerator as claimed in
2 Claim 2 wherein the portion of the displacer in
3 contact with the spring volume is a center piston
4 element extending axially from the main displacer
5 body through and beyond a warm portion of the
6 working volume.

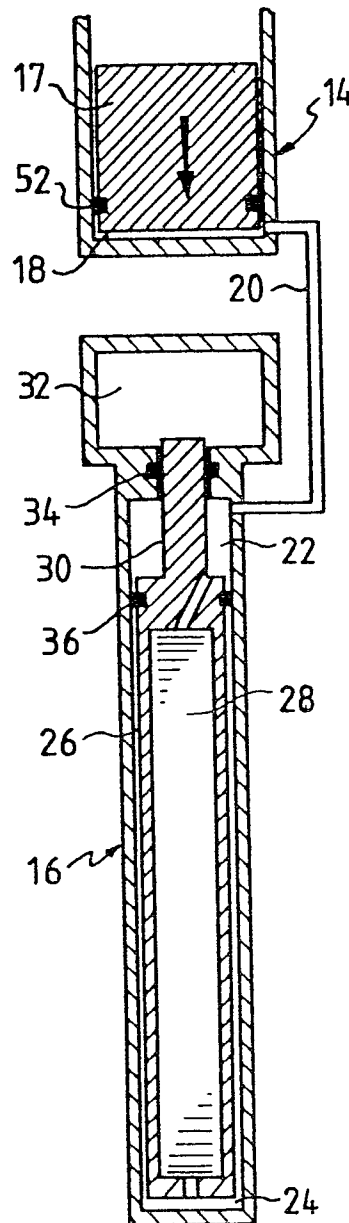


FIG. 1
(PRIOR ART)

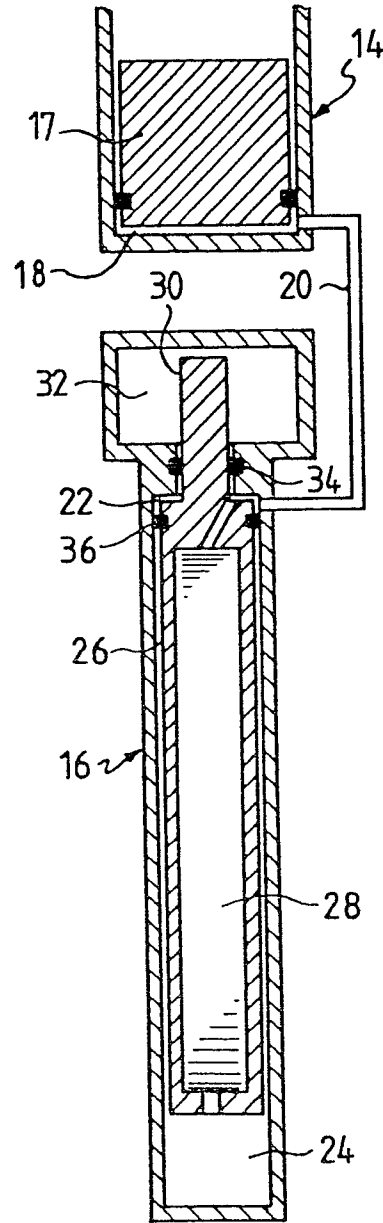


FIG. 2
(PRIOR ART)

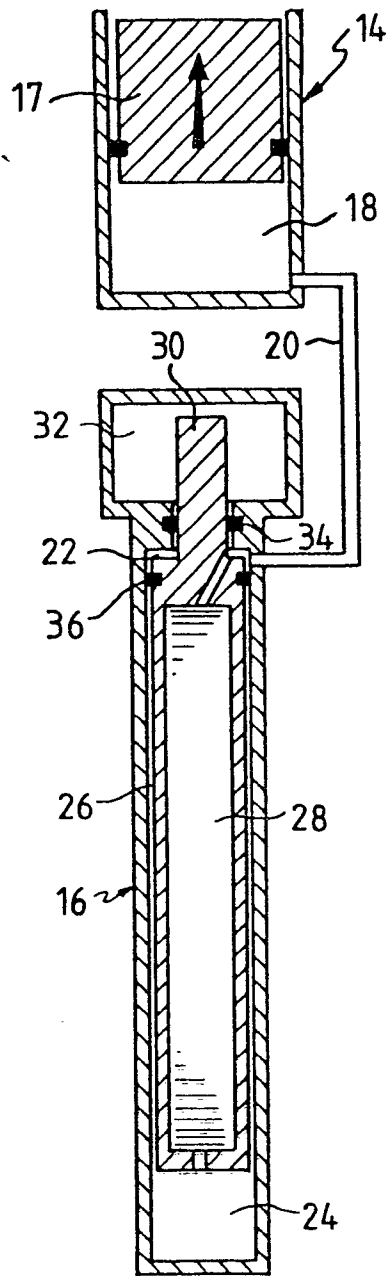


FIG. 3
(PRIOR ART)

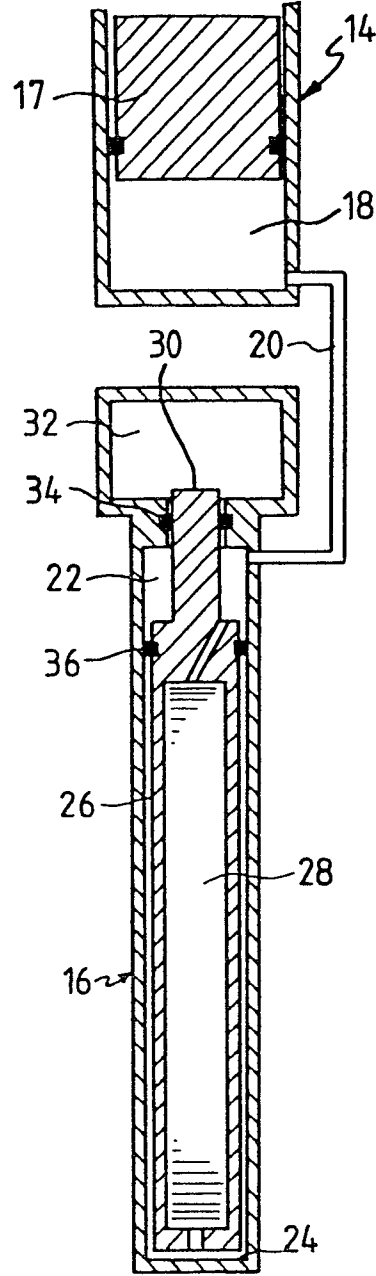


FIG. 4
(PRIOR ART)

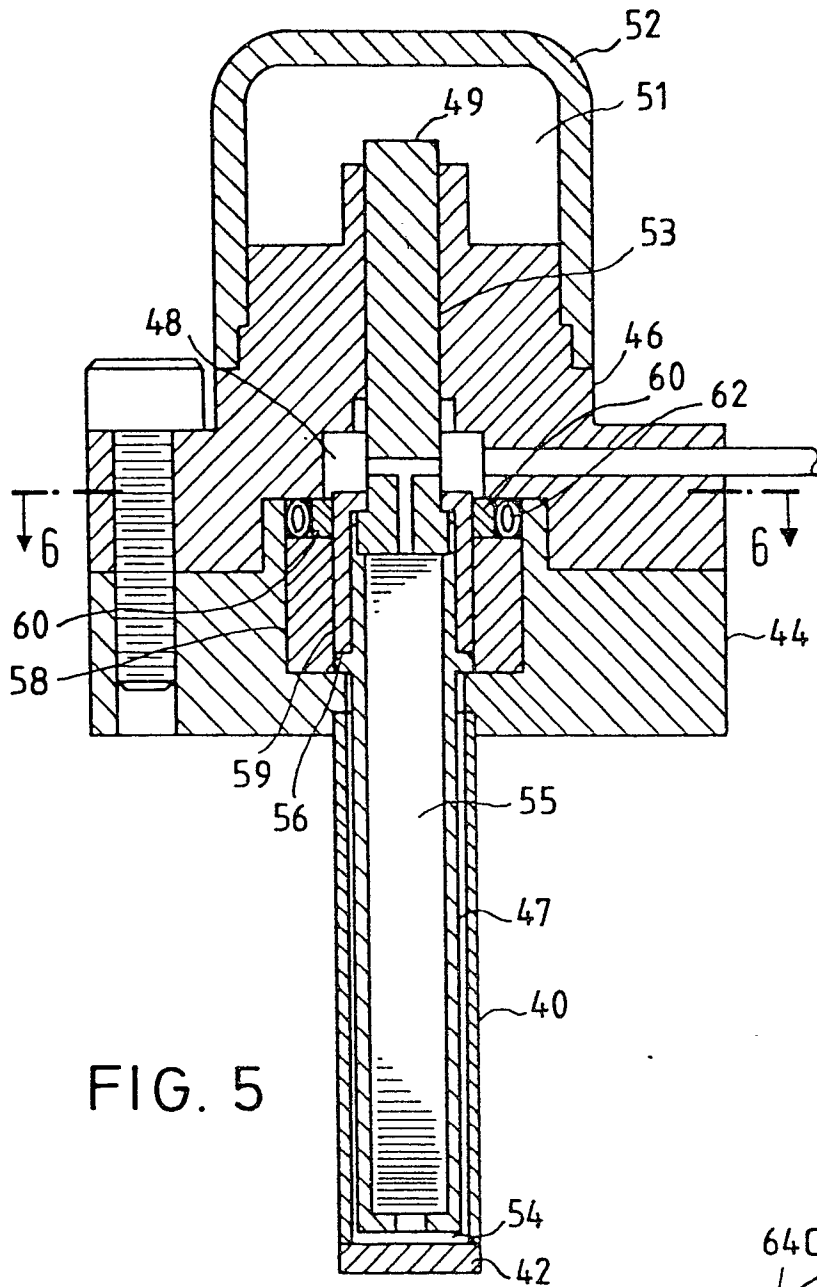


FIG. 6

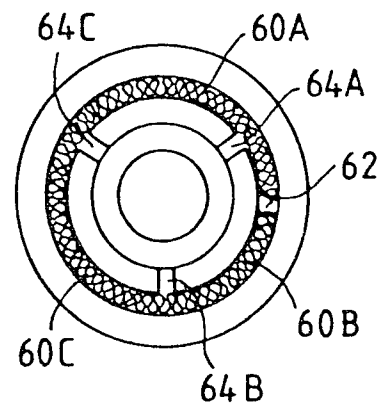


FIG. 7

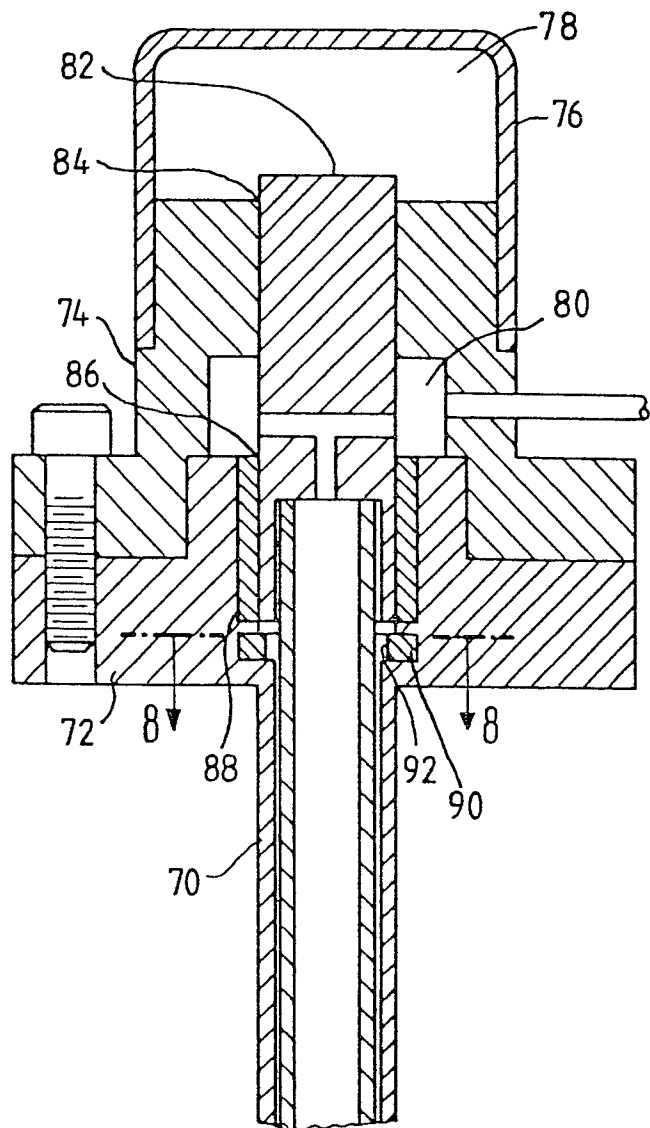
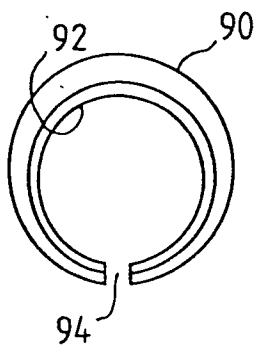


FIG. 8





European Patent
Office

EUROPEAN SEARCH REPORT

0037102

Application number

EP 81 10 2335

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.')
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	US - A - 4 019 335 (BROWNING) * column 2, lines 22-55; figure 30 * --	1	F 02 G 1/053 /F 25 B 9/00
	US - A - 4 036 018 (BEALE) * column 1, lines 16-30; column 3, lines 27-52; figure 1 * --	1	
	GB - A - 732 720 (PHILIPS) * page 2, lines 5-31, lines 75-84; figures 1,5 * --	1	TECHNICAL FIELDS SEARCHED (Int. Cl.')
	US - A - 3 958 841 (BRAUN) * column 1, lines 1-24, lines 54-68; figure 1 * -----	1	F 02 G F 16 J
			CATEGORY OF CITED DOCUMENTS
			X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons
			8. member of the same patent family, corresponding document
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
The Hague	22-06-1981	KOOIJMAN	