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⑤④ **Mineral sizers.**

⑤⑦ A mineral breaker including a pair of side by side breaker drums each having breaker teeth projecting radially therefrom, the teeth on each drum being arranged in circumferentially extending groups of teeth, the groups of teeth on one drum being located between adjacent groups of teeth on the other drum, the teeth on at least one of said pair of drums being arranged to define a series of discrete circumferentially spaced helical formations extending along the drum.

MINERAL SIZERS

The present invention relates to mineral sizing in particular to mineral sizer and a tooth construction.

According to one aspect of the present invention there is provided a mineral breaker including at least one breaker drum
5 having breaker teeth projecting radially therefrom, the teeth being arranged so as to define a series of discrete circumferentially spaced helical formations extending along the drum.

According to another aspect of the present invention there is provided a tooth construction for a mineral breaker
10 comprising a support and a removable tooth sheath which covers the support.

Advantageously, when assembling a drum composed of a series of annuli, the annuli may be either independantly keyed or splined to the common shaft or they may be rings being fixedly secured to one another to form said drum. The former is
15 presently preferred as it enables the drum to be disassembled. Alternatively the assembly of annuli and shaft may be cast integrally to provide a support for the tooth sheaths.

Preferably, the tooth sheaths when in position on all
20 projections serve to completely cover the support or drum to thereby protect it from abrasive wear caused by breakage of mineral.

According to another aspect of the present invention there is provided a mineral sizer having at least one rotatable drum assembly including a tooth construction as defined
25 above.

Various aspects of the present invention will now be described with reference to the accompanying drawings, in which:-

Figure 1 is a part perspective view of a mineral sizer
30 according to one aspect of the present invention;

Figure 2 is an end view, partly in section, of the sizer shown in Figure 1;

Figure 3 is a side view of the sizer shown in Figure 1;

Figure 4 is a longitudinal section through the sizer
35 shown in Figures 1 to 3 wherein the sizer teeth are arranged

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in lines parallel to the axis of rotation of the drums;

Figure 5 is an exploded perspective view of a tooth sheath and support according to another aspect of the present invention;

5 Figure 6 is a diagrammatic end view of the sizer drums shown in Figure 2;

Figure 7 is a diagrammatic view of the sizer drums shown in Figure 2;

10 Figure 8 is a similar view to Figure 4 showing an alternative embodiment according to the present invention;

Figure 9 shows a support ring for forming part of a breaker drum in a mineral sizer according to another embodiment of the present invention;

Figure 10 shows a section along line X-X in Figure 9;

15 Figure 11 shows a support ring similar to the support ring shown in Figure 9 but of reduced diameter;

Figure 12 is a front view of a tooth cap for fitting onto the support rings of Figures 9 to 11;

Figure 13 is a side view of tooth cap of Figure 12;

20 Figure 14 is a plan view of the tooth cap of Figure 12;

Figure 15 is a section along line VII-VII in Figure 14;

Figure 16 is a section along line VIII-VIII in Figure 14;

Figure 17 is a side view of a further tooth sheath construction according to the present invention;

25 Figure 18 is a section along line A-A in Figure 17;

Figure 19 is an end view as seen in the direction of arrow B in Figure 17;

Figure 20 is a side view of a further tooth sheath construction according to the present invention;

30 Figure 21 is a plan view taken along arrow C in Figure 20;

Figure 22 is a section view taken along line BB-BB in Figure 21 and showing the sheath seated on a corresponding support ring; and

35 Figure 23 is a part perspective view of a mineral sizer including drum assemblies made up of tooth sheaths and support rings illustrated in Figures 20 - 22.

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Referring initially to Figures 1 to 4 and 7 the sizer 10 includes a housing 11 having sides 12 and end walls 14. The housing 11 is conveniently fabricated from steel plate panels which are bolted and welded together.

5 Rotatably mounted to extend between the end walls 14 are a pair of breaker drum assemblies 15 each of which is geared at one end to the other so that they are driven from a common drive 18 to be rotated in opposite directions. In the embodiment illustrated in Figure 1 the drums are rotated so as to
10 direct material between them. The gear connection between the drums also serves to set the rotary positions of the drums relative to one another.

Each drum assembly 15 is provided with circumferentially extending groups 19 of breaker teeth 20, the groups 19 being
15 spaced axially along the drum assembly 15. The axial spacing of groups 19 on one drum assembly is staggered to that on the other drum assembly so the teeth 20 in a group 19 on one drum assembly pass between an adjacent pair of groups 19 on the other drum assembly.

20 As seen by reference to Figures 1 and 7, the teeth 20 are also preferably arranged to define a series of discrete helical formations 21 which are spaced circumferentially about each drum assembly 15. The helical formations 21 as shown in Figures 1 and 7 extend along the axes of each drum in a different sense, i.e. for the left hand drum as seen in Figure 1
25 the helical formations 21 extend away from the nearest end wall 14 in an anti-clockwise sense and for the right hand drum the helical formations 21 extend in a clockwise sense. Preferably each helical formation 21 in extending along its respective drum passes through an arc of about 90° .
30

The shape of teeth 20 and their relative positions and size are such that during use, two types of breaking action are present, viz a primary breaking action on larger pieces of mineral whereat the mineral is gripped between opposing leading
35 faces 46 of teeth on opposite drums and a secondary breaking action wherein mineral is trapped between the rear edges 47 of teeth and the leading face 46 of another tooth.

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Preferably the arc through which end helical formation passes is such as to ensure that a secondary breaking action occurs.

Additionally the spacing between the drums is chosen to that when the tips of teeth on one drum sweep passed the
5 trough defined between groups 19 of teeth on the other drum there is sufficient clearance so that compaction of material is avoided. Accordingly by a suitable choice of spacing it is possible for fine material to quickly pass through the sizer without compaction, thus leaving the sizer to break down
10 larger pieces of material either by the primary and/or secondary breaking action.

The shape of teeth 20 are designed bearing in mind the hardness and tensile strength of the mineral to be broken. Preferably the teeth are designed to provide as much bite as
15 possible for the primary type of breaking action for the diameter of the drum assembly so as to positively grip large pieces of material. Accordingly the ratio of height of teeth relative to drum diameter is normally large. For example, the tooth height to diameter of drum ratio can be 1 : 4. In this
20 respect, the cross-sectional extent of a bite region 70 for primary breaking is illustrated in Figure 6, the depth of the region 70 is defined by the trailing edge 47 of one tooth and the leading edge 46 of a succeeding tooth; and the length of the region 70 is defined between the leading face 46 of one
25 tooth and the leading face 46' of an opposed tooth on the opposite drum. In the embodiment of Figure 6, the trailing edge 47 which is slightly curved, but which may be straight if desired, is chosen to be approximately tangential to the drum diameter and the leading face 46 is chosen to be approximately
30 located radially relative to the drum. The grip region between teeth on the same group may be varied to alter the size of the grip region by either altering the size of tooth or by altering the number of teeth in each group 19, the maximum grip region being achieved when the point of intersection of
35 face 46 is on or behind (in the direction of rotation of the drum) the location whereat the trailing edge of the preceding tooth merges into the periphery of the drum.

When the teeth are arranged to form helical formations 21 as shown in Figures 1 and 7 the grip region varies in width longitudinally of the drums as illustrated in Figure 7. Accordingly a large piece of material 80 (shown in broken lines) 5 undergoes a succession of primary breaking actions and due to the helical formations 21 the large piece of material 80 is exposed to twisting forces and is urged to move axially along the drums. These actions on a large piece of material result in the piece being successively exposed to positive primary 10 breaking actions and cause it to dance on the drums and do not allow it to settle on them. A similar action is imposed during secondary breaking. Thus problems associated with pieces of mineral settling on the drums and becoming grooved by the rotating teeth are avoided.

15 A further advantage resulting from the actions imposed on a large piece of material by the helical formations is that the large piece is positively moved along the axes of the drums thereby permitting smaller pieces to pass downwardly thereby and pass through the mineral breaker. Accordingly the 20 mineral breaker is able to handle an in-fill of mineral which contains a large variation in size such as mineral obtained in open-cast quarrying which contains small particulate material as well as large lumps of mineral.

It will be appreciated that the teeth impose tensile 25 breaking forces onto the mineral and so positively breaks the material with minimal production of fines. Additionally since each tooth passes between groups of teeth on the opposite drum positive sizing of mineral occurs since the maximum size of mineral passing through the sizer is determined by the space 30 between the trailing edge 47 of one tooth and the leading face 46 of a succeeding tooth and the distance between adjacent groups 19 of teeth. Therefore if the in-fill material contains only large pieces of mineral the mineral on leaving the sizer will contain no pieces over a predetermined size and will con- 35 tain a small quantity of fines.

It is also envisaged that the breaker drums may be inclined to the horizontal and arranged so that large pieces of

mineral are made to climb up the incline by the helical formations. Due to the agitation of the large piece of mineral it is likely to fall down the incline and is accordingly repeatedly moved along the drums until it has been broken down sufficiently to be broken by the secondary breaking action.

As shown schematically in Figure 7, the mineral sizer according to the present invention is normally located above a takeaway conveyor TC so that the axes of the drums are generally parallel to the direction of travel of the conveyor TC. By setting the sizer so that the spacing between the drums is generally located above the longitudinal axis of the conveyor material being deposited by the sizer onto the conveyor TC is arranged centrally thereon. This is advantageous as it minimises spillage.

Referring now to the specific construction of the mineral sizer shown in Figure 1, each drum assembly 15 is shown in longitudinal section in Figure 4 and includes a stepped shaft 25 on which is keyed a support sleeve 26 made up of three support sleeve portions 26a, b and c. The centre sleeve 26b is of larger internal diameter so that it can be easily slid over most of the shaft 25 during assembly and disassembly. The sleeve portions 26a, b and c are fixedly secured to one another by weld lines 26d so as to form an integral sleeve 26 running the majority of the length of the shaft 25.

A series of annular support rings 28 are mounted on each sleeve 26 and are secured to one another and also to sleeve 26 by weld lines 30. Each ring 28 has a series of teeth support projections 34 integrally formed therewith which are spaced circumferentially about its periphery. Each ring 28 is conveniently formed from a cast metal.

Accordingly, the rotational position of each ring 28 may be easily set during assembly to align or stagger the teeth support projections 34 of adjacent rings 28 by rotating the rings 28 on sleeve 26 and then fixedly securing them in that position. In Figure 4, the projections 34 on adjacent rings 28 have been set so that the projections form longitudinally extending rows which are substantially parallel to the axis of

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rotation of the drum assembly 15 in contrast to the arrangement in Figure 1 wherein adjacent rings 28 have been set so that the projections 34 form the longitudinally extending helical formations 21.

5 In Figure 8 an alternative construction is illustrated wherein the annular support rings 28 are each keyed or splined directly onto the shaft 25. Each ring 28 is therefore only in abutment with its neighbour and the assembly of rings 28 are prevented from axial movement by virtue of a shoulder 25x and
10 a removable collar 25z. Accordingly should the shaft or a ring become damaged during use, the shaft and ring assembly may be disassembled for replacement of the damaged component. It will be appreciated that each ring may be easily angularly offset to its neighbour to provide the desired helical formation
15 ation 21, the amount of offsetting being determined in steps dictated by the pitch of the splines.

A further alternative is to cast the series of annular support rings and shaft integrally with one another.

A tooth sheath 40 is secured to each projection 34 via a
20 bolt 41, or other similar means such as a sprung spigot, which is located in pockets 42 in the sheath and are thus protected from damage during use. When all sheaths are in position they collectively form a cover over adjacent rings 28 so that the rings are protected from wear by mineral being sized.

25 Each sheath 40 has an annular base portion 43 which follows the contour of ring 28 and a hollow tooth portion 45 integrally connected to the base portion 43. The tooth portion 45 has an internal pocket which is of a complementary shape to a projection 34 so when the tooth portion is seated upon a
30 projection, loads imparted onto the tooth portion 45 during use are transmitted onto the projection 34.

In this respect, during use each tooth is exposed to two main sources of loadings; firstly a loading on its leading face 46 resulting from a primary or secondary breaking action
35 and secondly a loading on its trailing edge 47 resulting from a secondary breaking action. The shape of projection 34 and that of tooth portion 45 is chosen so that when the tooth is

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exposed to the first type of loading the face 46 transmits the loading onto the leading face 150 of projection 34 and is encouraged to move in a generally radially inward direction so that the sheath 40 is pressed onto the projection 34 and peripheral surface of ring 28. The shape of the trailing edge 47 and of the complementary surface 53 of projection 34 are chosen to provide a wedge effect to restrain movement of the sheath 40 in a generally circumferential direction about ring 28, the wedge effect serving also to transmit loadings on the trailing edge 47 onto the complementary surface 53. Accordingly loadings arising from breakage of mineral are transmitted on to the rings 28 and so bolts 41 are not exposed to loadings and merely act to retain its associated sheath on a projection 34.

As seen in Figure 2 a rebate 60 is preferably provided at the base of each face 46 to receive a marginal end portion of the annular base portion 43 of the preceding sheath 40. If desired the base of each tooth and the base portion 43 of each preceding sheath 40 may be joined together by welding to thereby form a more rigid annular cover for each ring 28.

It will be appreciated that during use, portions of each sheath 40 will wear away and that eventually the sheaths 40 will have to be replaced. This is easily and quickly done with the present sizer by removal of bolts 41 (and, if appropriate removal of weld) and so refurnishment of the sizer teeth may be quickly achieved on site by personnel without the need of heavy lifting gear. Additionally, the inner surfaces of the side walls and end walls may be lined with steel plate which act as wear plates 50, 51 respectively to protect the side and end walls from abrasive wear. The wear plates are removably secured in position so that they can be replaced periodically after excessive wear has occurred.

A row of teeth 62 are provided to extend longitudinally along each side wall to intermesh with teeth 20 to prevent material passing between the side wall and adjacent drum assembly. The teeth 62 are conveniently secured to wear plates 50 by welding.

An alternative ring and tooth construction is illustrated with reference to Figures 9 - 16 wherein similar parts are designated by similar reference numerals.

5 In Figures 9 and 11 there are shown two alternative support rings 28 which are intended to be keyed directly to a shaft as in the Figure 8 embodiment and which are of different external diameter but are intended to receive the same dimensioned tooth sheath 130.

10 Each support ring 28 shown in Figures 9 and 11 is provided with a series of teeth support projections 34 which are integrally cast with the support ring.

The tooth cap 130 illustrated in Figures 12 to 16 is cast from a suitable wear resistant material and its external shape is designed so as to be symmetrical about section lines 15 VII-VII and VIII-VIII respectively. The terminal end of each cap 130 terminates in the form of a ridge 136 which extends in the direction of rotation of the drum. By varying the length of the ridge 136 the strength of the tip of the tooth can be adjusted. The cap 130 has an internal pocket or recess 131 20 for receiving a projection 34, the recess 131 having a shape complementary to the shape of projection 34 so that loadings are transmitted onto the projection 34.

As seen in Figures 9 to 11 each projection 15 has a pair of recesses 118 (only one of which is visible in Figures 9 and 25 11) and the internal recess 131 of each cap 130 has inwardly projecting flanges 132 of complementary shapes to recesses 118 so that the flanges 132 and recesses 118 co-operate to positively key the tooth caps 130 in position. The caps 130 and projections 34 each have co-operating bores 134 passing there- 30 through to enable a bolt to be passed through for preventing removal of the cap from an associated projection.

By altering the diameter of the support rings but retaining the same shape of projection 34 it is possible to use the same size of caps 130 for different diameters of breaker 35 drums. This is illustrated by comparison between Figures 9 and 11 wherein the bottom edge of each tooth cap 130 is of the same radius of curvature as the diameter of ring 28 in Figure

11 whereas in Figure 9 the radius of curvature of the ring 28 is greater. Accordingly, in order to accommodate caps 130 on ring 28 shown in Figure 9, complementary curved support surfaces 139 are provided separated by ridges 138.

5 A further alternative of a tooth sheath is illustrated in Figures 17, 18 and 19 wherein the tooth sheaths 40 on a given support ring 28, in addition to being connected to a respective projection 34 by a bolt 41, the tooth sheaths are also connected to one another by a connection formation 200 which is
10 itself preferably tooth shaped. Accordingly, at one circumferential end of each sheath 40 is provided first part 201 of the formation 200 and at the other circumferential end with a second part 202 of the formation 200. The first part 201 is generally tooth shaped having a leading face 203 and trailing
15 face 204. The first part 201 is provided with a centrally located recess 206 into which the second part 202 of a preceding sheath 40 projects. Both the first part 201 and second part 202 are provided with through bores 208 which align when adjacent sheaths are positioned on a ring 28 and through which
20 a bolt (not shown) is passed in order to secure co-operating parts 201, 202 together. The provision of connection formations 200 stabilises the annulus of connected sheaths 40 extending about a given ring 28 and serves to reduce chatter between the sheaths 40 and ring 28 during use. In view of the
25 stabilising effect it has been found possible to provide the teeth 20 with a leading face 46 which has a positive rake as is clearly illustrated in Figure 17.

 A further alternative shape of tooth 20 and corresponding projection 34 is illustrated in Figures 20 to 23 wherein the
30 tooth 20 is in the form of a pick having a generally cylindrical body. In this embodiment the sheaths 40 are secured onto a given ring 28 by being connected to one another by connection formations 200 only.

 It is to be appreciated that drums assembled from any of
35 the tooth sheath constructions described above are preferably arranged so that the teeth form helical formations 20. By way of further example reference is made to Figure 23 which is a

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view similar to Figure 1 and in which each drum includes a series of sheaths as shown in Figures 20 - 22 arranged to define helical formations 21. It is however also possible in certain applications for the teeth 20 to be arranged in rows extending generally parallel to the axis of the drum. It is also envisaged that the helical formations 21 on both drums may extend about their respective axes in the same sense. In such a situation large pieces of mineral deposited on the drums will be acted upon by the helical formations on one drum to move in one axial direction and be acted upon by the helical formations on the opposite drum to be moved in the opposite axial direction. Such movement results in an agitation of the large pieces of mineral deposited on the drums and so assist gripping of the mineral by the teeth. A further alternative is for one drum to have a helical formation and the other drum to have teeth aligned in rows arranged parallel to the axis of the drum.

It is also envisaged that the drums may be rotated in opposite directions so that material deposited thereon is moved toward the side walls of the sizer for breaking. Additionally it is also envisaged that a sizer having a single breaker drum may be provided in which the teeth on the drum co-operates with a side wall of the sizer housing and/or static teeth mounted thereon for breakage of mineral.

CLAIMS

1. A mineral breaker including a pair of side by side breaker drums each having breaker teeth projecting radially therefrom, the teeth on each drum being arranged in circumferentially extending groups of teeth, the groups
5 of teeth on one drum being located between adjacent groups of teeth on the other drum, the teeth on at least one of said pair of drums being arranged to define a series of discrete circumferentially spaced helical formations extending along the drum.
- 10 2. A mineral breaker according to Claim 1 wherein the teeth on both drums are arranged in discrete helical formations extending along each drum.
3. A mineral breaker according to Claim 2 wherein in use the drums are arranged to rotate in opposite direc-
15 tions, the helical formations on one drum being arranged in an opposite sense to the helical formations on the other drum so that the helical formations on both drums tend to move large pieces of mineral deposited thereon in the same axial direction.
- 20 4. A mineral breaker according to Claim 3 wherein the rotational positions of the drums are arranged so that during rotation each helical formation on one drum projects into the spacing between adjacent helical formations on the other drum.
- 25 5. A mineral breaker according to Claim 2 wherein, in use, the drums are arranged to rotate in opposite directions, the helical formations on one drum being arranged in the same sense to the helical formations on the other drum so that the helical formations on one drum tend to
30 move large pieces of mineral in an opposite axial direction to the helical formations on the other drum.
6. A mineral breaker according to any preceding claim further including a belt conveyor positioned beneath the breaker drums, the direction of travel of the belt con-

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veyor extending in a direction generally parallel to the axes of the breaker drums.

7. A mineral breaker according to Claim 6 when depend-
ant on Claims 4 or 5 wherein the drums are arranged to
5 deposit mineral broken by the breaker centrally on the
belt conveyor.

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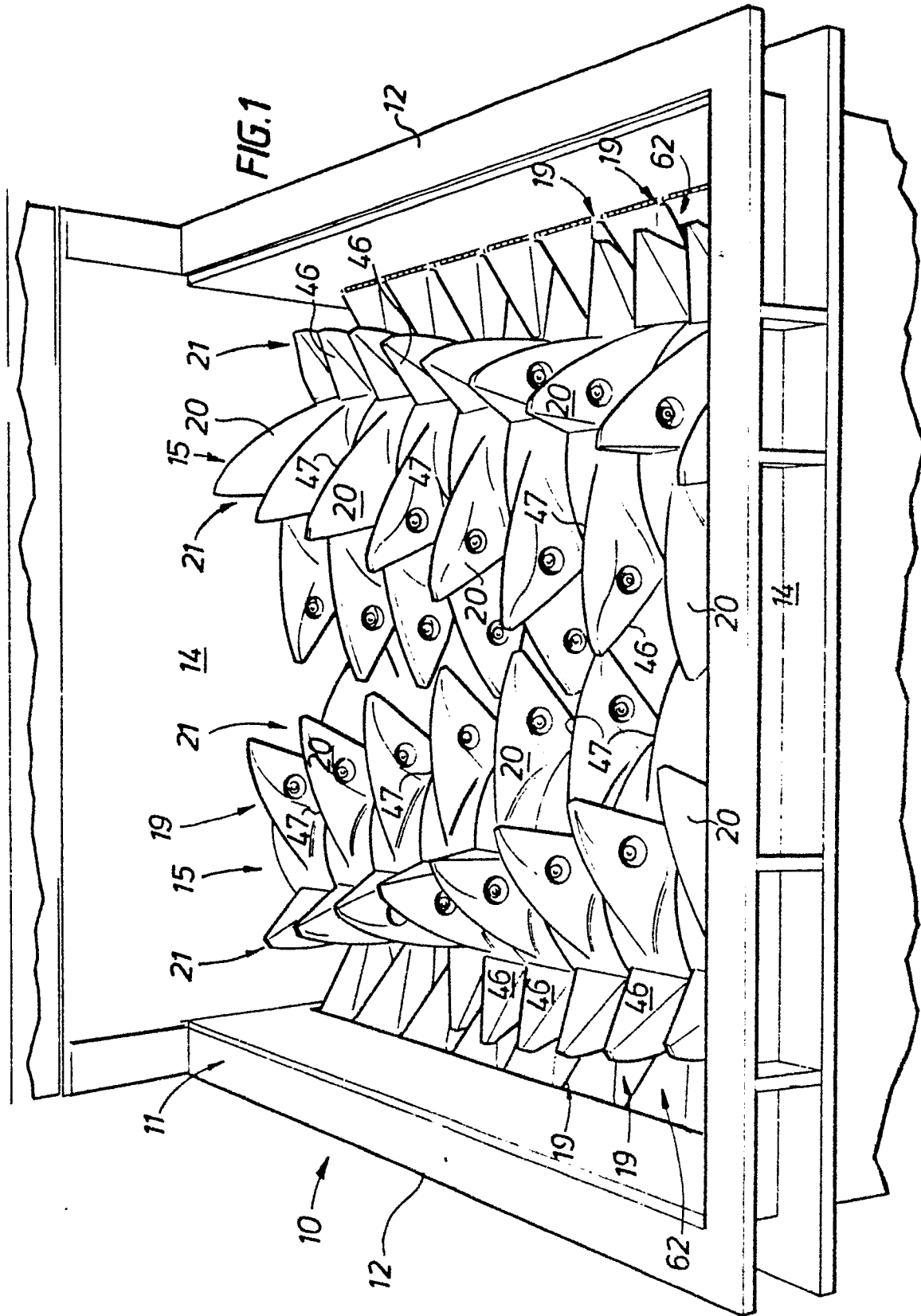
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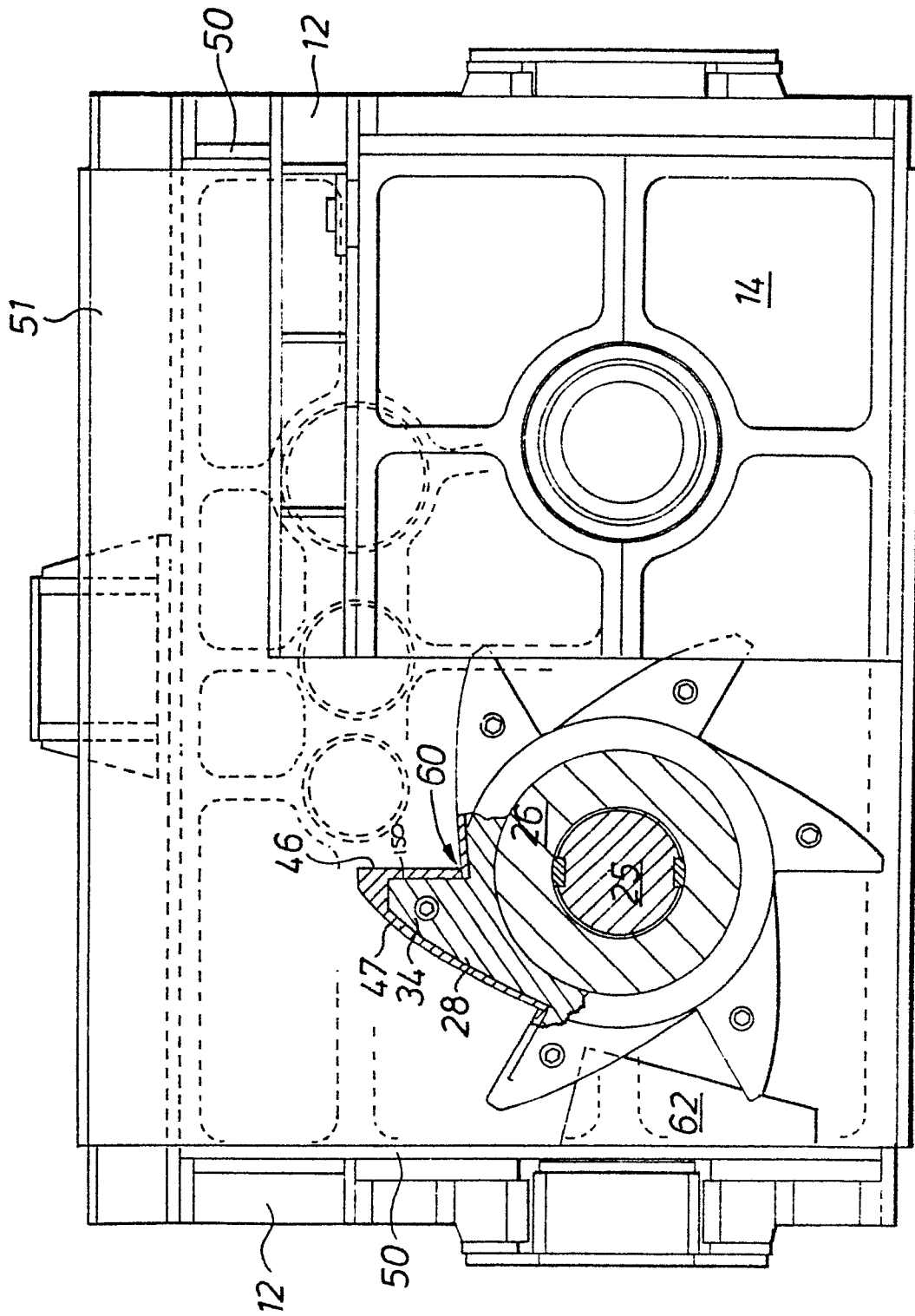


FIG. 2

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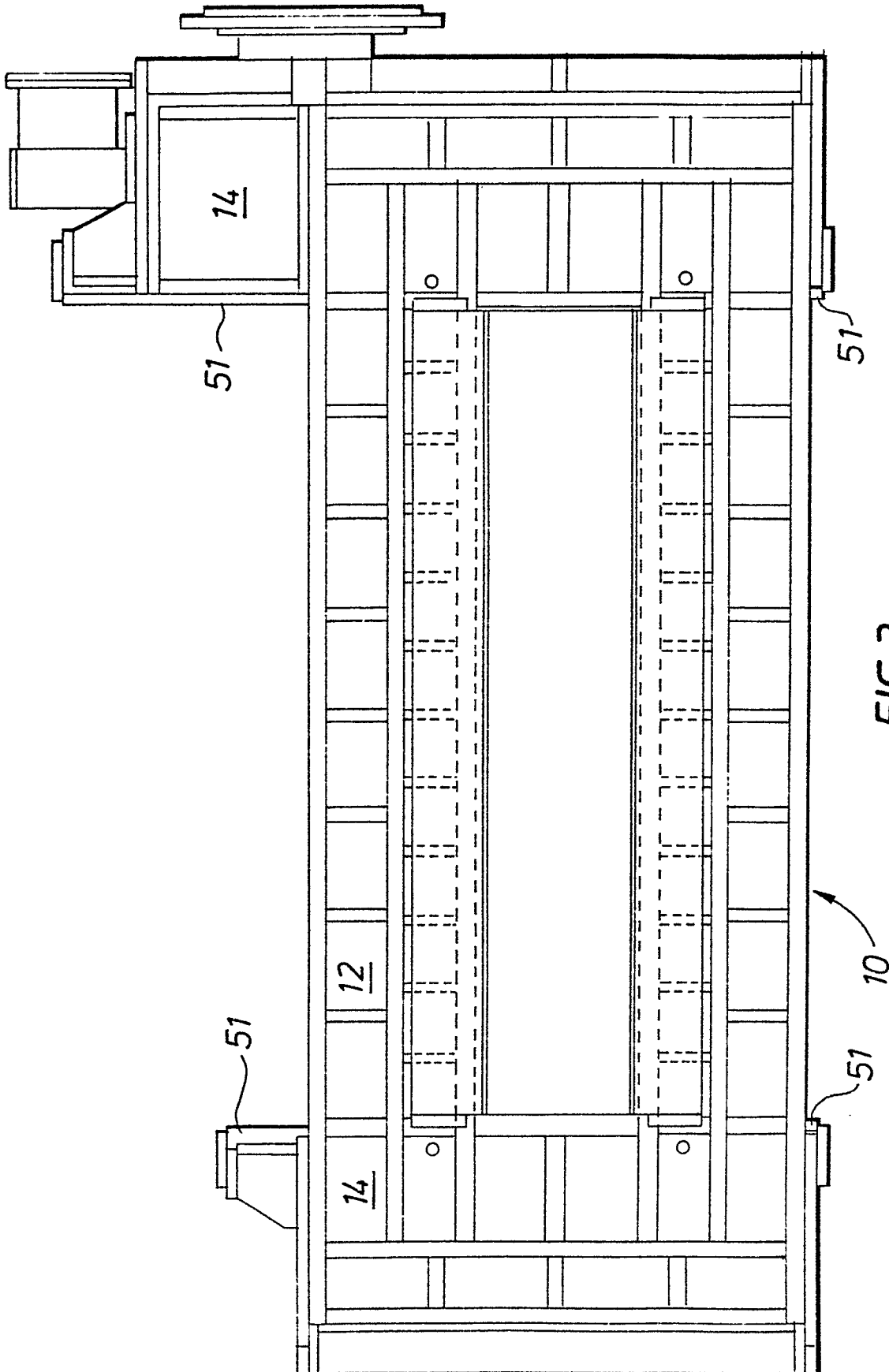
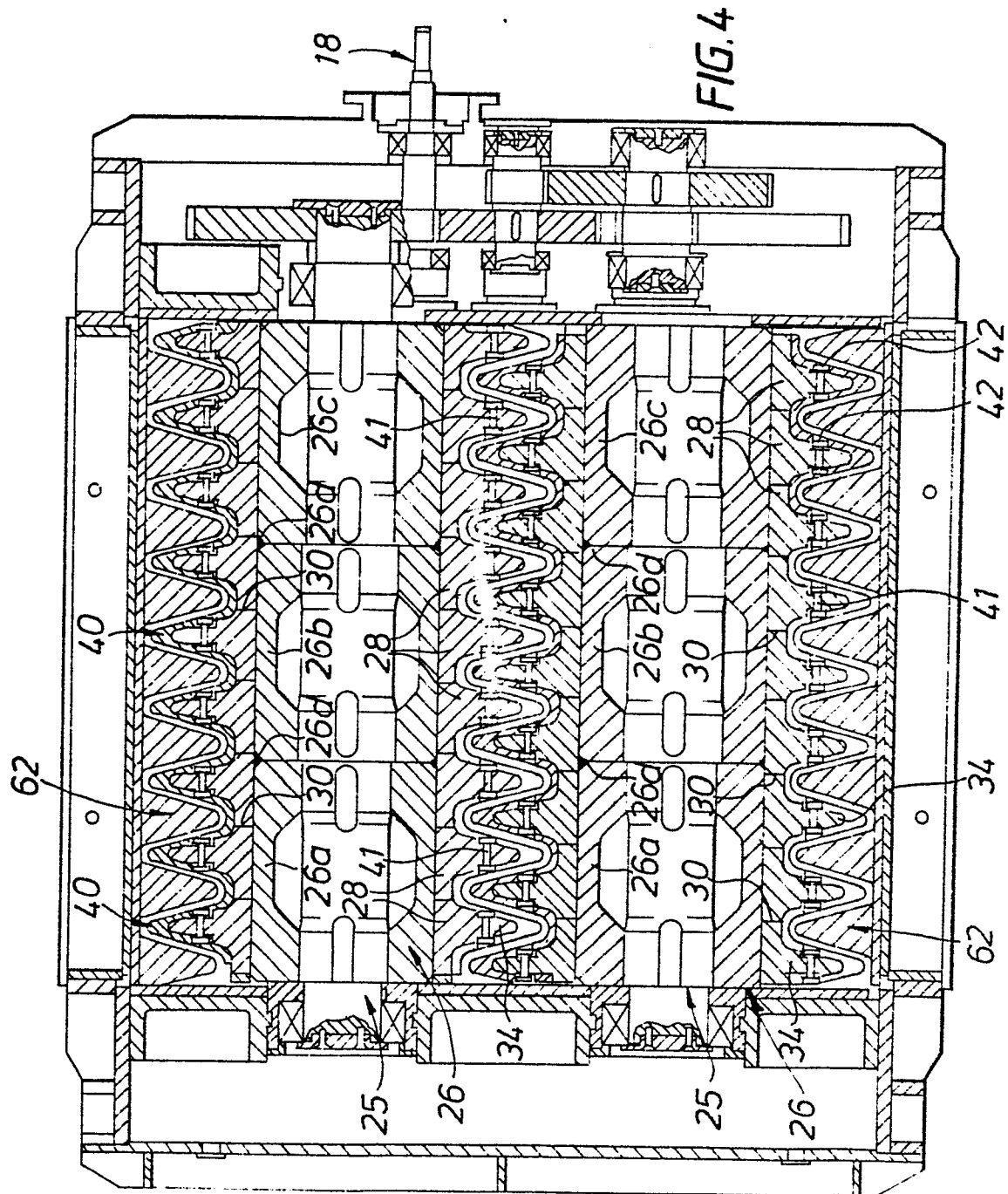


FIG. 3

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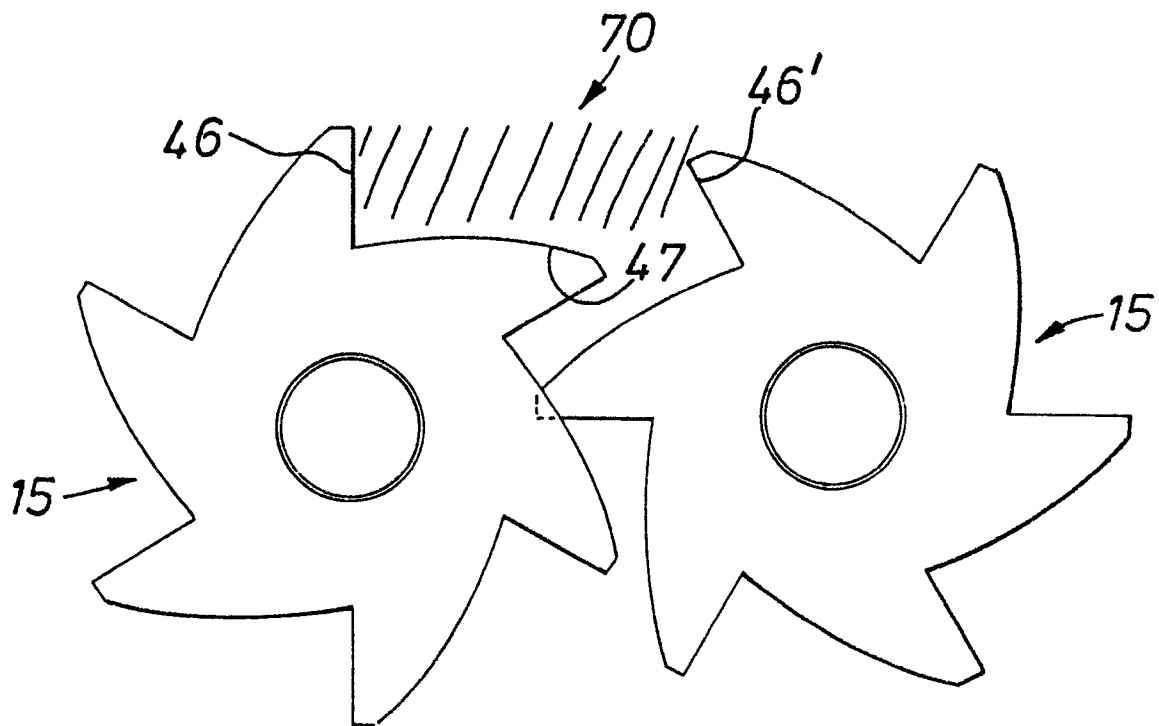


FIG. 6

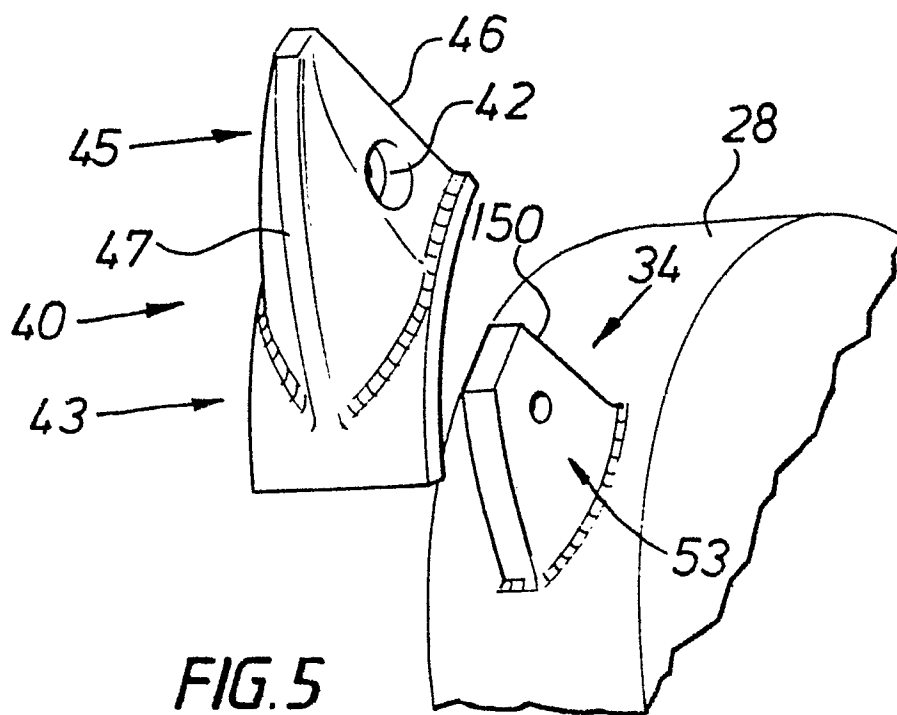


FIG. 5

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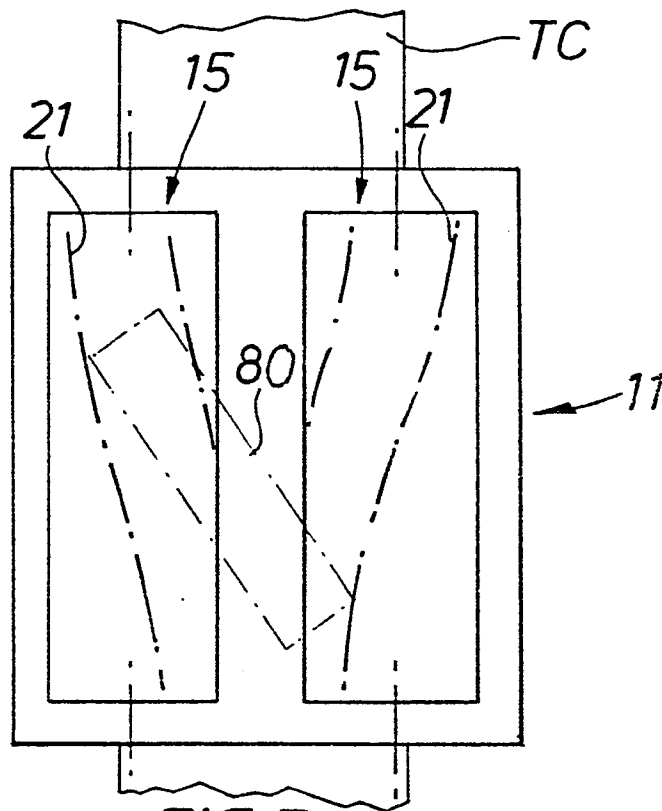


FIG. 7

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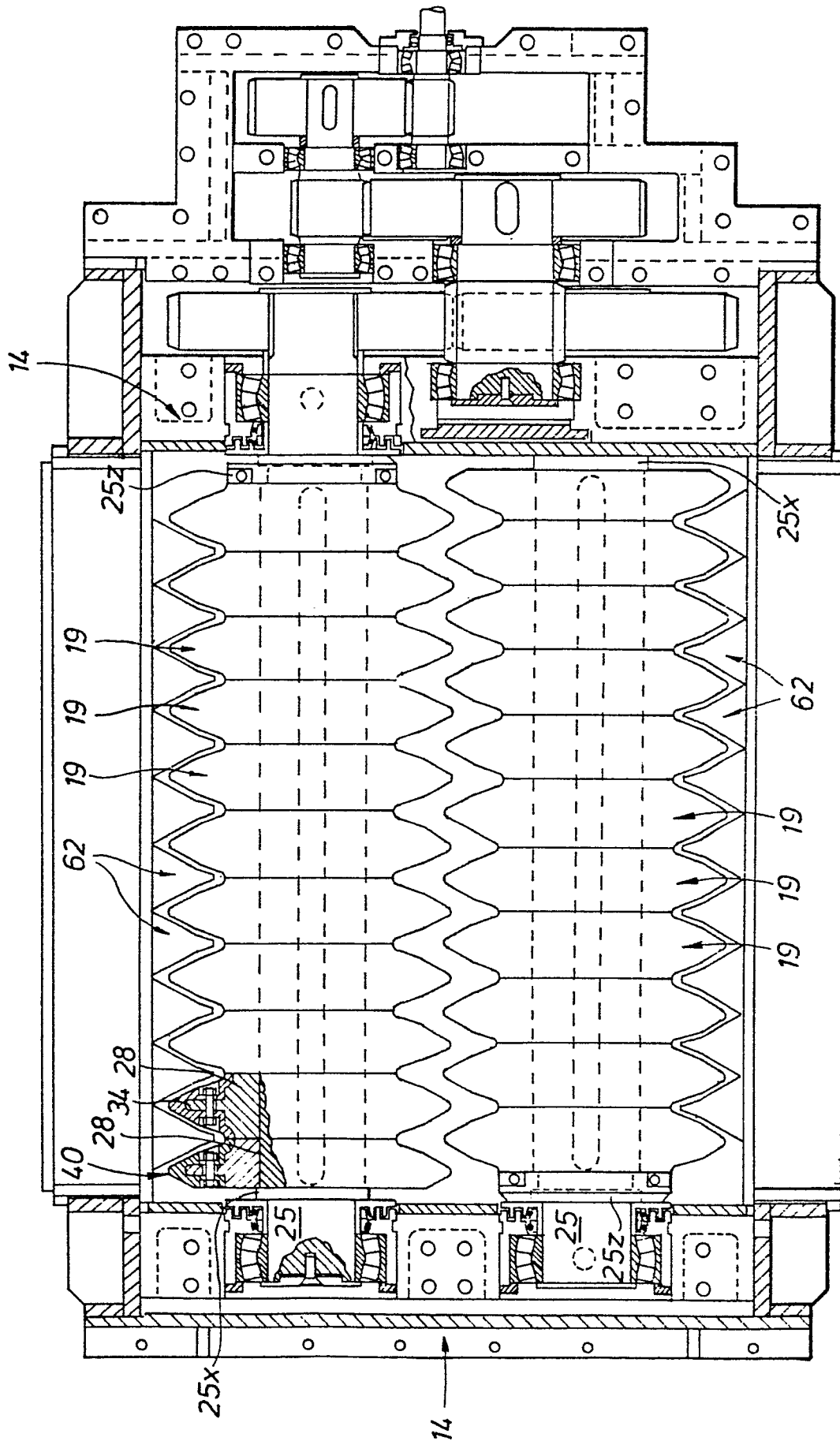


FIG. 8

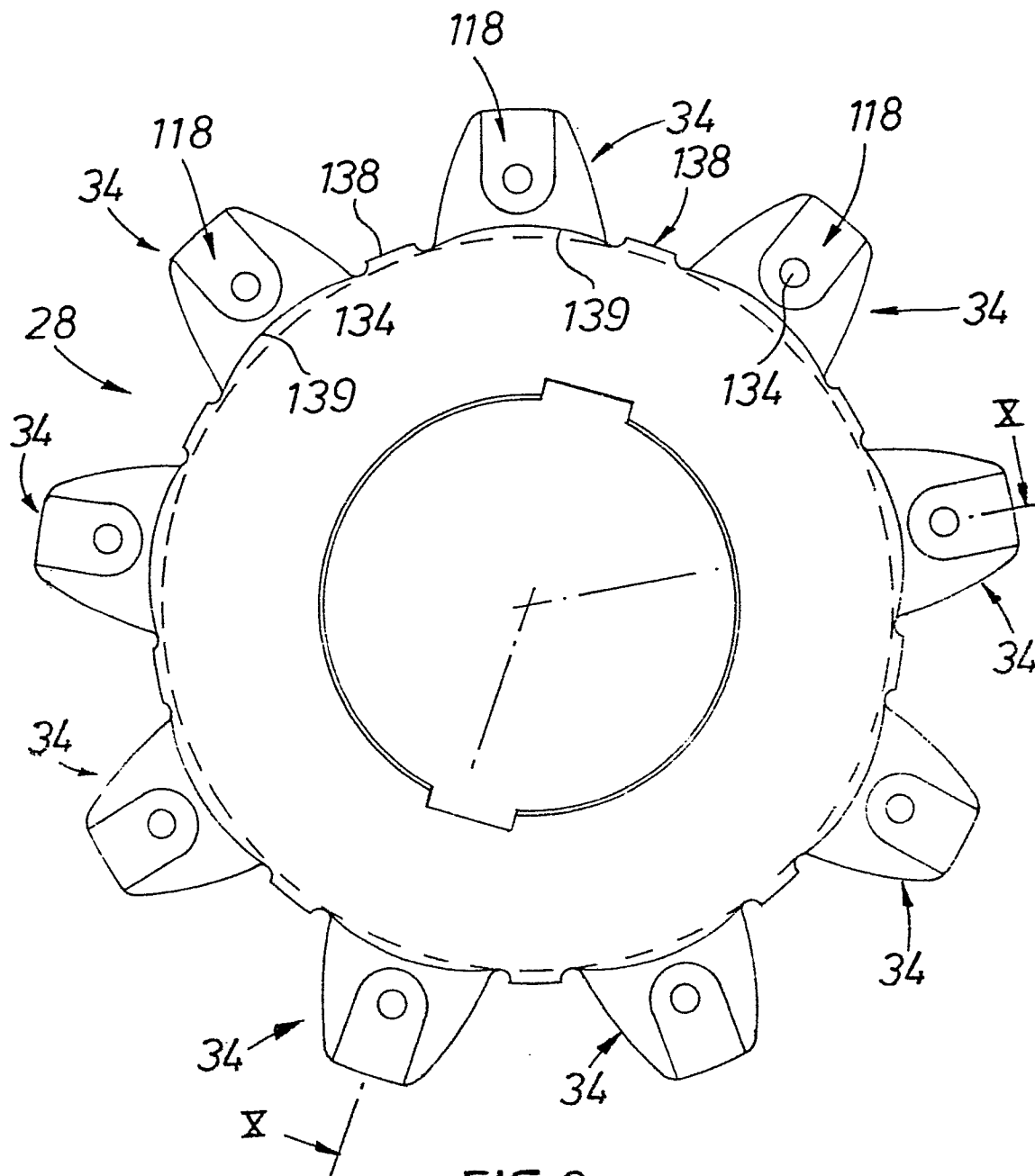
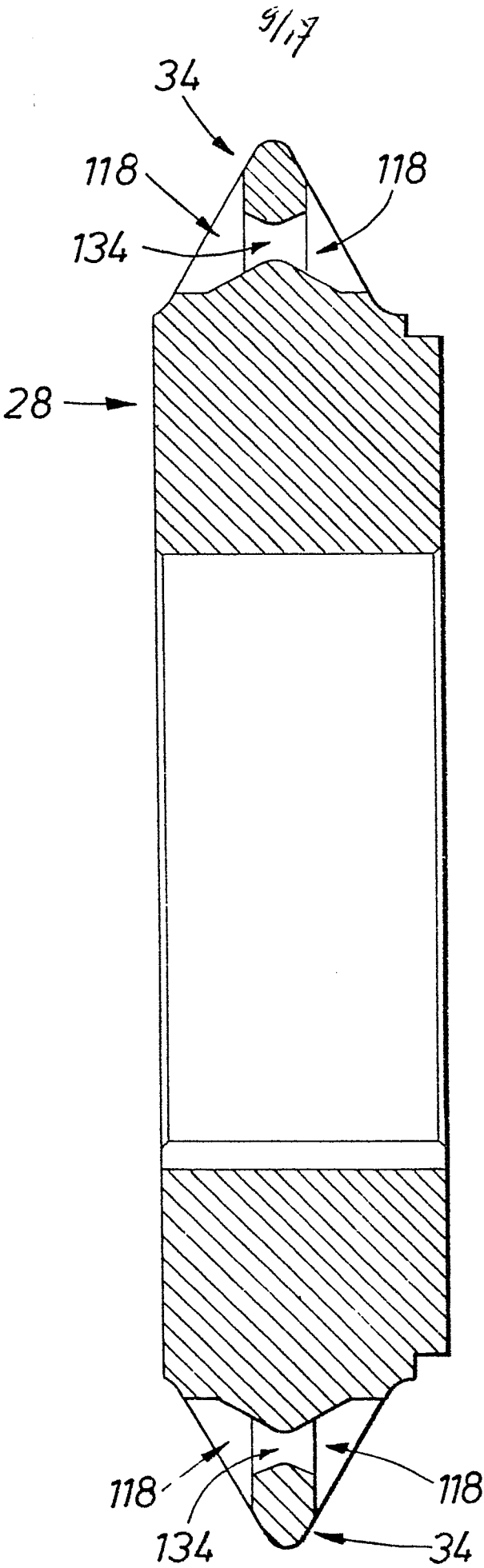


FIG. 9



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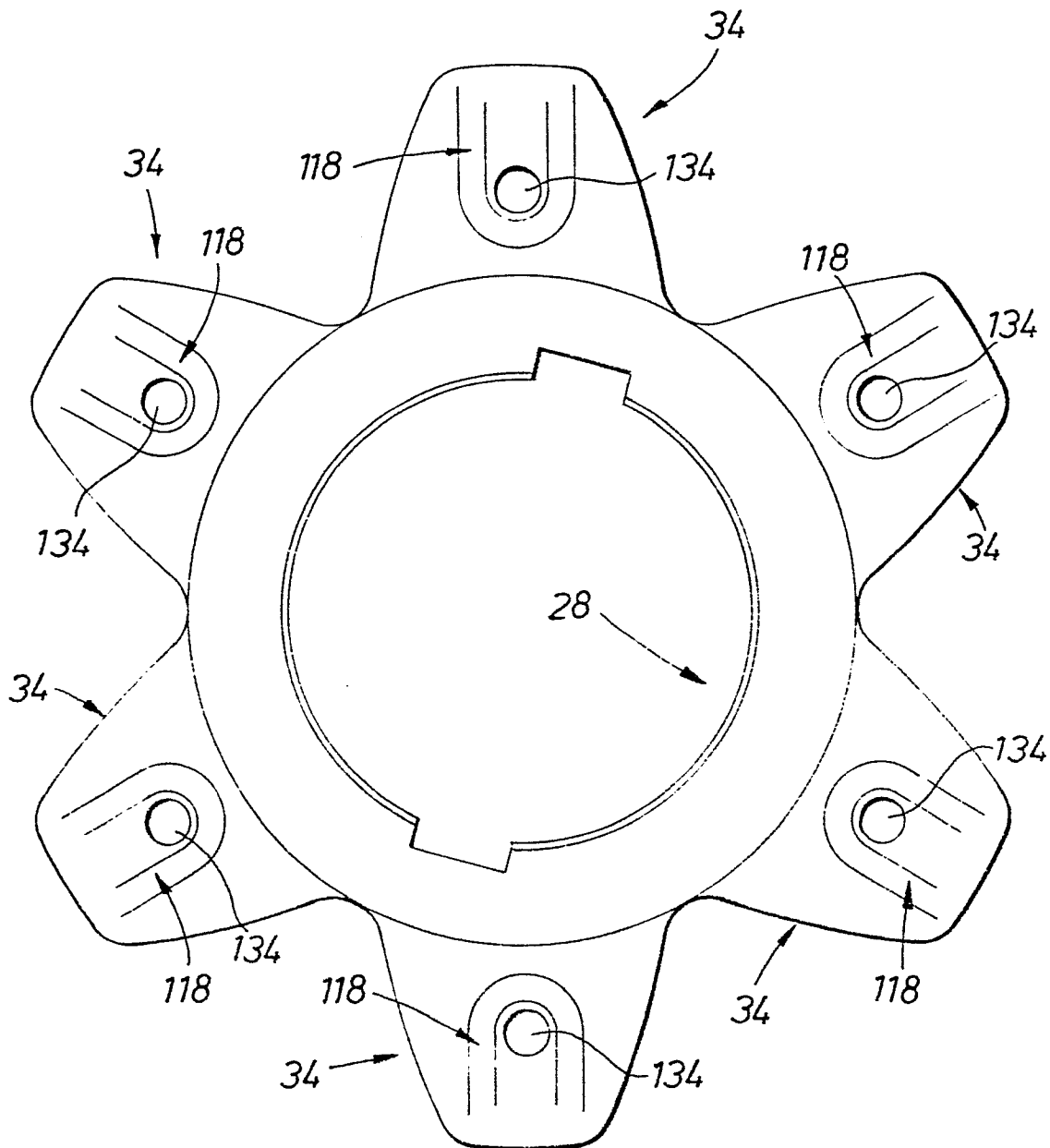


FIG. 11

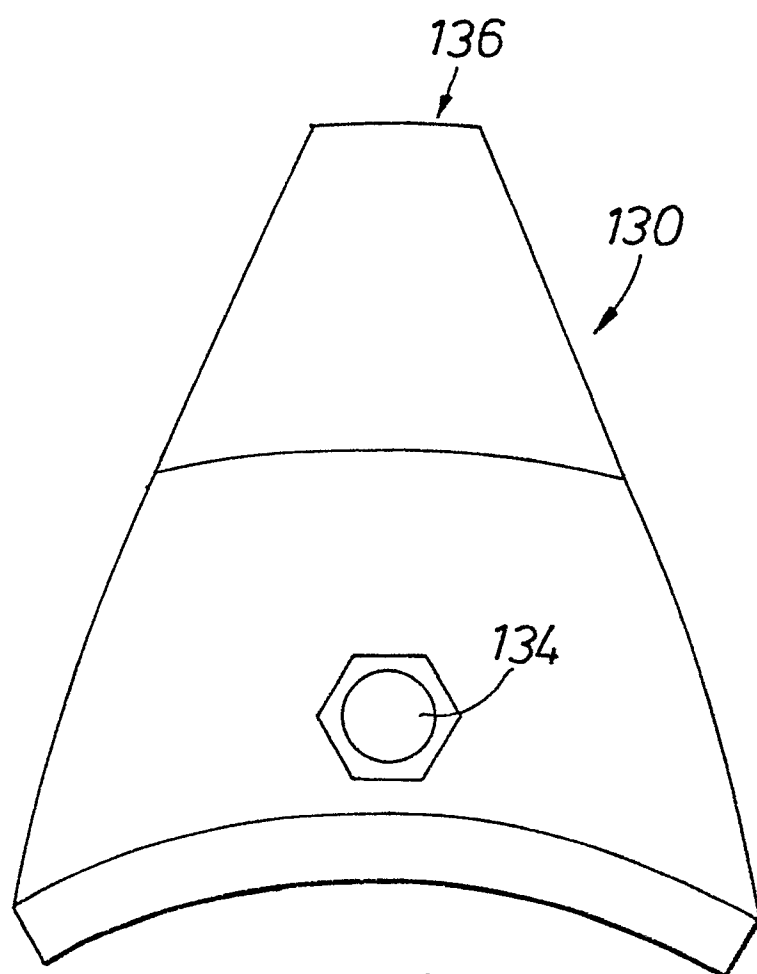


FIG. 13

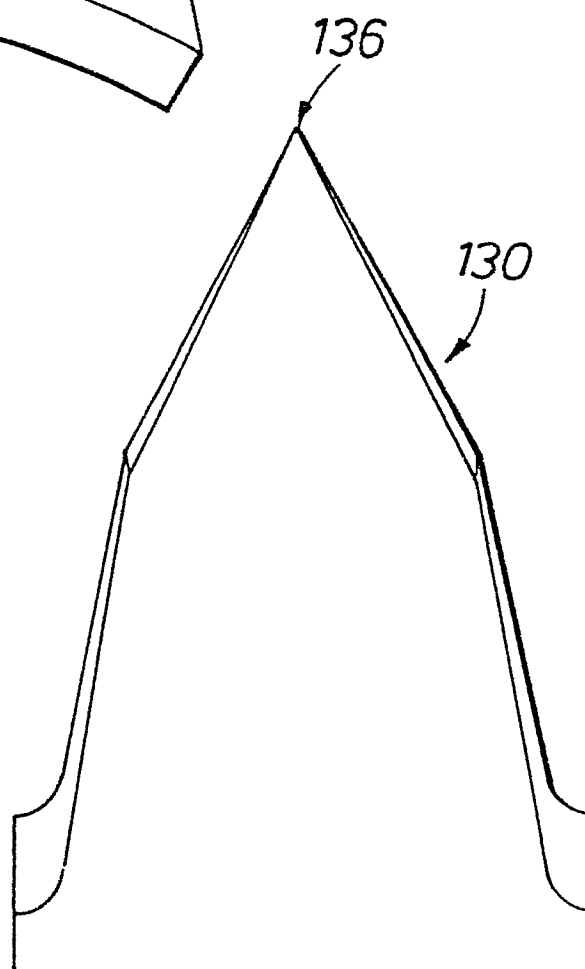


FIG. 12

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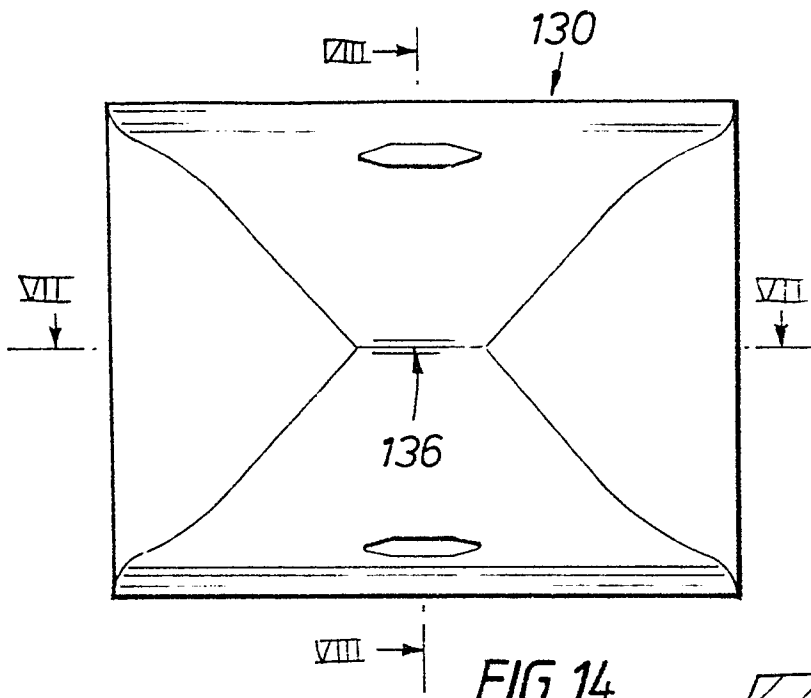


FIG. 14

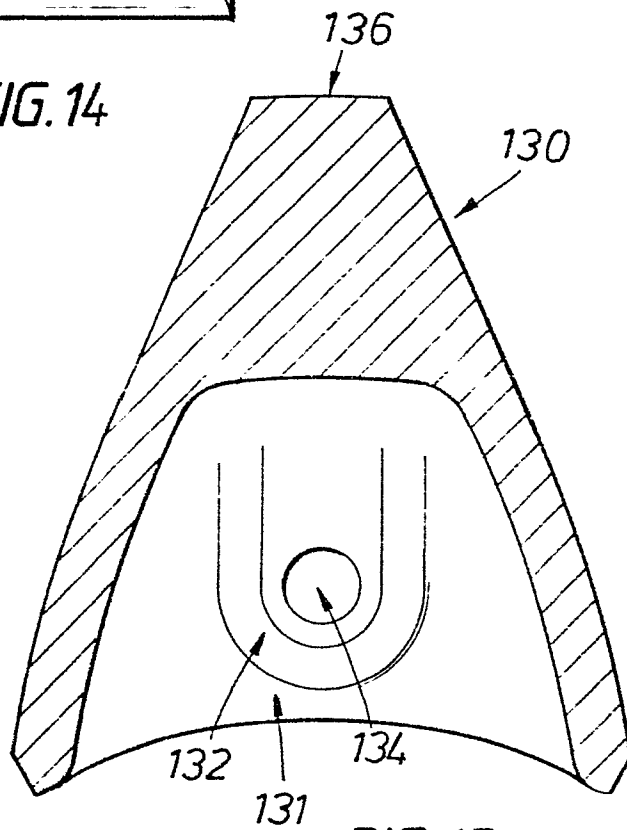


FIG. 15

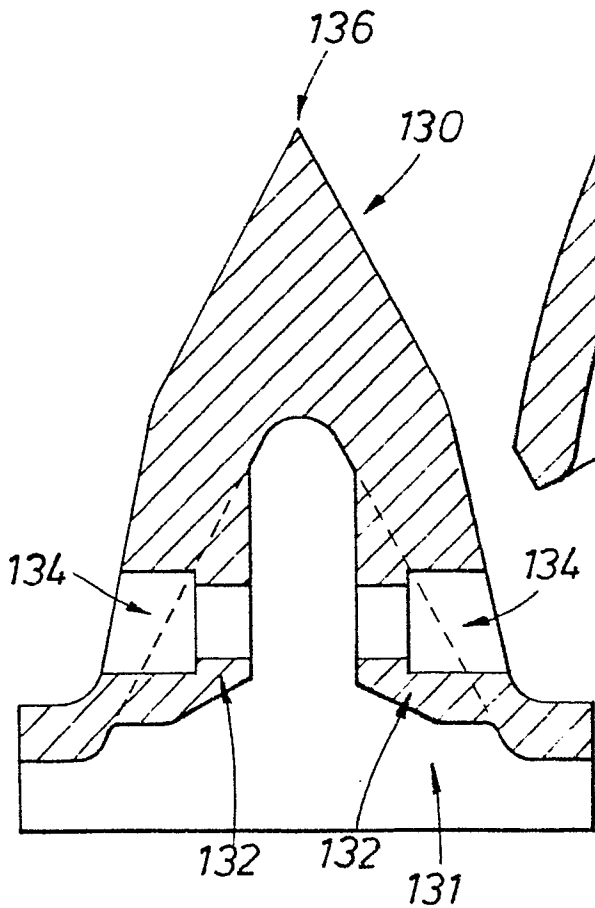


FIG. 16

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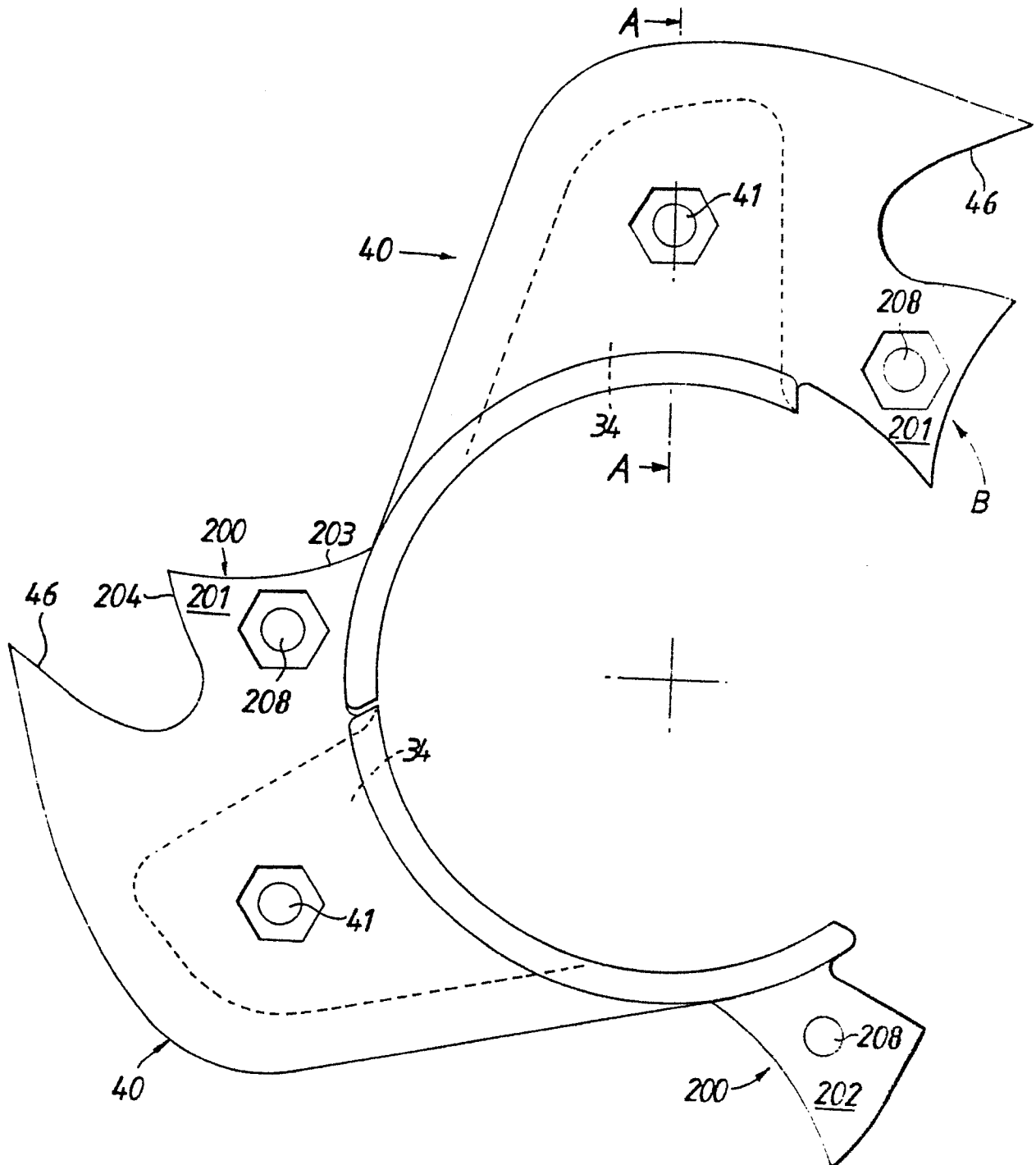


FIG 17

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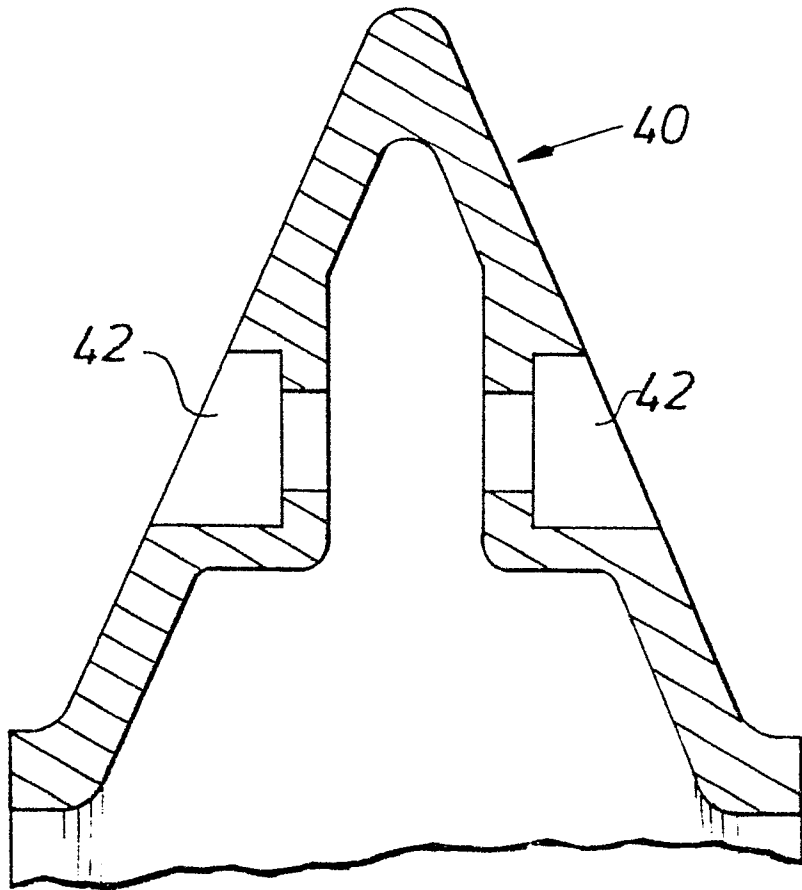


FIG 18

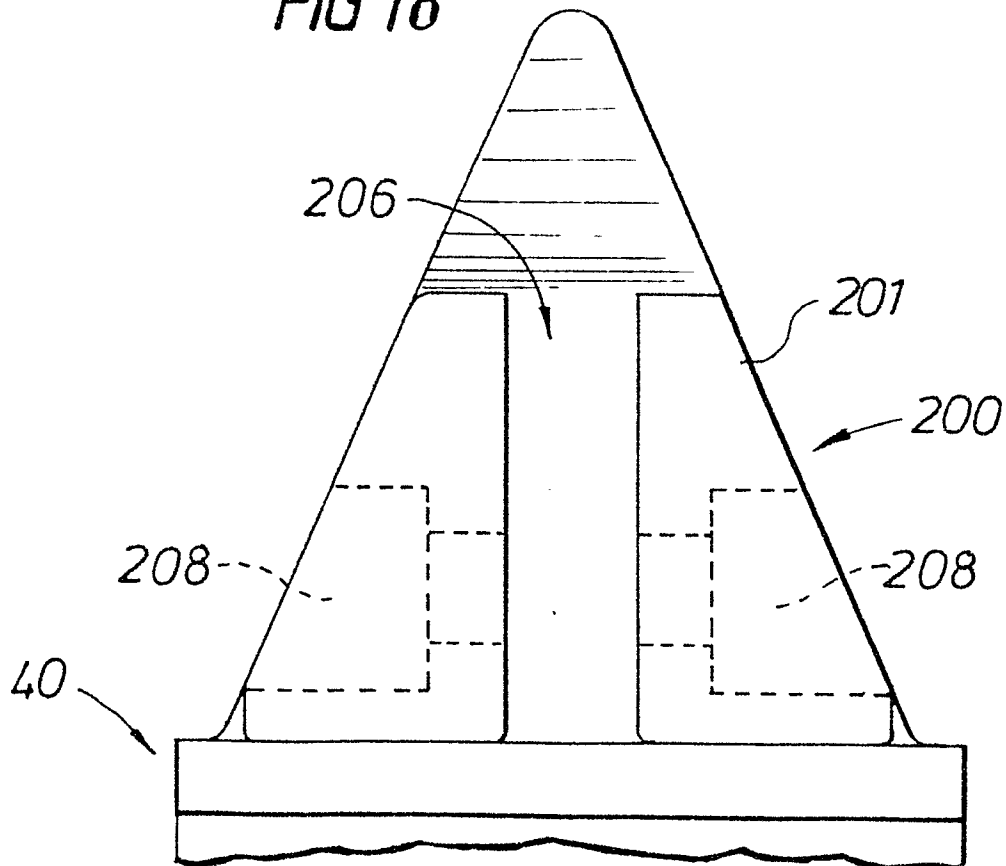


FIG. 19

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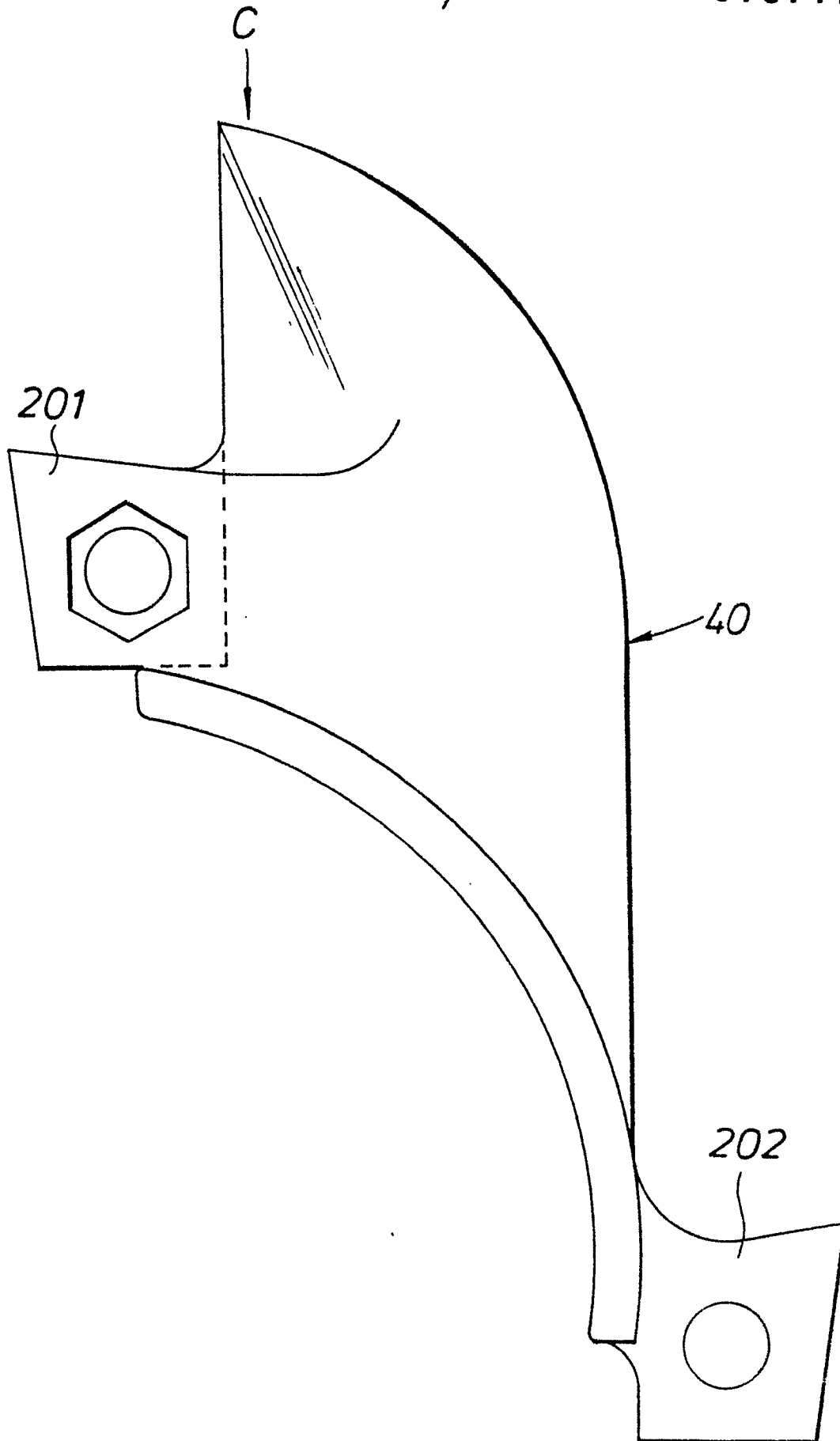
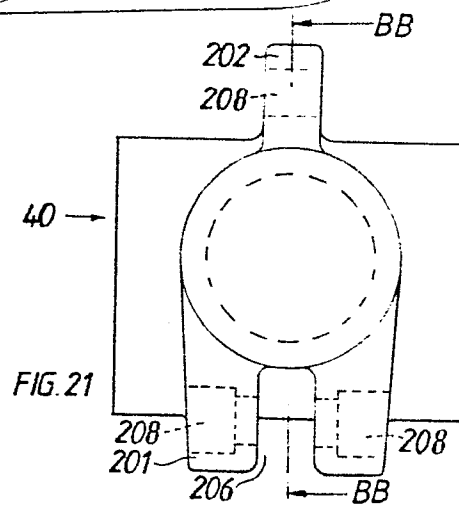
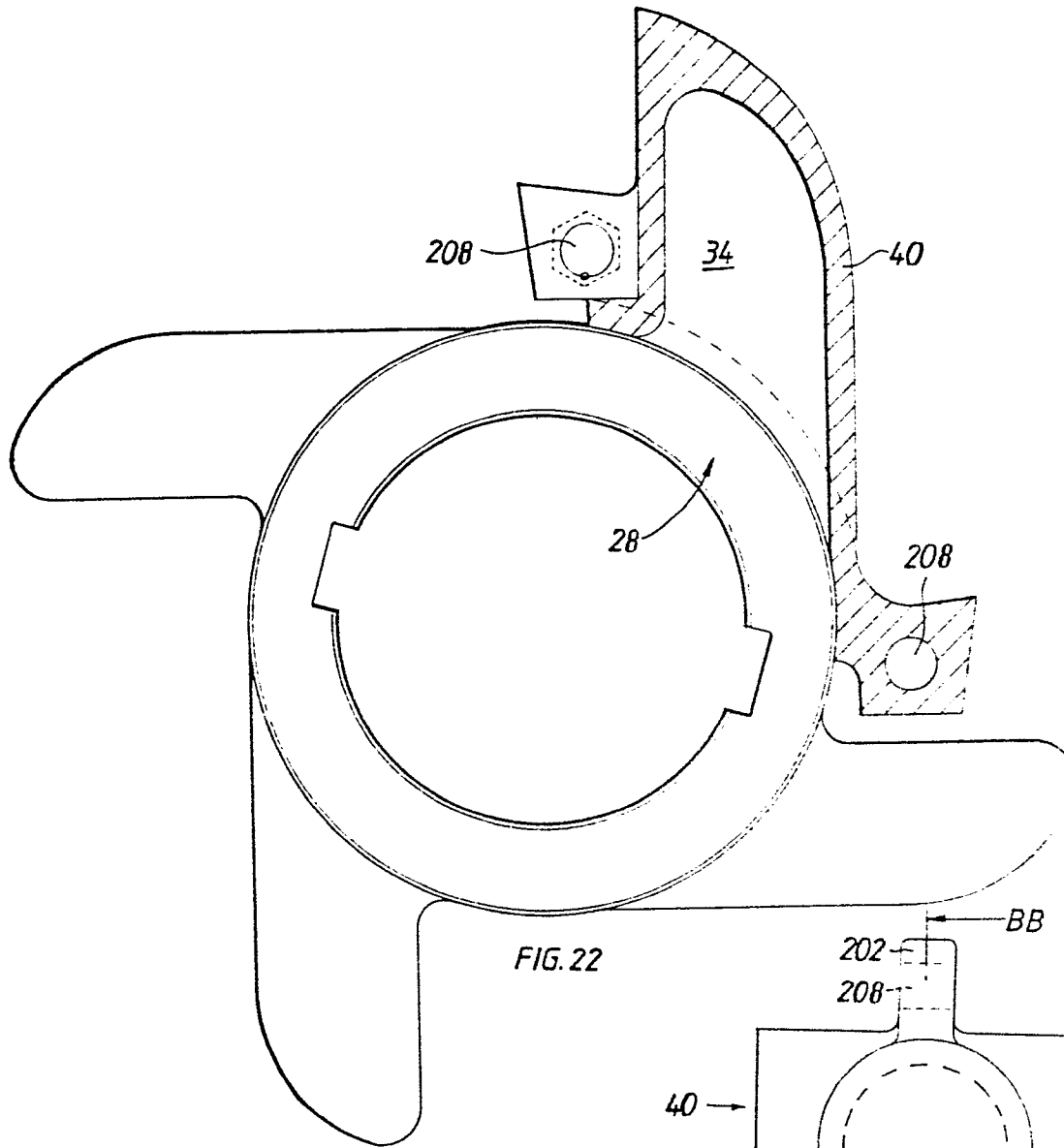


FIG. 20

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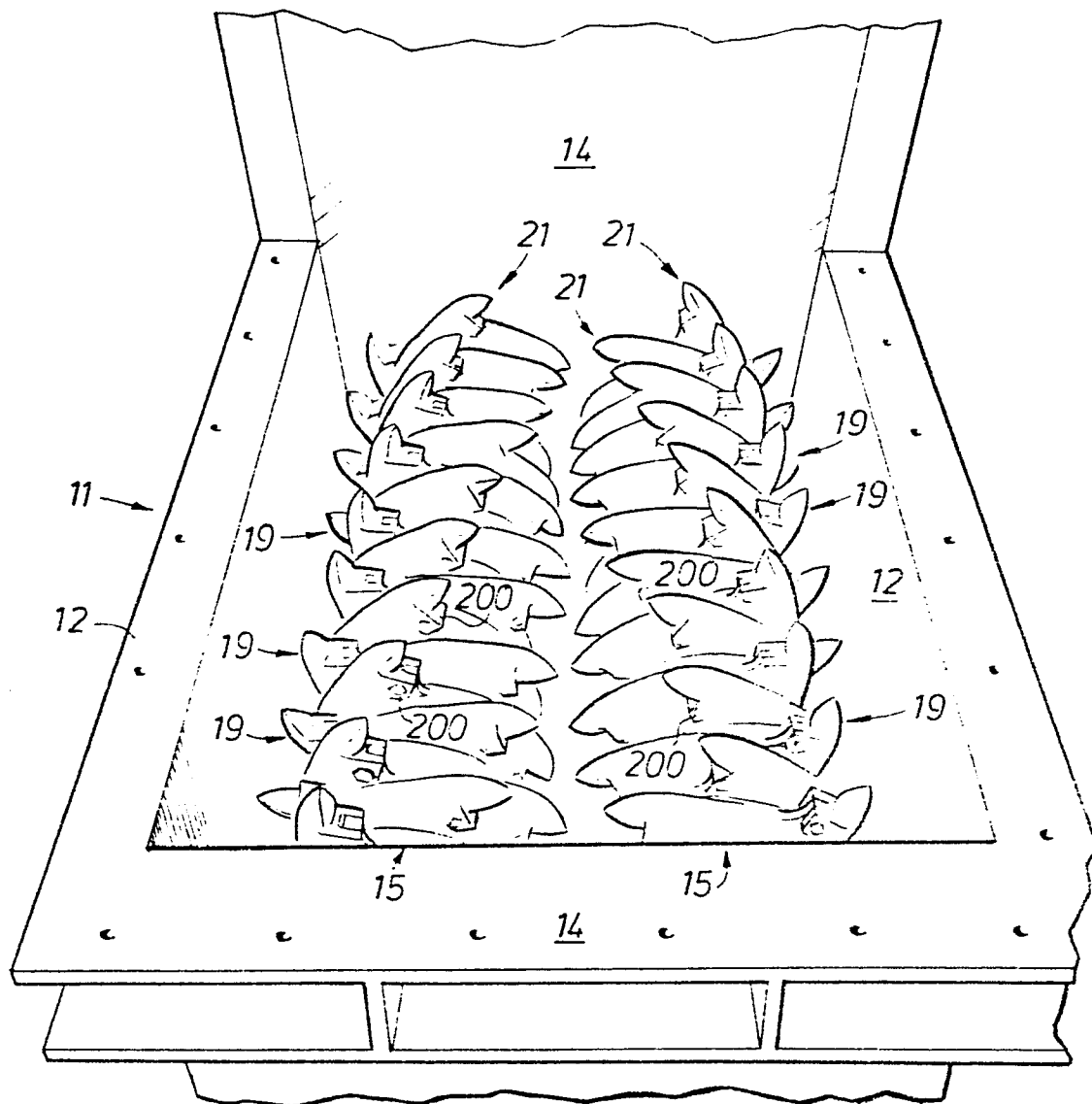


FIG. 23