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(54) Lubricant composition with stabilized metal detergent additive and friction reducing ester component.

(57) Oils with metal sulfonate or sulfurized phenate detergents and friction reducing dicarboxylic esters are stabilized against haze or sediment formation by treatment of this oil solution of metal additive, prior to ester incorporation, with a phosphosulfurized polyisobutylene or a polyisobutenyl succinic anhydride at 55° to 225°C for 2-30 hours.

EP 0 041 851 A2

1 This invention relates to oil compositions
2 which contain both an overbased metal detergent addi-
3 tive and a glycol ester friction modifier. More parti-
4 cularly, this invention relates to a method for formulat-
5 ing such compositions wherein the formation of haze and
6 sediment due to the incompatibility of these additives is
7 overcome.

8 Lubricating oil compositions containing metal de-
9 tergents additives being either the normal or basic (over-
10 based) magnesium or calcium sulfurized phenates or sulfon-
11 ates are well known in the art and are employed in various
12 motor oil formulations. Formulating these metal detergent
13 additives with other ingredients in a finished lubricating
14 oil blend has been known to create compatibility problems,
15 specifically the formation of sediment, separation of
16 phases, visible precipitation or haze and similar problems
17 which are evidence of incompatibility or unwanted inter-
18 action of components.

19 Resolution of this problem through techniques
20 known in the art is represented by U.S. Patent 3,714,042,
21 issued January 30, 1973 to Greenough, which discloses the
22 treatment of overbased complexes with a high molecular
23 weight aliphatic carboxylic acid or anhydride at elevated
24 temperatures. U.S. Patent 3,965,017, issued to Burnop
25 et al discloses stabilization through addition of small
26 proportions of a monocarboxylic acid, anhydride or salt
27 or the reaction product of a hydrocarbon with P_2S_5 and a
28 glycol or ether alcohol.

29 Lubricant compositions containing the polycar-
30 boxylic acid-glycol ester friction modifier additive used
31 in the compositions of the present invention are disclosed
32 in U.S. Patent 4,105,571 issued to Shaub et al.

33 The present invention is concerned with resolu-
34 tion of the specific problem of incompatibility encountered
35 when lubricating oil formulations are prepared which con-
36 tain both a metal or overbased metal sulfonate or a



1 sulfurized phenate detergent additive, particularly
2 where the metal is calcium or magnesium, and small pro-
3 portions of a glycol-polycarboxylic acid ester friction
4 reducing additive.

5 In accordance with the present invention, there
6 is provided a lubricating oil composition having a reduced
7 tendency toward sediment formation, which comprises a glycol-
8 polycarboxylic acid ester friction reducing additive and a
9 metal detergent additive being a metal or overbased metal
10 sulfonate or sulfurized phenate, which composition is prepared by
11 a process comprising the steps of:

- 12 (a) providing a lubricating oil mixture contain-
13 ing a lubricating oil base stock containing
14 about 0.1 to 10 percent by weight of a metal
15 or overbased metal sulfonate or sulfurized
16 phenate detergent additive;
- 17 (b) treating said mixture by reacting said metal
18 detergent additive with from about 50 to
19 100 percent by weight, based upon the weight
20 of the metal detergent additive, with either
21 (i) a phosphosulfurized polyisobutylene or
22 (ii) a polyisobutenyl succinic anhydride
23 at temperatures of from about 55°C to about
24 225°C for a period of from about 2 to 30
25 hours; and
- 26 (c) thereafter, adding to said treated mixture
27 about 0.01 to about 2.0 percent by weight,
28 based on the total weight of the composi-
29 tion, of said glycol ester friction modi-
30 fier additive, whereby said composition ex-
31 hibits a reduced tendency toward phase sepa-
32 ration or sediment or haze formation.

33 The metal detergent additives used in the present
34 invention are those metal or overbased metal sulfonate or
35 sulfurized phenate oil-soluble additives which are well
36 known in the art. The metal sulfonates are obtained from



1 sulfonic acids derived from sulfonating natural or syn-
2 thetic hydrocarbons, such as by treating oil base stocks
3 with concentrated or fuming sulfuric acid or by sulfonat-
4 ing alkylated aromatic hydrocarbons. The hydrocarbyl
5 sulfonate of these metal detergent additives is derived
6 from petroleum sulfonates and includes alkyl, alkylaryl
7 and aryl sulfonates and mixtures thereof having a molecular
8 weight of from about 300 to 1,000, such as barium nonyl-
9 benzene sulfonate, magnesium dodecylbenzene sulfonate and
10 the like. The sulfonates are usually the alkaline earth
11 metal sulfonates, usually calcium, barium, or magnesium,
12 but can also be alkali metal sulfonates, such as sodium
13 sulfonates. Overbased sulfonates are those which contain
14 metal base in excess that is required for simple neutrali-
15 zation. In preparing such overbased materials, the sulfon-
16 ic acid is typically reacted with an excess of metal base
17 and the excess base is usually neutralized with an acidic
18 gas, such as carbon dioxide. Such overbased sulfonates
19 have a total base number (ASTM-D-664) of about 50 to 500.

20 The sulfurized phenates are the metal salts of sul-
21 furized alkyl phenols, which contain about 2 to 14 percent
22 by weight sulfur based on the weight of the sulfurized
23 alkyl phenols. Such materials are well known in the art
24 and are derived from alkylated phenols, wherein the alkyl
25 is C₅-C₄₀, such as t-amyl phenol, t-octyl phenol, nonyl-
26 phenol, di-t-octyl phenol and phenols alkylated with suit-
27 able polymers of up to 40 carbon atoms obtained from propyl-
28 ene, butylene, amylenes or mixtures thereof. The sulfur-
29 ized phenols are prepared by well-known methods, for ex-
30 ample, by reacting the alkylated phenol with sulfur mono-
31 chloride, sulfur dichloride or elemental sulfur.

32 The metals employed for providing the phenate salts
33 are typically alkali metal, alkaline earth metal or mag-
34 nesium, principally calcium or magnesium. Overbased phe-
35 nates are prepared by the process comprising reacting the
36 phenol with excess base and the excess is neutralized with

1 carbon dioxide. Typical overbased metal sulfurized phe-
2 nates will have a total base number (ASTM-D-664) of about
3 50 to 100.

4 The treatment step of the present invention gener-
5 ally comprises incorporating the metal detergent additive
6 into a lubricating oil and conducting a reaction for about
7 2 to 30 hours at temperatures of from about 55°C to 225°C
8 with either a phosphosulfurized polyisobutylene or with a
9 polyisobutenyl succinic anhydride, and 25-100 percent, pref-
10 erably 50-100, percent by weight of these materials are
11 used based upon the weight of the metal detergent additive
12 present.

13 When employing a phosphosulfurized polyisobutylene,
14 it is preferable in most cases to conduct the treatment
15 step of the present invention at relatively higher tempera-
16 tures and longer periods of time. Thus, the preferred
17 treatment conditions for P_2S_5 -polyisobutylene treatment
18 are temperatures of about 100°C to 200°C and a treatment
19 period of about 10 to 25 hours, particularly when the metal
20 additive is an overbased calcium or magnesium sulfurized
21 phenate.

22 When the polyisobutenyl succinic anhydride is em-
23 ployed, preferred conditions of treatment in accordance
24 with this invention are temperatures of about 60°C to
25 85°C for about 2 to 7 hours.

26 Phosphosulfurized polyisobutylenes useful in the
27 present invention are prepared by methods well known in
28 the art comprising the reaction of sulfides of phosphorous
29 with polyisobutylene at elevated temperatures. While P_2S_5
30 is preferred, P_2S_3 , P_4S_3 and P_4S_5 are also useful as well
31 as mixtures thereof, as well as mixtures of elemental phos-
32 phorous and sulfur. The reaction is carried out at about
33 90°C to 315°C, preferably 150°C, to 290°C, using about 1
34 to 5 molar proportions of polyisobutylene to 1 molar
35 proportion of phosphorous sulfide. The reaction is usually
36 continued until the maximum amount of sulfur or phosphorous
37 sulfide has been added but this is not essential to provide



1 a useful product. Typical reaction times are about 2 to
2 10 hours. Generally, the polyisobutylenes have a molec-
3 ular weight of about 500 to 25,000, preferably 800 to
4 2,000. Particularly useful are polyisobutylenes of 700 to
5 1500 molecular weight reacted with about 10 to 15 percent
6 by weight of P_2S_5 .

7 The polyisobutenyl succinic anhydrides useful
8 herein for treating the metal detergent additives are also
9 known and are disclosed in the number of references, such
10 as U.S. Patent 3,288,714, issued to Osuch. These are oil-
11 soluble materials, which have desirable additive properties
12 themselves, principally as dispersants, prepared by react-
13 ing maleic anhydride with a polyisobutylene polymer having
14 a molecular weight of about 500 to 2,000. Particularly
15 preferred for use as treating agents in the present inven-
16 tion are those polyisobutenyl succinic anhydrides wherein
17 the polyisobutenyl group has a number average molecular
18 weight of about 700 to 1,500.

19 The lubricating oil base stock employed herein
20 generally comprises a hydrocarbon mineral oil of lubricating
21 viscosity including paraffinic, naphthenic and aromatic oils
22 preferably a mineral paraffinic oil having a viscosity of
23 about 20 to 100 cs. min. (100°F) and blends of such mineral
24 paraffinic oils. Synthetic oils may be used provided the
25 conditions of treatment do not adversely affect such syn-
26 thetic oils by causing an unwanted side reaction.

27 The finished formulation then may be prepared
28 by incorporating into the treated composition the friction
29 reducing polycarboxylic acid glycol ester which is employed
30 in amounts of about 0.01 to 2.0 percent preferably 0.05 to
31 0.3 percent by weight, typically, 0.1 to 0.3 percent by weight
32 based upon the total weight of the composition being used.

33 These friction reducing esters are described in more detail hereinbelow.

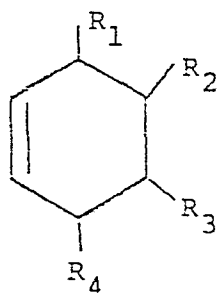
34 The friction reducing esters are generally de-
35 rived from the esterification of a polycarboxylic acid with
36 a glycol and may be partial esters or diesters of the formulas:



1 HO-R'-OOC-R-COOH and HO-R'-OOC-R-COOR"-OH
2 wherein R is the hydrocarbon radical of the acid and R'
3 and R" is either the hydrocarbon radical of an alkane diol
4 or the oxyalkylene radical from an oxa-alkane diol as de-
5 fined hereinbelow. The polycarboxylic acid may be an ali-
6 phatic saturated or unsaturated acid and will generally
7 have a total of about 24 to 90, preferably about 24 to 60,
8 carbon atoms and about 2 to 3, preferably about 2, carbox-
9 ylic acid groups with a least about 9 carbon atoms, prefer-
10 ably about 12 to 42, especially 16 to 22 carbon atoms be-
11 tween the carboxylic acid groups. Generally about 1-3
12 moles of glycol, preferably 1-2 moles of glycol, is used
13 per mole of acid to provide either a complete or partial
14 ester. Esters within the foregoing formula can also be
15 prepared by reaction of the acid with 1 mole or more of
16 ethylene oxide.

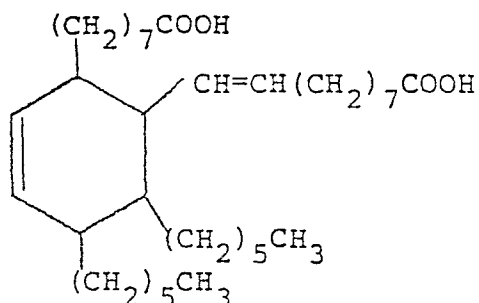
17 Also, esters can be obtained by esterifying a
18 dicarboxylic acid or mixture of such acids with a diol or
19 mixture of diols, R would then be the hydrocarbon radical
20 of the dicarboxylic acid and R' and R" would be the hydro-
21 carbon radical associated with the diols or diols.

22 Especially preferred are the dimer acid ester
23 friction reducing esters. The term dimer acid used herein
24 is meant to refer to those substituted cyclohexene dicar-
25 boxylic acids formed by a Diels-Alder-type reaction which
26 is a thermal condensation of C₁₈-C₂₂ unsaturated fatty
27 acids, such as tall oil fatty acids which typically con-
28 tain about 85 to 90 percent oleic or linoleic acids. Such
29 dimer acids typically contain about 36 carbon atoms. The
30 dimer acid structure can be generalized as follows:



-7-

1 with two of the R groups being carboxyl groups and two
 2 being hydrocarbon groups depending upon how the conden-
 3 sation of the carboxylic acid has occurred. The car-
 4 boxyl groups can be $-(CH_2)_8COOH$; $-CH=CH(CH_2)_7COOH$; $-(CH_2)_7$
 5 $COOH$; $-CH_2CH=CH(CH_2)_7COOH$; $-CH=CH(CH_2)_7COOH$ and the hydro-
 6 carbon terminating group can be represented by: $CH_3(CH_2)_4$;
 7 $CH_3(CH_2)_5$; $CH_3(CH_2)_7$; $-CH_3(CH_2)_4CH=CH-$; $CH_3(CH_2)_4CH=CHCH_2-$;
 8 $CH_3(CH_2)_4CH=CHCH_2-$; and the like. The dimer of linoleic
 9 acid which is the preferred embodiment can be expressed
 10 in the following formula:



19 Also the term dimer acid as used herein neces-
 20 sarily includes products containing up to about 24 per-
 21 cent by weight trimer, but more typically about 10 per-
 22 cent by weight trimer since, as is well known in the art,
 23 the dimerization reaction provides a product containing
 24 a trimer acid having molecular weight of about three times
 25 the molecular weight of the starting fatty acid.

26 The polycarboxylic acids or dimer acids noted
 27 above are esterified with a glycol, the glycol being an
 28 alkane diol or oxa-alkane diol represented by the formula
 29 $HO(RCH_2CH_2O)_xH$ wherein R is H or CH_3 and x is about 2 to
 30 100, preferably 2 to 25, with ethylene glycol and dieth-
 31 ylene glycol particularly preferred. A preferred embodi-
 32 ment is formation of the ester with about 1 to 2 moles
 33 of glycol per mole of dimer acid or polycarboxylic acid,
 34 such as the ester of diethylene glycol with dimerized
 35 linoleic acid.

36 Numerous other additives will of course normally
 be included in a finished lubricating oil composition such

-8-

1 as detergents and dispersants, oxidation and rust in-
 2 hibitors, viscosity index improvers, pour depressants,
 3 anti-wear agents and the like and these may be added
 4 prior to or subsequent to the addition of the friction
 5 reducing ester component.

6 EXAMPLES

7 Formulations were prepared which demonstrated
 8 the incompatibility of the metal detergent additive with
 9 a dimer acid ester friction modifier which in each formu-
 10 lation was diethylene glycol ester of dimerized linoleic
 11 acid. In each formulation set forth in Table I, the com-
 12 position was cloudy with visible separation of phases after
 13 standing for several days both at room temperature and at
 14 65°C. The base oil in each case was Solvent 150 Neutral
 15 oil, a mineral paraffinic oil having a viscosity of 31 cS.
 16 min. at 37.8°C.

17 TABLE I

18 <u>Component</u>	19 <u>Formulation - Weight Percent</u>				
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>
20 Overbased Ca Sulfurized	1.0	-	-	-	-
21 Phenate (1)					
22 Overbased Mg Sulfurized	-	0.8	-	-	-
23 Phenate (2)					
24 Overbased Mg Sulfonate (3)	-	-	1.04	-	-
25 Overbased Ca Sulfonate (4)	-	-	-	-	1.5
26 Ca Sulfurized Phenate (5)	-	-	-	1.5	-
27 Base Oil	98.9	99.1	98.36	98.4	98.4
28 Friction Modifier	0.1	0.1	0.1	0.1	0.1

29 In each formulation of Table I, in the absence
 30 of the friction modifier additive the formulations were
 31 clear with no evidence of instability after storage for
 32 equivalent periods of time under the same conditions.
 33 Total base numbers reported are according to ASTM-D-664.
 34 (1) Overbased calcium sulfurized dodecyl phenate sulfide
 35 having a total base number of 250.

- 1 (2) Overbased magnesium sulfurized nonylphenate, nonyl-
- 2 phenol sulfide having a total base number of 250.
- 3 (3) Overbased magnesium alkyl sulfonate having a total
- 4 base number of 395.
- 5 (4) Overbased calcium alkyl sulfonate having a total
- 6 base number of 300.
- 7 (5) Calcium sulfurized dodecyl phenate having a total
- 8 base number of 135.

9 A number of stabilized formulations were prepared
10 by first treating an oil concentrate containing 20-30 wt.
11 percent of the metal detergent additive with a P_2S_5 -
12 polyisobutylene (mol. wt. 780) and then blending with the
13 base oil and friction modifier to provide the finished
14 formulation. These are set forth in Table II which in-
15 cludes the various treatment times and temperatures used;
16 all formulations were clear with no evidence of instability
17 upon standing for 1 month at room temperature and 1 month
18 at 65°C. The metal additives and friction modifier are the
19 same as those reported in Table I.

20 Similarly, metal detergent additives were treated
21 with two types of polyisobutenyl succinic anhydrides; for-
22 mulations A & B used $\bar{M}_n=1,000$ and Sap No. 112 and formula-
23 tions C & D used $\bar{M}_n=1,300$ and Sap. No. 103 under varying
24 conditions of time and temperature and, thereafter, the
25 treated materials were blended into the formulations re-
26 ported in Table III each of which remained clear upon stor-
27 age for 1 month at room temperature and 1 month at 65°C
28 with no instability apparent. Again, the base oil, ad-
29 ditives and friction modifiers are those identified in
30 the prior examples.

-10-

TABLE II

	Formulation	Weight Percent				
		A	B	C	D	E
Component						
Overbased Ca Sulfurized Phenate	1.0	-	-	-	-	-
Overbased Mg Sulfurized Phenate	1	10	-	-	-	-
Overbased Mg Sulfonate	-	-	1.0	-	-	-
Ca Sulfurized Phenate	-	-	-	1.0	-	-
Overbased Ca Sulfonate	-	-	-	-	1.0	-
P ₂ S ₅ - Polyisobutylene	0.5	10	0.1	0.5	0.5	0.5
Base Oil	98.5	79.8	98.8	98.4	98.4	98.4
Friction Modifier	0.1	0.2	0.1	0.1	0.1	0.1
Treatment Conditions						
Hours	20	24	7	14	17	
Temperature °C	152°	200°	59°	68°	64°	

TABLE III

	Formulation	Weight Percent			
		A	B	C	D
Component					
Overbased Mg Sulfurized Phenate	1.0	-	1.0	-	-
Overbased Ca Sulfurized Phenate	-	1.0	-	1.0	-
Polyisobutenyl Succinic Anhydride	0.5	0.2	0.5	0.5	0.5
Base Oil	98.4	98.7	98.4	98.4	98.4
Friction Modifier	0.1	0.1	0.1	0.1	0.1
Treatment Conditions					
Hours	4	5	24	24	
Temperature °C	64°	70°	82°	82°	

EAL 10-11

-11-

1 Instead of carrying out the treatment of the deter-
2 gent additive in a lubricating oil, the same results are
3 obtained by carrying out the treatment in a lubricating
4 oil concentrate wherein said detergent additive is present
5 in amounts of 20 to 50 wt. percent, based on the total oil
6 composition, the base oil comprising 50 to 80 percent of
7 the composition, or a portion of the oil may be replaced,
8 by other additives, such as viscosity index improver, pour
9 depressants, dispersants, etc. Thus, 0.1 to 50 wt.
10 percent of the detergent additive admixed with the oil
11 can be used in the reaction with said phosphosulfurized
12 polyisobutylene or anhydride reactants.

WHAT WE CLAIM IS:

1. An oil composition comprising a lubricating oil base stock, a polycarboxylic acid glycol ester friction modifier additive and a metal or overbased metal sulfonate or sulfurized phenate detergent additive which composition is prepared by a process comprising the steps of: (a) providing a mixture containing a lubricating oil base stock and about 0.1 to 50 percent by weight of the metal detergent additive; (b) treating said mixture by reacting it with 25 to 100 percent by weight, based on the weight of the metal detergent additive, with either a phosphosulfurized polyisobutylene or a polyisobutenyl succinic anhydride at temperatures of from about 55° to about 225°C for about 2 to 30 hours, and (c) thereafter adding to said treated mixture about 0.01 to about 2.0 percent by weight, based on the total weight of the composition, of the glycol ester friction modifier additive, whereby said composition exhibits a reduced tendency toward sediment formation or phase separation.

2. The composition of claim 1 wherein the metal detergent additive is an overbased calcium or magnesium sulfonate.

3. A composition of claim 1 wherein the metal detergent additive is an overbased calcium or magnesium sulfurized phenate.

4. The composition of claims 1 or 2 wherein said treatment step is conducted with a polyisobutenyl succinic anhydride wherein the polyisobutenyl group has a molecular weight of from about 700 to 1,500.

5. The composition of claims 1-4 wherein the friction modifier is the diethylene glycol ester of the dimer acid of linoleic acid.



6. The composition of claim 5 wherein the concentration of said glycol ester is from about 0.05 to about 0.3 weight percent.

7. The composition of claims 1-3 wherein said treatment step is conducted with a polyisobutylene of 700 to 1500 molecular weight phosphosulfurized with P_2S_5 .

8. The composition of claim 7 wherein said treatment step is conducted at a temperature of from about 100°C to 200°C for a period of about 10 hours to 25 hours.

9. The composition of claim 4 wherein the treatment is conducted at a temperature of from about 60° to 85°C for about 2 to 7 hours.

10. The composition of claims 1-9 wherein said treatment is carried out on a mixture containing said lubricating oil base stock and about 0.1 to 10 percent by weight of said metal detergent additive, using 50 to 100 percent by weight, based on the weight of said metal detergent additive, of said phosphosulfurized polyisobutylene or of said anhydride.

