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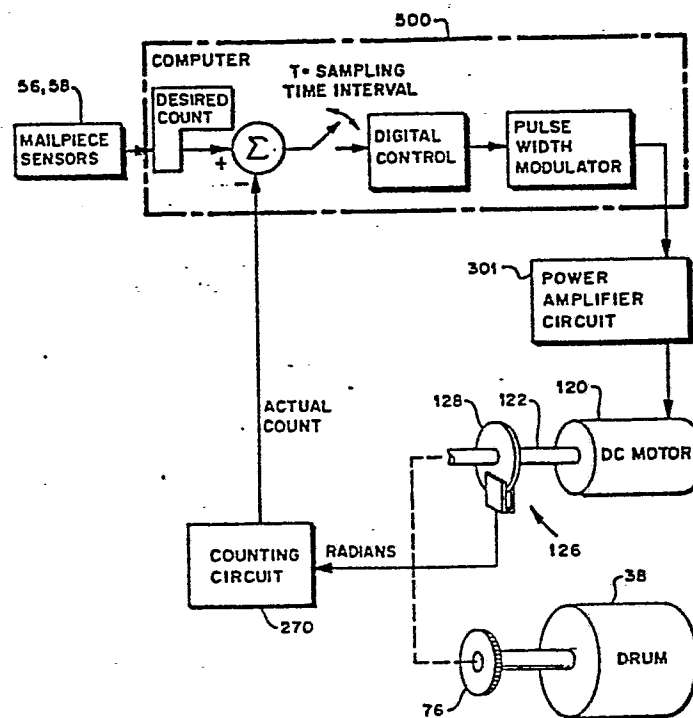
(54) **Postage meter apparatus having microprocessor-controlled D.C. motor and process for use therewith.**

(57) A postage meter includes a rotary drum (38) having a periphery adapted for feeding a sheet in a path of travel. A first device (56,58) senses a time interval during which a sheet is linearly displaced a predetermined distance in the path of travel. A d.c. motor (120) is coupled to the drum for rotation of the drum (38), and a second device (126) senses angular displacement of the drum (38). A computer (500) coupled to the first and second sensing devices (56,58,126) and to the d.c. motor (120) responds to the first sensing device (56,58) for providing respective amounts representative of desired angular displacements of the drum (38) during successive sampling time periods, responds to the second sensing device (126) for providing respective amounts representative of actual angular displacements of the drum (38) during successive sampling time periods, compensates for the difference between desired and actual angular displacements and generates a d.c. motor control signal for controlling rotation of the motor (120) to cause the linear displacement of the periphery of the drum (38) to substantially match the linear displacement of the sheet during respective sampling time periods. The computer (500) may also generate a d.c. motor control signal for controlling

rotation of the motor (120) to cause the linear displacement of indicia printing means of the drum to initially engage the sheet in the path of travel a predetermined marginal distance from the leading edge of the sheet.

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FIG. 10



POSTAGE METER APPARATUS HAVING MICROPROCESSOR -
CONTROLLED D.C. MOTOR AND PROCESS FOR USE THEREWITH

The present invention is generally concerned with postage meters and mailing machines, and processes for
5 operating such apparatus.

In U.S. Patent No. 2,934,009 issued April 26, 1960 to Bach, et al. and assigned to the assignee of the present invention there is described a postage meter which includes a drive mechanism connected by means of a drive train to a
10 postage meter drum. The drive mechanism includes a single revolution clutch for rotating the drum from a home position and into engagement with a letter fed to the drum. The drum prints a postage value on the letter while feeding the same downstream beneath the drum as the drum returns to the home
15 position. Each revolution of the single revolution clutch and thus the drum, is initiated by the letter engaging a trip lever to release the helical spring of the single revolution clutch. The velocity versus time profile of the periphery of a drum driven by the clutch approximates a trapezoidal
20 configuration, having acceleration, constant velocity and deceleration portions, fixed by the particular clutch and drive train used in the application. This being the case, the throughput rate of any mailing machine associated with the meter is dictated by the cycling speed of the postage
25 meter rather than by the speed with which the individual mailpieces are fed to the postage meter. Further, although

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the single revolution clutch structure has served as the
workhorse of the industry for many years it has long been
recognized that it is a complex mechanism which is relatively
expensive to construct and maintain, does not precisely
5 follow the ideal trapezoidal velocity vs. time motion profile
which is preferred for drum motion, tends to be unreliable in
high volume applications, and is noisy and thus irritating to
customers.

Accordingly, an object of the invention is to replace
10 the postage meter drum drive mechanism of the prior art with
the combination of a D.C. motor and a computer, and program
the computer for causing the D.C. motor to drive the drum in
accordance with an ideal trapezoidal-shaped velocity versus
time profile which is a function of the input velocity of a
15 mailpiece; and

Another object is to replace the trip lever as the
drive initiating device and utilize in its place a pair of
spaced apart sensing devices in the path of travel of a
mailpiece fed to the postage meter, and program the computer
20 to calculate the input velocity of a mailpiece, based upon
the time taken for the mailpiece to traverse the distance
between the sensing devices, and adjust the time delay and
acceleration of the drum before arrival of the mailpiece at a
position at which drum rotation is commenced to cause the
25 drum to timely engage the leading edge of the mailpiece.

According to one aspect of the invention,
in combination with a postage meter including a rotary
drum having a periphery adapted for feeding a sheet in a path
of travel, there is provided an improvement comprising:

5 first means for sensing a time interval during which a sheet
is linearly displaced a predetermined distance in the path of
travel; a d.c. motor coupled to the drum for rotation
thereof; second means for sensing angular displacement of the
drum; and computer means coupled to the first and second
10 sensing means and to the d.c. motor, the computer means
comprising: means responsive to the first sensing means for
providing respective amounts representative of desired
angular displacements of the drum during successive sampling
time periods, means responsive to the second sensing means
15 for providing respective amounts representative of actual
angular displacements of the drum during successive sampling
time periods, and means for compensating for the difference
between desired and actual angular displacements and
generating a d.c. motor control signal for controlling
20 rotation of the motor to cause the linear displacement of the
periphery of the drum to substantially match the linear
displacement of the sheet during respective sampling time
periods.

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Figure 8 is a truth table showing the status of the transistors in the power amplifying circuit for clockwise and counter-clockwise rotation of the D.C. motor;

Figure 9 shows the relationship between the encoder
5 output signals for various D.C. motor duty cycles;

Figure 10 shows a closed-loop servo system including the D.C. motor and computer;

Figure 11 is a block diagram portraying the laplace transform equations of the closed-loop servo system shown in
10 Fig. 10;

Figure 12 shows the equations for calculating the overall gain of the closed loop servo system of Fig. 10 before (Fig. 2a) and after (Fig. 2b) including a gain factor corresponding to the system friction at motor start up;

15 Figure 13 is a bode diagram including plots for the closed loop servo system before and after compensation to provide for system stability and maximization of the system's bandwidth;

Figure 14 shows the equation for calculating, in the
20 frequency domain, the value of the system compensator;

Figure 15 shows the equation for calculating the damping factor, overshoot and settling time of the servo controlled system;

Figure 16 shows the equation for the laplace operator
25 expressed in terms of the Z-transform operator;

Figure 17 shows the equation for calculating the value of the system compensator in the position domain;

Figure 18 shows the equations for converting the system compensator of Fig. 17 to the position domain;

Figure 19 shows the equation of the output of the system compensator in the time domain;

5 Figure 20 is a block diagram of a preferred microprocessor for use in controlling the D.C. Motor;

Figure 21 (including Figs. 21a, 21b and 21c) shows the time intervals during which the motor control signal and its separable components are calculated to permit early
10 application of the signal to the motor;

Figure 22 (including Figs. 22a and 22b) is a block diagram of the computer according to the invention; and

Figure 23 (including Figs. 23a-1, 23a-2, 23b and 23c) shows the flow charts portraying the processing steps of the
15 computer.

As shown in Fig. 1, the apparatus in which the invention may be incorporated generally includes an
20 electronic postage meter 10 which is suitably removably mounted on a conventional mailing machine 12, so as to form therewith a slot 14 (Fig. 2) through which sheets, including mailpieces 16, such as envelopes, cards or other sheet-like materials, may be fed in a downstream path of travel 18.

25 The postage meter 10 (Fig. 1) includes a keyboard 30 and display 32. The keyboard 30 includes a plurality of numeric keys, labeled 0-9 inclusive, a clear key, labeled "c" and a decimal point key, labeled ".", for selecting postage

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values to be entered; a set postage key, labeled "s", for entering selected postage values; and an arithmetic function key, labeled " $\pm$ ", for adding subsequently selected charges (such as special delivery costs) to a previously selected postage value before entry of the total value. In addition, there is provided a plurality of display keys, designated 34, each of which are provided with labels well known in the art for identifying information stored in the meter 10, and shown on the display 32 in response to depression of the particular key 34, such as the "postage used", "postage unused", "control sum", "piece count", "batch value" and "batch count" values. A more detailed description of the keys of the keyboard 30 and the display 32, and their respective functions may be found in U.S. Patent No. 4,283,721 issued August 11, 1981 to Eckert, et al. and assigned to the assignee of the present invention.

In addition, the meter 10 (Fig. 1) includes a casing 36, on which the keyboard 30 and display 32 are conventionally mounted, and which is adapted by well known means for carrying a cyclically operable, rotary, postage printing drum 38. The drum 38 (Fig. 2) is conventionally constructed and arranged for feeding the respective mailpieces 16 in the path of travel 18, which extends beneath the drum 38, and for printing entered postage on the upwardly disposed surface of each mailpiece 16. For postage value selecting purposes, the meter 10 (Fig. 1) also includes a conventional postage value selection mechanism 40, for example, of the type shown in U.S. Patent No. 4,287,825

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issued September 8, 1981 to Eckert, et al. and assigned to the assignee of the present invention. The mechanism 40 which is operably electrically coupled via the postage meter's computer 41 to the keyboard 30 and display 32, 5 includes a first stepper motor 42 for selecting any one of a plurality of racks 43, associated on a one for one basis with each of the print wheels 44, and a second stepper motor 45 for actuating each selected rack 43 for positioning the appropriate printing element of the associated print wheel 10 44. The rack selection stepper motor 42, which is referred to by skilled artisans as a bank selector motor, is appropriately energized via power lines 46 from the computer 41 for selecting the appropriate rack; and the rack actuating stepper motor 45, which is referred to by skilled artisans as 15 a digit selector motor, is appropriately energized via power lines 47 from the computer 41 to move the selected rack for selecting the appropriate digit element of the associated print wheel 44. A more detailed description of the value selection mechanism 40 may be found in the aforesaid U.S. 20 Patent No. 4,287,825.

The computer 41 for the postage meter 10 generally comprises a conventional, microcomputer system having a plurality of microcomputer modules including a control or keyboard and display module, 41a, an accounting module 41b 25 and a printing module 41c. The control module 41a is both operably electrically connected to the accounting module 41b and adapted to be operably electrically connected to an external device via respective two-way serial communications

channels, and the accounting module 41b is operably electrically connected to the printing module 41c via a corresponding two-way serial communication channel. In general, each of the modules 41a, 41b and 41c includes a
5 dedicated microprocessor 41d, 41e or 41f, respectively, having a separately controlled clock and programs. And two-way communications are conducted via the respective serial communication channels utilizing the echoplex communication discipline, wherein communications are in the form of
10 serially transmitted single byte header-only messages, consisting of ten bits including a start bit followed by an 8 bit byte which is in turn followed by a stop bit, or in the form of a multi-byte message consisting of a header and one or more additional bytes of information. Further, all
15 transmitted messages are followed by a no error pulse if the message was received error free. In operation, each of the modules 41a, 41b and 41c is capable of processing data independently and asynchronously of the other. In addition, to allow for compatibility between the postage meter 10 and
20 any external apparatus, all operational data transmitted to, from and between each of the three modules 41a, 41b and 41c, and all stored operator information, is accessible to the external device via the two-way communication channel, as a result of which the external apparatus (if any) may be
25 adapted to have complete control of the postage meter 10 as well as access to all current operational information in the postage meter 10. In addition, the flow of messages to, from and between the three internal modules 41a, 41b and 41c is in

a predetermined, hierarchical direction. For example, any command message from the control module 41a is communicated to the accounting module 41b, where it is processed either for local action in the accounting module 41b and/or as a
5 command message for the printing module 41c. On the other hand, any message from the printing module 41c is communicated to the accounting module 41b where it is either used as internal information or merged with additional data and communicated to the control module 41c. And, any message
10 from the accounting module 41b is initially directed to the printing module 41c or to the control module 41a. A more detailed description of the various prior art modules 41a, 41b and 41c, and various modifications thereof, may be found in U.S. Patent Nos. 4,280,180; 4,280,179; 4,283,721 and
15 4,301,507; each of which patents is assigned to the assignee of the present invention.

The mailing machine 12 (Fig. 2), which has a casing 19, includes a A.C. power supply 20 which is adapted by means of a power line 22 to be connected to a local source of
20 supply of A.C. power via a normally open main power switch 24 which may be closed by the operator. Upon such closure, the mailing machine's D.C. power supply 26 is energized via the power line 28. In addition, the mailing machine 12 includes a conventional belt-type conveyor 49, driven by an A.C. motor
25 50, which is connected for energization from the A.C. power supply 20 via a conventional, normally open solid state, A.C. motor, relay 52, which is timely energized by a computer 500 for closing the relay 52. Upon such closure the A.C.

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motor 50 drives the conveyor 49 for feeding mailpieces 16 to the drum 38. To facilitate operator control of the switch 24, the mailing machine preferably includes a keyboard 53 having a "start" key 53a and a "stop" key 53b, which are conventionally coupled to the main power switch 24 to permit the operator to selectively close and open the switch 24. Assuming the computer 500 has timely energized the relay 52, the A.C. motor 50 is energized from the A.C. power supply 20. Whereupon the conveyor 49 transports the individual mailpieces 16, at a velocity corresponding to the angular velocity of the motor 50, in the path of travel 18 to the postage printing platen 54.

According to the invention, the machine 12 includes first and second sensing devices respectively designated 56 and 58, which are spaced apart from each other a predetermined distance d_1 , i.e., the distance between points A and B in the path of travel 18. Preferably, each of the sensing devices 56 and 58, is an electro-optical device which is suitably electrically coupled to the computer 500; sensing device 56 being connected via communication line 60 and sensing device 58 being connected via communication line 62. The sensing devices 56, 58 respectively respond to the arrival of a mailpiece 16 at points A and B by providing a signal to the computer 500 on communication line 60 from sensing device 56 and on communication line 62 from sensing device 58. Thus, the rate of movement or velocity V_1 of any mailpiece 16 may be calculated by counting the elapsed time t_v (Fig. 3) between arrivals of the mailpiece 16 at points A

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and B, and dividing the distance d_1 , by the elapsed time t_v . To that end, the computer 500 is programmed for continuously polling the communications lines 60 and 62 each time instant T_n at the end of a predetermined sampling time period, T , preferably $T=1$ millisecond, and to commence counting the
5 number of time instants T_n when the leading edge of a given mailpiece 16 is detected at point A, as evidenced by a transition signal on communication line 60, and to end counting the time instants T_n when the given mailpiece 16 is detected at point B, as evidenced by a transition signal on
10 communication line 62. Since the distance d_1 , is a mechanical constant of the mailing machine 12, the velocity of the mailpiece may be expressed in terms of the total number N_t of time instants T_n which elapse as the given mailpiece traverses the distance d_1 . For example, assuming a
15 maximum velocity of 61 inches per second, $d_1=2.75$ inches and $T=1$ millisecond; the total number N_t of elapsed time instants T_n may be found by dividing $d_1=2.75$ inches by $V_1=61$ inches per second to obtain $N_t=45$, i.e., the total number of time instants T_n which elapse between arrivals of the mailpiece at
20 points A and B. Thus, the number $N_t=45$ corresponds to and is representative of a mailpiece velocity of $V_1=61$ inches per second.

Assuming normal operation of the transport system and calculation of the value of V_1 having been made, the time
25 delay t_d (Fig. 3) before arrival of the mailpiece 16 at point C may be calculated by dividing the distance d_2 between points B and C by the mailpiece's velocity V_1 , provided the

distance d_2 is known. Since the integral of the initial, triangularly-shaped, portion of the velocity versus time profile is equal to one-half of the value of the product of T_a and V_1 , and is equal to the arc d_3 described by point E on the drum 38, as the drum 38 is rotated counter-clockwise to point D, the distance between points C and D is equal to twice the arcuate distance d_3 . Accordingly, d_2 may be conventionally calculated, as may be the time delay t_d for the maximum throughput velocity. Assuming rotation of the drum 38 is commenced at the end of the time delay t_d and the drum 38 is linearly accelerated to the velocity V_1 to match that of the mailpiece 16 in the time interval T_a during which point E on the drum 38 arcuately traverses the distance d_3 to point D, T_a may be conventionally calculated. In addition, assuming commencement of rotation at the end of the time delay t_d and that the drum 38 is linearly accelerated to the velocity V_1 during the time interval T_a , the mailpiece 16 will arrive at point D coincident with the rotation of point E of the outer periphery 73 of the drum 38 to point D, with the result that the leading edge 73a of the drum's outer periphery 73, which edge 73a extends transverse to the path of travel 18 of the mailpiece 16, will engage substantially the leading edge of the mailpiece 16 for feeding purposes and the indicia printing portion 73b of the periphery 73 will be marginally spaced from the leading edge of the mailpiece 16 by a distance d_4 which is equal to the circumferential distance between points E and F on the drum 38. Since the circumferential distance d_5 on the drum 38 between points E and G is fixed, the time interval T_c during which the drum 38 is rotated at the constant velocity V_1 may also be calculated. When point G on the drum 38 is rotated out of engagement with the mailpiece 16, the drum 38 commences deceleration and continues to decelerate to rest

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during the time interval T_d . The distance d_6 which is traversed by point G, as the drum 38 is rotated to return point E to its original position of being spaced a distance d_3 from point D, is fixed, and, T_d may be chosen to provide a suitable deceleration rate for the drum, preferably less than T_a . In addition, a reasonable settling time interval T_s is preferably added to obtain the overall cycling time T_{cT} of the drum 38 to allow for damping any overshoot of the drum 38 before commencing the next drum cycle. For a typical maximum drum cycle time period T_{cT} of 234 milliseconds and a maximum mailpiece transport rate of 61 inches per second, typical values for the acceleration, constant velocity, deceleration and settling time intervals are $T_a=37$ milliseconds, $T_c=124$ milliseconds, $T_d=24$ milliseconds and $T_s=234-185=49$ milliseconds. Utilizing these values, the required acceleration and deceleration values for the drum 38 during the time intervals T_a and T_d may be conventionally calculated. In addition, since the integral of the velocity versus time profile is equal to the distance traversed by the circumference of the drum 38 during a single revolution of the drum 38, the desired position of the drum 38 at the end of any sampling time period of $T=1$ millisecond may be calculated. For target velocities V_1 which are less than the maximum throughput velocity, it is preferably assumed that integral of, and thus the area under, the velocity versus time profile remains constant, and equal to the area thereof at the maximum throughput velocity, to facilitate conventional calculation of the values of the time delay t_d ,

the time intervals T_a , T_c and T_d , and the acceleration and deceleration values for each of such lesser velocities V_l .

For computer implementation purposes, the computer 500 is programmed as hereinbefore discussed to continuously poll the communication lines 60 and 62, from the sensing devices 56 and 58, respectively, each time interval T_n , and count the time intervals T_n between arrivals of the mailpiece 16 at points A and B as evidenced by a transition signals on lines 60 or 62. Further, the computer 500 is programmed to calculate the current velocity of the mailpiece 16 in terms of the total number N_t of the counted time intervals T_n , store the current velocity and, preferably, take an average of that velocity and at least the next previously calculated velocity (if any) to establish the target velocity V_l . In addition, it is preferable that precalculated values for the time delay t_d , acceleration and deceleration corresponding to each of a plurality of target velocities be stored in the memory of the computer 500 for fetching as needed after calculation of the particular target velocity. In this connection it is noted that the velocity at any time " t " of the drum 38 may be expressed by adding to the original velocity V_0 each successive increment of the product of the acceleration and time during each time period of $T=1$ millisecond, each successive increment of constant velocity and each successive increment of the product of the deceleration and time during each time period T . Preferably, the acceleration and deceleration values are each stored in the form of an amount corresponding to a

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predetermined number of counts per millisecond square which are a function of the actual acceleration or deceleration value, as the case may be, and of the scale factor hereinafter discussed in connection with measuring the actual
5 angular displacement of the motor drive shaft 122; whereby the computer 500 may timely calculate the desired angular displacement of the motor drive shaft 122 during any sampling time interval T. In this connection it is noted that the summation of all such counts is representative of the desired
10 linear displacement of the circumference of the drum 38, and thus of the desired velocity versus time profile of drum rotation for timely accelerating the drum 38 to the target velocity V1, maintaining the drum velocity at V1 for feeding the particular mailpiece 16 and timely decelerating the drum
15 38 to rest. —

The postage meter 10 (Fig. 1) additionally includes a conventional, rotatably mounted, shaft 74 on which the drum 38 is fixedly mounted, and a conventional drive gear 76, which is fixedly attached to the shaft for rotation of the
20 shaft 74.

According to the invention, the mailing machine 12 (Fig. 1) includes an idler shaft 80 which is conventionally journaled to the casing 19 for rotation, and, operably coupled to the shaft 80, a conventional home position encoder
25 82. The encoder 82 includes a conventional circularly-shaped disc 84, which is fixedly attached to the shaft 80 for rotation therewith, and an optical sensing device 86, which is operably coupled to the disc 84 for detecting an opening

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88 formed therein and, upon such detection, signalling the computer 500. The machine 12, also includes an idler gear 90 which is fixedly attached to the shaft 80 for rotation therewith. Further, the machine 12 includes a D.C. motor 5 120, which is suitably attached to the casing 19 and has a drive shaft 122. The machine 12 also includes a pinion gear 124, which is fixedly attached to the drive shaft 122 for rotation by the shaft 122. The gear 124 is disposed in driving engagement with the idler gear 90. Accordingly, 10 rotation of the motor drive shaft 122 in a given direction, results in the same direction of rotation of the drum drive shaft 76 and thus the drum 38. Preferably, the pinion gear 124 has one-fifth the number of teeth as the drum drive gear 76, whereas the idler gear 90 and drum drive gear 76 each 15 have the same number of teeth. With this arrangement, five complete revolutions of the motor drive shaft 122 effectuate one complete revolution of the drum 38, whereas each revolution of the gear 90 results in one revolution of the gear 76. Since there is a one-to-one relationship between 20 revolutions, and thus incremental angular displacements, of the drum shaft 74 and idler shaft 90, the encoder disc 84 may be mounted on the idler shaft 90 such that the disc's opening 88 is aligned with the sensing device 86 when the drum 38 is disposed in its home position to provide for detection of the 25 home position of the drum shaft 74, and thus a position of the drum shaft 74 from which incremental angular displacements may be counted.

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For sensing actual incremental angular displacements of the motor drive shaft 122 (Fig. 1) from a home position, and thus incremental angular displacements of the drum 38 from its rest or home position as shown in Fig. 2, there is provided a quadrature encoder 126 (Fig. 1). The encoder 126 is preferably coupled to the motor drive shaft 122, rather than to the drum shaft 74, for providing higher mechanical stiffness between the armature of the d.c. motor 120 and the encoder 126 to avoid torsional resonance effects in the system. The encoder 126 includes a circularly-shaped disc 128, which is fixedly attached to the motor drive shaft 122 for operably connecting the encoder 126 to the motor 120. The disc 128 (Fig. 4) which is otherwise transparent to light, has a plurality of opaque lines 130 which are formed on the disc 128 at predetermined, equidistantly angularly-spaced, intervals along at least one of the disc's opposed major surfaces. Preferably the disc 128 includes one hundred and ninety-two lines 130 separated by a like number of transparent spaces 132. In addition, the encoder 126 includes an optical sensing device 134, which is conventionally attached to the casing 19 and disposed in operating relationship with respect to the disc 128, for serially detecting the presence of the respective opaque lines 130 as they successively pass two reference positions, for example, positions 136ra and 136rb, and for responding to such detection by providing two output signals, one on each of communications lines 136a and 136b, such as signal A (Fig. 5) on line 136a and signal B on line 136b. Since the disc

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128 (Fig. 4) includes 192 lines 130 and the gear ratio of the drum drive gear 76 (Fig. 1) to the motor pinion gear 124 is five-to-one, nine hundred and sixty signals A and B (Fig. 5) are provided on each of the communications lines 136a and 5 136b during five revolutions of the motor-drive shaft 122, and thus, during each cycle of rotation of the drum 38. Since the angular distance between successive lines 130 (Fig. 4) is a constant, the time interval between successive leading edges (Fig. 5) of each signal A and B is inversely 10 proportional to the actual velocity of rotation of the motor drive shaft (Fig. 1) and thus of the drum 38. The encoder 126 is conventionally constructed and arranged such that the respective reference positions 136a and 136b (Fig. 4) are located with respect to the spacing between line 130 to 15 provide signals A and B (Fig. 5) which are 90 electrical degrees out of phase. Accordingly, if signal A lags signal B by 90° (Fig. 5) the D.C. motor shaft 122 (Fig. 1), and thus the drum 38, is rotating clockwise, whereas if signal A leads signal B by 90° (Fig. 5) the shaft 122 and drum 38 are both 20 rotating counter-clockwise. Accordingly, the angular displacement in either direction of rotation of the drum 38 (Fig. 1) from its home position may be incrementally counted by counting the number of pulses A or B, (Fig. 5) as the case may be, and accounting for the lagging or leading 25 relationship of pulse A (Fig. 5) with respect to pulse B.

The quadrature encoder communication lines, 136a and 136b (Fig. 1), may be connected either directly to the computer 500 for pulse counting thereby or to the computer

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500 via a conventional counting circuit 270 (Fig. 6), depending on whether or not the internal counting circuitry of the computer 500 is or is not available for such counting purposes in consideration of other design demands of the system in which the computer 500 is being used. Assuming connection to the computer 500 via a counting circuit 270, the aforesaid communications lines, 136a and 136b are preferably connected via terminals A and B, to the counting circuit 270.

10 In general, the counting circuit 270 (Fig. 6) utilizes the pulses A (Fig. 5) to generate a clock signal and apply the same to a conventional binary counter 274 (Fig. 6), and to generate an up or down count depending on the lagging or leading relationship of pulse A (Fig. 5) relative to pulse B
15 and apply the up or down count to the binary counter 274 (Fig. 6) for counting thereby. More particularly, the pulses A and B (Fig. 5) which are applied to the counting circuit terminals A and B (Fig. 6) are respectively fed to Schmidt trigger inverters 276A and 276B. The output from the
20 inverter 276A is fed directly to one input of an XOR gate 278 and additionally via an R-C delay circuit 280 and an inverter 282 to the other input of the XOR gate 278. The output pulses from the XOR gate 278, which acts as a pulse frequency doubler, is fed to a conventional one-shot multivibrator 284
25 which detects the trailing edge of each pulse from the XOR gate 278 and outputs a clock pulse to the clock input CK of the binary counter 274 for each detected trailing edge. The output from the Schmidt trigger inverters 276A and 276B are

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respectively fed to a second XOR gate 286 which outputs a low logic level signal (zero), or up-count, to the up-down pins U/D of the binary counter 274 for each output pulse A (Fig. 5) which lags an output pulses B by 90 electrical degrees.

5 On the other hand the XOR gate 286 (Fig. 6) outputs a high logic level (one) or down-count, to the up-down input pins of the binary counter 274 for each encoder output pulse A (Fig. 5) which leads an output pulse B by 90° electrical degrees. Accordingly, the XOR gate 286 (Fig. 6) provides an output

10 signal for each increment of angular displacement of the encoded shaft 122 (Fig. 1) and identifies the direction, i.e., clockwise or counter-clockwise, of rotation of the encoded shaft 122. The binary counter 274 (Fig. 6) counts the up and down count signals from the XOR gate 286 whenever

15 any clock signal is received from the multivibrator 284, and updates the binary output signal 272 to reflect the count.

Accordingly, the counting circuit 270 converts the digital signals A and B, which are representative of incremental angular displacements of the drive shaft 122 in

20 either direction of rotation thereof, to an eight bit wide digital logic output signal 272 which corresponds to a summation count at any given time, of such displacements, multiplied by a factor of two, for use by the computer 500. Since the angular displacement of the shaft 122 from its home

25 position is proportional to the angular displacement of the drum 38 from its home position, the output signal 272 is a count which is proportional to the actual linear displacement of the outermost periphery of the drum 38 at the end of a

given time period of rotation of the drum 38 from its home position. For a typical postage meter drum 38, having a circumference, i.e., the arc described by the outermost periphery of the drum 38 in the course of revolution thereof, of 9.42 inches, which is connected to the motor drive shaft 122 via a mechanical transmission system having a 5:1 gear ratio between the motor 120 and drum 38, wherein the encoder disc 128 has 192 lines; the counting circuit 270 will provide an output of $2 \times 192 = 384$ counts per revolution of the shaft 122, and $5 \times 384 = 1920$ counts per revolution of the drum 38 which corresponds to 203.82 counts per inch of linear displacement of the periphery of the drum. Accordingly, the maximum mailpiece transport velocity of $V_1 = 61(10^{-3})$ inches per millisecond may be multiplied by a scale factor of 203.82 counts per inch to express the maximum transport velocity in terms of counts per millisecond, or, counts per sampling time period T where $T=1$ millisecond; i.e., $61(10^{-3})$ inches per millisecond times 203.82 counts per inch = 12.43 counts per sampling time period T . Similarly, any other target velocity V_1 , or any acceleration or deceleration value, may be expressed in terms of counts per sampling time interval T , or counts per square millisecond, as the case may be, by utilization of the aforesaid scale factor.

For energizing the D.C. motor 120 (Fig. 1) there is provided a power amplifying circuit 300. The power amplifying circuit 300 (Fig. 7) is conventionally operably connected to the motor terminals 302 and 304 via power lines 306 and 308 respectively. The power amplifying circuit 300

preferably comprises a conventional, H-type, push-pull, control signal amplifier 301 having input leads A, B, C and D, a plurality of optical-electrical isolator circuits 303 which are connected on a one-for-one basis between the leads
5 A-D and four output terminals of the computer 500 for coupling the control signals from the computer 500 to the input leads A, B, C, and D of the amplifier 301, and a plurality of conventional pull-up resistors 305 for coupling the respective leads A-D to the 5 volt source. The amplifier
10 301 includes four conventional darlington-type, pre-amplifier drive circuits including NPN transistors T1, T2, T3 and T4, and four, conventional, darlington-type power amplifier circuits including PNP transistors Q1, Q2, Q3 and Q4 which are respectively coupled on a one-for-one basis to the
15 collectors of transistors T1, T2, T3 and T4 for driving thereby. The optical-electrical isolator circuits 303 each include a light emitting diode D1 and a photo-responsive transistor T5. The cathodes of D1 are each connected to the 5 volt source, the emitters of T5 are each connected to
20 ground and the collectors of T5 are each coupled, on a one-for-one basis, to the base of one of the transistors T1, T2, T3 and T4. With respect to each of the opto-isolator circuits 303, when a low logic level signal is applied to the anode of D1, D1 conducts and illuminates the base of T5
25 thereby driving T5 into its conductive state; whereas when a high logic level signal is applied to the anode of D1, D1 is non-conductive, as a result of which T5 is in its non-conductive state. With respect to each of the combined

amplifier circuits, T1 and Q1, T2 and Q2, T3 and Q3, and T4 and Q4, when the lead A, B, C or D, as the case may be, is not connected to ground via the collector-emitter circuit of the associated opto-isolator circuit's transistor T5, the
5 base of T1, T2, T3 or T4, as the case may be, draws current from the 5 volt source via the associated pull-up resistor 305 to drive the transistor T1, T2, T3 or T4, as the case may be, into its conductive state. As a result, the base of transistor Q1, Q2, Q3 or Q4, as the case may be, is clamped
10 to ground via the emitter-collector circuit of its associated driver transistor T1, T2, T3 or T4, thereby driving the transistor Q1, Q2, Q3 or Q4, as the case may be, into its conductive state. Contrariwise, the transistor pairs T1 and Q1, T2 and Q2, T3 and Q3, and T4 and Q4 are respectively
15 biased to cut-off when lead A, B, C or D, as the case may be, is connected to ground via the collector-emitter circuit of the associated opto-isolator circuit's transistor T5. As shown in the truth table (Fig. 8) for clockwise motor rotation, Q1 and Q4 are turned on and Q2 and Q3 are turned
20 off; whereas for counter-clockwise motor rotation, Q2 and Q3 are turned on and Q1 and Q4 are turned off. Accordingly, for clockwise motor rotation: terminal 302 (Fig. 7) of the motor 120 is connected to the 30 volt source via the emitter-collector circuit of Q1, which occurs when Q2 is turned off
25 and the base of Q1 is grounded through the emitter-collector circuit of T1 due to the base of T1 drawing current from the 5 volt source in the presence of a high logic level control signal at input terminal A; and terminal 304 of the motor 120

is connected to ground via the emitter-collector circuit of Q4, which occurs when Q3 is turned off and the base of Q4 is grounded through the emitter-collector circuit of T4 due to the base of T4 drawing current from the 5 volt source in the presence of a high logic level signal at the input terminal D. On the other hand, for counter clockwise rotation of the motor 120: terminal 302 of the motor 120 is connected to ground via the emitter-collector circuit of Q2, which occurs when Q1 is turned off and the base of Q2 is grounded through the emitter-collector circuit of T2 due to the base of T2 drawing current from the 5 volt source in the presence of a high logic level control signal at the input terminal B; and terminal 304 of the motor 120 is connected to the 30 volt source via the emitter-collector circuit of Q3, which occurs when Q4 is turned off and the base of Q3 is grounded through the emitter-collector of T3 due to the base of T3 drawing current from the 5 volt source in the presence of a high logic level control signal at the input terminal C. For turning off the respective powers transistors Q1-Q4, on a two at a time basis, low level control signals are applied on a selective basis to the two terminals B and C, or A and D, as the case may be, to which high logic control level signals are not being applied; which occurs when the opto-isolator circuit's transistors T5 associated with the respective leads B and C or A and D are driven to their conductive states, When this occurs the bases of the transistors T2 and T3, or T1 and T4, as the case may be, are biased to open the emitter-collectors circuits of the transistors T2 and T3, or T1 and

T4, as the case may be, as a result of which the bases of the transistors Q2 and Q3, or Q1 and Q4, as the case may be, are biased to open the emitter-collector circuits of transistors Q2 and Q3, or Q1 and Q4, as the case may be.

5 The velocity of the motor 120 (Fig. 7) is controlled by modulating the pulse width and thus the duty cycle of the high logic level, constant frequency, control signals, i.e., pulse width modulated (PWM) signals, which are timely applied on a selective basis to two of the leads A-D, while applying
10 the low level logic signals to those of leads A-D which are not selected. For example, assuming PWM signals (Fig. 9) having a 50% duty cycle are applied to leads A and D (Fig. 7), and low level logic signals are applied to leads B and C, for clockwise rotation of the motor 120, the velocity of the
15 motor 120 will be greater than it would be if high logic level PWM signals (Fig. 9) having a 25% duty cycle were similarly applied and will be less than it would be if high logic level PWM signals having a 75% duty cycle were similarly applied. Accordingly, assuming rotation of the
20 motor 120 (Fig. 7) is commenced by utilizing high logic level PWM signals having a given duty cycle percentage, the velocity of the motor 120 may be decreased or increased, as the case may be, by respectively decreasing or increasing the duty cycle percentage of the applied high logic level PWM
25 signals. Further, assuming the motor 120 is rotating clockwise due to PWM signals having a selected positive average value being applied to leads A and D, in combination with low level logic signals being applied to leads B and C,

the motor 120 may be dynamically braked by temporarily applying high level PWM signals having a selected duty cycle corresponding to a given positive average value to leads B and C, in combination with low logic signals being applied to leads A and D. To avoid damage to the power transistors Q1, Q2, Q3 and Q4 which might otherwise result, for example, due to current spikes accompanying back emf surges which occur in the course of switching the circuit 301 from one mode of operation to the other, the emitter-collector circuits of the power transistors Q1, Q2, Q3 and Q4 are respectively shunted to the 30 volt source by appropriately poled diodes, D1, D2, D3 and D4 connected across the emitter-collector circuits of Q1, Q2, Q3 and Q4.

To control the motion of the drum 38 (Fig. 1) during each cycle of drum rotation, the D.C. motor 120 and its shaft encoder 126 are respectively connected to the computer 500 via the power amplifier circuit 300 and the counting circuit 270. And the computer 500 is programmed to calculate the duration of and timely apply PWM control signals to the power amplifier circuit 300 after each sampling time instant T_n , utilizing an algorithm based upon a digital compensator $D(s)$ derived from analysis of the motor 120, motor load 38, 74, 76, 90 and 124 amplifying circuit 300, encoder 126, counting circuit 270, and the digital compensator $D(s)$ in the closed-loop, sampled-data, servo-control system shown in Fig. 10.

With reference to Fig. 10, in general, at the end of each predetermined sampling time period of $T=1$ millisecond, the eight bit wide count representing the angular

displacement of the motor drive shaft 122, and thus the drum 38, from its home position is sampled by the computer 500 at the time instant T_n . Under the control of the program of the computer 500 (Fig. 10), a summation is taken of the aforesaid
 5 actual count and the previously calculated count representing the desired position of the motor drive shaft 122, and thus the drum 38, at the end of the time period T , and, under control of the computer program implementation of the algorithm, a PWM control signal which is a function of the
 10 summation of the respective counts, or error, is applied to the power amplifier circuit 301 for rotating the motor drive shaft 122 such that the error tends to become zero at the end of the next sampling time period T .

To derive the algorithm, the servo-controlled system
 15 of Fig. 10 is preferably analyzed in consideration of its equivalent Laplace transformation equations shown in Fig. 11, which are expressed in terms of the following Table of Parameters and Table of Assumptions.

20 Table I - Parameters

<u>Parameter</u>	<u>Symbol</u>	<u>Value and/or Dimension</u>
Zero-Order-Hold	ZOH	None
Laplace Operator	S	jw
25 Sampling Interval	T	Milliseconds
PWM D.C. Gain	K_v	Volts
PWM Pulse Amplitude	V_p	5 Volts

	PWM Pulse Width	t_1	10^{-6} Micro-seconds
	Power Switching Circuit Gain	K_a	None
	Motor back e.m.f. Constant	K_e	0.63 Volts/ radian/second
5	Motor Armature Resistance	R_a	1.65 Ohms
	Motor Armature Moment of Inertia	J_a	2.12 (10^{-5}) Kilograms
	Motor Torque Constant	K_t	0.063 Newton- Meters/amp
	Drum Moment of Inertia	J_1	70.63 (10^{-5}) Kilograms/meter ²
10	Gear Ratio, Motor to Load	G	5:1, None
	Motor Armature Inductance	L_a	2.76 Millihenrys
	Motor Shaft Encoder Gain	K_p	Counts/radian
	Motor Shaft Encoder Constant	K_b	192 Lines/ revolution
	Counting Circuit Multiplier	K_x	2, None
15	Motor Gain	K_m	16, None
	Poles in frequency domain	$f_1; f_2$	48,733 Radians/ second
	Starting Torque Gain	K_e	None
	System Overall Gain	K_o	None

20

Table II - Assumptions

ZOH: Since the output and input are held constant during each sampling period a zero-order-hold is assumed to approximate the analog time function being sampled.

25

Veq.: Since the integral of the voltage in time is assumed equal to the area under the PWM pulse, the output from the PWM is linear.

With reference to Fig. 10, $D(S)$ is the unknown transfer function of an open loop compensator in the frequency domain. Due to a key factor for providing acceptably fast motor response being the system's resonance between the motor and load, the derivation of the transfer function $D(S)$ for stabilization of the system is preferably considered with a view to maximizing the range of frequencies within which the system will be responsive, i.e., maximizing the system's bandwidth, BW. For calculation purposes a sampling period of $T=1$ millisecond was chosen, due to having chosen a Model 8051 microprocessor, available from Intel Corporation, Palo Alto California, for control purposes, and inasmuch as the Model 8051 microprocessor equipt with a 12 MHz crystal for providing a clock rate of 12 MHz, is able to conveniently implement a 1 KHz sampling rate and also implement application software routines, after control algorithm iterations, during the sampling period of $T=1$ millisecond. However, other sampling periods and other conventional microprocessors may be utilized without departing from the spirit and scope of the invention.

The open loop system gain $H_1(S)$ without compensation, of the servo-loop system of Fig. 10 is shown in Fig. 12(a). To tolerate inaccuracies in the transmission system between the motor and drum load, such as backlash, it was considered acceptable to maintain a steady-state count accuracy of plus or minus one count. To reflect this standard, the gain equation of Fig. 12(a) was adjusted to provide a corrective torque C_t with a motor shaft movement, in radians per count,

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equivalent to the inverse expressed in radians per count, of the gain K_p of the encoder counting circuit transform. Since the corrective torque C_t is primarily the friction of the transmission system which has to be overcome by the motor at start-up, the value of C_t may be assumed to be substantially equal to a maximum estimated numerical value based on actual measurements of the starting friction of the system, i.e., 35 ounce-inches, as a result of which a numerical value of the starting voltage V_s may be calculated from the expression $V_s = (C_t)R_a/K_t$, i.e., $V_s = 6.5$ volts, which, in turn, permits calculation of a numerical value for the minimum overall system gain K_o , at start-up, from the equation $K_o = V_s/K_p$, i.e., $K_o = 397$ volts per radian, or for simplification purposes, 400 volts/radian. Accordingly, the open-loop uncompensated gain $H_1(S)$ may be rewritten as $H_2(S)$ as shown in Fig. 12(b), in which a gain factor of K_c has been included, to account for the torque C_t and the value of K_o is substituted for the overall D.C. gain, i.e.,

$$(K_v)(K_m)(K_p)(K_a)(K_c) = K_o.$$

Although the numerical value of K_c may also be calculated, it is premature to do so, since it has not as yet been established that K_o , which has been adjusted by the value of K_c to provide a minimum value of K_o , is acceptable for system stability and performance purposes. Otherwise stated, K_o may not be the overall system gain which is needed for system compensation for maximizing the system bandwidth BW, as a result of which it is premature to conclude that K_c will be equivalent to the D.C. gain of the system compensator $D(S)$.

At this juncture, the bode diagram shown in Fig. 13, may be constructed due to having calculated a minimum value for K_0 . As shown in Fig. 13, the absolute value of $H_2(S)$, in decibels, has been plotted against the frequency W in radians per second, based on the calculated minimum value of K_0 , the selected value of T and calculated values of the poles f_1 and f_2 . From the Bode diagram, a numerical value of the cross-over frequency W_{c1} of the Bode plot of $H_2(S)$ may be determined, i.e., W_{c1} was found to be substantially 135 radians per second. And, since the value of W_{c1} is substantially equal to the bandwidth BW_u of the uncompensated open-loop system $H_2(S)$, a calculation may be made of the phase margin θ_m of the uncompensated system from the expression $\theta_m = 180^\circ - \theta [H(S)]$ at W_{c1} , or, otherwise stated:

$$\theta_m = 180^\circ - \tan^{-1}(\omega T/2) - \tan^{-1}(W_{c1}/f_1) - \tan^{-1}(W_{c1}/f_2) - \tan^{-1}(W_{c1}T/2).$$

From this calculation, there was obtained a phase margin value which was much, much, less (i.e., 5°) than 45° , which, for the purposes of the calculations was taken to be a minimum desirable value for the phase margin θ_m in a position-type servo system. Accordingly, it was found that the uncompensated system $H_2(S)$ was unstable if not compensated. Since an increase in phase lead results in an increase in bandwidth BW , and the design criteria calls for maximizing the bandwidth BW and increasing the phase margin to at least 45° ; phase lead compensation was utilized.

By definition, a phase lead compensator $D(S)$ has the Laplace transform shown in Fig. 14, wherein K_c is the phase lead D.C. gain, and f_z and f_p are respectively a zero pole

frequency and a phase lead pole frequency. Adding the transfer function of the phase lead compensator $D(S)$ to the Bode plot of the uncompensated system's transfer function $H_2(S)$, results in the Bode plot of the compensated system transfer function $H_3(S)$, if the zero pole f_z of the phase lead compensator $D(S)$ is chosen to be equivalent to f_1 in order to cancel the lag due to the mechanical time constant of the uncompensated transfer function H_2S . As shown in Fig. 13, the cross-over frequency W_{c2} for the compensated system $H_3(S)$ may be read from the Bode diagram, i.e., W_{c2} was found to be substantially equal to 400 radians per second. And, since by definition the pole frequency f_p lies at the geometric means of f_p and W_{c2} , the value of the f_p may be established by doubling the linear distance between W_{c2} and $W=0$, as measured along the W -axis, and reading the value of f_p from the Bode diagram, i.e., f_p was found to be substantially equal to 3,400 radians per second. Since numerical values may thus be assigned to both W_{c2} and f_p from the Bode diagram, the compensated phase margin ϕ_{mc} , i.e., the phase margin for the phase lead compensated system $H_3(S)$ in which f_z has been equated to f_1 , may be found from the expression $\phi_{mc} = 180^\circ - 90^\circ - \tan^{-1}(W_{c2}/f_2) - \tan^{-1}(W_{c2}T/2)$. Upon calculating the compensated phase margin ϕ_{mc} it was found to be 50° and, therefore, greater than the minimum phase margin criteria of 45° . In addition, the value of W_{c2} for the compensated system $H_3(S)$ was found to be substantially three times that of the uncompensated system $H_2(S)$, as a result of

which the bandwidth BW of the system $H(S)$ was increased by a factor of substantially three to BW_C .

At this juncture, the compensated system $H_3(S)$ is preferably analyzed with reference to the system's overshoot O_S and settling time t_S based on a calculation of the system damping factor d_f and the assumption that the system will settle in five times constants, i.e., $t_S = 5t_x$. The relevant values may be calculated or estimated, as the case may be, from the expressions, for d_f , O_S , t_x and t_S shown in Fig. 15.

In connection with this analysis, reference is also made to the typical mailing machines hereinbefore described, wherein a maximum drum cycle time period T_{ct} (Fig. 3) of 234 milliseconds and a maximum mailpiece transport speed (Fig. 2) of 61 inches per second are typical values. Assuming the velocity profile of Fig. 3, and, as previously discussed an acceleration time period of $T_a = 37$ milliseconds, a constant velocity time period of $T_c = 124$ milliseconds and deceleration time period of $T_d = 24$ milliseconds, the longest permissible settling time for the system was calculated, i.e., $T_{ct} - (T_a + T_c + T_d) = 234 - 185 = 49$ milliseconds. For analysis purposes a series of calculations of the aforesaid system characteristics and phase margin were performed, assuming incremental increases in the overall system gain K_O , while holding $f_z = f_1$. The results of such calculations are shown in the following Table III.

Table III - $H_3(S)$ with $f_z=f_1$

	K_O =system gain (db)	W_C =BW (rad./sec.)	θ_m =phase Margin (deg.)	O_S =overshoot (percent)	t_S =settling time (MS.)
5	400	400	50	28	28.67
	447	450	46	31	27.78
	501	500	42	34	27.50
	562	550	38	38	27.41

As shown in Table III, the system bandwidth BW may be maximized at 450 radians per second while maintaining a phase margin ϕ_m of at least 45° the two design criteria discussed above. Although this results in an increase in system overshoot O_S accompanied by a negligible decrease in the settling time t_S , the settling time t_S is well within the maximum allowable settling time, $T_S=49$ milliseconds. On the other hand, if a bandwidth of 400 radians per second is acceptable, it is desirable to reduce the percentage of overshoot O_S , and increase the phase margin to $\theta_{mc}=50$ to provide for greater system stability than would be available with a phase margin value (i.e., 46°) which is substantially equal to the design criteria minimum of 45° ; in which instance it is preferable to choose the bandwidth of $BW=400$ radians per second, overshoot of $O_S=28\%$ and compensated phase margin of $\theta_{mc}=50^\circ$. For the example given, a compensated Bandwidth of $BW_C=400$ radians per second is acceptable inasmuch as worst case load conditions were assumed. In this connection it is noted that the foregoing analysis is based on controlling a postage meter drum, which has a high moment of inertia, contributes high system friction, and

calls for a cyclical start-stop mode of operation during which the load follows a predetermined displacement versus time trajectory to accommodate the maximum mailpiece transport speed in a typical mailing machine. Accordingly, 5 the compensated system bandwidth $BW_C=400$ radians per second may be chosen, as a result of which the overall system gain K_O may be fixed at $K_O=400$, and the value of K_C may be calculated from the expression $K_C=K_O/((K_V)(K_A)(K_P))$. Since $f_z=f_1$, and f_1 and f_p are also known, the Bode plot of the 10 compensator $D(S)$, Fig. 14, may be added to the Bode diagram (Fig. 13) wherein the system compensator $D(S)$ is shown as a dashed line.

Since the analog compensator $D(S)$ was derived in the frequency domain, $D(S)$ was converted to its Z-transform 15 equivalent $D(Z)$ in the sampled data domain for realization in the form of a numerical algorithm for implementation by a computer. Of the numerous well-known techniques for transforming a function in the frequency domain to a function in the sampled-data domain, the bi-linear transformation may 20 be chosen. For bi-linear transformation purposes the Laplace operator S is defined by the expression shown in Fig. 16. Using the values $K_C=13.64$, $f_z=f_1=48$, and $f_p=3,400$ in the expression for $D(S)$ shown in Fig. 14, and substituting the bi-linear transformation expression for S shown in Fig. 16 and 25 the sampling interval $T=1$ millisecond, in the expression shown in Fig. 14 results in the expression for $D(Z)$ shown in Fig. 17. As shown in Fig. 11, $D(T)=\text{output}/\text{input}=g(T)/e(T)$, which, in the sampled data domain is expressed by the

equation $D(Z)=G(Z)/E(Z)$. Accordingly, the expression for $D(Z)$ shown in Fig. 17 may be rewritten as shown in Fig. 18a. Cross-multiplying the equivalency of Fig. 18a results in the expression shown in Fig. 18b, which defines the output $G(Z)$ in the sampled data domain of the system compensator $D(S)$. Taking the inverse Z-transform of the expression shown in Fig. 18b, results in the expression shown in Fig. 19 which defines the output $G(T_n)$ in the time domain of the system compensator $D(S)$, and is a numerical expression of the algorithm to be implemented by the computer for system compensation purposes. As shown by the expression in Fig. 19 and in the following Table IV the output of the digital compensator for any current sampling instant T_n is a function of the position error at the then current sampling time instant T_n , is a function of the position error at the end of the next previous sampling time instant T_{n-1} and is a function of the algorithm output at the end of the next previous sampling time instant T_{n-1} .

20

TABLE IV

<u>Function</u>	<u>Definition</u>
$G(T_n)$	Algorithm output for current sampling time instant T_n
$E(T_n)$	Position error for current sampling time instant T_n
25 $G(T_{n-1})$	Algorithm output for next previous sampling time instant T_{n-1}
$E(T_{n-1})$	Position error for next previous sampling time instant T_{n-1}

K_1 , K_2 & K_3 Constants of the compensated system which are a function of the parameters of the motor load and system friction for a sampling time period of $T=1$ millisecond.

5 Accordingly, the algorithm which is to be implemented by the computer 500 for system compensation purposes is a function of a plurality of historical increments of sampled data for computing an input value for controlling a load to follow a predetermined position trajectory in a closed loop
10 sampled-data servo-control system.

 As shown in Fig. 20 the computer 500 preferably includes a conventional, inexpensively commercially available, high speed microprocessor 502, such as the Model 8051 single chip microprocessor commercially available from
15 Intel Corporation, 3065 Bowers Avenue, Santa Clara, California 95051. The microprocessor 502, generally comprises a plurality of discrete circuits, including those of a control processor unit or CPU 504, an oscillator and clock 506, a program memory 508, a data memory 510, timer and
20 event counters 512, programmable serial ports 514, programmable I/O ports 516 and control circuits 518, which are respectively constructed and arranged by well known means for executing instructions from the program memory 508 that pertain to internal data, data from the clock 506, data
25 memory 510, timer and event counter 512, serial ports 514, I/O ports 514 interrupts 520 and/or bus 522 and providing appropriate outputs from the clock 506, serial ports 514, I/O ports 516 and timer 512. A more detailed discussion of the internal structural and functional characteristics and

features of the Model 8051 microprocessor, including optional methods of programming port 3 for use as a conventional bi-directional port, may be found in the Intel Corporation publication entitled MCS-51 Family of Single-Chip

5 Microcomputers Users Manual, dated January 1981.

For implementing the sampling time period of $T=1$ millisecond, one of the microprocessor's timer and event counters 512 (Fig. 20) is conventionally programmed as a sampling time period clock source. To that end, a timer 512
10 is programmed for providing an interrupt signal each 250 microseconds, and each successive fourth interrupt signal is utilized as a clock signal for timing the commencement of successive sampling time periods of $T=1$ millisecond.

In general, as shown in Fig. 21, at the commencement
15 of each sampling time period of $T=1$ millisecond, during the sampling instant T_n , a sample is taken of the count representative of the actual angular displacement of the motor drive shaft and, substantially immediately thereafter, the actual count is summed with the count representative of
20 the desired angular displacement of the motor drive shaft which was calculated during the next preceeding time period T in order to obtain the then current error value $E(T_n)$ for calculating the then current compensation algorithm output value $G(T_n)$. Due to the recursive mathematical expression
25 for $G(T_n)$ [Fig. 19] being a function of the then current error value $E(T_n)$, the next previous error value $E(T_{n-1})$ and the next previous compensation algorithm output value $G(T_{n-1})$, the expression for $G(T_n)$ is preferably separated

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into two components for calculation purposes, i.e., $G(T_n) = g_1 + g_2$; wherein $g_1 = K_1 \times E(T_n)$, and wherein $g_2 = -[K_2 \times E(T_{n-1}) + K_3 \times G(T_{n-1})]$, to permit calculation of the value of g_2 in advance of the time period T when it is to be added to the value of g_1 for calculating the value of $G(T_n)$, thereby reducing to a negligible value (in view of the time period T) the time delay T_{dy} before completion of sampling the actual displacement of the motor drive shaft at the instant T_n and applying the PWM motor control signal to the output ports of the microprocessor. For example, when calculating the value of $G(T_n)$ based upon the first error value resulting from the summation of the counts representing the desired and actual angular displacements of the motor drive shaft, the value of g_2 is by definition equal to zero since the error signal $E(T_{n-1})$ is equal to zero, due to the desired and actual angular displacement values during the next previous sampling time period T having been equal to each other. Accordingly, upon obtaining the value of the first error signal $E_1(T_n)$, the value of $G_1(T_n)$ may be calculated as being equivalent to g_1 , i.e., $G_1(T_n) = g_1 = K_1 \times E_1(T_n)$. And, upon calculating $G_1(T_n)$ the value of g_2 for use in calculating the next successive compensation algorithm output value $G(T_{n+1})$ may be calculated for subsequent use, since $g_2(T_{n+1}) = -[K_2 \times E_1(T_n) + K_3 \times G_1(T_n)]$, and K_2 , K_3 , $E_1(T_n)$ and $G_1(T_n)$ are all known values. In addition, during any given time period T , a calculation may be made of the desired angular displacement of the motor drive shaft for the next subsequent time period T . Preferably, the

microprocessor is programmed for implementation of the aforesaid calculation process to facilitate early utilization of the compensation algorithm output value $G(T_n)$ for driving the D.C. motor. Accordingly, the microprocessor is

- 5 preferably programmed for: during the first-sampling time period T_1 , sampling the count representative of the actual angular displacement of the motor drive shaft at the time instant T_n , then taking the summation of that count and the previously calculated value of the desired angular
- 10 displacement of the motor drive shaft to obtain the first error value $E_1(T_n)$, then calculating the first compensation algorithm output value $G_1(T_n) = K_1 \times E_1(T_n) + g_2$, wherein $g_2=0$, and generating a PWM motor control signal representative of $G_1(T_n)$, then calculating the value of g_2
- 15 for the next sampling time period, i.e., $g_2 = -[K_2 \times E_1(T_n) + K_3 \times G_1(T_n)]$, and then calculating the count representing the desired angular displacement of the motor drive shaft for use during the next sampling time period T_2 ; during the second sampling time period T_2 , sampling the count representative of
- 20 the actual angular displacement of the motor drive shaft and taking the summation of that count and the previously calculated desired count to obtain the error value $E_2(T_{n+1})$, calculating the compensation algorithm output value $G_2(T_{n+1}) = K_1 \times E_2(T_{n+1}) + g_2 = K_1 \times E_2(T_{n+1}) - K_2 \times E_1(T_n) - K_3 \times$
- 25 $G_1(T_n)$, and generating a PWM motor control signal representative thereof, then calculating the value of g_2 for the next sampling time period T_3 , i.e., $g_2 = -[K_2 \times E_2(T_{n+1}) + K_3 \times G_2(T_{n+1})]$, and then calculating the count representative

of the desired angular displacement of the motor drive shaft for use during the time period T_3 ; and so on, during each successive sampling time period.

Accordingly, as shown in Fig. 21, the microprocessor
5 is programmed for immediately after calculating the then
current compensation algorithm output value $G(T_n)$, and thus
while the calculation of the value of g_2 for the next
sampling time period is in progress, generating a motor
control signal for energizing the power amplifier. For this
10 purpose, the relative voltage levels of motor control signal
are determined by the sign, i.e., plus or minus, of the
compensation algorithm output value $G(T_n)$, and the duty cycle
of the control signal is determined by the absolute value of
the compensation algorithm output value $G(T_n)$. Preferably,
15 for timing the duration of the motor control signal, the
other timer and event counter 512, i.e., the timer 512 which
was not used as a sampling time period clock source, is
utilized for timing the duration of the duty cycle of the
motor control signal. For example, by loading the absolute
20 value of the $G(T_n)$ into the other timer 512, commencing the
count, and timely invoking an interrupt for terminating the
duty cycle of the control signal. As shown in Fig. 21(c),
the time delay T_{dy} from commencement of the time period T to
updating the PWM motor control signal at the output ports of
25 the microprocessor is substantially 55 microseconds, and the
time interval allocated for calculating the value of g_2 and
the count representative of the desired angular displacement
of the motor drive shaft for use during the next time period

is substantially 352 microseconds. As a result, substantially 593 microseconds of microprocessor calculation time is available during any given sampling time period $T=1$ millisecond for implementing non-motor control applications.

5 As shown in Fig. 22 the computer 500 is preferably modularly constructed for segregating the components of the logic circuit 501a and analog circuit 501b of the computer 500 from each other. To that end, the respective circuits 501a and 501b may be mounted on separate printed circuit
10 boards which are electrically isolated from each other and adapted to be interconnected by means of connectors located along the respective dot-dash lines 516, 527 and 528. In any event, the components of the logic circuit 521a and analog circuit 521b are preferably electrically isolated from each
15 other. To that end, the logic circuit 501a preferably includes 5V and ground leads from the mailing machine's power supply for providing the logic circuit 501a with a local 5 volt source 530 having 5V and GND leads shunted by filter capacitors C1 and C2. And the analog circuit 501b includes
20 30 volt and ground return leads from the mailing machine's power supply for providing the analog circuit 501b with a local 30 volt source 536 including 30V and GND leads shunted by filter capacitors C3 and C4. In addition, the analog circuit 501b includes a conventional 30 volt detection
25 circuit 542 having its input conventionally connected to the analog circuit's 30 volt source 536, and its output coupled to a power up/down lead from the analog circuit via a conventional optical-electrical isolator circuit 544.

Further, to provide the analog circuit 501b with a local 5 volt source 546, the analog circuit 501b is equipped with a conventional regulated power supply having its input appropriately connected to the analog circuit's 30 volt source 536 via a series connected resistor R1 and a 5 volt, voltage regulator 548. A zener diode D1, having its cathode shunted to ground and having its anode connected to the input of the 5V regulator 548 and also connected via the resistor R1 to the 30 volt terminal line, is provided for maintaining the input to the 5V regulator 548 at substantially a 5 volt level. In addition, a pair of capacitors C5 and C6 are provided across the output of the regulator 548 for filtration purposes.

To accommodate interfacing the postage meter's computer 41 (Fig. 1) with the computer 500, any two available ports of the computer 41 may be programmed for two-way serial communications purposes and coupled to the computer 500. For example, the postage meter's printing module 41a may be conventionally modified to include an additional two-way serial communications channel for communication with the computer 500.

Assuming the latter arrangement, serial input communications to the computer 500 (Fig. 22) are received from the postage meter computer's printing module 41c via the serial input lead to the logic circuit 501a (Fig. 22), which is operably coupled to port P30 of the microprocessor 502 by means of a conventional inverting buffer circuit 550. Accordingly, port P30 is preferably programmed for serial

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input communications, and the input to the buffer circuit 550 is resistively coupled to the logic circuit's 5 volt source 530 via a conventional pull-up resistor R2. Serial output communications from the microprocessor 502 are transmitted 5 from port P3₁. Accordingly, port P3₁ is preferably programmed for serial output communications, and is operably coupled to the input of a conventional inverting buffer 552, the output of which is resistively coupled to the logic circuit's 5V source 530 via a suitable pull-up resistor R2 10 and is additionally electrically connected to the serial output lead from the logic circuit 501a.

Since it is preferable that the microprocessor 502 be reset in response to energization of the logic circuit 501a, the logic circuit's 5V source 530 is connected in series with 15 an R-C delay circuit and a conventional inverting buffer circuit 554 to the reset pin, RST, of the microprocessor 502. The R-C circuit includes a suitable resistor R3 which is connected in series with the logic circuit's local 5V source 530 and a suitable capacitor C7 which has one end connected 20 between the resistor R3 and the input to the buffer circuit 554, and the other end connected to the logic circuit's ground return.

In addition to the VCC and VSS terminals of the microprocessor 502 being respectively conventionally 25 connected to the logic circuit's 5 volt source and ground, since the microprocessor 502 does not utilize an external program memory, the $\overline{EA}$ terminal is connected to the logic circuit's 5V source. And, since no other external memory is

position lead of the logic circuit, which, in turn, is connected to one input of a differential amplifier 562, the output of which is connected to the other input of the differential amplifier 562 via a feedback resistor R4. The

5 aforesaid other input to the amplifier 562 is also resistively coupled, by means of a resistor R5, to the mid-point of a voltage divider circuit including resistors R6 and R7. Resistors R6 and R7 are connected in series with each other and across the logic circuit's 5V source and ground

10 return leads. The LED sensors 56 and 58, which are utilized for successively sensing the leading edges of each envelope being fed by the letter transport, are separately coupled to the computer 500 via the envelope sensor-1 and envelope sensor-2 input leads of the logic circuit 501a. In the logic

15 circuit 501a, the envelope sensor-1 and sensor-2 leads are connected on a one-for-one basis to one of the inputs of a pair of conventional amplifiers 564, the other inputs of which are connected together and to the mid-point of a voltage divider including resistors R8 and R9. Resistors R8

20 and R9 are connected in series with each other and across the logic circuit's 5V source and ground return leads. Further, the three output signals from the differential amplifier 562 and the two amplifiers 564 are connected on a one-for-one basis to the three input ports PO₀₋₂ of the microprocessor

25 502, each via a conventional tri-state buffer circuit 566, one of which is shown. The input signals A and B from the D.C. motor shaft encoder 126 are coupled to the logic circuit 501a

position lead of the logic circuit, which, in turn, is connected to one input of a differential amplifier 562, the output of which is connected to the other input of the differential amplifier 562 via a feedback resistor R4. The

5 aforesaid other input to the amplifier 562 is also resistively coupled, by means of a resistor R5, to the mid-point of a voltage divider circuit including resistors R6 and R7. Resistors R6 and R7 are connected in series with each other and across the logic circuit's 5V source and ground

10 return leads. The LED sensors 56 and 58, which are utilized for successively sensing the leading edges of each envelope being fed by the letter transport, are separately coupled to the computer 500 via the envelope sensor-1 and envelope sensor-2 input leads of the logic circuit 501a. In the logic

15 circuit 501a, the envelope sensor-1 and sensor-2 leads are connected on a one-for-one basis to one of the inputs of a pair of conventional amplifiers 564, the other inputs of which are connected together and to the mid-point of a voltage divider including resistors R8 and R9. Resistors R8

20 and R9 are connected in series with each other and across the logic circuit's 5V source and ground return leads. Further, the three output signals from the differential amplifier 562 and the two amplifiers 564 are connected on a one-for-one basis to the three input ports PO₀₋₂ of the microprocessor

25 502, each via a conventional tri-state buffer circuit 566, one of which is shown. The input signals A and B from the D.C. motor shaft encoder 126 are coupled to the logic circuit 501a

by means of leads A and B, which are conventially electrically connected to the counting circuit 270 to provide the microprocessor 502 the the count representative of the actual angular displacement of the motor shaft 122 from its home position. The counting circuit's leads Q0-Q7 are electrically connected on a one-for-one basis to Ports P0₀-P0₇ of the microcomputer 502 via one of eight conventional tri-state buffer circuits 568, one of which is shown, having their respective control input leads connected to each other and to the output of a conventional inverting buffer circuit 570, which has its input conventionally connected port P3₄ of the microprocessor 502. Thus, either the three input signals, i.e., from the drum home position and the two envelope position sensors are operably electrically coupled to Ports P0₀-P0₂ of the microprocessor 502, or the eight input signals Q0-Q7 from the counter circuit 270 are operably electrically coupled to ports P0₀-P0₇ of the microprocessor 502, for scanning purposes, in response to an appropriate control signal being applied to the respective buffer circuits 566 and 568 from port P3₄ of the microprocessor 502. In operation, assuming a low logic level signal is required for activating either of the sets of buffers 566 or 568; when the microprocessor 502 applies such a signal to port P3₄, the buffer circuits 566 operate, whereas since the buffer circuit 570 inverts this signal to a high logic level signal before applying the same to the buffer circuit 568, the latter is inoperative. Conversely, a high logic level signal from port P3₄ will operate buffer circuits 568 and not operate the

buffer circuits 566. Accordingly, depending upon the level, high or low, of the signal from port P3₄ of the microprocessor 502, the eight bit input to one or the other buffer circuits 566 or 568 will be made available to port P0 5 for scanning purposes. Aside from the foregoing, to permit the microprocessor 502 to clear the counter 270 for any reason in the course of execution of the program, port P3₅ is connected to the clear pin CLR of the counter 270 via a conventional inverting buffer 572, and the microprocessor 502 10 is programmed for timely applying the appropriate signal to port P3₅ which, when inverted, causes the counting circuit 270 to be cleared.

In general, ports P1₀-P1₃ are utilized by the microprocessor 502 for providing pulse width modulated (PWM) 15 motor control signals for controlling energization of the D.C. motor 120 and port P1₄ is utilized by the microprocessor 502 for controlling energization of the solid state, A.C. motor, relay 52 and thus operation of the mailpiece conveyor 49. To that end, ports P1₀-P1₄ of the microprocessor 502 are 20 each conventionally electrically connected on a one-for-one basis to the input of a conventional inverting buffer circuit 580, one of which is shown. The outputs of each of the buffer circuits 580 are connected on a one-for-one basis, via a conventional resistor R10, to output leads from the logic 25 circuit 501b, one of which is designated solid state, A.C. motor, relay, and four of which are respectively designated T1, T3, T2 and T4, since, as shown in Fig. 7, the four preamplifier stages of the power amplifier utilized for

opto-isolator's photo-transistor when the light emitting diode D1 is lit in response to the D.C. supply voltage level matching the internal reference voltage level, e.g., 30 volts, of the 30 volt detection circuit.

5 In the analog circuit 501b each of the outputs from the photo-transistors of each of the opto-isolators 303 are resistively coupled to the analog circuits 5V source by means of a conventional pull-up resistor 305, and the emitters of the photo-transistors T5 are connected to the analog
10 circuit's ground system. In addition, the collectors of the photodiodes of the opto-isolators 303, which are utilized for transmitting the motor control signals from ports P1₀-P1₃ of the microprocessor 502 are connected on a one-for-one basis to the appropriate input leads A, B, C and D of the power
15 amplifiers shown in Fig. 7, the outputs of which are connected to the D.C. motor 120. Further, the collector of the photodiode of the opto-isolator 303 which is utilized for transmitting the A.C. relay control signals from port P1₄ of the microprocessor 502 is connected to the input lead of a
20 conventional darlington-type power amplifier 550, the output of which is conventionally connected to the mailing machine's 30 volt D.C. source via a solid state, A.C. motor, relay 52, which is turn conventionally connected for energizing the A.C. motor 50 from the local A.C. source.

25 In general, the computer 500 includes three software programs, including a main line program Fig. 23, a transmit and receive program and a command execution program, respectively identified by the 600, 700 and 800 series of

opto-isolator's photo-transistor when the light emitting diode D1 is lit in response to the D.C. supply voltage level matching the internal reference voltage level, e.g., 30 volts, of the 30 volt detection circuit.

5 In the analog circuit 501b each of the outputs from the photo-transistors of each of the opto-isolators 303 are resistively coupled to the analog circuits 5V source by means of a conventional pull-up resistor 305, and the emitters of the photo-transistors T5 are connected to the analog
10 circuit's ground system. In addition, the collectors of the photodiodes of the opto-isolators 303, which are utilized for transmitting the motor control signals from ports P10-P13 of the microprocessor 502 are connected on a one-for-one basis to the appropriate input leads A, B, C and D of the power
15 amplifiers shown in Fig. 7, the outputs of which are connected to the D.C. motor 120. Further, the collector of the photodiode of the opto-isolator 303 which is utilized for transmitting the A.C. relay control signals from port P14 of the microprocessor 502 is connected to the input lead of a
20 conventional darlington-type power amplifier 550, the output of which is conventionally connected to the mailing machine's 30 volt D.C. source via a solid state, A.C. motor, relay 52, which is turn conventionally connected for energizing the A.C. motor 50 from the local A.C. source.

25 In general, the computer 500 includes three software programs, including a main line program Fig. 23, a transmit and receive program and a command execution program, respectively identified by the 600, 700 and 800 series of

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numbers. When the mailing machine 10 is energized by
actuation of the main power switch 24, the resulting low
level logic signal from D.C. supply is applied to the reset
terminal RST of the computer's microprocessor 502, thereby
5 enabling the microprocessor 502. Whereupon, as shown in Fig.
23, the microprocessor 502 commences execution of the main
line program 600.

The main line program 600 (Fig. 23) commences with
the step of conventionally initializing the microprocessor
10 602, which generally includes establishing the initial
voltage levels at the microprocessor's ports, and interrupts,
and setting the timers and counters. Thereafter, the D.C.
motor drive unit is initialized 604. Step 604 entails
scanning the motor home position sensor input port PO_0 , to
15 determine whether or not the D.C. motor 120 is located in its
home position and, if it is not, driving the motor 120 to its
home position. Assuming the D.C. motor 120 is in its home
position, either before or after the initialization step 604,
the program then enters an idle loop routine 606.

20 In the idle loop routine 606, a determination is
initially made as to whether or not the sampling time period
of $T=1$ millisecond has elapsed, step 608, it being noted that
each successive sample is taken at the time instant T_n
immediately after and in response to the fourth 250
25 millisecond interrupt generated by the timer utilized for
implementing the sampling time period T . Assuming the time
period T has not elapsed, the program loops to idle 606. On
the other hand, assuming the time period T has elapsed, the

microprocessor 502 updates the servo-control system, step 610. For the purpose of explaining step 610 it will be assumed until otherwise stated that the desired location of the postage meter drum 38, and thus the motor drive shaft 5 122, is the home position. Step 610 includes the successive steps 610a and 610b, respectively, of sampling the count of the actual position P_a of the motor drive shaft 122 at the sampling time instant T_n , and fetching the previously computed count representing the desired position P_d of the 10 shaft 122 at the same sampling time instant T_n . If for any reason the motor drive shaft 122 is not located in its home position when the value of the desired position count $P_d(T_n)$ is representative of the home position location, then the values of $P_a(T_n)$ and $P_d(T_n)$ will be different. On the other 15 hand, if the motor drive shaft 122 is located in its home position when the desired position count $P_d(T_n)$ is representative of the home position location, then the values of $P_a(T_n)$ and $P_d(T_n)$ will be the same. Accordingly, computation of the error count, 610c, may or may not result 20 in an error count value $E(T_n)$ of zero. Further, independently of the computed value of $E(T_n)$, the computed value $G(T_n)$ of the motor control signal, step 610d, may or may not result in a value of $G(T_n)$ of zero; it being noted that although step 610c results in a computed value of 25 $E(T_n)=0$, the value of g_2 may not be equal to zero due to the computed value of the error for the next previous sampling time instant $E(T_{n-1})$ having resulted in a non-zero value, step 610g. Assuming steps 610c and 610d both result in zero

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shaft 122 out of the home position, until a mailpiece 16 is fed to the drum 38.

At this juncture it will be assumed that the enable flag is set, as a result of which the inquiry of step 612 is answered affirmatively, or, as above stated, a mailpiece 16 is being fed to the drum 38. Accordingly, the microprocessor 502 commences polling the ports connected to the envelope sensors 56 and 58, step 614. Since polling occurs at one millisecond time intervals, the polling sequence is continuous. As shown by the following step 616, between successive time instants T_n , the program continuously loops to idle 606 and through steps 608-616 inclusive until the envelope sensing sequence for a given envelope is complete. Whereupon the microprocessor commences executing step 618, which includes the steps of calculating the envelope's velocity, 618a; then fetching from memory the corresponding acceleration, deceleration and constant velocity constants, 618b, for computation of the desired position counts P_d at each successive time instant T_n in advance of sampling the actual position counts P_a as hereinbefore discussed in connection with step 610; then fetching and implementing the time delay t_d for timely commencing acceleration of the drum 38 to the target velocity V_1 ; and then commencing drum rotation by generating the desired position P_d for the initial one millisecond sampling time instant of acceleration of the motor drive shaft 122 and storing the value for subsequent use in step 601b. Accordingly, the value of P_d

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shaft 122 out of the home position, until a mailpiece 16 is fed to the drum 38.

At this juncture it will be assumed that the enable flag is set, as a result of which the inquiry of step 612 is answered affirmatively, or, as above stated, a mailpiece 16 is being fed to the drum 38. Accordingly, the microprocessor 502 commences polling the ports connected to the envelope sensors 56 and 58, step 614. Since polling occurs at one millisecond time intervals, the polling sequence is continuous. As shown by the following step 616, between successive time instants T_n , the program continuously loops to idle 606 and through steps 608-616 inclusive until the envelope sensing sequence for a given envelope is complete. Whereupon the microprocessor commences executing step 618, which includes the steps of calculating the envelope's velocity, 618a; then fetching from memory the corresponding acceleration, deceleration and constant velocity constants, 618b, for computation of the desired position counts P_d at each successive time instant T_n in advance of sampling the actual position counts P_a as hereinbefore discussed in connection with step 610; then fetching and implementing the time delay t_d for timely commencing acceleration of the drum 38 to the target velocity V_l ; and then commencing drum rotation by generating the desired position P_d for the initial one millisecond sampling time instant of acceleration of the motor drive shaft 122 and storing the value for subsequent use in step 601b. Accordingly, the value of P_d

will no longer be assumed to be the value representative of the home position.

Thereafter, the inquiry is made as to whether or not the drum cycle is complete, step 620. Assuming as stated 5 above that only the initial desired value of P_d has been computed and stored, the inquiry of step 620 will be answered in the negative. Whereupon the microprocessor 502 transmits a status message, step 622, to the postage meter's computer 41 and the program loops to idle 606. Thereafter the 10 microprocessor 502 continuously executes steps 608-620 until the entire P_d count sequence 618d for the trapezoidal-shaped velocity versus time profile for the target velocity V_1 has been exhausted. In this connection it is noted that the drum cycle T_{ct} is not complete until the settling time interval T_s 15 which is allowed for damping any overshoot of the motor drive shaft 122 is complete. During the settling time interval T_s the value of P_d is a constant and representative of the home position of the shaft 122 and thus the drum 38. Assuming that the drum cycle is complete, the inquiry of step 620 will 20 be answered affirmatively. Whereupon the microprocessor 502 transmits a status message, step 624, to the postage meter's computer 41 and the program loops to idle 606. Thereafter, the foregoing steps 606-622 of the main line, servo-control, idle loop are continuously executed by the microprocessor 502 25 in accordance with the above discussion until the main power switch 24 is opened by the operator.

The serial communications program 700 includes the transmit status routine 704. The latter routine 704 includes

the steps of receiving and decoding any message, step 706, and invoking the execute command routine, step 708, both of which steps are self explanatory.

Assuming the execute command routine 800 has been
5 invoked, step 708, the microprocessor 502 executes the routine 800 commencing with the step 802 of inquiring whether or not the decoded message is an enable command. Assuming the answer is yes, an enable status flag is set, step 804, to indicate that an envelope is to be fed to the drum 38.
10 Whereupon the A.C. motor relay 52 is energized, step 806, for feeding the envelope to the drum 38, and the transmit status routine is invoked, step 808. On the other hand, assuming the decoded message is not an enable command, step 802, a enable status flag is cleared, step 810. Whereupon the A.C.
15 relay is deenergized, step 812, and the status transmit routine is invoked 808.

Assuming the status transmit routine 702 has been invoked, step 806, the microprocessor 502 executes the routine 702 commencing with the step 710 of inquiring whether
20 or not the drum cycle is complete. Assuming completion of the drum cycle, a drum cycle complete message is transmitted to the postage meter's computer 41, step 712. On the other hand, assuming the drum cycle is not complete, an inquiry is made as to whether or not the A.C. relay is energized, step
25 716, and, if it is, an A.C. relay energized message is transmitted to the postage meter's computer 41, step 718. If however the drum cycle is not complete, step 710, and the A.C. relay is not energized, step 716, then, an A.C. relay

deenergized message is transmitted to the postage meter's computer 41, step 720. Upon transmitting any of the messages, drum cycle complete, step 710, A.C. relay energized, step 716, or A.C. relay deenergized, step 720, the
5 microprocessor 502 returns to the idle 606 of the main line program 600.

The term postage meter as used herein includes any device for affixing a value or other indicia on a sheet or sheet like material for governmental or private carrier
10 parcel, envelope or package delivery, or other purposes. For example, private parcel or freight services purchase and employ postage meters for providing unit value pricing on tape for application on individual parcels.

For a more detailed description of the programs
15 herein-before discussed, reference is directed to the attached APPENDIX forming part of this specification which discloses a program listing which describes in greater detail the various routines incorporated in, and used in the operation of, the postage meter.

20 Although the invention disclosed herein has been described with reference to a simple embodiment thereof, variations and modifications may be made therein by persons skilled in the art without departing from the spirit and scope of the invention. Accordingly, it is intended that the
25 following claims cover the disclosed invention and such variations and modifications thereof as fall within the true spirit and scope of the invention.

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APPENDIX

(our ref: 42 699)
(B-931)

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PAGE: 1

<<< ASSEMBLY COMMAND STRING >>>

"070RC1."

<<< end of assembly command string >>>

LINE	ADDR	OBJECT	TYPE
1		#ARS	
2		#NOGEN	
3		SENORPRINT	
4		\$INCLUDE(DECLARE.DMS)	
5		*****	
6		? INTERNAL POS1 PAX'S DECLARATION	
7		*****	
8		? must have directly addressable bits.	
9		*****	
10		DSF0	
11		ORC	120H
12	0020	FLAGS	DS
13	0025	SAV_SEMSR	DS
14	0026	STAT-HEADER	DS
15	0027	MSG1-STAT	DS
16	0028	MSG2-STAT	DS
17	0029	MISTRIP-CTR	DS
18	002A	ERR-CNT	DS
19	002B	K2H1	DS
20	002C	K2L1	DS
21	002D	CMMD-HEADER	DS
22	002E	POSH-ACCI	DS
23	0030	RASE-INDEX	DS
24	0032	RUN_SPEED	DS
25	0033	VEL-OFFST	DS
26	0034	GP-LATCH	DS
27	0035	MARGIN	DS
28	0036	AUX-REG	DS
29	0037	ACCEL-CNT	DS
30	0039	DECCN-INT	DS
31	003A	CYC-CTR	DS
32	003B	TOTAL-CNT	DS
33	003P	ACCELX	DS
34	003E	SLCKX	DS
35	003F	ROFFS	DS
36	0041	DECCELX	DS
37	0042	PLIM-ERR	DS
38	0043	WLNH-ERR	DS
39	0044	PORTX-LATCH	DS
40	0045	TRIP-CTR	DS
41	0047	SAV2-AREA	DS
42	0049	DRUM-DECCEL	DS
43	004B	GP-PTX	DS
44	004D	START-OF-STACK	DS

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```

ER  LINE  ADDR  OBJECT  TYPE
46      *****
47      REGISTER BANK 0 *****
48      *****
49      USED BY MAIN LINE ROUTINE. *****
50      R0 = general purposes for indirect addressing modes.
51      R1 = general purposes for indirect addressing modes.
52      R2 = local in Stepper drive loop.
53      R3 = 1ms-interval counter.
54      R4 = 256-ms interval counter
55      R5 = general purpose register.
56      R4-R50      EQU 04
57      R5 = accel/decel timer high byte.
58      R6 = 1ms-increment time delay counter.
59      R7 = accel/decel timer low byte.

61      *****
62      REGISTER BANK 1 *****
63      *****
64      R4 is exclusively used by Communication r/n.
65      *****
66      NSFG
67      NHC      08
68      NS      1
69      NS      1
70      NS      1
71      NS      1
72      NS      1
73      NS      1
74      CSFG
75      COMPR-CTR      EQU 04
76      GP1-SAVE      EQU 90-R0
77      GP2-SAVE      EQU 91-R01

```

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ER	LINE	ADDR	OBJECT	TYPE
	79		*****	
	80		REGISTER BANK 2	
	81		*****	
	82		RU = trajectory computed count.	
	83		R1 = accum save location during int rtn.	
	84		R2 = control algorithm partial result storage (1byte).	
	85		R3 = control algorithm partial result storage (1byte).	
	86		R4 = scratchpad	
	87		R5 = scratchpad	
	88		R6 = 'on-the-fly' count latch	
	89		R7 = T1 timeout counter.	
	90		NSFG	
	91		NS	10H
	92	0010	COMP_CNT1	1
	93	0011	TEMP1	1
	94	0012	K111	1
	95	0013	K111	1
	96	0014	R4-RR21	1
	97	0015	R5-RR21	1
	98	0016	SAVE_LATCH1	1
	99	0017	T1_CTL1	1
	101		*****	
	102		REGISTER BANK 3	
	103		*****	
	104		RECEIVED MESSAGE ARRAY	
	106	0018	CHK01	NS
	107	001D	OLD_CHK01	NS
				5
				1
				PREVIOUS COMMAND.

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ER  LINE  ADDR  OBJECT  TYPE
109
110          *****
111          FLAGS DECLARATION
112          *****
113          15 (20H-24H) BYTES WITH DIRECTLY-ADDRESSABLE BITS RESERVED
114          1Bit address 0 to 7H.
115          *****
116          NSFG
117          ORG          00
118          COM_PSRV1
119          RTHDRF-FLG1  DBIT  5
120          COMERR-FLG1  DBIT  1
121          DCMOTR-FLG1  DBIT  1
122          RUN-FLG1     DBIT  1
123          ACCEL-FLG1   DBIT  1
124          PROF-FLG1    DBIT  1
125          INIT-FLG1    DBIT  1
126          TR1-FLG1     DBIT  1
127          TR2-FLG1     DBIT  1
128          MSG-FLG1     DBIT  1
129          SHAL-FLG1    DBIT  1
130          COM1-FLG1    DBIT  1
131          SKIP-FLG1     DBIT  1
132          CMDSRC-FLG1   DBIT  1
133          RES-FLG1      DBIT  1
134          SAVED-RTN1    DBIT  1
135          RETWR-FLG1    DBIT  1
136          DCMOVE-FLG1   DBIT  1

          COM_PSRV1
          RTHDRF-FLG1  DBIT  5
          COMERR-FLG1  DBIT  1
          DCMOTR-FLG1  DBIT  1
          RUN-FLG1     DBIT  1
          ACCEL-FLG1   DBIT  1
          PROF-FLG1    DBIT  1
          INIT-FLG1    DBIT  1
          TR1-FLG1     DBIT  1
          TR2-FLG1     DBIT  1
          MSG-FLG1     DBIT  1
          SHAL-FLG1    DBIT  1
          COM1-FLG1    DBIT  1
          SKIP-FLG1     DBIT  1
          CMDSRC-FLG1   DBIT  1
          RES-FLG1      DBIT  1
          SAVED-RTN1    DBIT  1
          RETWR-FLG1    DBIT  1
          DCMOVE-FLG1   DBIT  1

          *****
          1Bit Mode communication.
          1Communication error flag.
          1DC motor dir -CCW: 1=CA.
          1Slew mode flag.
          1Accel/decel flag
          10 point-to-point: 1=velocity-position
          1Initialization note.
          1First mail detect.
          1Second mail detect.
          1Message queue flag.
          1Load have indicator.
          15 counter or 155 flag.
          1Continuous mode flag.
          1Flow skip flag.
          1Command source flag.
          1Rest mode flag.
          1Bit temp storage.
          1Transmission receiver.
          1DC motor in active motion.

```


LINE	ADDR	OBJECT	TYPE
1	000000	000000	000000
2	000001	000001	000001
3	000002	000002	000002
4	000003	000003	000003
5	000004	000004	000004
6	000005	000005	000005
7	000006	000006	000006
8	000007	000007	000007
9	000008	000008	000008
10	000009	000009	000009
11	000010	000010	000010
12	000011	000011	000011
13	000012	000012	000012
14	000013	000013	000013
15	000014	000014	000014
16	000015	000015	000015
17	000016	000016	000016
18	000017	000017	000017
19	000018	000018	000018
20	000019	000019	000019
21	000020	000020	000020
22	000021	000021	000021
23	000022	000022	000022
24	000023	000023	000023
25	000024	000024	000024
26	000025	000025	000025
27	000026	000026	000026
28	000027	000027	000027
29	000028	000028	000028
30	000029	000029	000029
31	000030	000030	000030
32	000031	000031	000031
33	000032	000032	000032
34	000033	000033	000033
35	000034	000034	000034
36	000035	000035	000035
37	000036	000036	000036
38	000037	000037	000037
39	000038	000038	000038
40	000039	000039	000039
41	000040	000040	000040
42	000041	000041	000041
43	000042	000042	000042
44	000043	000043	000043
45	000044	000044	000044
46	000045	000045	000045
47	000046	000046	000046
48	000047	000047	000047
49	000048	000048	000048
50	000049	000049	000049
51	000050	000050	000050
52	000051	000051	000051
53	000052	000052	000052
54	000053	000053	000053
55	000054	000054	000054
56	000055	000055	000055
57	000056	000056	000056
58	000057	000057	000057
59	000058	000058	000058
60	000059	000059	000059
61	000060	000060	000060
62	000061	000061	000061
63	000062	000062	000062
64	000063	000063	000063
65	000064	000064	000064
66	000065	000065	000065
67	000066	000066	000066
68	000067	000067	000067
69	000068	000068	000068
70	000069	000069	000069
71	000070	000070	000070
72	000071	000071	000071
73	000072	000072	000072
74	000073	000073	000073
75	000074	000074	000074
76	000075	000075	000075
77	000076	000076	000076
78	000077	000077	000077
79	000078	000078	000078
80	000079		

```

1139 /***** STATUS BITS EQUATES *****/
1140 /
1141 / (REGISTERS MSG_STAT)
1142 / *****/
1143 CSEG
1144     FJH      MSG1_STAT.0      Program flow catchdog.
1145     EQU      MSG1_STAT.2      Drive system enable
1146     FJH      MSG1_STAT.3      Status-change flag.
1147     FJH      MSG1_STAT.4      Sensor stucken on.
1148     FJH      MSG1_STAT.5      Trip logic enable flag.
1149     EQU      MSG1_STAT.6      DC motor bind
1150
1151     FJH      MSG2_STAT.0      Low 30 VDC supply.
1152     EQU      MSG2_STAT.1      Bad feet (paper jammed/missing)
1153     FJH      MSG2_STAT.2      Stalled flag.
1154     FJH      MSG2_STAT.5      Transport path not clear
1155     EQU      MSG2_STAT.6      Bad communication line.
1156     FJH      MSG2_STAT.7      Initialization error.

```


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```

ER  LINE  ADDR  OBJECT  TYPE
192
193
194
195
196  BR00
197
198
199
200  BR01
201  BR02
202  BR03
203  9000
204  1000
205
206
207
208
209  E00F
210  E006
211  E018
212  E015
213  E01E
214  E64C
215  E625
216  E1C8
217  C000
218
219
220

```

 R155'S MEMORY & I/O ADDRESS MAP

 P8155 F000 00800H SDK emulation = 07800H
 J2732A error = 07800H.

 IF HIGH(P8155) F0 000H
 PORTA F000 00014 JPort A address
 PORTB F000 00024 JPort B address
 PORTC F000 00034 JPort C address
 PORTX F000 9000H JPort X address
 EXRAM1 F000 1000H J8155 start of RAM.

 SDK-51 AUXILIARY RTS ENTRY

 CLRDSF F000 0E00FH JClear SDK display.
 DSPCHR F000 0E006H JDisplay an ASCII character.
 DSP2BY F000 0E018H JDisplay 2-byte hex.
 DSP1BY F000 0E015H JDisplay 1-byte hex.
 DSPMSG F000 0E01EH JDisplay ASCII string.
 UPI_IN F000 0E64CH
 UPI_CMD F000 0E625H
 CSYERR F000 0E1C8H JDisplay checksum err msg.
 KEYBD F000 0C000H
 FALSE
 FNDIF
 \$INCLUDE(INVECTOR.DMS)

LR	LINE	ADDR	OBJECT	TYPE
	222		*****	
	223		PROGRAM STARTS HERE	
	224		*****	
	225		ORG 00	
	226	0000	ORG \$	
	227	0000 01 99	AJMP POWER_ON	.C..
			Power-up initialization routine.	
	229		*****	
	230		LOOPS FOREVER	
	231		*****	
	232		ORG 03	
	233	0003 02 00 03	LJMP \$	.C..
	234	0006 00 00	CHECK_SUM	
	235	0008 00 03	PUSH DPH	.D..
	236	000A 32	RETI	
			loops forever if checksum error.	
	238		*****	
	239		TO INTERRUPT SERVICE ROUTINE	
	240		*****	
	241		Used to keep track of the PWM turn-on time interval.	
	242		Timer is reloaded and started in the TI_ISR interrupt routine	
	243		every sampling interval with computed servo output	
	244		value (PWM turn-on time for the next sampling interval.)	
	245		Used by communication routine as watchdog.	
	246		Not used by servo control (output Xfers always off) when	
	247		used by communication routine.	
	248		*****	
	249		ORG 00H	
	250	000H 43 00 03	ORG	.D..
	251	000F 10 06 01	PL, 00000011R	.D..
	252	0011 37	JBC CUMERR_FLAG, \$+4	
	253	0012 90 0A 8F	RETI	
	254	0015 8E 01	MOV DPTR, 00000000H	
	255		MOV SP, R6	
	256		*****	
	257		SPECIFY RETURN ADDRESS	
	258		FOR FORCED RETURN	
	259	0017 00 02	PUSH DPH	.D..
	260	0019 80 ED	SJMP TUCONT	.R..
			Push to stack PC return address.	

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ER LINE ADDR OBJECT TYPE

```

262 *****
263 INAME: TIVER1_INT
264 ;
265 ;
266 ;ABSTRACT: Invokes by the sampling interval timeout; computes
267 ; the desired duty cycle for the next sampling interval
268 ; based on the sampled error count, last error count, and
269 ; last output (PWM turn-on time).
270 ;
271 ;INPUTS: SYS_WTCHDOG, K1U, K1H, ERR_CMT, NC40VE_RUG, DPTR
272 ;
273 ;OUTPUTS: SGN(PW4 turn-on time) in K2H, K2L.
274 ; ARSPWM turn-on time) in Timer 0 and start timer.
275 ;
276 ;VARIABLES MODIFIED: R01 registers, FRP_CMT, IO matches, T0U, 01
277 ; K2H, K2L, Carry C, SYS_WTCHDOG
278 ;
279 ;RESTRICTIONS:
280 ; For logic correctness and servo loop stability, this
281 ; interrupt service rtn is position and time sensitive.
282 ; Timer 1 interrupt must have WAIT_J1 loop of 10000-50000
283 ; module as its only background routine to synchronize
284 ; the system to the servo sampling interval. The time to
285 ; compute the servo output must be insignificant relative
286 ; to the sampling period, ie., time delay between sampling
287 ; and outputting of PWM motor control must approach zero.
288 ; Hence, DPTR, B register, and PW4 are preset to P20H,
289 ; 10H(COFF0), and Register Bank 2 respectively.
290 ;
291 ;SUBRTNS ACCESSED: None
292 *****
293
294 001H D5 17 7A .DR.
295 001E C2 RC .R..
296 0020 F9

```

ARG 18H
 TIVER1_INT: T1_CTR, T1_EXIT
 CLR TMO
 MOV R1, A
 ;Stop P44 timer.
 ;Save accn of background rtn.

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LN	LINE	ADDR	OBJECT	TYPE	CODE	COMMENT
298					-----	-----
299					COMPUTF FRQDR COUNT	
300					-----	-----
301	0021	E0			MOVX A,ADPTR	
302	0022	F0			MOV R5,A	ISADP actual position.
303	0023	E0			MOVX A,ADPTR	
304	0024	B5 15 02	.RR.		CJNE A,R5,R02,REFAD	
305	0027	R0 02	.R..		SJMP COMP_ERR	
306	0029	E0			MOVX A,ADPTR	
307	002A	F0			MOV R5,A	
308	002B	E8			MOV A,R0	
309	002C	C1			CLR C	
310	002D	90			MOV A,R5	
311	002E	F5 2A	.D..		FRQ-CVT,A	Get desired position count.
312	0030	20 E7 02	.RR.		ACC.7,\$15	IACC=desired ICOMP_CVT=desired.
313	0031	80 02	.R..		SJMP	Error count=desired count=desired.
314	0035	F4			CHK-TOLE-TOI	Determine sign of error.
315	0036	04			INC A	Get absolute value of error if error
316	0037	20 17 06	.RR.		MOV A,101,COMP_PWH	Is mode still in active or error?
317	003A	B4 01 03	.R..		CJNE A,101,COMP_PWH	Is count tolerance if in error?
318	003D	E4			CLR A	ie, error count is made 0.
319	003E	F5 2A	.D..		MOV FRQ-CVT,A	
320					-----	-----
321					COMPUTF SERV0 OUTPUT	
322					-----	-----
323					COMP_PWH	
324	0040	FC			MOV R4,A	
325	0041	A4			MUL AB	IACC=ABS(ERR CNT)=94.
326	0042	CC			XCH A,R4	IH=constant (IACC/ERRF0).
327	0043	25 F0	.D..		ADD A,R	
328	0045	CA			XCH A,R2	
329	0046	20 57 05	.RR.		JB FRQ-CVT,7,NUS	Is CTRF0 x err cnt = 94? HIGH 20/.
330	0049	2C			ADD A,P4	
331	004A	CA			XCH A,R3	IR2(100),H(101) registers hold the error
332	004B	3A			ADDC A,R2	I(-CHERR) x (H(101) - CTRF0) x (H(101) -
333	004C	80 04	.R..		SJMP MPD_PWH	Output G(x) is in R3=byte, acc=byte.
334	004E	C1			CLR C	
335	004F	9C			SUB A,R4	
336	0050	CA			XCH A,R3	
337	0051	9A			SUB A,R2	
338					-----	-----
339					MPD_PWH	
340					UPDATE PWH DRIVE	
341					-----	-----
342	0052	84 2C	.D..		MOV R2,R1	
343	0054	20 4F 05	.RR.		JB R2H,7,\$18	Determine previous output sign bit.
344	0057	20 E7 07	.RR.		JR ACC.7,SIGNC_NEG	Output sign change from + to -.
345	005A	80 1F	.R..		SJMP SAME_POS	no change + to +.

LINE	ADDR	OBJECT	TYPE	INSTR	COMMENT
346	005C	30 F7 15	.RR.	ACC,7,SIGHC_PDS	Changed from - to +.
347	005F	80 07	.R..	SAVE_NEG	NO CHANGE - LO -.
348	0061	43 90 0F	.D..	PI,PO0001111R	Turn off output store if sign
349	0064	7C 08		R4,00B	Changed to avoid per supply short.
350	0066	DC FE	.R..	R4,5	Turn-off delay time.
351	0068	F5 2B	.D..	R2H,A	Save output.
352	006A	F5 AC	.D..	THO,A	Load timer registers.
353	006C	8R 8A	.D..	TLO,R3	
354	006E	00		PI,PI11110110R	Turn on Xtor C1 pair.
355	006F	53 90 F6	.D..	ON_TIMER	Turn on Xtor C2 pair.
356	0072	80 12	.R..	PI,PO0001111R	Turn on Xtor C2 pair.
357	0074	43 90 0F	.D..	R4,00B	Turn on Xtor C2 pair.
358	0077	7C 08		R4,5	Turn on Xtor C2 pair.
359	0079	DC FE	.R..	R2H,A	Turn on Xtor C2 pair.
360	007B	F5 2B	.D..	A	Turn on Xtor C2 pair.
361	007D	F4		A,R3	Turn on Xtor C2 pair.
362	007E	CH		A	Turn on Xtor C2 pair.
363	007F	F4		TLO,A	Turn on Xtor C2 pair.
364	0080	F5 RA	.D..	PI,PI1111001R	Turn on Xtor C2 pair.
365	0082	53 90 F9	.D..	THO,R3	Turn on Xtor C2 pair.
366	0085	8R AC	.D..	TRN	Turn on Xtor C2 pair.
367	0087	D2 RC	.D..	TRN	Turn on Xtor C2 pair.
369	0089	E9		A,R1	Turn on Xtor C2 pair.
370	008A	10 18 0R	.RR.	WCHNDC-FLG,T1-EVIT	Turn on Xtor C2 pair.
371	008D	D2 18	.D..	WCHNDC-FLG	Turn on Xtor C2 pair.
372	008F	D0 4B	.D..	GP_PTR	Turn on Xtor C2 pair.
373	0091	D0 4C	.D..	GP_PTR+1	Turn on Xtor C2 pair.
374	0093	90 02 01	.D..	GP_PTR+1	Turn on Xtor C2 pair.
375	0096	01 17	.C..	OPTR,IFATAL	Turn on Xtor C2 pair.
376	0098	12	.C..	FORCET	Turn on Xtor C2 pair.
377				TI-EXIT	Turn on Xtor C2 pair.
378				SIGCHUNE(PNWRN,UDS)	Turn on Xtor C2 pair.

SR	LINE	ADDR	OBJECT	TYPE
379				
380				
381				
383				
384				
385				
386	0099	30	R3 F0	.NR.
387	009C	90	00 00	.C.
388	009F	7F	00	
389	00A1	E4		
390	00A2	93		
391	00A3	2F		
392	00A4	FF		
393	00A5	A3		
394	00A6	E5	R3	.D..
395	00A8	B4	40 F6	.D..
396	00AB	EF		
397	00AC	60	03	.D..
398	00AE	02	F3 C8	
400				
401				
402				
403	0081	C2	R1	.B..
404	00B3	32	E0 0F	
405	00B6	74	1C	
406	00B8	90	B8 00	
407	00BA	F0		
408	00BC	74	FF	
409	00BE	F5	90	.B..
410	00C0	75	R2 03	.D..
411	00C3	F0		
412	00C4	90	90 00	
413	00C7	F0		

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ER	LINE	ADDR	OBJECT	TYPE
	415		-----	
	416		CLAP INTERNAL RAMS	
	417		SET UP TIMERS, INTERRUPTS, STACK	
	418		-----	
	419	00C8	E4	
	420	00C9	78 7F	
	421	00CA	F6	
	422	00CB	0A FD	.R..
	423	00CC	F5 B8	.D..
	424	00CD	F5 A8	.D..
	425	00CE	F4	
	426	00CF	F5 44	.D..
	427	00D0	75 B8 02	.D..
	428	00D1	75 A9 21	.D..
	429	00D2	75 AD 06	.D..
	430	00D3	75 B1 4C	.D..
	431	00D4	43 AB 9A	.D..
	432			
	433			
	434			
	435			
	436	00E4	75 3D AE	.D..
	437	00E5	0F	
	438	00E6	12 09 42	.C..
	439	00E7	25 4A	.D..
	440	00E8	F5 4A	.D..
	441	00E9	B1 11 F5	.R..
	442	00EA	8F 49	.D..
	443	00EB	75 35 46	.D..
	444			

```

;-----
; CLAP INTERNAL RAMS
; SET UP TIMERS, INTERRUPTS, STACK
;-----
CLR A
MOV R0,7FH
MOV R0,A
MOV R0,CLR_8031
MOV TCON,A
MOV IE,A
CPL A
MOV MOV PORTX_LATCH,A
MOV TP,02
MOV TH0,021H
MOV TH1,(1-TC_TINT)
MOV SP,START_OF_STACK-1
ORL IE,01011111B
; Clear 8051 internal ram's.
; Clear all interrupt flags.
; and interrupt enables.
; Put FFH to Port A latch.
; To highest priority
; TI = mode 2; T0 = mode 1.
; Timer 1 interval constant.
; First stack location.
; Enable interrupts except P1.

;-----
; COMPUTE CONSTANT PARAMETERS
;-----
MOV ACCELX,0DECH
; Given decel rate and running speed,
; compute decel distance and
; decel time interval.
MOV INC R7
ICALL COMP_ACCEL
ADD A,0001-DECEL+1
MOV DRUM-DECEL+1,A
CME R4,DRUM,ITERUN
MOV DRUM-DECEL,R7
MOV MARGIN,170
; Initialize MARGIN to 1/4 inch.
; INCLUDE(INITLOAD.OVS)

```

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ER	LINE	ADDR	OBJECT	TYPE
	446		***** ***** INITIALIZE MECHANICAL BASE ***** *****	
	447		*****	
	448		*****	
	449	00F7 02 3A	SETB SYS_ENABLE	.R..
	450	00F9 91 34	ACALL START_SERVO	.C..
	452		***** ***** CHECK OPTICAL SENSORS ***** *****	
	453		*****	
	454		*****	
	455	00F8 90 88 01	MOV OPTR,PORTA	
	456	00FE E0	MOVX A,00FFH	
	457	00FF 44 38	ORL A,00110000	
	458	0101 84 FF 02	CJNE A,00FFH,STUCKEN	
	459	0104 80 04	SJMP ENBLE_OPTO	.R..
	460	0106 02 3C	SETB RADSFVS_FLG	.P..
	461	0108 21 1F	AJMP FAIL_INITZ	.R..
	462	010A 7C EF	MOV R4,01101111H	.C..
	463	010C 91 94	ACALL ON_BIT	.C..
	465		***** ***** FIND MAIN DRIVE SHAFT HOME ***** *****	
	466		*****	
	467		*****	
	468	010F 12 05 05	LCALL HOME_CHK	.C..
	469	0111 60 06	JZ ALIGNED	.R..
	470	0113 12 04 ED	LCALL HOME_SPCN	.R..
	471	0116 10 3H 06	JOC STAF_FLG,FAIL_INITZ	.R..
	472	0119 15 30	MOV RASE_INDEX,A	.R..
	473	011B F5 11	MOV RASE_INDEX+1,A	.R..
	474	011D 21 23	AJMP EX_INITZJAD	.C..
	476		***** ***** INITIALIZATION FAILURE ***** *****	
	477		*****	
	478		*****	
	479	011F 07 47	SETB INITZERR_FLG	.R..
	480	0121 41 03	AJMP JFATAL	.C..
	481	0123	EX_INITZLOAD FDI	
	482		SINCLUDE(MAINING.MS) 5	
			***** ***** Enable system. ***** Start servo control. *****	
			***** ***** Check for stucked sensors. *****	
			***** ***** Enable notices if all off. ***** Set status bit for "senser fail". *****	
			***** ***** Enable system optical sensors. *****	
			***** ***** Head base home sensr. ***** Head home if not 0. ***** Initialize main drv shaft home. *****	
			***** ***** Preset nose index sensr. *****	
			***** ***** Tell of initial'n failure. ***** Proceed to fatal load. *****	

[illegible]

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CR	LINE	ADDR	OBJECT	TYPE	
	655	0227	50 08	.R..	
	656	0229	12 0A 14	.C..	JLNDP
	657	022C	DC FE	.R..	PECV_45G
	658	022E	12 09 7C	.C..	P4,3
	659	0231	DC FE	.R..	X41F-STAT
	660	0233	DC FE	.R..	R4,3
	661	0235	DA FB	.R..	R4,3
	662	0237	80 E7	.R..	R2,LODRIMS
					FATAL_LUNP
	664	0239	03 45 3D 20		3, 'E' ,
					DB
					STRINGI

JLNDP
PECV_45G
P4,3
X41F-STAT
R4,3
R4,3
R2,LODRIMS
FATAL_LUNP
JLNDP forever.

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FR	LINE	ADDR	OBJECT	TYPE	
	714	0265	CC		
	715	0266	C1		
	716	0267	9C		
	717	0268	60 12	.R..	
	718	026A	50 0D	.R..	
	719	026C	C2 0C	.R..	
	720	026E	D7 42	.R..	
	721	0270	05 29	.D..	
	722	0272	24 02		
	723	0274	FE		
	724	0275	91 81	.C..	
	725	0277	21 23	.C..	
					NO_PRINT:
	727	0279	FE		
	728	027A	91 81	.C..	
	729	027C	51 80	.C..	
	730	027E	21 C0	.C..	
	731				

XCH
 CLR
 SUBP
 JZ
 JNC
 CLR
 SETB
 JNC
 ADD
 MOV
 ACALL
 JMP
 NO_PRINT:

A,R4
 C
 A,R4
 DRV_DRUM
 LOAD_DELAY
 TRI_FLG
 STRIP_FLG
 MISSTRIP_CTR
 A,B210
 R6,A
 DELAY_LOOP
 TOP_LOOP

R6,A
 DELAY_LOOP
 MOVE_DRUM
 CHWD_COMPLETE

MOV
 ACALL
 ACALL
 JMP
 SINGLEDONE(MOTION,045)

remainder = time delay before start
 of drum print cycle.
 PC on positive valid letters 380.
 1 streamfeed error!
 PC = 1 negative 120 too close.
 1 not enough time for complete cycle
 12's cri adj'n.
 1 pad in delay to complete cycle.
 1 skip print on passing mail.

1 print on mail.

[illegible]

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```

ER  LINE: ADDR  OBJECT.  TYPE
775          *****
776          MOTION PROFILE REQUIREMENTS
777          *****
778          The caller has to supply the following variables.
779          -----
780          11. ACCELRK = acceleration constant (counts/ms^2)
781          12. DECCFLK = deceleration constant (counts/ms^2)
782          13. SLEWRK = running velocity constant (counts/ms)
783          14. TOTAL_CNT = total distance to be traversed (counts)
784          15. CONT_FLAG = incremental or continuous motion
785          16. PROF_FLAG = profile or position-only (point-to-point) control.
786          17. LIM_ERR = max error count before calling a fault condition.
787          -----
788          *****
789          HUNT_MOVE:      MOV     TOTAL_CNT,LOW(HBASE-IRFV) ;Specifies drum rotation
790                          MOV     TOTAL_CNT+1,HIGH(HBASE-IRFV) ;velocity profile and
791                          MOV     ACCELRK,ACCCH ;type of control.
792                          MOV     DECCFLK,DECCD
793                          MOV     SLEWRK,SRWHD
794                          MOV     DECCFL_INT,DRUM_DECCFL
795                          MOV     ACCELR_CNT,DRUM_DECCFL+1
796                          MOV     ACCELR_CNT+1,PON
797                          SETB    PROF_FLAG
798                          MOV     LIM_ERR,PHAPDEST
799                          MOV     HUNT_ERR,1(-HAPDEST)
800                          JMP     START_MOTION
801
802          HUNT_MOVE:      CLR
803                          MOV     TOTAL_CNT+1,A ;Search for a home position signal.
804                          MOV     CYC_CTR,A ;Will stop in SRCH_CNT once home
805                          MOV     TOTAL_CNT,PSRCH_CNT ;The home posn signal is seen.
806                          SETB    CONT_FLAG ;Run continuously
807                          SETB    HOME_FLAG ;Set satollina handler to
808                          MOV     LIM_ERR,1(SRCH_CNT) ;look for the signal.
809                          MOV     NLTN_ERR,1(-SRCH_CNT)
810                          JMP
811
812          ENDSTOP_MOVE:   MOV     TOTAL_CNT,POFFH ;Move towards an endstop.
813                          MOV     TOTAL_CNT+1,IOFFH ;Load max 16 bit count.
814
815          INITZ_MOVE:     MOV     LIM_ERR,1(SOFTERR) ;Lowest error limit for
816                          MOV     NLTN_ERR,1(-SOFTERR) ;Soft collision at endstop.
817                          MOV     SUPR_K,INITZ_SPEED ;Slow speed= 1 cnt/sample.
818                          MOV     ACCELRK,INITZ_ACCEL
819                          JMP     TRAP7PROF
820          ONREV_MOVE:     MOV     TOTAL_CNT,LOW(HBASE-IRFV) ;One rotation move
821                          MOV     TOTAL_CNT+1,HIGH(HBASE-IRFV) ;at base drv shaft.
822                          MOV     ACCELRK,1NACT ;Base point-to-point drive.

```

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```

ER  LINE  ADDR  OBJECT  TYPE
823 0109 75 3E 1A .D..
824 010C 75 42 30 .D..
825 010F 75 43 00 .D..

827 -----
828 / INITIALIZE MOTION CONTROL LOOP
829 / HOUSEKEEPING
830 /-----
831 TRAPZPROF1 ACALL COMP_PROF /Compute a trapezoidal motion profile.
832 START_MOTION1 CLR A
833 MOV R5,A
834 MOV POSN-ACC,A /Clear position accumulator.
835 MOV POSN-ACC+1,A
836 TNC A
837 MOV R7,A /Initialize accel/decel/settle timer.
838 A,R05 /Check for size of displacement.
839 CJNE A,TOTAL_CNT,&4 / 15 counts or less= single step
840 CLR C / by 1 count/sample.
841 JC PROCEED /Else, proceed with trapz profile.
842 CLR A
843 CJNE A,TOTAL_CNT+1,PROCEED
844 CJNE A,TOTAL_CNT,LESS5
845 RET
846 LESS5 SETB RUN_FLG
847 CLR RUN_FLG
848 MOV RUN_SPEED,R01
849 JMP NCURCOP
850 SETB RUN_FLG
851 CLR SMOVE_FLG
852 SETB SMOVE_FLG /Start of denotor motion.

MOV SMAX_PUN
PUTX_ERR,HARDPR /load max. error count limit
WLTX_ERR,(-HARDPR) /harder stop).

```

REF	LINE	ANDR	OBJECT	TYPE
1	1	1	1	1
2	2	2	2	2
3	3	3	3	3
4	4	4	4	4
5	5	5	5	5
6	6	6	6	6
7	7	7	7	7
8	8	8	8	8
9	9	9	9	9
10	10	10	10	10
11	11	11	11	11
12	12	12	12	12
13	13	13	13	13
14	14	14	14	14
15	15	15	15	15
16	16	16	16	16
17	17	17	17	17
18	18	18	18	18
19	19	19	19	19
20	20	20	20	20
21	21	21	21	21
22	22	22	22	22
23	23	23	23	23
24	24	24	24	24
25	25	25	25	25
26	26	26	26	26
27	27	27	27	27
28	28	28	28	28
29	29	29	29	29
30	30	30	30	30
31	31	31	31	31
32	32	32	32	32
33	33	33	33	33
34	34	34	34	34
35	35	35	35	35
36	36	36	36	36
37	37	37	37	37
38	38	38	38	38
39	39	39	39	39
40	40	40	40	40
41	41	41	41	41
42	42	42	42	42
43	43	43	43	43
44	44	44	44	44
45	45	45	45	45
46	46	46	46	46
47	47	47	47	47
48	48	48	48	48
49	49	49	49	49
50	50	50	50	50
51	51	51	51	51
52	52	52	52	52
53	53	53	53	53
54	54	54	54	54
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56	56	56	56	56
57	57	57	57	57
58	58	58	58	58
59	59	59	59	59
60	60	60	60	60
61	61	61	61	61
62	62	62	62	62
63	63	63	63	63
64	64	64	64	64
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67	67	67	67	67
68	68	68	68	68
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70	70	70	70	70
71	71	71	71	71
72	72	72	72	72
73	73	73	73	73
74	74	74	74	74
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76	76	76	76	76
77	77	77	77	77
78	78	78	78	78
79	79	79	79	79
80	80	80	80	80
81	81	81	81	81
82	82	82	82	82
83	83	83	83	83
84	84	84	84	84
85	85	85	85	85
86	86	86	86	86
87	87	87	87	87</

```

*****
***** DC MOTOR MOTION CONTROL LOOP *****
*****
***** here during dc motor servo control of a
***** desired motion profile.
***** RUN_Flg and ACCRU_Flg are modified to reflect
***** a trapezoidal motion profile.
***** without decision is used at the next sampling
***** instant generation of the target trajectory.
*****
*****-----*****
DCMDLOOP1          DCALG.      UPDATE servo control.
      JGV          A,ERR,CNT          IACC.7 at next cntlnz nzccz.
      JH           ACC.7,CNT_NEG      ICheck if error count is within
      CJNE         A,PLIN_ERR,5+4    ;allowable limit = 0ns(MAPPRD)
      STB          C
      JMC          FAULT
      AJMP         COMP_FIXING
      CJNE         A,NLCL_ERR,0+4
      CLR          C
      JNC          COMP_FIXING
*****-----*****
***** DC MOTOR CONTROL LOOP EXIT *****
*****-----*****
FAULT1            PRNF_Flg,SHUTOFF
      SETB         STAT_Flg
      SJMP         COMP_FIXING
*****-----*****
SHUTOFF1          SYS_ENABLE
      CLR          MSG1_STAT,1010010000
      DRI          PI,1000000110
      MOV          RUN_SPEED,100
      MOV_Flg      RUN_Flg
      CLR          ACCRU_Flg
      JH           STAT_Flg,EX_DCMVLOOP
      JB           PI.7,LONG_SETTLE
      JNB          INITZ_Flg,LONG_SETTLE
      ORL          DEL05%
      SJMP         FX_DCMVLOOP
      ACALL        DEL20%
      CLR          DCMOVE_Flg
*****-----*****
END_OF_MOTION1
      MOV          LONG_SETTLE1
      SJMP         FX_DCMVLOOP1
*****-----*****
FX_DCMVLOOP1
      ACALL        RET
*****

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ER LINE ADDR OBJECT TYPE

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895 *****
896 / TRAP2NDIAL MOTION PROFILE *****
897 /
898 / HOUSEKEEPING *****
899 /
900 / Decides whether the motion is in accel phase,
901 / constant velocity phase, decel phase, or in
902 / settling phase based on the motion specs and
903 / control mode inputs.
904 / Insure the motion stops at final position count.
905 / Uses the following registers and control flags:
906 / TOTAL_CNT = desired total displacement count
907 / POSN_ACC = accumulated displacement count wrt time
908 / ACCEL_CNT = POSN_ACC value when in accel phase.
909 / RUN_SPEED = computed target speed last sampling instant
910 / VEL_OFFSET = offset count to insure total displ. = desired.
911 / ACCELK = desired accel rate
912 / SLEWK = desired slew rate (running speed)
913 / DECELEK = desired decel rate
914 / CYC_CTR = desired displacement multiplier.
915 / RUN_FLG = 0 constant velocity phase; 1 accel/decel
916 / ACCEL_FLG = 0 accel phase; 1 decel phase
917 / PROF_FLG = 0 accel rate = decel rate; 1 not equal
918 / CNT_FLG = 0 start-stop mode; 1 continuous run mode
919 / START_FLG = 0 TOTAL_CNT > 5; 1 not > 5.
920 / R7 and R5 (RUN) as a 16-bit register for
921 / keeping track of accel/decel time interval.
922 / Modifies RUN_FLG, ACCEL_FLG, R7, R5 for next sampling
923 / instant generation of the target position count.
924 /
925 *****
926 / COMP-TIMING: JH RUN_FLG,NOTCV / Examine last sampling
927 / NOTCV: AJMP CONST_VEL, / Instant's motion phase,
928 / JNR ACCEL_FLG,ACCEL_VEL, / is const velocity? accel?
929 / AJMP DECEL_VEL, / decel phase?
930 /
931 / -----
932 / ACCELERATION PHASE
933 /
934 / ACCEL_VEL: JH PROF_FLG,CHK_SPEDLIM / motion in accel mode if
935 / C / PROF_FLG < TOTAL_CNT/A / PSH_ACC < TOTAL_CNT/A
936 / MOV A,POSN_ACC / for RUN_SPEED < SLEWK
937 / SUBB A,ACCEL_CNT / USE motion in constant vel mode.
938 / MOV A,POSN_ACCL1
939 / SUBB A,ACCEL_CNT+1
940 / JNC FND_ACCEL / check sign (posn-accel).
941 / MOV A,RUN_SPEED / if not end of accel, is con-
942 / CJNE A,SLEWK,$15 / stant speed = target running
943 / SJB FND_ACCEL, / is speed? End of accel if it is.
944 / INC R7 / else, increment accel/decel

```


ER	LINE	ADDR	OBJECT	TYPE	ACALL	CHKRD	Comments
	992	03F7	91 RD	.C..		CHKRD	
	993	03F4	40 03	.P..		PST_CYCTR	
	994	03F6	D5 3A 05	.DR..		CYC_CTR,CHKSHALG	
	995	03F9	75 3A 01	.D..		CYC_CTR,EOI	
	996	03FC	80 0A	.R..		STOP_MOTION	
	997	03FE	30 10 2A	.RR..		SHALG_FLG,EXIT_TIMING	
	998	0401	E4				
	999	0402	F5 2E	.D..		POSH_ACC,A	
	1000	0404	F5 2F	.D..		POSH_ACC+1,A	
	1001	0406	B1 29	.C..		EXIT_TIMING	
	1002	0408	C2 11	.R..		CUNT_FLG	
	1003	040A	20 10 17	.RR..		SHALG_FLG,DECR	
	1004	040D	D2 12	.R..		SKIP_FLG	
	1005	040F	D2 08	.R..		RUN_FLG	
	1006	0411	D2 09	.R..		ACCEL_FLG	
	1007	0413	85 41 3D	.DD..		ACCEL,DECELR	
	1008	0416	B1 29	.C..		EXIT_TIMING	
	1009						
	1010						
	1011						
	1012	0418	30 12 09	.RR..		SKIP_FLG,DECR	
	1013	041B	E5 33	.D..		A,VEL_OFFS	
	1014	041D	B5 32 04	.DR..		A,RUN_SPEED,DECR	
	1015	0420	C2 12	.R..		SKIP_FLG	
	1016	0422	80 05	.R..		EXIT_TIMING	
	1017	0424	1F			R7	
	1018	0425	B6 FF 01	.R..		R7,OFFH,EXIT_TIMING	
	1019	0428	1D			R5	
	1020						
	1021						
	1022						
	1023	0429	B6 00 03	.R..		R7,100,CHKFLG	
	1024	042C	B0 00 02	.R..		R5,100,CHKFLG	
	1025	042F	61 60	.C..		END_OF_MOTION	
	1026	0431	00				
	1027	0432	61 1B	.C..		NOCHGDP	
	1028						

;Indicates start of decel phase.
 ;Motion to be stopped if in
 ;continuous run mode?
 ;Reset cycle counter.
 ;Reset POSH if in continuous
 ;run mode and SHALG_FLG set,
 ;ie., TOTAL_C=5.
 ;Yes, motion is to be stopped.
 ;No decel phase if SHALG_FLG
 ;is set.
 ;Indicate decel phase.
 ;Load decel rate.
 ;-----
 ; DECELERATION PHASE
 ;-----
 ; Motion in decel mode if
 ; R7 is > 0 ELSE motion is stopped.
 ; Adjust with offset velocity to
 ; arrive at exact target count
 ; if absolute.
 ; Decrement accel/decel timekeeping
 ; registers.
 ;-----
 ; END OF MOTION?
 ;-----
 ; EXIT_TIMING: R7,100,CHKFLG R7=R5=0 end of cycle.
 ; R5,100,CHKFLG
 ; AJMP END_OF_MOTION
 ; CHKFLG: NOP
 ; AJMP NOCHGDP
 ; INCLUDE(CHAINSHR.UNS)

FR	LINE	ADDR	OBJECT	TYPE	CHKMSG:	CUR	C	PC = 1 Incoming MSG! C = 0 none.
	1078	0460	C1			JMP	PJ.0,CHK_KEY	
	1079	0461	30 00 04	.NR.				
	1080	0464	D3			SETB	C	
	1081	0465	C2 13	.R..			CHMSRC_FUG	!Command source is serial line.
	1082	0467	22			RET		
	1083	0468	91 00	.C..		ACALL	CHKRD	
	1084	046A	50 02	.R..		JNC	EX_CHKMSG	
	1085	046C	D2 13	.R..		SETB	CMSRC_FUG	!Command source is keyboard.
	1086	046E	22			RET		
	1088				*****			
	1089				! DELAY LUNPS 14 MILLISEC INCREMENT			
	1090				*****			
	1091	046F	7E 05	.R..	DELU5MS!	MOV	R6,ASHORT_TC	!Short settling time.
	1092	0471	80 0E			SJMP	DELAY_LUNP	
	1093	0473	7E 14	.R..	DELU20MS!	MOV	R6,11JUG_IC	!Long settling time.
	1094	0475	80 0A			SJMP	DELAY_LUNP	
	1095	0477	7E 3C	.R..	DELU60MS!	MOV	R6,160	!60ms delay.
	1096	0479	80 06			SJMP	DELAY_LUNP	
	1097	047B	7E 78	.R..	DELU120MS!	MOV	R6,1120	!120ms delay.
	1098	047D	80 02			SJMP	DELAY_LUNP	
	1099	047F	7E F0	.R..	DELU240MS!	MOV	R6,11240	!240ms delay.
	1101	0481	12 08 02	.C..	DELAY_LUNP!	LCALL	UPDTE_SERV0	
	1102	0484	DE F8	.R..		RJNZ	R6,DELAY_LUNP	
	1103	0486	22			RET		

ER	LINE	ADDR	OBJECT	TYPE
	1105		***** / UPDATE AUXILIARY PORT X /*****	
	1106		***** /*****	
	1107		***** /*****	
	1108		***** /*****	
	1109		***** /*****	
	1110	0487 55 44	ON_SOLI	.D..
	1111	0489 80 02	ANL A,PORTX_LATCH SJB	.R..
	1112	048A 45 44	ORL A,PORTX_LATCH	.D..
	1113	048B F5 44	MOV PORTX_LATCH,A	.D..
	1114	048C 90 90 00	MOV DPTR,PORTX	
	1115	0492 F0	MOVX ADPTR,A	
	1116	0493 22	RET	
	1118		***** /*****	
	1119		***** /*****	
	1120		***** /*****	
	1121	0494 90 88 03	ON_BIT	
	1122	0497 E0	MOV DPTR,PORTC	
	1123	0498 5C	MOVX A,ADPTR	
	1124	0499 F0	ANL A,R4	
	1125	049A 22	MOVX ADPTR,A	
	1126	049B 90 88 03	RET	
	1127	049C E0	DPTR,PORTC	
	1128	049F 4C	MOVX A,ADPTR	
	1129	04A0 F0	ORL A,R4	
	1130	04A1 22	MOVX ADPTR,A	
	1130		***** /*****	

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CR	LINE	ADDR	OBJECT	TYPE	
	1132		POINT-TO-POINT PROFILE		POINT-TO-POINT motion.
	1133		POINT-TO-POINT PROFILE		Estimated accel distance equals
	1134		POINT-TO-POINT PROFILE		total count / 4.
	1135		Determines accel/decel distances for a point-to-point		
	1136		trapezoidal velocity profile.		
	1137		COMP_PROF		
	1138	04A2 85 10 41	MOV	.RD.	ACCEL, ACCEL
	1139	04A5 C2 0A	CLR	.R..	PROF_FLAG
	1140	04A7 7C 02	MOV		R4, R02
	1141	04A9 85 3C 38	MOV	.RD.	ACCEL_CNT+1, TOTAL_CNT+1
	1142	04AC 85 3B 37	MOV	.RD.	ACCEL_CNT, TOTAL_CNT
	1143	04AF E5 38	MOV	.R..	A, ACCEL_CNT+1
	1144	04B1 C1	CLR		C
	1145	04B7 13	PRC		A
	1146	04B3 F5 38	MOV	.D..	ACCEL_CNT+1, A
	1147	04B5 E5 37	MOV	.R..	A, ACCEL_CNT
	1148	04B7 13	PRC		A
	1149	04B8 F5 17	MOV	.D..	ACCEL_CNT, A
	1150	04BA 0C F3	DJNZ	.R..	R4, DIV_FOUR
	1151	04BC 22	RET		
			EX_PACCEL		
	1151		CHECK FOR KEY DEPRESSION		
	1154		CHECK FOR KEY DEPRESSION		
	1155		CHECK FOR KEY DEPRESSION		
	1156	04B0 90 C0 00	MOV	.R..	OPTR, KEYTRN
	1157	04C0 E0	MOV		A, OPTR
	1158	04C1 A2 E1	MOV		C, ACCN
	1159	04C3 22	RET		

LINE	ADDR	OBJECT	TYPE
1161			
1162			
1163			
1164			
1165			
1166			
1167			
1168			
1169	04C4	90 B8 01	
1170	04C7	E0	
1171	04C8	F5 75	.D..
1172	04CA	20 20 04	.RR.
1173	04CD	02 14	.R..
1174	04CF	80 02	.R..
1175	04D1	C7 14	.D..
1176	04D1	00	
1195			
1196			
1197			
1198	04ED	75 1A 05	.D..
1199	04F0	02 3A	.D..
1200	04F2	51 77 05	.D..
1201	04F5	51 08	.C..
1202	04F7	20 18 05	.RR.
1203	04FA	20 0F 02	.RR.
1204	04FD	E4	
1205	04FF	22	
1206	04FF	05 3A EE	.RR.
1207	0502	02 3B	.D..
1208	0504	22	

ER	LINE	ADDR	ORJECT	TYPE
	1210			*****
	1211			! HEAD HOME SIGNAL
	1212			*****
	1213	0505 91 73		HOME_CHK: CALL DEL2045
	1214	0507 90 R8 01		MOV OPTR,IPORIA
	1215	050A E0		MOVX A,OPTR
	1216	050B 54 04		AND A,#4
	1217	050D 22		RET
	1219			*****
	1220			! CHECK FOR ZERO DUTY CYCLE
	1221			*****
	1222	050E E5 7C		MOV A,X2L
	1223	0510 70 02		JNZ FX_CHKZDC
	1224	0512 65 7H		XRI A,X2H
	1225	0514 22		RET
	1226	0514		FX_CHKZDCI FOR EX_CHKZDC
	1227			OUT_STEP
				!INCLUDE(UPDSERVO.OVS)

!Head (n none signal input.

!Returns 0 in acc if dc = 0.

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```

ER  LINE  ADDR  OBJECT  TYPE
1229          *****
1230          ***** UPDATE SERVO CONTROL ELEMENTS *****
1231          *****
1232          ***** RUNH *****
1233          ***** CLR C *****
1234          ***** RET *****
1235          ***** IFOR dummy call when SRX-S1
1236          ***** is not in used. *****
1237          *****
1238          ***** COMPUTE MOTION TRAJECTORY *****
1239          *****
1240          ***** UPDATE_SERVO *****
1241          ***** ANI, PSN, 11100111H *****
1242          ***** RUN_FUG, CONST_SPEED *****
1243          ***** ACALL, COMP_ARCEL *****
1244          ***** MOV, RUN_SPEED, A *****
1245          ***** CONST_SPEED *****
1246          ***** MOV, AUX_REG, RUN_SPEED *****
1247          ***** MOV, R, R0 *****
1248          ***** MOV, R0, EPSN_ACC *****
1249          ***** ACALL, INTEGRATE *****
1250          *****
1251          ***** UPDATE ABSOLUTE POSITIONS *****
1252          *****
1253          ***** INR, INCRDIR_FUG, INCR_INDEX *****
1254          ***** MOV, A, AUX_REG *****
1255          ***** JZ, INCR_INDEX *****
1256          ***** CPI, A *****
1257          ***** JNC, A *****
1258          ***** MOV, AUX_REG, A *****
1259          ***** MOV, A, 10FFFH *****
1260          ***** INCR_INDEX *****
1261          ***** MOV, TRACK_RASE *****
1262          ***** MOV, R0, INCR_CMT *****
1263          ***** ACALL, INTEGRATE *****
1264          *****
1265          ***** COMPUTE ALGORITHM VARIABLES *****
1266          ***** FOR NEXT SAMPLING INSTANT *****
1267          ***** COMP_K1K2 *****
1268          ***** MOV, PSN, 4 *****
1269          ***** MOV, OPTRA_COEFFI *****
1270          ***** MOV, A, FRR_CMT *****
1271          ***** JNR, ACC, 7, POS_FRR *****
1272          ***** CPI, A *****
1273          ***** JNC, A *****
1274          ***** ACALL, YRTN *****
1275          ***** SJMP, SAV_K1 *****
1276          ***** ACALL, XRTN *****
1277          ***** ACALL, TANS_CPL *****
1278          *****
1279          ***** SELECT REGISTER BANK 2 *****
1280          ***** K1 = (COEFFI * signed last error cnt) *****
1281          ***** GET last sampling instant's err cnt. *****
1282          ***** GET absolute value if negative. *****
1283          *****
1284          ***** Result is +, ie., -(K1). *****
1285          ***** Result is -, ie., -(+K1). *****

```

ER	LINE	ADDR	OBJECT	TYPE	SAV_K11	MOV	R2,A R3,B	ISAVE RESULT.
	1277	0R3F	FA	.D..		MOV		
	1278	0R40	AR F0			MOV		
	1279							
	1280	0R42	2D 5F 0C	.RR.	CMPTK21	JD	K2H,7,NEG_DC	K2 = -ICNEFF2/256 x signed last output
	1281	0R45	85 2B 83	.DD.	POS_DC1	MOV	DPH,K2H	Get abs value of last sampling
	1282	0R48	85 2C 82	.DD.		MOV	DPH,K2L	Instant's algorithm output is (-).
	1283	0R4A	31 2D	.C..		MOV	COMP_K2	
	1284	0R4D	31 71	.C..		ACALL	TXNS_CPL	Multiply with CNEFF2 constant.
	1285	0R4F	80 0E	.R..		SJMP	PARTIAL	Result is (-), ie., -K2.
	1286	0R51	E5 2C F0	.D..	NEG_DC1	MOV	A,K2L	
	1287	0R53	85 2B F0	.DD.		MOV	A,K2H	
	1288	0R56	31 71	.C..		ACALL	TXNS_CPL	
	1289	0R5A	F5 R2	.D..		MOV	DPH,A	
	1290	0R5A	85 F0 81	.DD.		MOV	DPH,H	
	1291	0R5D	31 2D	.C..		ACALL	COMP_K7	Result is (+), ie., -(-K2).
	1292	0R5F	2A		PARTIAL1	ADD	A,R2	Compute algorithm partial result.
	1293	0R60	FA			MOV	R2,A	
	1294	0R61	E5 F0	.D..		MOV	A,A	
	1295	0R63	3R			ADDC	A,P3	
	1296	0R64	FA			MOV	R3,A	

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LINE	ADDR	OBJECT	TYPE
1298			
1299			
1300			
1301	0865	90 B8 03	
1302	086A	E0	R..
1303	0869	B2 E5	
1304	086B	F0	
1305	086C	B7 R5	P..
1306	086E	15 R2	D..
1307	0870	75 F0 6A	D..
1308	0873	D2 38	R..
1309	0875	30 38 19	RR.
1310	087R	30 0F FA	RR.
1311	087R	C2 AF	R..
1312	087D	15 R2	D..
1313	087F	E0	
1314	0880	A1	
1315	0881	D2 AF	R..
1316	0881	54 04	
1317	0885	70 EE	P..
1318	0887	31 1D	C..
1319	0889	FE	
1320	088A	C2 0F	R..
1321	088C	75 3A 01	D..
1322	088F	80 E4	R..
1324	0891	A3	
1325	0892	E0	
1326	0893	B2 E5	R..
1327	0895	F0	
1328	089A	B2 R5	R..
1329	0898	7F 04	
1330	089A	C2 04	
1331	089C	31 27	R..
1332	089E	20 A3 05	C..
1333	08A1	D2 40	RR.
1334	08A1	07 00 8F	R..
1335	08A6	20 3D 01	C..
1336	08A9	22	R..

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ER LINE ADDR OBJECT TYPE

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1338 .....
1339 ..... CHECK "ATL FEED WHEN IN PRINT CYCLE" .....
1340 .....
1341 .....
1342 ..... Detects trips at the transport path to give the ff. info
1343 .....
1344 ..... 1. Line when next rail is detected at TRIP1 for its speed
1345 ..... calculation in next cycle.
1346 .....
1347 .....
1348 .....
1349 ..... Returns to main routine with:
1350 ..... 1. TRIP sensors status updated.
1351 ..... 2. TR1-FLG set if TRIP1 sensor is tripped (0 to 1 transition).
1352 ..... 3. TR2-FLG set if TRIP2 sensor is tripped.
1353 ..... 4. No change in flags' state if no trip is detected.
1354 .....
1355 .....
1356 .....
1357 .....
1358 .....
1359 .....
1360 .....
1361 .....
1362 .....
1363 .....
1364 .....
1365 .....
1366 .....
1367 .....
1368 .....
1369 .....
1370 .....
1371 .....
1372 .....
1373 .....
1374 .....
1375 .....
1376 .....

```

```

1381 .....
1382 .....
1383 .....
1384 .....
1385 .....

```

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LINE	ADDR	OBJECT	TYPE	ACALL- MOV	COMP_ARSI	INTEGRATE DPTR,IRASE,-IREV	integrate computed velocity. DUPR = base drv 1 rev count.
1386	08E4	31 10	.C..	MOV		A,ARO	
1387	08E6	90 0A 00		MOV		ACC,7,ABS1	
1388	08E9	E6		JNR		RO	
1389	08ED	18	.RR.	DEC		A,ARO	Convert index to a positive value
1390	08EE	C6		XCH		A,DPL	relative to the nose position count.
1391	08EF	25 A2	.D..	ADD		A,ARO	IF SCH(index) is negative
1392	08F1	C6		XCH		A,DPH	IFEN index=index + 1 rev count
1393	08F2	35 A3	.D..	INC		RO	IFUS
1394	08F4	08		MOV		ARO,A	
1395	08F5	F6		DEC		RO	IFendif.
1396	08F6	1A		CLR		C	Convert positive index value to an
1397	08F7	C3		MOV		A,DPL	absolute position count starting from
1398	08F8	E5 A2	.D..	SURH		A,ARO	home (zero) count.
1399	08FA	96		MOV		R4,A	ITEMP = 1 rev count - index
1400	08FB	FC		MOV		A,DPH	
1401	08FC	E5 A3	.D..	INC		RO	
1402	08FE	08		SURH		A,ARO	
1403	08FF	96		JNR		ACC,7,FX-ARS	IF SCH(temp) is negative
1404	0900	30 F7 0C	.RR.	XCH		A,R4	IT4F4 index = (-temp)
1405	0901	CC		CPL		A	IFUS
1406	0903	C6		ADD		A,RO1	
1407	0904	F4		DEC		RO	
1408	0905	24 01		MOV		ARO,A	
1409	0907	18		XCH		A,R4	
1410	0908	F6		CPL		A	
1411	0909	CC		ADD		A,ROO	
1412	090A	F4		INC		RO	
1413	090B	34 00		MOV		ARO,A	
1414	090D	08		RET			
1415	090E	F6					
1416	090F	22					

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ER	LINE	ADDR	OBJECT	TYPE
	1418		***** INTEGRATE: VELOCITY COUNT *****	
	1419		*****	
	1420		*****	
	1421	0910	EA 36	
	1422	0911	F5 36	.D..
	1423	0913	F6	
	1424	0914	08	
	1425	0915	E5 F0	.D..
	1426	0917	36	
	1427	0918	F6	
	1428	0919	22	
	1430		***** READ EXTERNAL, COUNTER RUFFER *****	
	1431		*****	
	1432		*****	
	1433	091A	90 B8 02	
	1434	091D	E0	
	1435	091E	F5 36	.D..
	1436	0920	E0	
	1437	0921	B5 36 01	.DR.
	1438	0924	22	
	1439	0925	E0	
	1440	0926	22	
	1442		***** RE-READ: EX-READXCTR: RET *****	
	1443		*****	
	1444		*****	
	1445	0927	0A 00 01	.R.
	1446	0928	BA 00 01	
	1447	092B	08	
	1448	092C	22	

IR0 holds index address 10byte.
 I AUX_RFG =signed velocity count
 I in counts/sample.
 I R2 counts 1ms-Interval.
 I R3 counts 256ms-Interval.
 I must be in R0.

LINE	ADDR	OBJECT	TYPE
1450			
1451			
1452			
1453			
1454			
1455			
1456	0920	C1	
1457	092E	74 F8	
1458	0930	95 R2	.D..
1459	0932	74 D3	
1460	0934	95 R3	.D..
1461	0936	50 06	.R..
1462	0938	75 R3 03	.D..
1463	093B	75 R2 ER	.D..
1464	093E	74 50	
1465	0940	80 06	.R..
1467			
1468			
1469			
1470			
1471			
1472			
1473	0942	8F R2	.D..
1474	0944	80 R3	.D..
1475	0946	E5 3D	.D..
1477			
1478			
1479			
1480			
1481			
1482			
1483	0948	31 57	.C..
1484	094A	A2 F7	.R..
1485	094C	E5 F0	.D..
1486	094E	34 00	
1487	0950	CC	
1488	0951	34 00	
1489	0953	F5 F0	
1490	0955	EC	
1491	0956	22	

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ER	LINE	ADDR	OBJECT	TYPE
	1493			
	1494			
	1495			
	1496			
	1497			
	1498			
	1499			
	1500			
	1501	0957	FC	
	1502	0958	85 82 F0	.DD.
	1503	0959	A4	
	1504	095C	C0 F0	.D..
	1505	095E	C0 F0	.D..
	1506	0960	EC	
	1507	0961	85 83 F0	.DD.
	1508	0964	A4	
	1509	0965	D0 83	.D..
	1510	0967	25 83	.D..
	1511	0969	C5 F0	.D..
	1512	096A	34 00	
	1513	096D	FC	
	1514	096E	D0 E0	.D..
	1515	0970	22	
	1517			
	1518			
	1519			
	1520			
	1521	0971	F4	
	1522	0972	24 01	.D..
	1523	0974	C5 F0	
	1524	0976	F4	
	1525	0977	34 00	
	1526	0979	C5 F0	.D..
	1527	097A	22	
	1528			

```

*****
/ DOUBLE-PRECISION INTER
/ MULTIPLICATION
*****
Multiplier (positive 8 bits) = ACC
Multiplicand (positive 16 bits) = DPTR
Product result in R4 (msb), B, ACC (lsb).
*****
XRTN: MOV R4,A ;Compute product low byte.
      MOV R,DPL; ;Load multiplicand low byte
      MUL AB ;Multiplier saved to R4.
      PUSH ACC ;Save product low byte.
      PUSHL R ;Save partial product high byte.
      MOV A,R4 ;Compute product high byte.
      MOV R,DPH ;Load multiplicand high byte.
      MUL AB
      POP DPH
      ADH A,DPH ;Set intermediate prod high byte.
      XCH A,R ;Sub is final prod high byte.
      ADNC A,100 ;Prod 2nd byte = R.
      MOV R4,A ;Prod 3rd byte (15H) = R1.
      POP ACC ;Prod 1st byte (05H) = ACC
      RET ;Return to caller.
*****
/ DOUBLE-PRECISION
/ T-OS COMPLETENT
*****
TRANS-CPL: CPL A
      ADD A,101 ;ACC = 10 byte.
      XCH A,R ;R = 01 byte.
      CPL A
      ADNC A,100
      XCH A,R
      RET
*****
$INCLUDE(NEXTCOMP.H.DMS)

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1530 *****
1531 / COMMUNICATION ROUTINES
1532 / TIME DELAY DECLARATIONS
1533 *****
1534 / Transmitter echoplex protocol time
1535 / constants in microseconds.
1536 /-----
1537 BITTX EQU 104 ;1st-to-1st xmit/echo-sample time.
1538 SBTX EQU 170 ;CTS detect to start bit time.
1539 NBTX EQU 140 ;No-Error-Pulse width.
1540 BYTETX EQU 1135 ;Byte-to-byte xmit time.
1541 DELAY1 EQU (BITTX-12) ;Delay before xmitting 1st data bit.
1542 DELAY2 EQU (BITTX-19) ;Delay before xmitting next data bit.
1543 DELAY3 EQU (BITTX-12) ;Delay before sampling EN4/EN3.
1544 DELAY4 EQU (BYTETX-(BITTX*10)-4) ;Delay before next byte xmit.
1545 /-----
1546 / Receiver echoplex protocol time constants.
1547 /-----
1548 CTSRX EQU 100 ;ATS detect to CTS xmit time.
1549 SBRX EQU 42 ;SA detect to 1st echo time.
1550 BITRX EQU 120 ;SA detect to 1st bit sample time.
1551 ECHIRX EQU 140 ;SA detect to 1st data bit echo time.
1552 BITRX EQU 106 ;1st-to-1st sample/xmit-echo time.
1553 WPERX EQU 1188 ;SA detect to 1st sample time.
1554 RYTERX EQU 1552 ;Time until next receiver activity.
1555 DELAY5 EQU (CTSRX-20) ;Delay before xmitting CTS.
1556 DELAY6 EQU (BITRX-SBRX-3) ;Delay before sampling 1st data bit.
1557 DELAY7 EQU (ECHIRX-BITRX-7) ;Delay before echoing recvd bit.
1558 DELAY8 EQU (BITRX-DELAY7-R) ;Delay before sampling next data bit.
1559 DELAY9 EQU (RYTERX-(BITRX+BITRX*8)-25) ;Delay before next byte recv.
1560 DELAY10 EQU (WPERX-BYTERX+DELAY9) ;Delay before sampling NPI.
1561 DELAY11 EQU (HYPERX-WPERX) ;Delay before recv pin exit.
1562 /-----
1563 / MACRO TO GENERATE CODE FOR
1564 / TIME DELAYS
1565 /-----
1566 TIME
1567 MACKD DWD
1568 IF (DWD MOD 2) EQ 0
1569 MOV R2,1((DWD-2)/2)
1570 DJNZ R2,S
1571 NOP
1572 ELSE
1573 MOV R2,(DWD/2)
1574 DJNZ R2,S
1575 ENDF
1576 ENDH

```

ER	LINE	ADDR	OBJECT	TYPE	
	1574	097C	E4		*****
	1579	097D	51 D1		TRANSMIT MESSAGE TO SOURCE
	1580	097F	30 16 0C		*****
	1581	0980	12 E0 0F		RECEIVER-FLG = 0 Xmit thru serial line/ = 1 thru display.
	1582	0985	AA 28		*****
	1583	0987	AR 27		XMIT-STAT: CUR A
	1584	098C	41 12		ACALL: XCDPRFP
	1585	098E	79 26		JNR PCVFRFLG,STAT_SERIAL,
	1586	0990	7D 03		LCALL: CLRDSP
	1587	0992	75 26 80		MOV R2,MSG7-STAT
	1588	0995	21 AF		MOV R3,MSG1-STAT
	1589	0997	74 02		LCALL: DSP2RY
	1590	0999	51 D1		MOV RND-OF-XMIT
	1591	099B	30 16 0A		MOV R1,STAT-HEADER
	1592	099E	12 E0 0F		MOV R5,R03
	1593	09A1	AA 46		MOV STAT-HEADER,B00H
	1594	09A6	41 12		MOV XMIT-RTN
	1595	09A8	79 2D		MOV A,R07
	1596	09AC	75 2D 83		*****
	1597				TRANSMIT COMMAND-execution-complete.
	1598				*****
	1599				TRANSMISSION ECHO/PLEX ROUTINE
	1600				(12 Mhz CLOCK)
	1601				*****
	1602				CAUTION: Instruction code, sequence, and loops
	1603				are critical to time delay computations.
	1604				R0 = pointer to time constant watchdog.
	1605				R1 = start addr of xmitting buffer.
	1606				R2 = timer delay constants register.
	1607				R3 = save area for byte to be xmitted.
	1608				R4 = communication failure counter.
	1609				R5 = no. of bytes to be xmitted.
	1610				R6 = stack pointer save area for watchdog timeout.
	1611				R7 = save area for no. of data bits per byte.
	1612				*****
	1613				XMIT-RTN: SETB R3,1
	1614				JNR R3,0,5
	1615				TIME
	1616				START-XMIT: MOV R7,R0B
	1617				*****
	1618				*****
	1619				*****
	1620				*****
	1621				*****
	1622				*****
	1623				*****
	1624				*****
	1625				*****
	1626				*****
	1627				*****
	1628				*****
	1629				*****
	1630				*****
	1631				*****

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ER	LINE	ADDR	OBJECT	TYPE
	1632	09B0	C3	
	1633	09B0	92 15	.R..
	1634	09C0	E7	
	1635	09C1	F8	
	1636	09C2	09	
	1637	09C3		
	1638	09C4	EA	
	1639	09C5	11	
	1640	09C6	FA	
	1641	09C7	92 B1	.R..
	1642	09C8	51 FC	.C..
	1643	09C9	30 06 3A	.RR.
	1644	09D0	92 15	.R..
	1645	09D1		
	1646	09D2	0F FE	.R..
	1647	09D3	00	
	1648	09D4	00 18	.R..
	1649	09D5	C2 H1	.R..
	1650	09D6	51 FC	.C..
	1651	09D7	30 06 26	.RR.
	1652	09D8		
	1653	09D9	20 00 1F	.RR.
	1654	09DA	D2 B1	.R..
	1655	09DB		
	1656	09DC	80 1D	.R..
	1657	09DD	D2 H1	.R..
	1658	09DE	51 FC	.C..
	1659	09DF	30 06 0F	.RR.
	1660	09E0		
	1661	09E1	30 00 06	.RR.
	1662	09E2		
	1663	09E3	21 A9	.C..
	1664	09E4	C2 06	.R..
	1665	09E5	C2 H1	.R..
	1666	09E6	DA FE	.R..
	1667	09E7	DA FE	.R..
	1668	09E8	41 AC	.C..

C
 SAVEI_RIT,C
 A,RI
 RJ,A
 RI
 DELAY1
 A,RJ
 A
 RJ,A
 RJ,A
 P3.1,C
 CHK_ECHO
 CORR_FLG,XMITERR
 SAVEI_RIT,C
 DELAY2
 P7,BITOUT
 R5,XMIT_ERR
 P3.1
 CHK_ECHO
 CORR_FLG,XMITERR
 DELAY3
 P3.0,XMITERR
 P3.1
 NEXTX
 END_OF_XMIT
 P3.1
 CHK_ECHO
 CORR_FLG,XMITERR
 DELAY3
 P3.0,XMITERR
 DELAY4
 START_XMIT
 CORR_FLG
 P3.1
 RJ,S
 RJ,Z
 CHK_ERR
 END_OF_XMIT:

IFIRST 8-1 bit is start bit, i.e., 0.
 1st byte to be xmitted.
 1save to work area.
 1points to next byte.
 1delay before xmitting first data bit.
 1place bit into C.
 1transmit nth bit (C).
 1check echo of 1-1 bit.
 1echo error if set.
 1save 8 bit, i.e., 8-1 bit = 0.
 1delay before xmitting next data bit.
 1all data bits xmitted?
 1NOP to balance bit-to-bit delay.
 1end-of-word if zero, else, end-of-byte.
 1xmit flag.
 1check echo of last data bit.
 1delay before reading RXN/RXN echo.
 1check RXN echo.
 1everything is OK, xmit next.
 1delay for HEP valid.
 1end of xmission.
 1xmit flag.
 1check echo of last data bit.
 1check RXN echo.
 1delay before start of next byte xmit.
 1start xmitting next byte.
 1indicate communication error.
 1drop xmit line.
 1force an EOV error.
 1check for xmit error.

LINE	ADDR	OBJECT	TYPE
1781	0A67	D F ED	.R..
1782	0A69	A2 R0	.B..
1783	0A6A		
1790	0A70	92 R1	.B..
1791	0A72	A7 OB	.D..
1792	0A74	09	
1793	0A75	50 O7	.R..
1794	0A77		
1801	0A7C	41 A6	.C..
1802	0A7E		
1808	0A82	20 R0 O2	.RR.
1809	0A85	C2 O6	.R..
1810	0A87		
1817	0ABC		
1819			
1820			
1821			
1822	0A8C	I0 06 OD	.RR.
1823	0ABF	D2 J8	.D..
1824	0A91	BC FF 05	.R..
1825	0A94	O2 46	.R..
1826	0A96	O2 02 O3	.C..
1827	0A99	OC	
1828	0A9A	80 O2	.R..
1829	0A9C	7C O0	
1830	0A9E	C2 8C	.R..
1831	0AA0	C2 R1	.R..
1832	0AA2	C2 D3	.R..
1833	0AA4	C3	
1834	0AA5	E5 BA	.D..
1835	0AA7	25 A2	.D..
1836	0AA9	FC	
1837	0AAA	E5 AC	.D..
1838	0AAC	35 A3	.D..
1839	0AAF	CC	
1840	0AAF	C3	
1841	0AB0	94 E8	
1842	0AB2	CC	
1843	0AB3	94 O3	
1844	0AB5	40 OA	.R..
1845	0AB7	J1 27	.C..
1846	0AB9	B0 FJ	.R..
1847	0ABA	CC	
1848	0ABC	BC FO	.D..
1849	0ABE	J1 71	.C..
1850	0AC0	C3	
1851	0AC1	94 F4	

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Claims:

1. A postage meter (10) including a rotary drum (38) having a periphery adapted for feeding a sheet (16) in a path of travel (18), characterised by:

a) first means (56,58) for sensing a time interval during which a sheet (16) is linearly displaced a predetermined distance in the path of travel (18);

b) a d.c. motor (120) coupled to the drum (38) for rotation thereof;

c) second means (86,126) for sensing angular displacement of the drum (38); and

d) computer means (500) coupled to the first (56,58) and second (86,126) sensing means and to the d.c. motor (120), the computer means (500) comprising:

i) means responsive to the first sensing means (56,58) for providing respective amounts representative of desired angular displacements of the drum (38) during successive sampling time periods,

ii) means responsive to the second sensing means (86,126) for providing respective amounts representative of actual angular displacements of the drum (38) during successive sampling time periods, and

iii) means for compensating for the difference between desired and actual angular displacements and generating a d.c. motor control signal for controlling rotation of the motor (120) to cause the linear displacement of the periphery of the drum (38) to substantially match the linear displacement of the sheet (16) during respective sampling time periods.

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2. A meter according to claim 1, wherein the first sensing means comprises first (56) and second (58) sensing devices spaced apart from each other a predetermined distance (d_1) for sensing successive arrivals of a sheet (16) at two spaced apart locations in the path of travel (18).

3. A meter according to claim 1 or 2 wherein the motor (120) has an output shaft (122), and the second sensing means comprises quadrature encoder means (126) coupled to the output shaft (122).

4. A meter according to any one of claims 1 to 3 wherein the computer means (500) includes means (504) for comparing amounts representative of the desired and actual angular displacements and generating an error signal representative of the difference therebetween, the compensation means responsive to said error signal for generating the motor control signal, and the motor control signal compensating for the difference between said desired and actual angular displacements.

5. A meter according to any one of claims 1 to 4 including power amplifier means (301) for coupling the computer means (500) to the d.c. motor (120).

6. A meter according to any one of claims 1 to 5 wherein the drum (38) has a cycle of rotation, and the motor control signal accelerating the periphery of the drum (38) to the linear velocity of the sheet (16) substantially coincident with the periphery of the drum (38) engaging the leading edge of the sheet.

7. A meter according to claim 2, wherein the first sensing means comprises a mailing machine (12) including said first and second sensing devices.

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8. A meter according to claim 3 including counting means (270) for coupling the quadrature encoder means to the computer means.

9. A meter according to Claim 4, wherein the motor control signal comprises a pulse width modulated control signal.

10. A meter according to Claim 4, wherein the motor control signal comprises a function of a regressive mathematical expression.

11. A meter according to Claim 4, wherein the motor control signal comprises a function of the error signal and a prior error signal.

12. A meter according to Claim 4, wherein the motor control signal comprises a function of the error signal and a prior motor control signal.

13. A meter according to claim 6 wherein the motor control signal is such as to decelerate the drum (38) from said velocity thereof to rest subsequent to disengagement of the drum (38) and sheet (16).

14. A meter according to claim 8 wherein the counting means (270) comprises means for providing an output signal for the computer means (500) which is representative of the angular displacement and direction of rotation of the motor drive shaft (122).

15. A meter according to Claim 12, wherein the prior motor control signal comprises a function of a prior error signal.

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16. For use in a postage meter including a rotary drum (38), wherein the drum (38) includes a periphery adapted for feeding a sheet (16) in a path of travel (18), a process for controlling rotation of the drum (38) as a function of the velocity of the sheet (16), the process characterised by:

a) sensing a time interval during which a sheet (16) is linearly displaced a predetermined distance in the path of travel (18) and in response thereto providing amounts representative of respective desired angular displacements of the drum (38) during successive sampling time periods;

b) providing a d.c. motor (120) for rotating the drum (38);

c) sensing angular displacement of the drum (38) and in response thereto providing amounts representative of respective actual angular displacements of the drum (38) during successive sampling time periods; and

d) digitally compensating for the difference between desired and actual angular displacements and generating a motor control signal for controlling rotation of the drum (38) to cause the linear displacement of the periphery of the drum to substantially match the linear displacement of the sheet (16) during respective sampling time periods.

17. A process according to Claim 16, wherein step (a) includes the step of sensing successive arrivals of a sheet (16) at two spaced apart locations in the path of travel (18).

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18. A process according to Claim 16, wherein step (c) includes the step of sensing the direction of angular displacement of the d.c. motor (120).

19. A process according to Claim 16, wherein step (d) includes the steps of:

1. comparing amounts representative of respective desired and actual angular displacements,

2. generating an error signal representative of the difference between respective desired and actual angular displacements and in response thereto generating a motor control signal which compensates for the difference between said desired and actual angular displacements.

20. A process according to Claim 16, wherein step (c) includes the step of accelerating the periphery of the drum (38) to the velocity of the sheet (16) substantially coincident with engagement of the drum and sheet.

21. A process according to Claim 16, wherein step (d) includes the step of calculating the motor control signal from a function of a regressive mathematical expression.

22. A process according to Claim 16, wherein step (a) includes the step of generating respective counts representative of desired angular displacements of the drum (38).

23. A process according to Claim 16, wherein step (c) includes the step of generating respective counts representative of actual angular displacements of the drum (38).

24. A process according to Claim 16, wherein step (d) includes the steps of:

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1. generating a pulse width modulated motor control signal,
2. amplifying said pulse width modulated control signal, and
3. applying the amplified pulse width modulated control signal to said d.c. motor (120).

25. A process according to Claim 20, wherein step (c) includes the step of decelerating the periphery of the drum (38) to rest subsequent to disengagement of the drum (38) and sheet (16).

26. Apparatus including rotary means (38) having a periphery, the periphery including indicia printing means (44), and the periphery being adapted for feeding a sheet (16) in a path of travel (18), characterised by:

- a) first means (56,58) for sensing a time interval during which a sheet (16) having a leading edge is linearly displaced a predetermined distance in the path of travel (18);
- b) a d.c. motor (120) coupled to the rotary means (38) for rotation thereof;
- c) second means (86,126) for sensing angular displacement of the rotary means (38); and
- d) computer means (500) coupled to the first (56,58) and second (86,126) sensing means and to the d.c. motor (120), the computer means (500) comprising:
 - i) means responsive to the first sensing means (56,58) for providing respective amounts representative of desired angular displacements of the rotary means (38) during successive sampling time periods,

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ii) means responsive to the second sensing means (86,126) for providing respective amounts representative of actual angular displacements of the rotary means (38) during successive sampling time periods, and

5 iii) means for compensating for the difference between desired and actual angular displacements and generating a d.c. motor control signal for controlling rotation of the motor (120) to cause the indicia printing means (44) to initially engage the sheet (16) in the path of travel (18) a
10 predetermined marginal distance from the leading edge of the sheet (16).

27. Apparatus according to claim 26 wherein the first sensing means comprises first (56) and second (58) sensing
15 devices spaced apart from each other a predetermined distance (d₁) for sensing successive arrivals of a sheet (16) at two spaced apart locations in the path of travel (18).

28. Apparatus according to claim 26 or 27 wherein the motor (120) has an output shaft (122), and the second sensing means comprises quadrature encoder means (126) coupled to the
20 output shaft (122).

29. Apparatus according to any one of claims 26 to 28 wherein the computer means (500) includes means for comparing amounts representative of the desired and actual angular
25 displacements and generating an error signal representative of the difference therebetween, the compensation means responsive to said error signal for generating the motor control signal, and the motor control signal compensating for the difference between said desired and actual angular displacements.

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30. Apparatus according to any one of claims 26 to 29 including power amplifier means (301) for coupling the computer means (500) to the d.c. motor (120).

31. Apparatus according to any one of claims 26 to 30 wherein the
5 apparatus comprises a postage meter (10), the rotary means includes a postage meter drum (38), the drum has a cycle of rotation, and the motor control signal is arranged to accelerate the periphery of the drum (38) to the linear velocity of the sheet (16) substantially coincident with the periphery of the drum (38)
10 engaging the leading edge of the sheet (16).

32. Apparatus according to claim 27 wherein the apparatus comprises a postage meter (10), the rotary means includes a postage meter drum (38), and the first sensing means comprises a mailing machine (12) including said first and second
15 sensing devices (56,58).

33. Apparatus according to claim 28 including counting means (270) for coupling the quadrature encoder means (126) to the computer means (500).

34. Apparatus according to claim 29 wherein the
20 motor control signal comprises a pulse width modulated control signal.

35. Apparatus according to claim 29 wherein the motor control signal comprises a function of a regressive mathematical expression.

25 36. Apparatus according to claim 29 wherein the motor control signal comprises a function of the error signal and a prior error signal.

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37. Apparatus according to claim 29 wherein the motor control signal comprises a function of the error signal and a prior motor control signal.

38. Apparatus according to claim 31 including the motor control signal decelerating the drum (38) from said velocity thereof to rest subsequent to disengagement of the drum (38) and sheet (16).

39. Apparatus according to claim 33 wherein the counting means (270) comprises means for providing an output signal for the computer means (500) which is representative of the angular displacement and direction of rotation of the motor drive shaft (122).

40. Apparatus according to claim 37 wherein the prior motor control signal comprises a function of a prior error signal.

41. For use with apparatus including rotary means (38), wherein the rotary means includes a periphery having indicia printing means (44) and is adapted for feeding a sheet (16) having a leading edge in a path of travel (18), a process for controlling rotation of the rotary means (38) for controlling engagement of the indicia printing means (44) with the sheet, the process characterised by:

a) sensing a time interval during which a sheet (16) is linearly displaced a predetermined distance in the path of travel (18) and in response thereto providing amounts representative of respective desired angular displacements of the rotary means (38) during successive sampling time periods;

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b) providing a d.c. motor (120) for rotating the rotary means (38);

c) sensing angular displacement of the rotary means (38) and in response thereto providing amounts representative of respective actual angular displacements of the rotary means (38) during successive sampling time periods; and

d) digitally compensating for the difference between desired and actual angular displacements and generating a motor control signal for controlling rotation of the rotary means (38) to cause the indicia printing means (44) to initially engage the sheet (16) in the path of travel (18) a predetermined distance from the leading edge of the sheet (16).

42. A process according to claim 41 wherein step (a) includes the step of sensing successive arrivals of a sheet (16) at two spaced apart locations in the path of travel (18).

43. A process according to claim 41 or 42 wherein step (c) includes the step of sensing the direction of angular displacement of the d.c. motor (120).

44. A process according to any one of claims 41 to 43 wherein step (d) includes the steps of:

1. comparing amounts representative of respective desired and actual angular displacements, and

2. generating an error signal representative of the difference between respective desired and actual angular displacements and in response thereto generating

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a motor control signal which compensates for the difference between said desired and actual angular displacements.

45. A process according to any one of claims 41 to 44 wherein step (c)
5 includes the step of accelerating the periphery of the rotary means (38) to the velocity of the sheet (16) substantially coincident with engagement of the periphery and sheet (16).

46. A process according to any one of claims 41 to 45 wherein step (d)
10 includes the step of calculating the motor control signal from a function of a regressive mathematical expression.

47. A process according to any one of claims 41 to 46 wherein step (a)
includes the step of generating respective counts representative of desired angular displacements of the rotary means.

15 48. A process according to any one of claims 41 to 47 wherein step (c) includes the step of generating respective counts representative of actual angular displacements of the rotary means (38).

20 49. A process according to any one of claims 41 to 48 wherein step (d) includes the steps of:

1. generating a pulse width modulated motor control signal,

2. amplifying said pulse width modulated control signal, and

25 3. applying the amplified pulse width modulated control signal to said d.c. motor (120).

50. A process according to claim 45 wherein step (c) includes the step of decelerating the periphery of the rotary means (38) to rest subsequent to disengagement of the periphery
30 and sheet (16).

FIG. 1

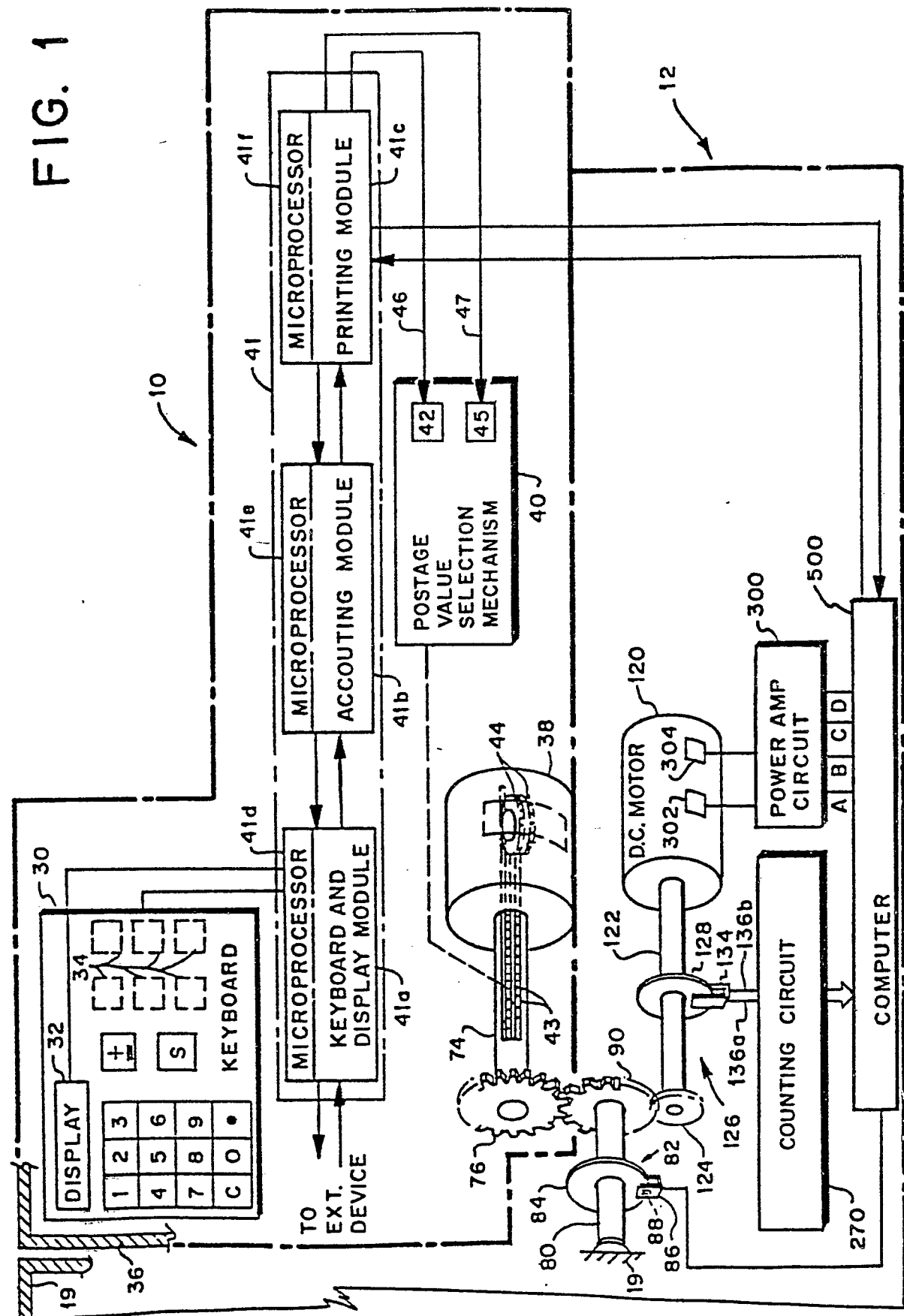
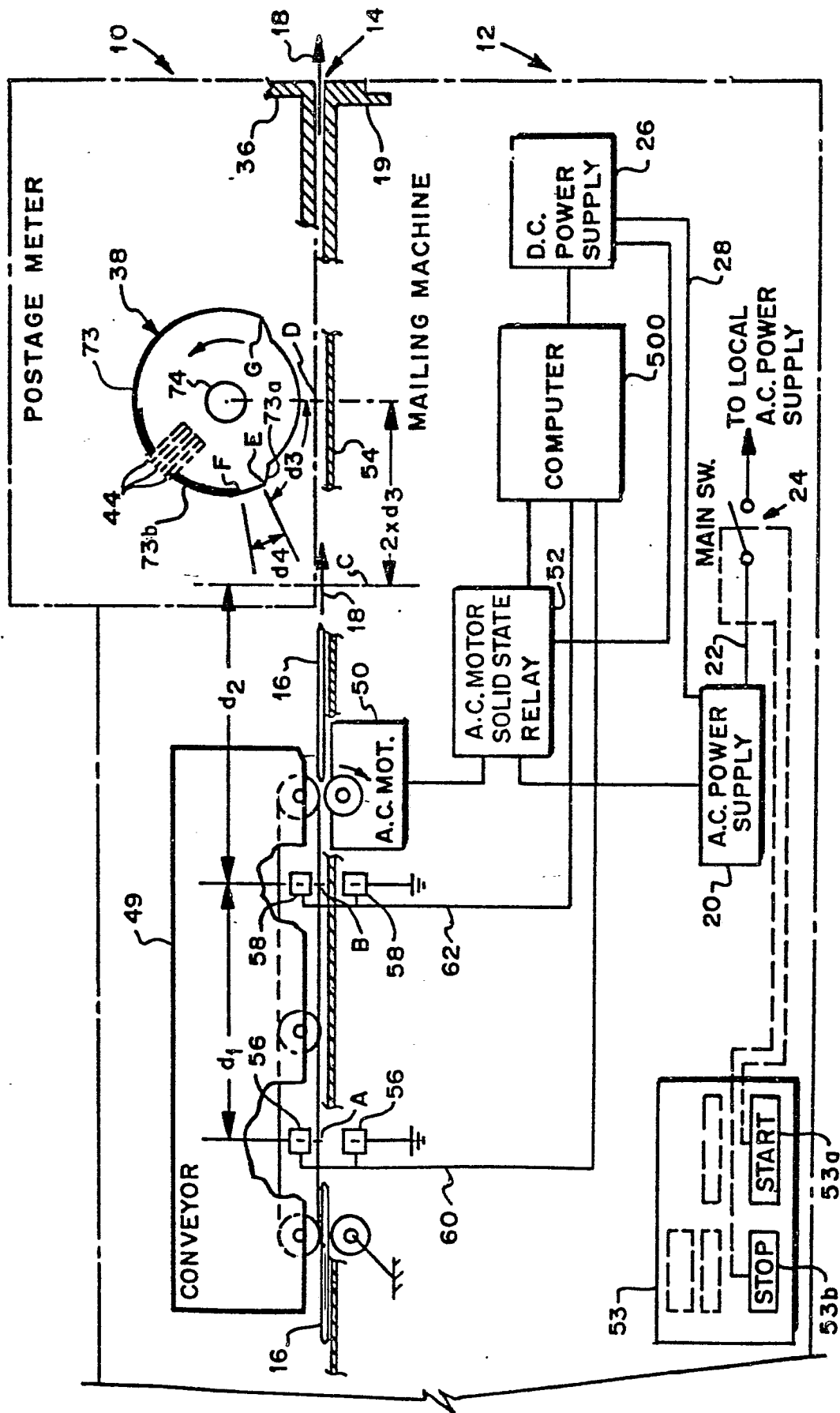
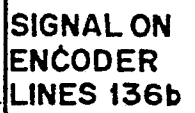


FIG. 2



CW MOTOR SHAFT ROTATION



Letter



FIG. 7

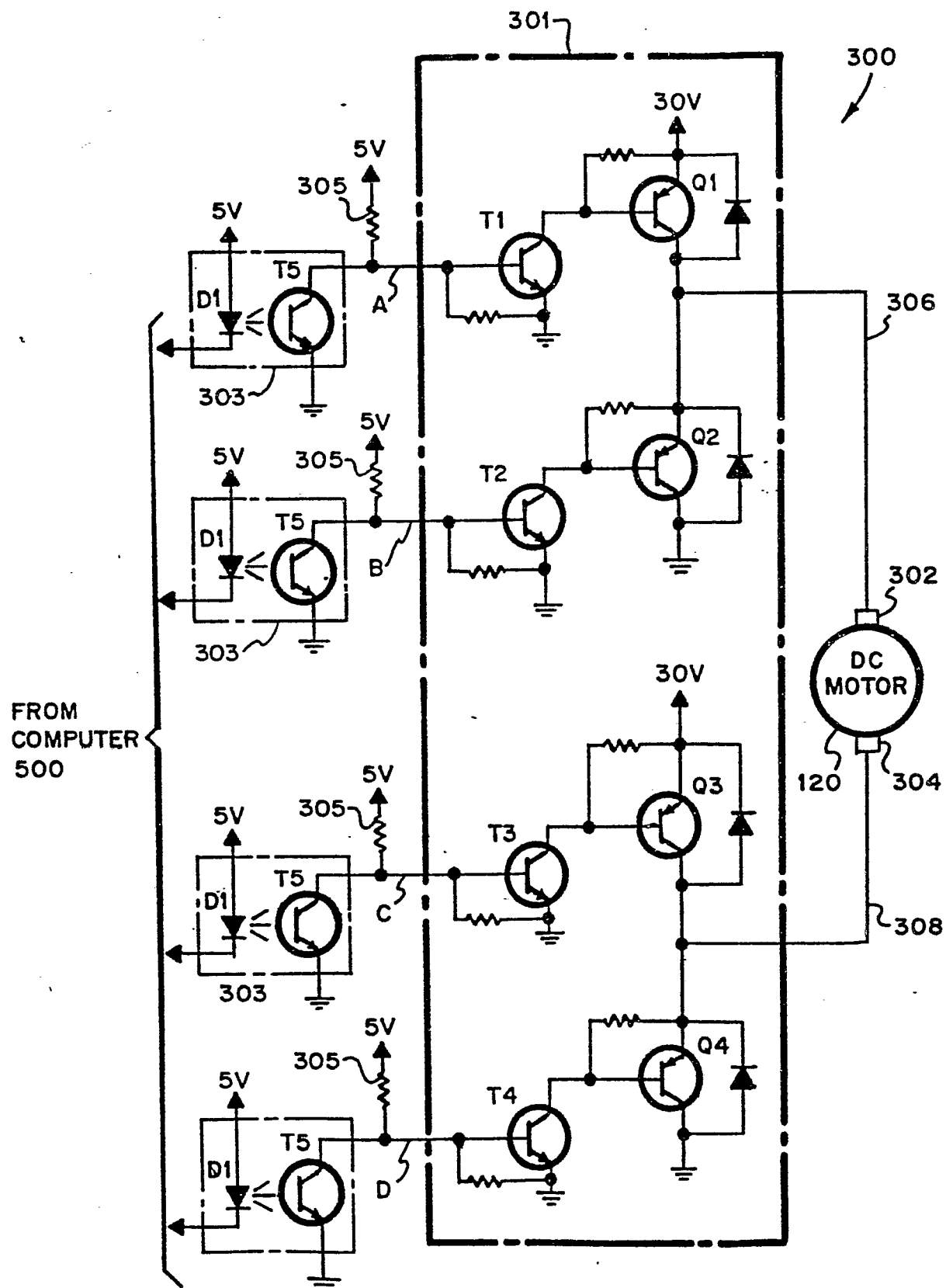


FIG. 8

MOTOR ROTATION	Q1	Q2	Q3	Q4	T1	T2	T3	T4	A	B	C	D	302	304
CW	ON	OFF	OFF	ON	ON	OFF	OFF	ON	HIGH	LOW	LOW	HIGH	+	-
CCW	OFF	ON	ON	OFF	OFF	ON	ON	OFF	LOW	HIGH	HIGH	LOW	-	+

FIG. 9

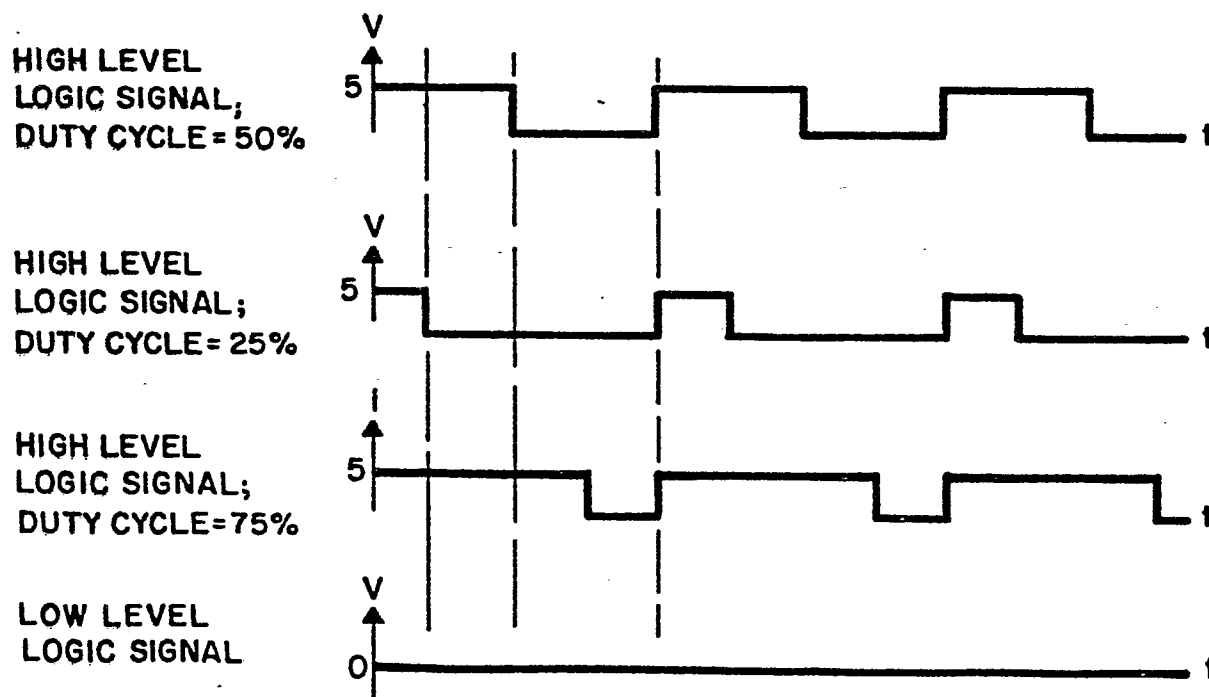


FIG. 10

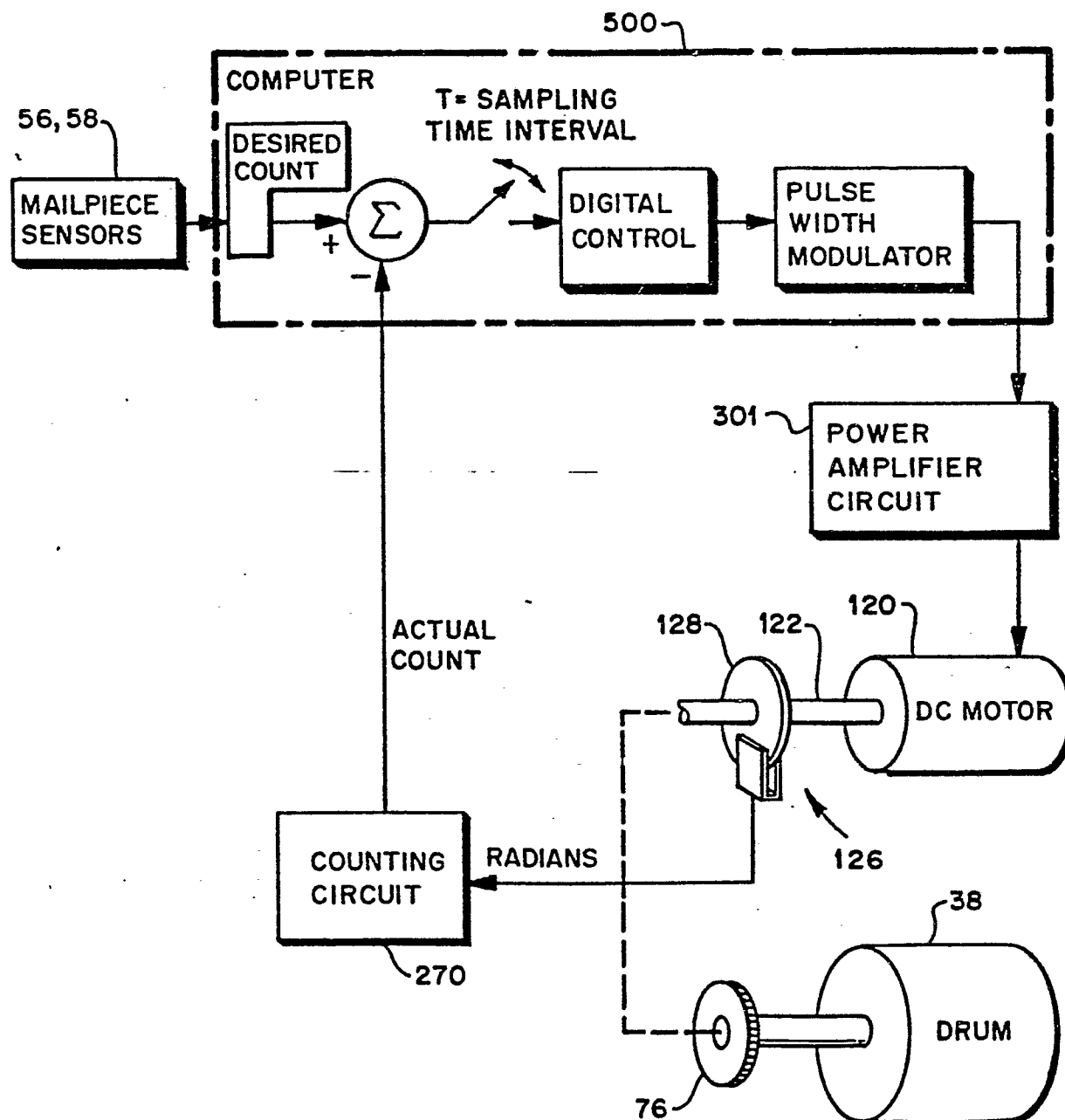


FIG. 11

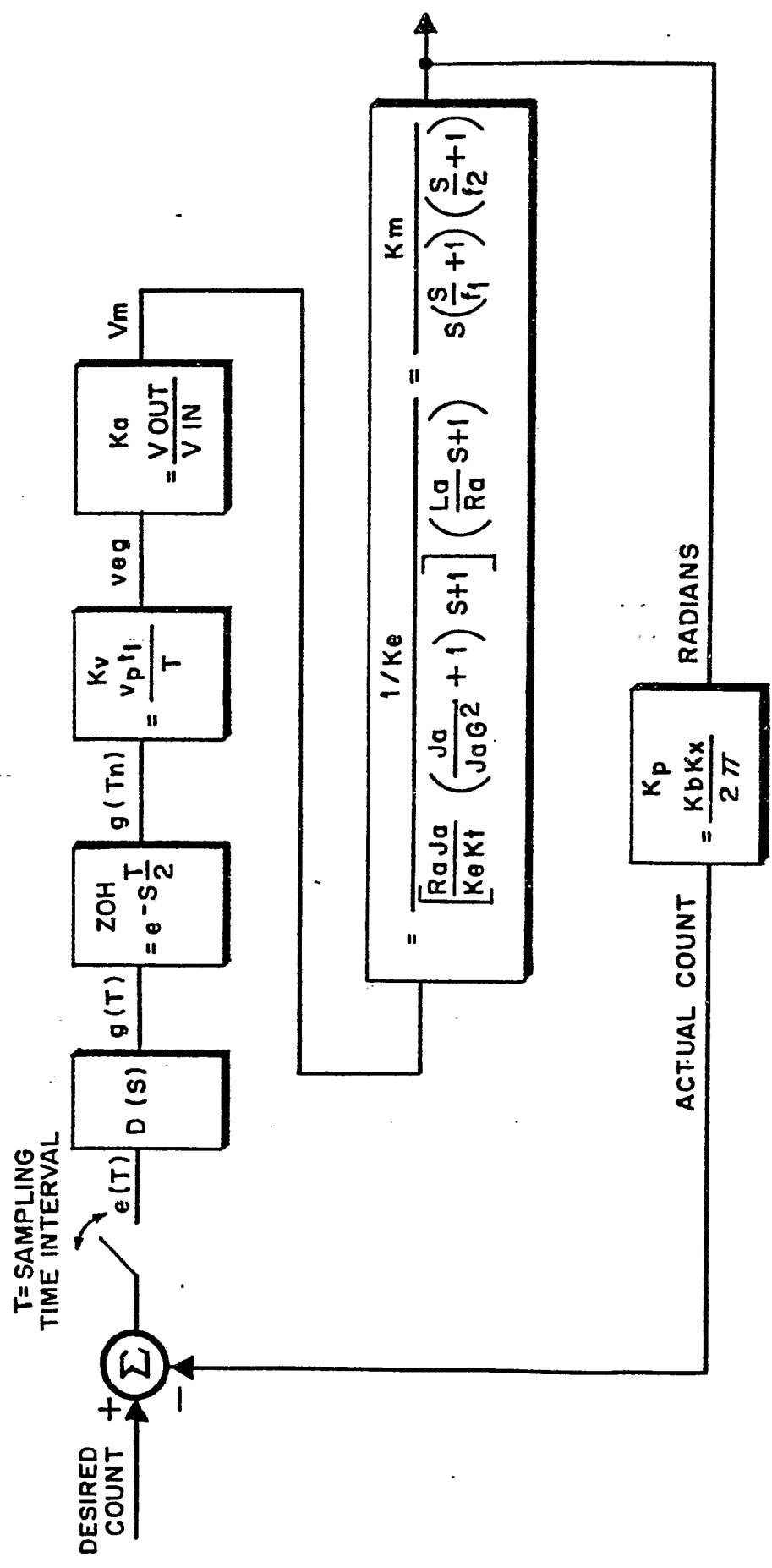


FIG. 12

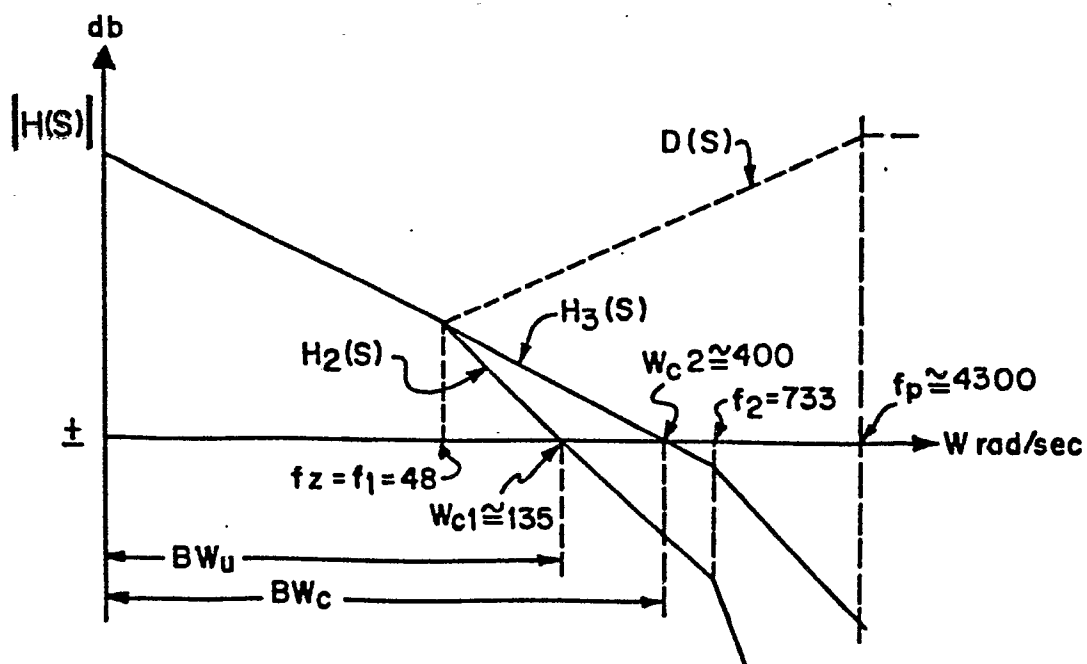
$$(a) \quad H_1(S) = ZOH(K_V)(K_a) \frac{K_m}{s\left(\frac{S}{f_1} + 1\right)\left(\frac{S}{f_2} + 1\right)} K_p$$

$$(b) \quad H_2(S) = ZOH(K_V)(K_a) \frac{K_m}{s\left(\frac{S}{f_1} + 1\right)\left(\frac{S}{f_2} + 1\right)} (K_p)(K_c)$$

$$= \frac{e^{S \frac{T}{2}} (K_V)(K_a)(K_m)(K_p)(K_c)}{s\left(\frac{S}{f_1} + 1\right)\left(\frac{S}{f_2} + 1\right)}$$

$$= \frac{K_0 e^{S \frac{T}{2}}}{s\left(\frac{S}{f_1} + 1\right)\left(\frac{S}{f_2} + 1\right)} = \frac{400 e^{-0.001 \frac{S}{2}}}{s\left(\frac{S}{48} + 1\right)\left(\frac{S}{733} + 1\right)}$$

FIG. 13



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$$D(S) = K_c \frac{\left(\frac{S}{f_z} + 1\right)}{\left(\frac{S}{f_p} + 1\right)} \quad \text{FIG. 14}$$

$$= 13.64 \frac{\frac{S}{48} + 1}{\frac{S}{3400} + 1} = 966 \frac{(S+48)}{(S+3400)}$$

$$(a) \quad d_f = \theta_m \frac{\pi}{360^\circ}$$

$$(b) \quad O_S = 100 \frac{e^{\frac{\pi}{d_f}}}{\sqrt{1-d_f^2}}$$

$$(c) \quad t_x = \frac{1}{d_f} (W_h) \approx \frac{1}{d_f} (W_c)$$

$$(d) \quad t_s \approx 5 t_x$$

FIG. 15

$$s = \frac{2}{T} \times \frac{z-1}{z+1}$$

FIG. 16

FIG. 17

$$\begin{aligned}
 D(Z) &\approx 366 \left(\frac{Z - 0.953}{Z + 0.259} \right) \\
 &= 366 \left(\frac{1 - 0.953Z^{-1}}{1 + 0.259Z^{-1}} \right)
 \end{aligned}$$

FIG. 18

$$(a) \quad D(Z) = \frac{G(Z)}{E(Z)} = 366 \left(\frac{1 - 0.953Z^{-1}}{1 + 0.259Z^{-1}} \right)$$

$$(b) \quad G(Z) = 366E(Z) - 348E(Z)Z^{-1} - 0.259G(Z)Z^{-1}$$

FIG. 19

$$\begin{aligned}
 G(T_n) &= 366E(T_n) - 348E(T_n - 1) - 0.259G(T_n - 1) \\
 &= K_1 E(T_n) - K_2 E(T_n - 1) - K_3 G(T_n - 1)
 \end{aligned}$$

FIG. 20

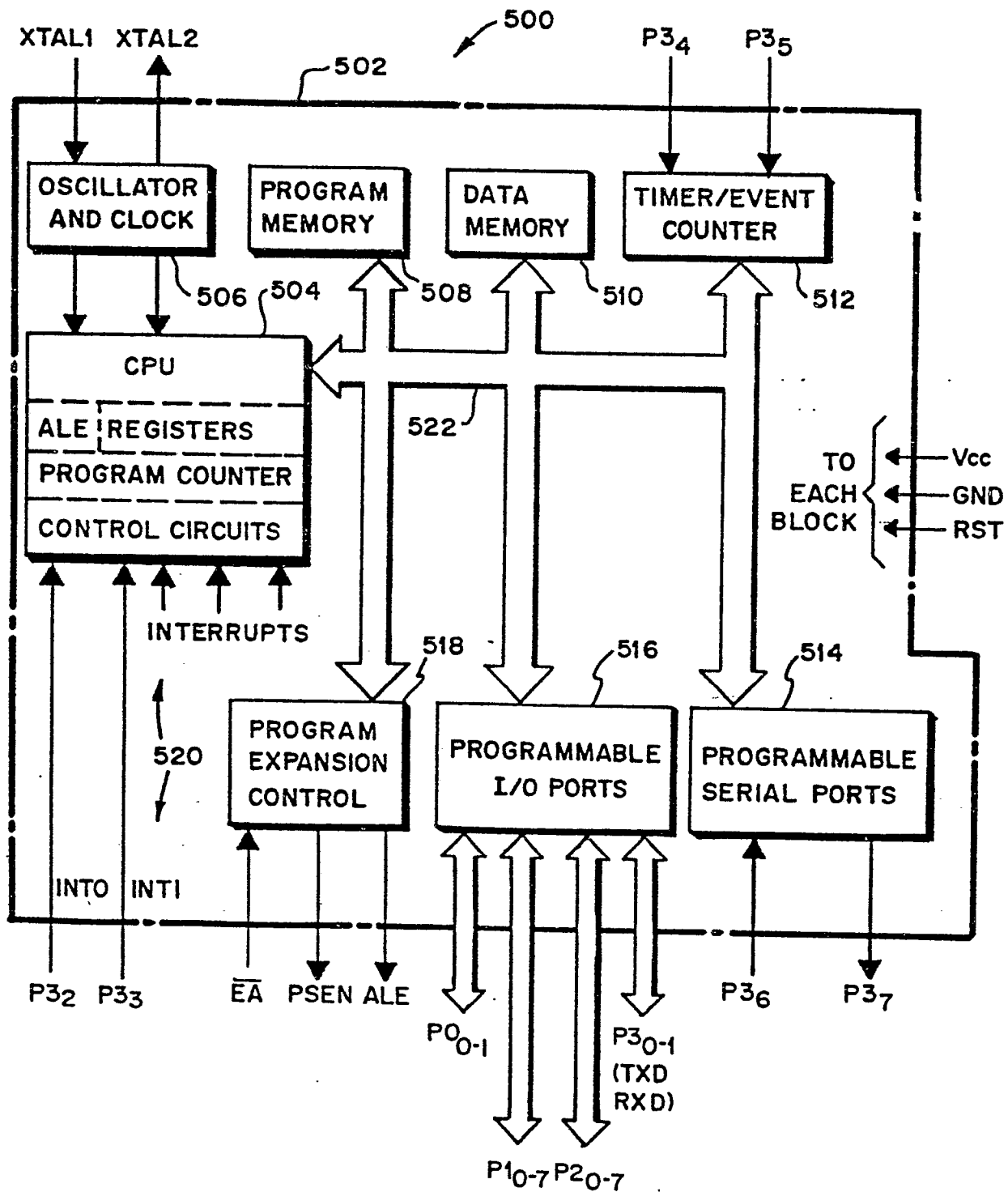
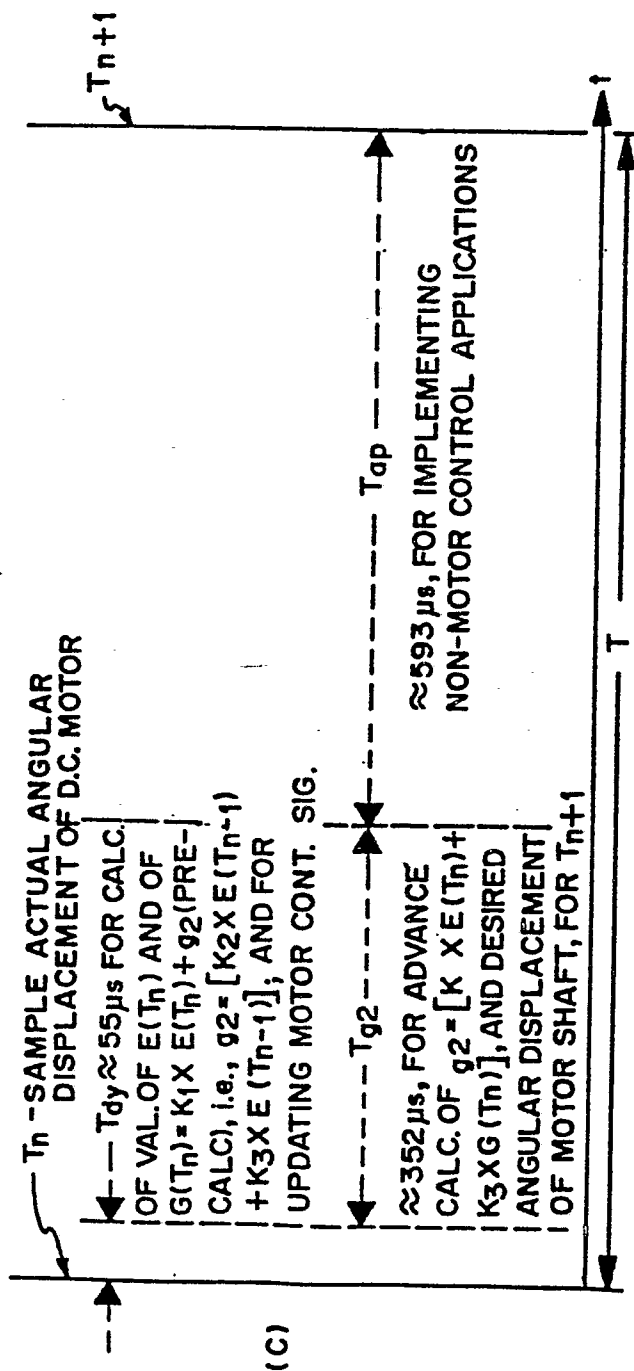
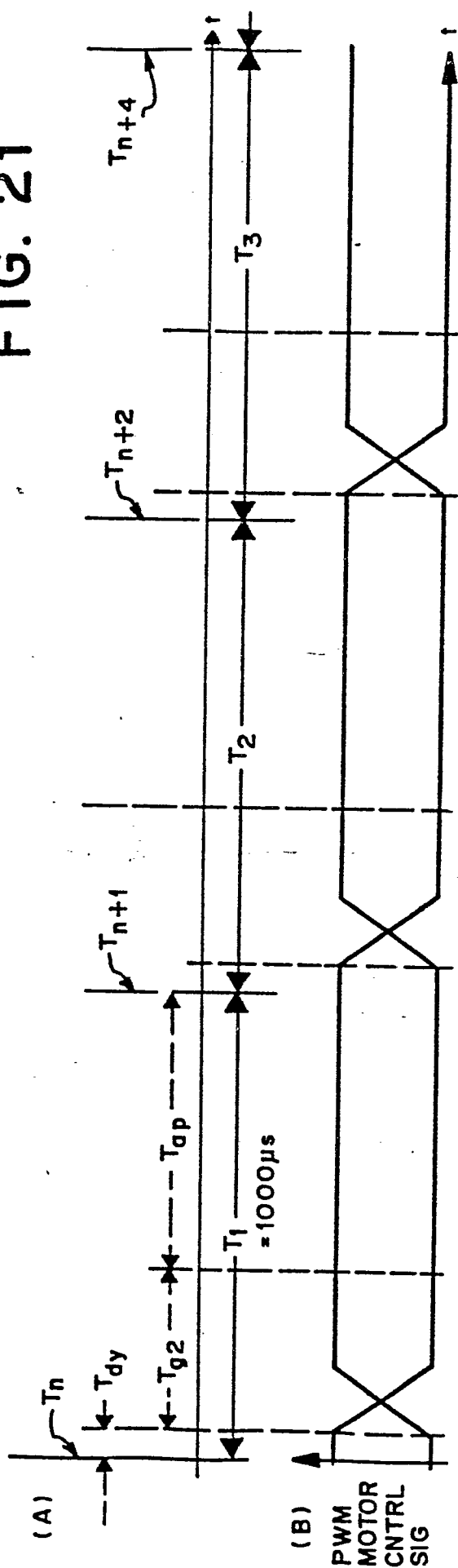


FIG. 21



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FIG. 23a-1

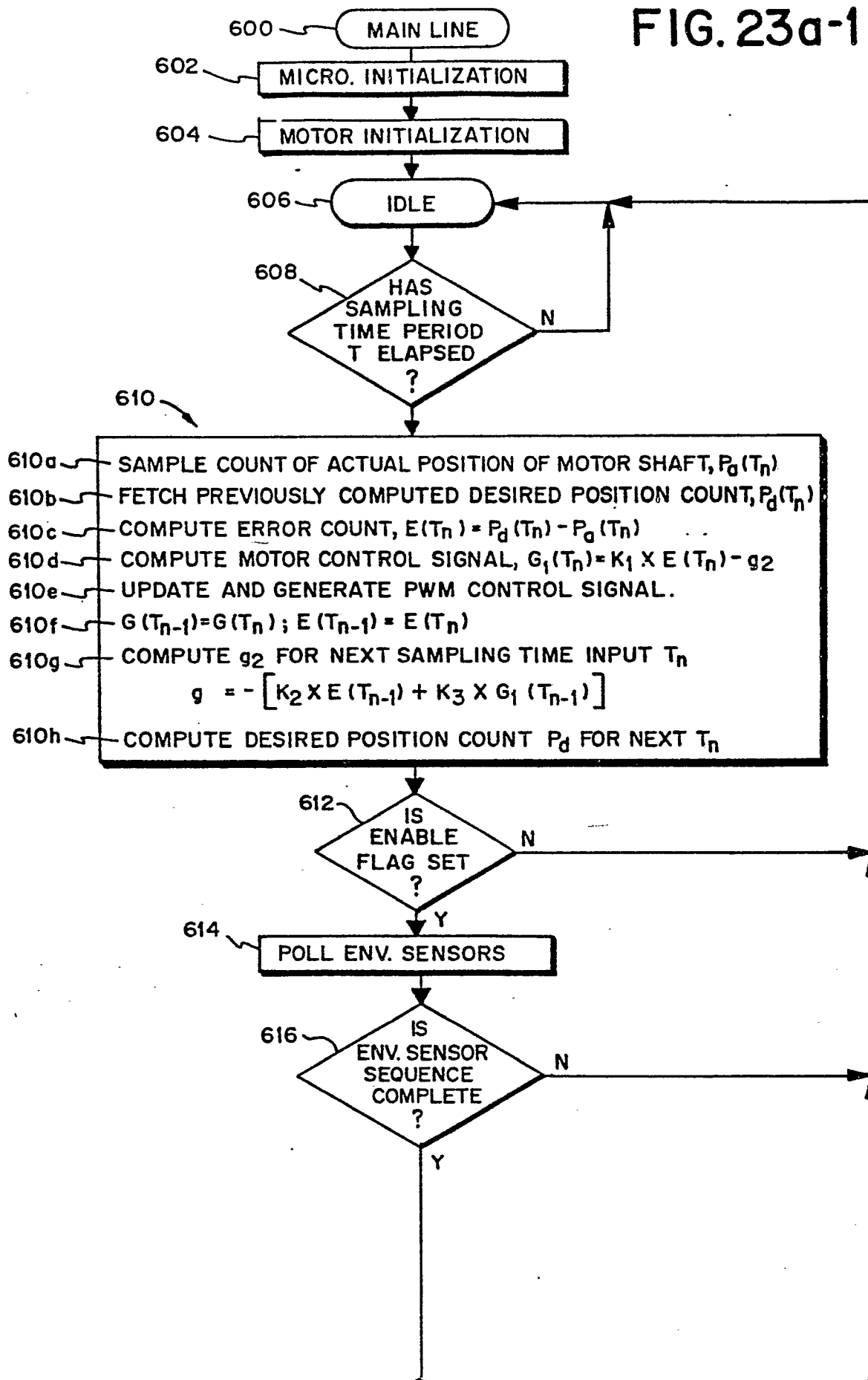
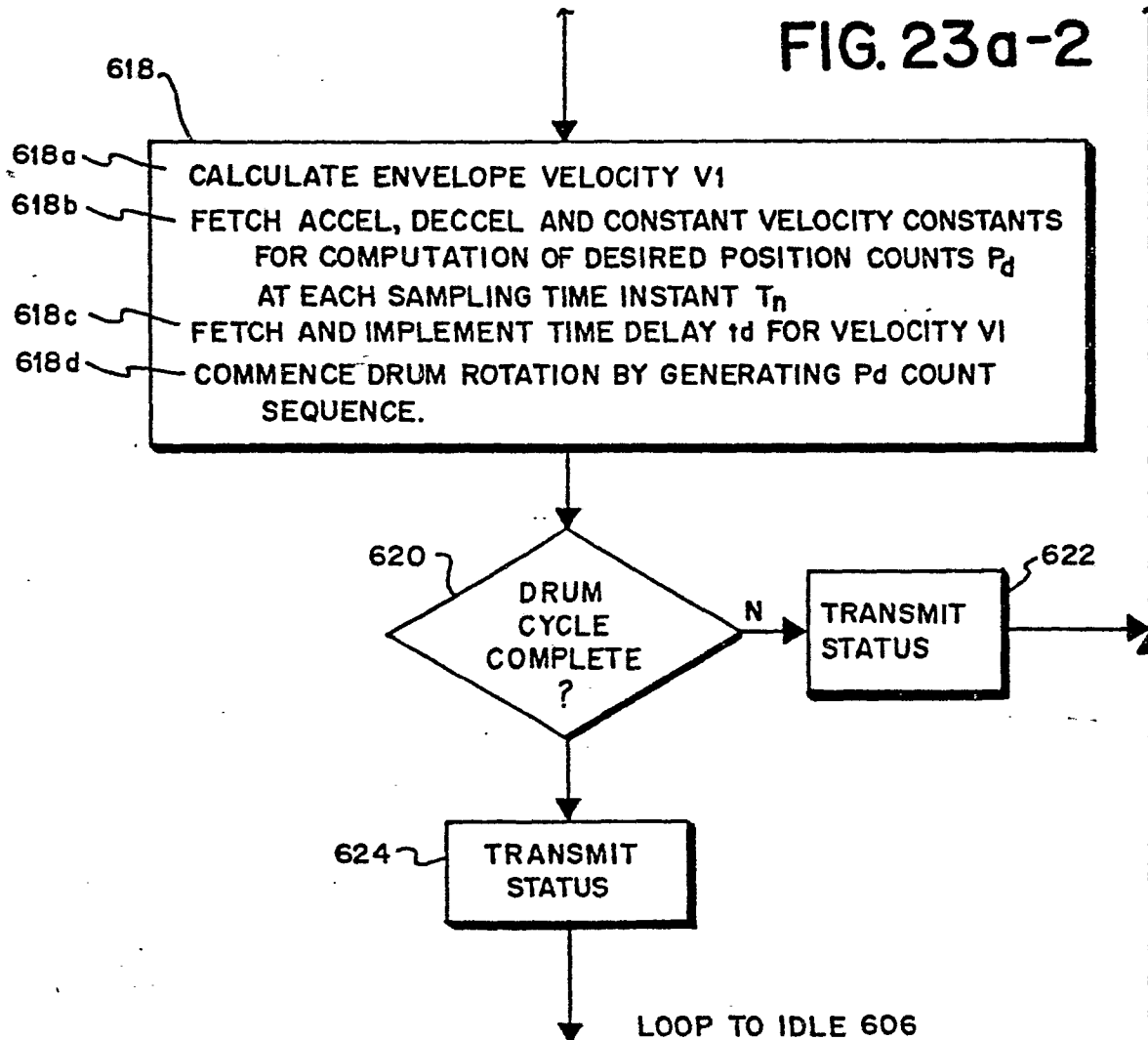


FIG. 23a-2



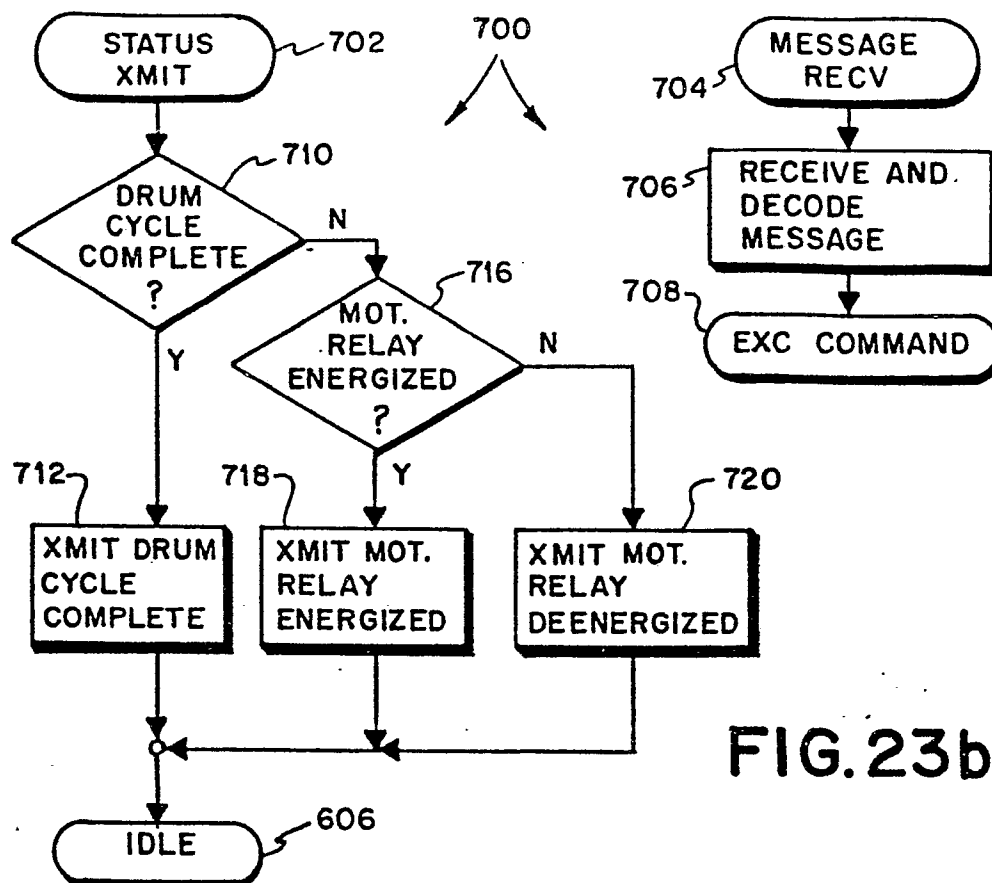


FIG. 23c

