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## Description

The fluidized catalytic cracking, or FCC, process is one of the work horses of modern refineries.

In somewhat oversimplified terms, hot catalyst contacts a relatively heavy oil feed, producing coked catalyst and cracked products. The coked catalyst is regenerated by burning the coke from coked catalyst in a regenerator. The catalyst is heated during the regeneration, because the coke burns. The hot regenerated catalyst is recycled to contact more heavy oil feed.

In 1940's vintage FCC units, the heavy oil feed contacted the catalyst in a relatively short transfer line which mixed the catalyst and oil together, and discharged the catalyst/oil mixture into a dense bed reactor.

Gradually refiners learned that riser cracking (with a very short residence time, typically on the order of under ten seconds) was more beneficial than dense bed cracking (with catalyst/oil residence times on the order of 10 seconds – 60 seconds or more).

The desired reactions happened quickly in the catalyst riser. Some additional conversion occurred in the dense bed reactor, but a significant amount of overcracking also occurred in the dense bed and in the reactor vessel.

Modest conversions of feed to fuel oil and gasoline fractions occurred in the riser reactor. Very modest incremental conversion of feed to lighter components was obtained in the dense bed reactor, but there was also a significant amount of cracking of very valuable gasoline and fuel oil components to coke and light gases.

Accordingly refiners have attempted to maximize riser cracking, and minimize dense bed cracking. Generally this has been done by extending the catalyst riser and cutting down on the amount of catalyst inventory in the relatively large vessel into which the riser reactor discharged.

Some FCC units have attempted to practically eliminate dense bed cracking, by causing the riser reactor to discharge into a rough cut cyclone, or to discharge down toward the dense bed without agitating it, whereby substantial separation of cracked products from deactivated catalyst can be quickly obtained. Such an approach is shown in U.S. 3 785 962.

Because of the number and size of FCC units in modern refiners, there has been tremendous incentive to improve this process even more.

A profound improvement was the shift to the use of zeolite based catalyst which resulted in a tremendous increase in catalyst activity.

Another development was the CO-afterburning regenerator which resulted in more complete combustion of coke to CO<sub>2</sub>, rather than CO, in the FCC regenerator.

U.S. 4 072 600 disclosed adding Pt, Pd, etc. to the circulating catalyst inventory to promote afterburning of CO to CO<sub>2</sub> in the FCC regenerator.

Despite the revolutionary changes which have improved the FCC process, we were not satisfied that the process was operating at its maximum efficiency.

We discovered that other workers in this area overlooked one problem, or if they recognized the problem, failed to see its solution.

The problem was the thermal cracking that occurred after riser cracking but before the cracked products could be removed from the reactor vessel and subjected to conventional product recovery techniques.

We discovered a way to significantly minimize the unnecessary losses of valuable normally liquid products which occurred due to thermal cracking after riser cracking had been completed, but before the cracked product could be removed from the reactor and subjected to conventional product recovery.

Accordingly the present invention provides an improved FCC process wherein a conventional fluidizable catalytic cracking catalyst and a hydrocarbon feed are charged to a reactor riser at catalytic riser cracking conditions to form catalytically cracked vapor product and spent catalyst which are discharged into a reactor vessel via a riser reactor outlet connective with a separation means to produce a catalyst lean phase comprising a majority of said cracked product, and a catalyst rich phase comprising a majority of said spent catalyst, is discharged into a dense bed of catalyst maintained below said riser outlet and said catalyst lean phase is discharged into said vessel and then withdrawn from said vessel via a vessel outlet, the improvement comprising addition of a quenching stream into said vessel above said dense bed of catalyst.

Figure 1 shows an FCC riser reactor with quench steam ring.

Figure 2 shows a detail of an FCC reactor with a closed cyclone configuration and quench steam ring installed.

## FEED

Any conventional feed to an FCC unit can be used. Usually the feed to an FCC unit comprises gas oils, vacuum gas oils, topped crudes, etc. Heavy feeds, such as tar sands, shale oil, and asphaltic fractions may be used, if the unit can tolerate the high metals concentrations and coking tendencies of these

feeds. The present invention is not the discovery of a new feed to an FCC unit, but a way to make better use of feeds now used for FCC units.

#### CATALYST

Any catalyst suitable for use in an FCC unit can be used in the process of the present invention. Preferably the catalyst is one of the many commercially available zeolite based catalysts, but it is also possible to obtain benefits from practicing the present invention when amorphous materials such as alumina, or amorphous silica/alumina are used as the catalyst.

Especially preferred catalysts are rare earth exchanged Y zeolites in an amorphous matrix. The catalyst may contain one or more of the following types of promoters.

1. CO oxidation promoters, such as disclosed in U.S. 4 072 600.
2. Metals passivation promoters, such as various antimony compounds.
3. Any other promoters hereafter developed for use in conjunction with FCC catalyst.

Neither the catalyst, nor any of the catalyst promoters, form any part of the present invention. The present invention helps FCC units operating with conventional catalyst to operate more efficiently.

#### FCC RISER REACTOR

Any conventional riser reactor, and riser reactor discharge means, can be used in the present invention.

Preferably the riser reactor discharges directly into a rough cut cyclone, or other separation means, whereby a very quick separation of cracked products from catalyst may be contained.

If there's no room within the reactor to locate a rough cut cyclone on the discharge of the riser reactor, it is preferred that the riser reactor discharge down into the dense bed reactor, from a relatively high distance above the dense bed catalyst level. This minimizes stirring up of the dense bed, and minimizes contact of cracked products/catalyst.

It is also acceptable, although not preferred, if the riser reactor discharges directly into a dense bed of catalyst, either in a vertical up direction, or horizontally. Such an operation tends to promote dense bed cracking, and should be avoided. Many older FCC units were built at a time when dense bed cracking was more highly regarded, and it is not possible to economically change the configuration of the units. It is harder to see the benefits of the present invention in such units, because a lot of hot catalyst is tossed about within the vessel containing the dense bed of catalyst, minimizing the temperature quenching effect of the steam quench.

Integrating the above discussion, the preferred riser reactor provides a residence time of less than 10 seconds, preferably on the order of 1-5 seconds, and it discharges directly into a rough cut cyclone to effect rapid separation of cracked products from catalyst.

The riser reactor may operate in upflow, or downflow, though an upflow riser reactor is preferred because there is much more operating experience available for such a unit.

The riser reactor may actually be two or more reactors in series, or in parallel. Although such riser reactor designs are contemplated for use herein, they form no part of the present invention.

#### FCC DENSE BED REACTOR

As discussed above, the riser reactor discharges into a vessel designed to contain a dense bed of catalyst. Conventional FCC dense bed reactor designs call for a relatively large vessel, usually several orders of magnitude larger in volume than the riser reactor, which serves to collect spent catalyst in the lower portion of the reactor. The spent catalyst is withdrawn from the bottom of the reactor, usually through a stripper zone containing baffles, and removed from the reactor. Stripping steam is added at the bottom of the reactor vessel to displace easily strippable hydrocarbons from the spent catalyst, so that these strippable hydrocarbons will not be burned in the regenerator.

#### FCC REGENERATOR

Any conventional FCC regenerator may be used in conjunction with the present invention.

CO afterburning regenerators are, in most situations, preferred as far as maximum efficiency in the total FCC unit is concerned, however the present invention will work equally well with CO afterburning and non-CO afterburning regenerators. The regenerator is an essential portion of an FCC unit, but the regenerator section, by itself, forms no portion of the present invention.

An especially effective regenerator design is a stacked regenerator with a first dense bed, or coke combustor, a dilute phase transport riser and a second dense bed of hot regenerated catalyst maintained generally above the coke combustor. Some recycle of hot regenerated catalyst to the coke combustor generally improves operation in the coke combustor.

REACTOR QUENCH

Preferably one or more quench means are disposed within the reactor vessel into which the riser reactor discharges. Steam is the preferred quenching medium. Steam is preferably admitted via a radially disposed steam injection ring disposed just above the dense bed of catalyst.

The function of the steam quench is twofold. It reduces the temperature of the cracked products in the vapor phase above the dense bed of catalyst. It also displaces the cracked hydrocarbons from the reactor vessel, thereby decreasing the residence time of these materials in the reactor vessel. The combination of these two effects, reduction in temperature and reduction in vapor residence time, significantly reduces the amount of thermal cracking that occurs in the riser reactor.

If the steam quench rings are located too near the surface of the dense bed of catalyst, there is a risk that the hot catalyst will be stirred up by the steam injection, which will result in some catalyst displacement into the dilute phase, leading to overcracking of cracked products, and leading to increased temperatures in this zone. The generally small amounts of steam quench that are added are effective to reduce the temperature and residence time of cracked products, but we prefer not to add enough steam to reduce the temperature of the hot catalyst. This is largely a matter of economics, to significantly cool the hot catalyst would require relatively large amounts of steam, and would, in most instances, simply waste heat.

As the steam quench point rises in the reactor vessel, the effectiveness of the steam quench gradually diminishes.

It may be beneficial to add steam quench at the very outlet of the reactor. There would be no reduction in temperature or residence time of cracked vapors in the reactor, but there would be a quenching effect, and a reduction of residence time, in the transfer line going to downstream product recovery units.

The amount of steam quench injected, and the precise location of the steam quench injection point within the vessel containing the dense bed of spent catalyst, will determine the change in residence time of cracked vapors within the reactor. The temperature, and amount of steam quench will determine the temperature change of cracked product within the reactor.

The temperature of the steam will have a significant effect on the quenching effect, or temperature reduction of cracked products. It is also possible to simply add water and let the water vaporize within the reactor, or provide enough surface area in the steam quench ring so that the water will vaporize and become steam before entering the reactor. This would give maximum cooling per weight of water added, the cooling effect being vaporization of water to steam, followed by an increase in sensible heat of the steam produced.

To minimize corrosion problems, and possibilities of temperature shock within the reaction zone, it is usually preferred to simply add some low grade steam, such as 450 kPa (50 psig) steam which is usually a very cheap and readily available commodity within a refinery.

Addition of a vaporizable liquid hydrocarbon is also possible, with naphtha and gas oil or distillate fractions being preferred. These all vaporize, and are believed at least moderately resistant to thermal cracking.

Because the optimum amount of quench will vary with each refinery unit's configuration, and indeed with different cargestocks and operating conditions, it is not possible to specify one unique quantity and temperature of quench for best results. Instead some general guidelines can be given, with the following discussion focusing the steam addition.

Improved results can be obtained when steam, or water, equivalent to about 0.1–20 wt% of the cracked hydrocarbon vapors is added to the steam quench means. Preferably, an amount of steam equal to 0.5–5 wt% of the cracked vapors is added.

In some situations, addition of this much steam will have little effect upon the temperature in the dilute phase, above the dense bed of catalyst in the reactor vessel, but even here significant operating improvements can be obtained. Whenever the riser reactor discharges into an open cyclone, there is a significant amount of hydrocarbon vapor that remains a long time in the dilute phase above the dense bed of spent catalyst. There is also some, 1–2% hot catalyst that finds its way into the dilute phase, and this hot catalyst tends to heat up the dilute phase above the dense bed. In these operations it is believed that the primary benefit of the present invention is from reduced residence time of hydrocarbon products in the dilute phase, rather than from any temperature drop, although the small drop in temperature that occurs in such an operation is certainly beneficial. It is also possible that some of the beneficial effect of our steam quench operation is one additional stage of stripping of catalyst, but this is not believed to be a significant part of the improved results seen, because well over 90 percent of the catalyst simply bypasses our steam quench ring and never sees the steam injection.

The most noticeable improvement in operation, and the greatest drop in temperature of the hydrocarbon phase above the dense bed of spent catalyst, occurs when closed cyclones are used.

In this type of operation, the riser reactor discharges into a primary cyclone, which makes a rough, but fairly effective, separation of catalyst from cracked products. The vapor from the primary cyclone is discharged directly into a secondary cyclone which is able to effect a far more complete separation of catalyst from cracked products than could be achieved in the rough cut cyclone attached directly to the riser reactor outlet.

In such a design, with closed cyclones, relatively minor amounts of steam injection result in significant decreases in reactor temperature, typically 10–20 times as great as those obtained in an open cyclone system. Despite almost an order of magnitude or more greater drop in temperature of dilute phase vapors above the dense bed of catalyst, the results as far as increased gasoline and light fuel oil make, are only slightly better than those achieved in the open cyclone case. This is probably because only a small portion of the vapors remain in the reactor vessel with the closed cyclone (3 wt%).

The extent of undesirable thermal cracking that goes on in a reactor may be estimated by calculating the residence time in the reactor at a given temperature. These two numbers can be used to devise an ERT or Equivalent Reaction Time at 427°C (800°F). More details about ERT are provided in U.S. 4 379 747 and U.S. 4 428 824. Another way of evaluating relative reaction velocities in thermal cracking is to compare S.F. or Soaking Factors. By definition, the ERT and SF are 1.0 at 427°C (800°F). As the temperature increases, the reaction rate increases, to 2.0 at 439°C (822°F), and so on.

The amount of thermal cracking will be cut about in half by reducing the residence time of the catalytically cracked product by one half, or by reducing the vapor temperature from 439 to 427°C (822 to 800°F), or some combination of these.

When closed cyclones are used, the same amount of steam injection profoundly reduces temperature and ERT, reducing ERT by more than 50%.

When open cyclones are used, much smaller declines in ERT may be expected; usually on the order of 3–50% decreases in ERT will be experienced. This is much less reduction in thermal cracking severity, but 10 to 20 times the material is involved, as compared to the closed cyclone case. Preferably ERT is reduced by at least 4%.

Regardless of the cyclone configuration used, the amount of quench added should be sufficient to reduce thermal cracking enough to increase the yield of gasoline and light fuel oil products at least 0.5%, and preferably 1 to 2%, or more.

The present invention may be better understood by reviewing it in conjunction with the drawing.

The drawing is schematic, many details such as instrumentation, etc. have been left out.

In Figure 1, a mixture of hot regenerated catalyst, from a catalyst regenerator not shown, and fresh feed is mixed together and passed up through reactor riser 4. The catalyst oil mixture leaves reactor riser 4, and enters primary cyclone 2 which effects a rough separation of spent catalyst from cracked products. Most of the spent catalyst is discharged from primary cyclone 2 via dipleg 12 and flapper valve 11. Cracked vapors leave the top of cyclone 2 via outlet 3 and enter into the dilute phase 15 within reactor 1.

The terminology used in the specification is consistent with terminology used in modern refineries, however it should be pointed out that what is referred to as reactor riser 4 is in actuality the reactor where well over 90 percent of the desired catalytic cracking reactions occur. Ideally, 100 percent of the reactions would take place in reactor riser 4, and no reaction whatever would take place in reactor 1. In time, refiners may revise their vocabulary to refer to riser 4 as the reactor, and vessel 1 as a spent catalyst/cracked product separation means, but such usage would be confusing to those skilled in the FCC arts.

Vapors leaving primary cyclone 2 enter into the dilute space above the top of dense bed of catalyst 17. Dense bed 20, with upper surface or interface level 17 is the collection of catalyst from the diplegs of the cyclones within reactor 1. The dense bed/dilute phase interface 17 may be below the catalyst diplegs, as shown in the drawing, or the dense bed level may be raised, or the diplegs extended, so that the diplegs are immersed within the dense bed of catalyst 20.

Cracked product in dilute space 15, along with relatively minor amounts of catalyst entrained in the vapor phase enter the secondary cyclone means 6 via inlet 5. Catalyst fines are withdrawn via dipleg 16 and discharged into the dense bed of catalyst, although only the upper portion of the dipleg is shown in this drawing.

Cracked product vapors are removed via vapor outlet 7 from cyclone 6 and discharged into third stage separation means 8, another cyclone. Catalyst removed from the third stage cyclone is removed via dipleg 18 and discharged through flapper valve 19 into dense bed 20 of catalyst at the bottom of reactor 1.

Catalytically cracked products are removed from reactor 1 via lines 9 and 13 into reactor outlet plenum 14 and then sent via line 10 to product recovery means not shown. To simplify the drawing, only a single cyclone is shown for primary cyclone 2, secondary cyclone 6 and third stage cyclone 8. In actuality, there usually would be a plurality of primary, secondary, and third stage cyclones. The second inlet line 13 to plenum 14 is intended to show that other third stage cyclones will be present.

The spent catalyst which collects as dense bed 20 in the bottom of reactor 1 is subjected to stripping to remove easily strippable hydrocarbon vapors from the spent catalyst before it is sent to a catalyst regenerator, not shown. This steam stripping of spent catalyst, which is conventional, is conducted at reactor stripper 21. A steam supply, shown as line 30, admits steam via either line 22 and/or 24 to lower and upper stripper steam rings, respectively.

Steam is also admitted via line 26 to quench steam ring 27, located above the interface level 17 of dense bed of catalyst 20. Only a single quench steam ring is shown in the drawing, extending radially around the reactor, it is also possible to have multiple quench steam rings at different elevations within

the reactor vessel 1, or to use steam injection means other than a ring. One or more stab-in steam spargers could be used to add steam, or steam may be injected to counter any naturally occurring swirl of catalyst that occurs at the bottom of the reactor.

Steam quench should be conducted so as to minimize disruption of dense bed of catalyst 20. For this reason, quench steam injection should always be at, or preferably somewhat above, the interface 17 between dilute phase 15 and dense bed 20.

The configuration shown in Figure 1 is referred to as an open cyclone configuration, because there is no direct connection between primary cyclone 2 and secondary cyclone 6.

It is also possible, and preferable, to operate with closed cyclones, in which case inlet 5 to cyclone 6 would resemble an inverted funnel which was radially aligned with, and above outlet 3 of primary cyclone 2, as shown in Figure 2. Such a configuration is not, strictly speaking, "closed", because it is still possible, and very desirable, for cracked hydrocarbon products, and quench steam, to enter inlet 5 in the annular space between outlet 3 and inlet 5. There has to be some way provided of allowing cracked vapor and quench steam and stripping steam to eventually enter the outlet plenum 14, and the closed cyclone modification described above works very well in this service. When operating with a closed cyclone, it is beneficial to immerse dipleg 12 about 50 cm past the dense bed/dilute phase interface 17. This minimizes leakage of vapors down dipleg 12, as the catalyst seals the outlet of dipleg 12.

A characteristic of "closed cyclone" configuration is that 90% of the cracked vapor product will pass from the primary cyclone outlet and enter the secondary cyclone inlet in less than 1 second, preferably in less than 0.5 second.

Although not shown in the drawing, it is also possible to eliminate entirely the primary cyclone 3, and merely have the riser reactor discharge down towards interface 17, from a distance 3-10 meters above it. This does only a mediocre job of separating catalyst from cracked vapors, but in many existing reactors, it's not possible to support primary cyclones 2 at the reactor riser outlet, either because of lack of strength or lack of room. In such circumstances, a downward discharge of spent catalyst/cracked product from 3-10 meters above the dense bed interface provides a way to achieve some semblance of quick quench of the riser cracking reaction. If such an approach is taken, it may be desirable to use multiple quench steam rings. Quench steam ring 27 shown in the drawing would reduce the residence time of cracked products in space 15, but would do little or nothing towards reducing the temperature of the cracked products, because of the large amount of hot spent catalyst present. In such a circumstance, it may be beneficial to move the quench steam ring to an elevation equal to, or slightly above the reactor riser outlet, so that steam quench will have a noticeable cooling effect on reactor vapors. In some circumstances, a combination of steam quench via quench ring 27 shown in the drawing and another quench ring located above the riser reactor outlet, and not shown in the drawing, would be beneficial.

The two illustrative embodiments which follow do not represent commercial or laboratory tests. They are based on computer simulations of commercial operation, and are believed to be accurate predictors of what will happen in commercial operation.

The feedstock used was similar to the Joliet Sour Heavy Gas Oil described hereafter.

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Table I

	Chargestock	Joliet Sour Heavy Gas Oil (JSHGO)
5	Density, g/cm <sup>3</sup>	0.90
	Gravity, °API	24.3
	Aniline Pt., °F/°C	171/77
	Sulfur, wt.%	1.87
10	Nitrogen, wt.%	0.10
	Basic Nitrogen, ppm	327
	Conradson Carbon, wt.%	0.28
15	Viscosity, KV at 210°F/99°C	3.6
	Bromine No.	4.2
	R. I. at 70°F/21°C	1.5080
	Hydrogen, wt.%	12.3
20	Molecular Weight	358
	Pour Point, °F/°C	85/29
	Paraffins, wt.%	23.5
	Naphthenes, wt.%	32.0
25	Aromatics, wt.%	44.5
	C <sub>A</sub> , wt.%	18.9

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Table II

Base Case Operating Conditions		
5	Fresh Feed, BPD	34,200
	Fresh Feed, m <sup>3</sup> /second	0.0626
	Combined Feed Ratio	1.0
10	Riser Top, °F/°C	995/135
	Combined Feed, °F/°C	365/185
	Regen. Dense Bed, °F/°C	1,310/710
15	Regen. Air, °F/°C	386/197
	Reactor Press., psig	28.0
	Reactor Press., kPa	287
20	Regen. Press, psig	31.7
	Regen. Press, kPa	320
	Cat Activity, CB FAI	59.0
25	Cat Circ., tons/minute	28.0
	Cat Circ., kg/sec	423
	Catalyst/Oil	7.30
30	Stripping Steam, g/kg Cat	3.06
	Riser Dispersion Steam, lb/hr	2000
	Riser Dispersion Steam, kg/sec	0.252
35	Regen. Air, MSCFM	77.6
	Regen. Air, M <sup>3</sup> /s @ std. conditions	0.366
	H <sub>2</sub> in Coke, wt %	6.50
40	Coke Make, lb/hr	26,691
	Coke Make, kg/sec	3.36
	Air/Coke, wt/wt	13.0
45	CO <sub>2</sub> /CO Ratio	17,200

Based upon the above assumptions, and using our computer simulation of the FCC process, we calculated the effect that would be obtained by adding 0.567 Kg/sec (4500 pounds per hour) of quench steam, equivalent to about 1.125 wt% of the hydrocarbon feed to the unit.



Table III

Yield Benefits for Quench Steam Ring Open Cyclone Arrangement – wt %

	Base Case	Change with Quench Steam Ring
Conversion	62.0	-0.1
Gasoline	39.5	+0.2
Light Fuel Oil	28.5	+0.3
Heavy Fuel Oil	9.5	-0.2
C <sub>4</sub> =	5.3	-0.1
nC <sub>4</sub>	0.6	0
iC <sub>4</sub>	1.6	0
C <sub>3</sub> =	4.6	0
C <sub>3</sub>	1.4	0
C <sub>2</sub> =	3.3	-0.2
Coke	5.8	0
Reactor Vessel Temp., °F/°C	995	992
Quench Steam Rate, lb/hr	0	5000
Quench Steam Rate, kg/s		0.63

As can be seen from Table III, there was a significant increase, of 0.5 wt%, in production of gasoline and light fuel oil. Gasoline production went from 39.5 wt% of feed to 39.7 wt% of feed. Light Fuel Oil increased from 28.5 wt% to 28.8 wt%.

There would be no significant change in the octane number of the gasoline, depending on the O.N. of catalytically cracked gasoline versus thermally cracked gasoline. It is possible that the octane may actually drop a little.

In this example, the amount of steam quench added did little towards reducing the reactor vessel temperature, resulting in a decrease of only 1.7°C (3°F) from 535.0°C (995°F) to 533.3°C (992°F). This change in temperature reduces the ERT from 104 to 100. Here reactor vessel temperature refers to the vapor outlet temperature, measured at the top of the reactor. The reason the reactor vessel temperature did not change much was because in the open cyclone configuration, corresponding roughly to the one shown in the drawing, the steam is in contact with significant amounts of hydrocarbon exiting the vessel and some catalyst.

The reduction in vapor residence time in the dilute phase portion of reactor vessel 1 is estimated to be about 10–15%, or a reduction of about 4 to 6 seconds residence time. A unit weight of water occupies almost 10 times the volume of a unit weight of cracked product in the reactor, based on 18 mw for water and an assumed average mw of 180 for cracked product.

This exercise was repeated, but based upon a slightly different set of assumptions. In this simulation, a closed cyclone configuration was used, wherein more than 97% of the vapors from the primary cyclone outlet went directly into the secondary cyclone inlet. Quench steam rate was 0.567 Kg/sec (4500 pounds per hour), equivalent to 1.125 wt% on reactor hydrocarbon feed.

Results of this computer simulation are reported in Table IV.

Table IV

Yield Benefits for Quench Steam Ring Closed Cyclones – wt %		Base Case	Quench Steam Ring
5	Conversion	61.1	-0.1
	Gasoline	40.4	+0.2
	Light Fuel Oil	30.3	+0.4
	Heavy Fuel Oil	8.6	-0.3
10	C <sub>4</sub> 's		
	C <sub>4</sub> =	4.9	-0.2
	iC <sub>4</sub>	1.7	0
15	nC <sub>4</sub>	-0.5	0
	C <sub>3</sub> 's		
	C <sub>3</sub> =	4.3	-0.1
	nC <sub>3</sub>	1.3	0
20	C <sub>2</sub> =	2.3	-0.1
	Coke	5.8	0
	Reactor Vessel Temp., °F/°C	995/535.0	945/507.2
	Quench Steam Rate, lb/hr	0	4500
25	Quench Steam Rate, kg/s	0	0.567

In this instance, reactor vessel temperature refers to the temperature at the top of the reactor vessel, which is not the same thing as the temperature of the vapor leaving the reactor. The vapor leaving the unquenched reactor would have a temperature of about 535.0°C (995°F). The supercooling of the reactor vessel dilute phase temperature by quench steam was due to the fact that the closed cyclone configuration resulted in significantly less cracked vapor and entrained catalyst being discharged into the dilute phase within reactor vessel 1. The quench steam was far more effective in cooling down this greatly reduced weight of material, in the closed cyclone configuration case, than when the quench steam was being inundated by vast amounts of cracked vapors and spent catalyst, as in the open cyclone configuration discussed in conjunction with Table III.

The reduction in severity (ERT), due to temperature change alone, is equal to 104/43.6, for reduction in thermal cracking of almost 60%.

The 0.5 wt% increase in valuable products is significant, because on a commercially sized unit this incremental yield translates into a projected increase in production of gasoline and light fuel oil of almost 15,000 m<sup>3</sup> (4 million gallons) per year, based on a 0.0823 m<sup>3</sup>/sec (45,000 BPD) FCC unit. The cost of adding a steam quench ring, and using low grade refinery steam, is insignificant in comparison to the increased production of gasoline and light fuel oil that can be obtained.

If we were designing an FCC unit today, and wanted to incorporate steam quench, we would use a riser reactor with a closed cyclone configuration, i.e. one in which the riser reactor discharged directly into a primary cyclone separator. The vapor outlet from the primary cyclone separator would be closely connected with the inlet to a secondary cyclone separator, so that most of the vapor phase would very quickly leave the reactor vessel. Steam quench would be added to a steam quench ring located about 1 meter above the top of the dense bed of catalyst in the reactor. Steam quench, equivalent to 1 wt% of feed, would be added. Steam source would be 450 kPa (50 psig) steam from a refinery steam line.

Preferably the separator comprises a primary cyclone attached to the riser outlet, and wherein a secondary cyclone is provided at an elevation above the dense bed and connective with the vessel outlet, and the quench is added to the vessel at an elevation intermediate the dense bed and the secondary cyclone.

## Claims

1. In a fluidized catalytic cracking process wherein a conventional fluidizable catalytic cracking catalyst and a hydrocarbon feed are charged to a reactor riser at catalytic riser cracking conditions to form catalytically cracked vapor product and spent catalyst which are discharged into a reactor vessel via a riser reactor outlet connective with a separator to produce a catalyst lean phase comprising a majority of the cracked product, and a catalyst rich phase comprising a majority of the spent catalyst, the catalyst rich phase is discharged into a dense bed of catalyst maintained below the riser outlet and the catalyst lean phase is discharged into the vessel and then withdrawn from the vessel via a vessel outlet, the improvement comprising addition of a quenching stream into the vessel above the dense bed of catalyst.

2. Process of claim 1 wherein the quenching stream is selected from the group of water, steam and vaporizable liquid hydrocarbons.

3. Process of claim 1 wherein the quenching stream is steam.

4. Process of claim 3 wherein the amount of steam quench added to the vessel, expressed as weight percent of the hydrocarbon feed, is 0.1 to 20 wt%.

5. Process of claim 4 wherein 0.5 to 5 wt% steam is added as quench.

6. Process of any preceeding claim wherein the separator comprises at least one cyclone separator connected to the reactor riser outlet.

7. Process of claim 6 wherein the amount and temperature of quench addition to the reactor are sufficient to reduce thermal cracking as measured by equivalent reaction time at 427°C, by at least 50%.

8. Process of any of claims 1 to 5 wherein the separator comprises a downwardly discharging reactor riser outlet, positioned 3 to 20 meters above the dense bed if catalyst.

9. Process of claim 7 wherein the amount and temperature of quench addition to the reactor are sufficient to reduce thermal cracking, as measured by equivalent reaction time at 427°C (800°F), by at least 4%.

10. Process of any of claims 1 to 7 wherein the separator comprises a primary cyclone attached to the riser outlet, and wherein a secondary cyclone is provided at an elevation above the dense bed and connective with the vessel outlet, and the quench is added to the vessels at an elevation intermediate the dense bed and the secondary cyclone.

## Revendications

1. Un procédé de craquage catalytique en lit fluidisé (FCC) dans lequel un catalyseur de craquage catalytique classique pouvant être fluidisé et une charge hydrocarbonée sont introduits dans la zone ascendante d'un réacteur, dans des conditions de craquage catalytique en zone ascendante, pour former des vapeurs de produits craqués par voie catalytique et du catalyseur usé que l'on décharge dans un réacteur par une sortie de réacteur en zone ascendante connectée à des moyens de séparation pour obtenir une phase pauvre en catalyseur comprenant la majeure partie du produit craqué et une phase riche en catalyseur comprenant la majorité du catalyseur usé, ce catalyseur étant déchargé dans un lit dense de catalyseur maintenu en-dessous de la sortie de cette zone ascendante et cette phase pauvre en catalyseur étant évacuée dans ce récipient et étant ensuite retirée de ce récipient par une sortie de récipient, caractérisé en ce que l'on introduit un courant de trempe dans ce récipient au-dessus de ce lit dense de catalyseur.

2. Procédé selon la revendication 1, dans lequel le courant de trempe est choisi dans le groupe constitué par eau, vapeur et hydrocarbures liquides vaporisables.

3. Procédé selon la revendication 1, dans lequel le courant de trempe est constitué de vapeur.

4. Procédé selon la revendication 3, dans lequel la quantité de vapeur de trempe ajoutée au récipient, exprimée en % en poids de la charge d'hydrocarbures, est comprise entre 0,1 et 20% en poids.

5. Procédé selon la revendication 4, dans lequel on ajoute de 0,5 à 5% en poids de vapeur comme vapeur de trempe.

6. Procédé selon l'une quelconque des revendications précédentes, dans lequel le séparateur comprend au moins un séparateur à cyclone rattaché à la sortie de la zone ascendante du réacteur.

7. Procédé selon la revendication 6, dans lequel la quantité et la température de vapeur de trempe ajoutée au réacteur sont suffisantes pour réduire d'au moins 50% le craquage thermique tel que mesuré à 27°C pour un temps de réaction équivalent.

8. Procédé selon l'une quelconque des revendications 1 à 5, dans lequel le séparateur comprend une sortie de réacteur en zone ascendante se déchargeant vers le bas et disposée à une hauteur de 3 à 20 m au-dessus du niveau du lit dense de catalyseur.

9. Procédé selon la revendication 7, dans lequel la quantité et la température de vapeur de trempe introduite dans le réacteur sont suffisantes pour diminuer le craquage thermique d'au moins 4%, tel que mesuré à 427°C (800°F) pour un temps de réaction équivalent.

10. Procédé selon l'une quelconque des revendications 1 à 7, dans lequel le séparateur comprend un cyclone primaire rattaché à la sortie du réacteur en zone ascendante et dans lequel un cyclone secondaire est disposé à un niveau se trouvant au-dessus du niveau du lit dense du réacteur et rattaché à la sortie du réacteur, la vapeur de trempe étant introduite dans le réacteur à un niveau intermédiaire entre celui du lit dense et du cyclone secondaire.

## Patentansprüche

1. Katalytisches Wirbelschichtcrackverfahren, bei dem ein herkömmlicher fluidisierbarer katalytischer Crackkatalysator und eine Kohlenwasserstoffzufuhr unter katalytischen Riser crackbedingungen einem Riserreaktor zugeführt werden, um ein katalytisch gecracktes Dampfprodukt und verbrauchten Katalysator zu bilden, die über den Riserreaktorauslaß in ein Reaktorgefäß abgegeben werden, das mit einem Separator in Verbindung steht, um eine katalysatorarme Phase, die den Hauptteil des gecrackten Produktes umfaßt, und eine katalysatorreiche Phase zu erzeugen, die den Hauptanteil des ver-

brauchten Katalysators umfaßt, die katalysatorreiche Phase in das dichte Bett des Katalysators abgegeben wird, das unter dem Riserenauslaß gehalten wird, und die katalysatorarme Phase in das Gefäß abgegeben wird und danach über den Gefäßauslaß aus dem Gefäß abgezogen wird, wobei die Verbesserung die Zugabe eines Abschreckstroms in dieses Gefäß oberhalb des dichten Katalysatorbettes umfaßt.

5 2. Verfahren nach Anspruch 1, worin der Abschreckstrom aus der Gruppe von Wasser, Dampf und verdampfbaren, verflüssigbaren Kohlenwasserstoffen ausgewählt ist.

3. Verfahren nach Anspruch 1, worin der Abschreckstrom Dampf ist.

4. Verfahren nach Anspruch 3, worin die Menge des dem Gefäß zugeführten Abschreckdampfes, als Gew.-% der Kohlenwasserstoffzufuhr ausgedrückt, 0,1 bis 20 Gew.-% beträgt.

10 5. Verfahren nach Anspruch 4, worin 0,5 bis 5 Gew.-% Dampf zum Abschrecken zugesetzt werden.

6. Verfahren nach einem der vorstehenden Ansprüche, worin der Separator zumindest einen Zyklonseparator umfaßt, der an den Riserreaktorauslaß verbunden ist.

7. Verfahren nach Anspruch 6, worin die Menge und die Temperatur des Abschreckzusatzes zum Reaktor ausreichend sind, um das thermische Cracken um mindestens 50% zu verringern, gemessen durch die äquivalente Reaktionszeit bei 427°C (800°F).

8. Verfahren nach einem der Ansprüche 1 bis 5, worin der Separator einen nach unten abgebenden Riserreaktorauslaß umfaßt, der 3 bis 20 Meter oberhalb des dichten Katalysatorbettes angeordnet ist.

9. Verfahren nach Anspruch 7, worin die Menge und die Temperatur des Abschreckzusatzes zum Reaktor ausreichend sind, um das thermische Cracken um mindestens 4% zu verringern, gemessen durch die äquivalente Reaktionszeit bei 427°C (800°F).

10. Verfahren nach einem der Ansprüche 1 bis 7, worin der Separator einen primären Zyklon umfaßt, der an den Riserenauslaß verbunden ist, und worin in einer Höhe oberhalb des dichten Bettes und in Verbindung mit dem Gefäßauslaß ein sekundärer Zyklon vorgesehen ist, und die Abschreckung dem Gefäß in einer Höhe zwischen dem dichten Bett und dem sekundären Zyklon zugeführt wird.

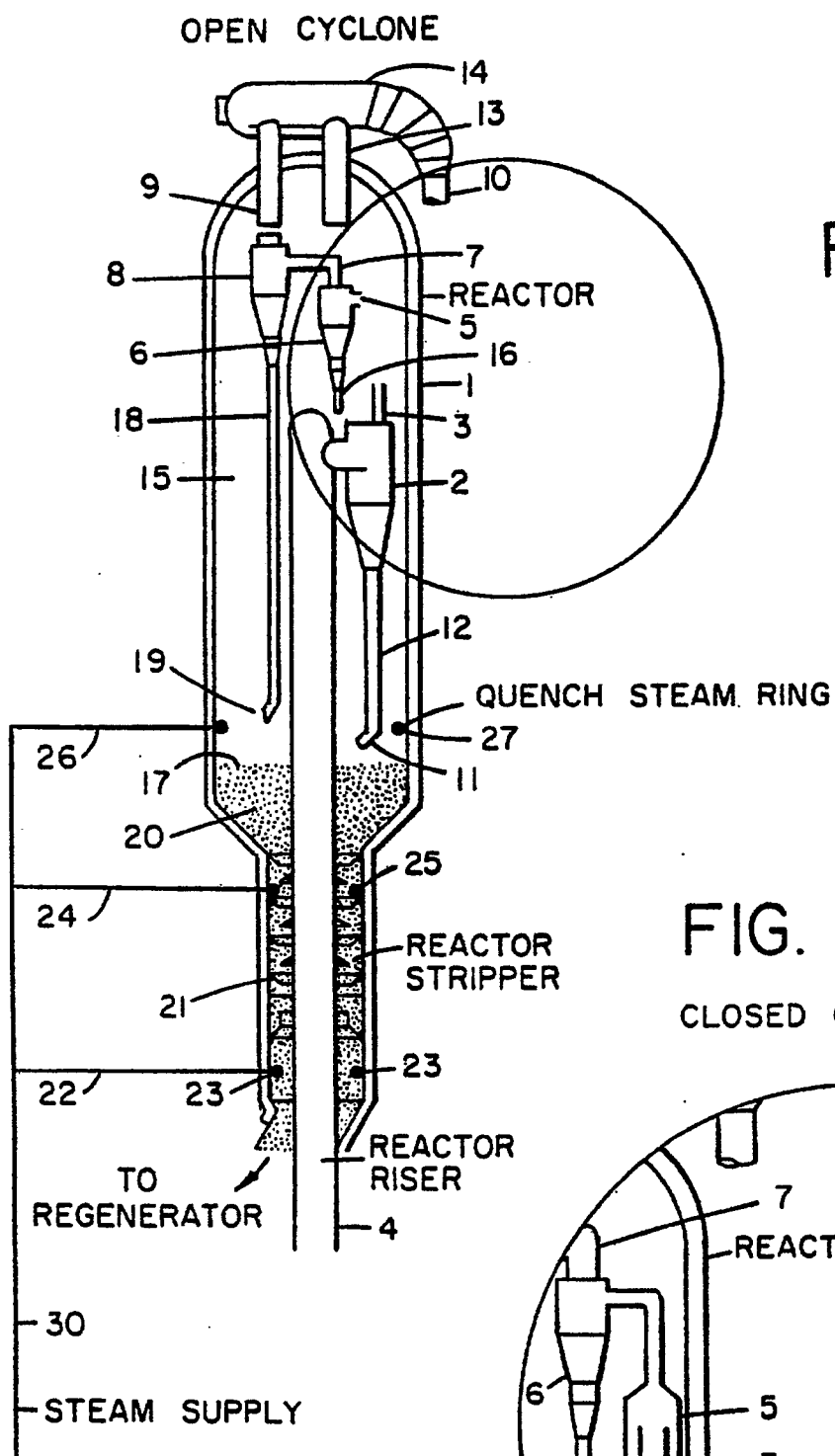


FIG. 1

FIG. 2  
CLOSED CYCLONE

