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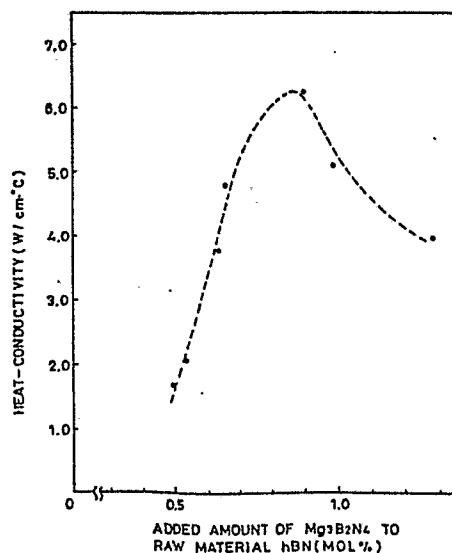
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⑯ Sintered body having high heat-conductivity and method of manufacturing thereof.

⑰ A sintered body of high heat-conductivity comprised of cubic system boron nitride is obtained by a process in which boron nitride of an alkaline earth metal or alkali metal in an amount of from 0.6 mol % to 1.2 mol % is uniformly diffused and held in a hexagonal system boron nitride body and the body is sintered at a high temperature of 1350°C and above under a thermodynamically stabilized condition of the cubic system boron nitride.

FIG. 2



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TITLE OF THE INVENTION

Sintered Body Having High Heat-Conductivity and
Method of Manufacturing Thereof

BACKGROUND OF THE INVENTION

5 The present invention relates to a sintered body having high heat-conductivity suitable for a heat sink material to be used for example in a semiconductor laser, a microwave device or an IC device, and a method of manufacturing of the above stated sintered body.

10 Description of the Prior Art

Cubic system boron nitride (hereinafter referred to simply as cBN) possesses hardness next to that of diamond and it has extremely excellent characteristics in thermal and chemical stability. Therefore, special interest has 15 been attracted toward cubic system boron nitride as the material for a working tool. In addition, cBN has high heat-conductivity also next to that of diamond and accordingly, it is expected to be used for purposes such as the material of a heat-radiation substrate.

20 As the material of a heat-radiation substrate, various materials having characteristics as shown in Table 1 have been used conventionally.

Table 1

Material	Characteristics			
	Heat Conductivity (at room temperature) W/cm ² ·°C	Thermal Expansion Coefficient (at room temperature to 400°C)	Permittivity (1 MHz at room temperature)	Resistivity (at room temperature) Ω·cm
SiC	2.7	3.7	45	10^{13}
BeO	2.6	7.6	6~8	10^{14}
AlN	0.6~1.6	4.0	8	10^{12}
Al_2O_3	0.2	6.7	8~10	10^{14}
Si	1.3	3.6	12	$10^{-3~3}$
Diamond	20	2.3	5.7	10^{16}

From Table 1, it is understood that diamond has extremely high heat-conductivity compared with other materials.

On the other side, Slack predicted in J. Phys. Chem. 5 Solids, Vol. 34 (1972) page 321 that pure single crystal cBN would have heat-conductivity as high as approximately 13 W/cm²·°C at room temperature and suggested the possibility of using it as the material of a radiation substrate.

10 However, large-sized cBN single crystal has not been obtained yet and accordingly, the heat-conductivity of 13 W/cm²·°C has not been confirmed.

In addition, the largest value reported up to the present as the heat-conductivity of a cBN sintered body containing a binding phase is only 2 W/cm.^oC. The reason for this is supposed to be that the binding phase acts as 5 an important factor of phonon scattering, causing the heat-conductivity to be lowered excessively.

Furthermore, as a method for manufacturing a high heat-conductivity cBN sintered body not containing a binding phase, U.S. Patent No. 4,188,194 issued on 10 February 12, 1980 for example discloses a method in which a high density cBN sintered body having high heat-conductivity is manufactured by a direct conversion process using pyrolysis type boron nitride (pBN) as the starting raw material.

15 However, in the method of the U.S. Patent No. 4,188,194, very high pressure and high temperature conditions of 7GPa and 2000°C or more respectively are required to manufacture a sintered body having heat-conductivity of 4 W/cm.^oC or more and there is also a 20 problem in reproducibility. In addition, pBN is a very expensive material.

On the other hand, a method for manufacturing a cBN sintered body not containing a binding phase under relatively mild conditions and at low cost is disclosed 25 for example in the paper by Wakatsuki et al. in Mat. Res.

Bull, Vol. 7 (1972) page 999, in which a cBN sintered body is obtained by a direct conversion process using hexagonal system boron nitride of low degree of crystallization.

However, the hBN of low degree of crystallization used as the starting raw material lacks chemical stability and is liable to react with the oxygen in the air, which makes it difficult to obtain a homogenous body uniformly and sufficiently sintered overall.

The inventors of the present application conducted 10 experiments on synthetic materials using various methods in order to manufacture a sintered body of high heat-conductivity at low cost and with good reproductivity. As a result, they found it most suitable to use methods as disclosed in USP 4,469,802 issued to 15 Endo et al. on September 4, 1984 where boron nitride of an alkaline earth metal or alkali metal is mixed or diffused and held in hBN and then the material is subjected to a high temperature of 1350°C or above under a thermodynamically stabilized pressure condition of cBN.

20 Although the method in this prior art intends primarily to provide a sintered body having good light-transmitting property, not to provide a sintered body having good heat-conductivity, a part or all of the added boro-nitride is diffused and removed out of the system in the above 25 stated method at the time of sintering under a high

pressure and in consequence, a sintered body comprised of substantially 100 % cBN can be easily obtained.

As a result of measuring the heat-conductivity of a sintered body obtained as described above, it was made 5 clear that the heat-conductivity of such a sintered body was a relatively high value of 2 to 3 W/cm·°C on the average compared with other sintered bodies using binding materials. However, it was also made clear that the heat-conductivity of such a sintered body was in some 10 cases as low as 1.7 W/cm·°C and thus the measured values were scattered in a rather wide range.

SUMMARY OF THE INVENTION

Therefore, an object of the present invention is to provide a sintered body of cBN having good 15 heat-conductivity which can be manufactured stably at low cost.

The inventors of the present application conducted many experiments under various conditions and as a result, they discovered that the heat-conductivity of a sintered 20 body depends not on the conditions of sintering but considerably on the composition of the material before it undergoes the sintering treatment, that is, the amount of addition of alkaline earth metal or alkali metal boron nitride to hBN. In addition, it was also made clear that 25 it is necessary to control the amount of addition of

alkaline earth metal or alkali metal boron nitride within a range of from 0.6 mol % to 1.2 mol %.

Accordingly, the present invention intends to provide a sintered body of high heat-conductivity comprised of substantially 100 % cubic system boron nitride and a method of manufacturing thereof, the above described sintered body of high heat-conductivity being obtained by uniformly diffusing boron nitride of an alkaline earth metal or alkali metal in an amount of from 0.6 to 1.2 mol % into hexagonal system boron nitride and then sintering the material at a temperature of 1350°C and above under a high pressure under a thermodynamically stabilized condition of the cubic system boron nitride.

These object and other objects, features, aspects and advantages of the present invention will become more apparent from the following detailed description of the present invention when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a graph showing a relation between the treatment temperature for diffusion of $Mg_3B_2N_4$ into a hBN body and the added amount of $Mg_3B_2N_4$.

Fig. 2 is a graph showing a relation between the heat-conductivity of a sintered body of the present

invention and the added amount of $Mg_3B_2N_4$ into the hBN as the raw material.

Fig. 3 is a graph showing a relation between the unit particle diameter of a sintered body of the present invention and the added amount of $Mg_3B_2N_4$ into the hBN as the raw material.

Fig. 4 is a graph showing a relation between the Vicker's hardness of a sintered body of the present invention and the heat-conductivity thereof.

Figs. 5A and 5B are respectively plane and side sectional views showing an IC device where the first example of a heat sink in accordance with the present invention is applied.

Figs. 6A and 6B are respectively plane and side sectional views of an IC device where the second example of a heat sink in accordance with the present invention is applied.

Figs. 7A and 7B are respectively plane and side sectional views of an IC device where the third example of a heat sink in accordance with the present invention is applied.

Figs. 8A and 8B are respectively plane and side sectional views of an IC device where the fourth example of a heat sink in accordance with the present invention is applied.

Figs. 9A and 9B are respectively plane and side sectional views of an IC device where the fifth example of a heat sink in accordance with the present invention is applied.

5 Figs. 10A and 10B are respectively plane and side sectional views of an IC device where the sixth example of a heat sink in accordance with the present invention is applied.

10 Figs. 11A and 11B are respectively plane and side sectional views of an IC device where the seventh example of a heat sink in accordance with the present invention is applied.

15 Figs. 12A and 12B are respectively plane and side sectional views of an IC device where the eighth example of a heat sink in accordance with the present invention is applied.

Fig. 13 is a partial front section for explaining the process for manufacturing the heat sink of the eighth example.

20 DETAILED DESCRIPTION OF THE INVENTION

The present invention will be specifically described in the following in connection with a case in which hot-pressed hBN body is used as the raw material and magnesium boron nitride ($Mg_3B_2N_4$) is used as an additive.

First, an amount of adding $Mg_3B_2N_4$ was added to the hBN with the temperature condition being changed and thus, a relation as shown in Fig. 1 was established between the treatment temperature and the added amount to $Mg_3B_2N_4$.

5 Then, based on the result shown in Fig. 1, several materials containing different amounts of addition of $Mg_3B_2N_4$ were prepared and were subjected respectively to a treatment under prescribed temperature and pressure conditions, whereby sintered bodies were obtained 10 respectively. The heat-conductivity of each of the thus obtained sintered bodies was measured and a relation thereof with the added amount of $Mg_3B_2N_4$ to the material was examined. Fig. 2 shows the results.

From Fig. 2, it can be seen that in the case of the 15 added amount of $Mg_3B_2N_4$ less than approximately 0.8 mol %, the heat-conductivity becomes high according to the increase of the added amount of $Mg_3B_2N_4$. This is suppose to be due to the fact that as the added amount of $Mg_3B_2N_4$ increase, the unit particle diameter of cBN becomes large 20 to decrease phonon scattering in the particle boundary, which results in the heat-conductivity being high. Fig. 3 shows a relation between the added amount of $Mg_3B_2N_4$ and an average unit particle diameter of an obtained sintered body. From Fig. 3, it can be understood that the particle

diameter becomes large according to the increase of the added amount of $Mg_3B_2N_4$.

However, from Fig. 2, it can be seen that the heat-conductivity has the maximum value $6.2 \text{ W/cm} \cdot ^\circ\text{C}$ with 5 the added amount of $Mg_3B_2N_4$ being about 0.9 mol % and it is lowered reversely with the added amount of $Mg_3B_2N_4$ being more than 0.9 mol %. If $Mg_3B_2N_4$ is added in an amount of more than 0.9 mol %, the obtained sintered body contains Mg or more than 0.5 % by weight. This remaining 10 Mg is considered to act as a determining cause of phonon scattering, causing the heat conductivity to be lowered.

Fig. 4 shows a relation between the heat-conductivity of the respective sintered bodies synthesized with the added amount of $Mg_3B_2N_4$ being changed and the Vickers 15 hardness thereof. It can be seen from Fig. 1 that a sintered body having heat-conductivity in a rage from 2 to 3 $\text{W/cm} \cdot ^\circ\text{C}$ has hardness partially lowered and the sintered state thereof is not uniform. It is supposed that in the portion where the sintered state is not good, that is, in 20 the portion where the hardness is lowered, phonon scattering in the particle boundary develops conspicuously on account of insufficient bonding of particles and as a result, the sintered body as a whole has a relatively low value of heat-conductivity. On the other hand, a sintered 25 body having uniform hardness of 5000 kg/mm^2 or more

possesses heat-conductivity 4 W/cm·°C or above. From the relation between the added amount of $Mg_3B_2N_4$ and the heat-conductivity shown in Fig. 2, it is understood that a sintered body having high heat-conductivity of 4 W/cm·°C 5 or above can be stably obtained with the added amount of $Mg_3B_2N_4$ being in a range from 0.6 mol % to 1.2 mol %.

Furthermore, the inventors of the present application also discovered that in a CBN sintered body, (a) the volume ratio of the cubic system boron nitride in the 10 sintered body, (b) the lattice constant of the boron nitride in the sintered body and (c) the proportion of substantial continuity with the adjoining particle of the cubic system boron nitride particle surface contribute to the heat-conductivity. More specifically, as a result of 15 measuring heat conductivity with the volume ratio of the cubic system boron nitride in a sintered body being changed from 60 % to 100 %, it was found that the heat-conductivity of a sintered body having a volume ratio of 95 % or more becomes remarkably high and any sintered 20 body having a volume ratio of 98 % or more has heat-conductivity of 4 W/(cm·°C) or above. Accordingly, the volume ratio of the CBN in the CBN sintered body is preferably 98 % or more.

In addition, the sintering conditions were selected 25 so that the lattice constant of the cubic system boron

nitride may be changed from 3.608 \AA to 3.630 \AA , and under those conditions, the heat-conductivity was measured. As the result, the maximum value of the heat-conductivity was exhibited in the vicinity of 3.615 \AA and high values of heat-conductivity of $4.0 \text{ W}/(\text{cm} \cdot ^\circ\text{C})$ and above were shown in a range from 3.610 \AA to 3.625 \AA . Accordingly, the lattice constant of the cBN in the cBN sintered body is preferable in a range from 3.610 \AA to 3.625 \AA . This is because a deviation from the stoichiometrical BN would increase lattice defects to cause phonon scattering. In such case, if the amount of nitrogen is small, the lattice constant would be increased.

The inventors of the present application manufactured sintered bodies with the sintered conditions being changed and the binding state of the cubic system boron nitride particle was observed by wrapping the sintered bodies thus obtained. Then, the heat-conductivity values of those sintered bodies were measured and it was made clear that a sintered body having substantial continuity of 60 % or more with the adjoining particles has a high value of heat-conductivity of $4.0 \text{ W}/(\text{cm} \cdot ^\circ\text{C})$ or above. The reason for this is considered to be that the influence of phonon scattering in the particle boundary contributes to the heat-conductivity.

According to the present invention, a cBN sintered body obtained as described above exhibits heat-conductivity as high as $4.0 \text{ W}/(\text{cm} \cdot ^\circ\text{C})$ and above and consequently, it becomes possible to provide a heat sink 5 of an excellent quality for use in an electronic device.

A sintered body having heat-conductivity of $4 \text{ W}/\text{cm} \cdot ^\circ\text{C}$ or above has a particle diameter of $5 \mu\text{m}$ or more, a Vickers hardness of $5000 \text{ kg}/\text{mm}^2$ or more and a content of Mg of 0.5 % by weight or less. This means that from the 10 hardness and the impurity content, to the contrary, the heat-conductivity of the sintered body can be known.

(Embodiments)

Example 1

As raw materials were used hBN bodies obtained by 15 forming hBN powder with hot-press method or CIP(cold isostatic pressurizing). The hBN bodies obtained were held in N_2 gas at $2000\sim 2100^\circ\text{C}$ for 4 hours to highly purify them. Impurities contained in the hBN bodies were not more than 0.05 % by weight of O_2 , not more than 0.02 % by 20 weight of carbon and not more than 200 ppm of metal impurities such as Fe, Ca or the like, and the density of the hBN bodies were in a range of $1.75\sim 1.85 \text{ g}/\text{cm}^3$.

Under the normal pressure in a nitrogen atmosphere at various temperature in a range from 1160 to 1175°C , Mg_3N_2 25 was diffused and contained in the hBN of high purity

described above and eight specimens having different amounts of $Mg_3B_2N_4$ in a range from 0.4 to 1.3 mol % were obtained as a result of reaction in the hBN body. These specimens were respectively put in recipients and subjected 5 to the conditions of 5.5 GPa and 1450°C for 30 minutes using a belt-type device.

The obtained sintered bodies were monophase high-density sintered bodies each having a diameter of 30 mm and a thickness of approximately 1.5 mm. In the 10 sintered body of specimen 1, the hBN not converted were remaining partially, while the other specimens appeared to be in a homogeneously and strongly sintered state over the whole surface. In consequence, it is understood that for 100 % conversion to cBN, the amount of $Mg_3B_2N_4$ added 15 to the raw material hBN body is required to be approximately 0.45 mol % or more.

From the sintered bodies of specimens 2 to 8, pieces of 2.5 x 2.5 x 1.5 mm were extracted respectively and the heat-conductivity of each piece was measured at room 20 temperature by a direct measuring method using an InSb infrared radiation microscope. The results obtained were shown in Table 2 below.

Table 2

Specimen No.	Added Amount	Appearance of Sintered Body	Heat-conductivity
1	0.439 mol %	gray and not transparent	not measured (partially white)
2	0.498 mol %	gray and not transparent	1.7 W/cm·°C
3	0.544 mol %	gray and not transparent	2.1 W/cm·°C
4	0.639 mol %	green and semi-transparent	3.8 W/cm·°C
5	0.665 mol %	bluish green and semi-transparent	4.8 W/cm·°C
6	0.909 mol %	bluish green and semi-transparent	6.2 W/cm·°C
7	0.995 mol %	brown and semi-transparent	5.1 W/cm·°C
8	1.291 mol %	brown and semi-transparent	4.0 W/cm·°C

It is understood from Table 2 that a sintered body obtained with the added amount of $Mg_3B_2N_4$ to the material hBN body being in a range from 0.6 mol % to 1.2 mol % has heat-conductivity of approximately 4 W/cm·°C or above.

5 Example 2

For the purpose of examining the characteristics required for a sintered body of the heat-conductivity, the particle diameter, the hardness and the impurity content of each of the specimens 2 to 8 obtained in the example 1 10 were measured.

The particle diameter was measured by a scanning type electronic microscope (SEM) after the surface of each

specimen was etched with KOH to make clear the particle boundaries.

The hardness was examined by using a Vicker's penetrator under the load of 10 kg for 15 seconds.

5 The content of impurity, that is the content of Mg was measured by using an ion microanalyzer.

The results are shown in Table 3.

Table 3

Sepeimen No. No.	Particle Diameter (μm)	Vickers Hardness (kg/mm ²)	Mg content (% by weight)
2	2~10	2900~6300	< 0.1
3	2~12	4100~6100	< 0.1
4	5~12	5300~6100	0.1
5	7~15	6100~7100	0.1
6	10~17	5300~6100	0.3
7	12~20	5000~6100	0.5
8	12~27	6100~6900	0.7

10 Impurities other than Mg were analized by using an ion microanalyzer for each specimen and C, Al, Ca and Si were detected, the amount of each of them being less than 200 ppm.

From the example 1 and the results shown in Table 3, it is understood that a sintered body having heat-conductivity of $4\text{W}/\text{cm}\cdot^{\circ}\text{C}$ or above has a unit particle diameter of $5\mu\text{m}$ or more, Vickers hardness of $5000\text{ kg}/\text{mm}^2$ or more and the Mg content of 0.5 % by weight or less.

Example 3

Instead of the $\text{Mg}_3\text{B}_2\text{N}_4$ in the example 1, Li_3BN_2 , $\text{Ca}_3\text{B}_2\text{N}_4$ and $\text{Sr}_3\text{B}_2\text{N}_4$ were respectively diffused and contained in an amount of from 0.6 to 1.2 mol % in the hBN and sintered bodies were obtained in the same manner as in the example 1. In all of the sintered bodies thus obtained, the heat-conductivity was $4\text{W}/\text{cm}\cdot^{\circ}\text{C}$ or above and the particle diameter, the hardness and the impurity content were almost the same as the results of the example 15 2.

Example 4

hBN bodies containing 0.8~0.9 mol % of $\text{Mg}_3\text{B}_2\text{N}_4$ were obtained in the same manner as in the Example 1. After that, the body was put in a recipient and using a 20 belt-type device, six sintered bodies were formed under the conditions of 55 kw and 1400°C , with the holding time being changed. The proportions of transformation to cubic system boron nitride in the obtained sintered bodies were respectively 60 %, 80 %, 90 %, 95 %, 98 % and 100 %. The

remaining portions were compounds of the hexagonal system boron nitride not transformed and the catalyst.

The heat-conductivity of each of the above stated sintered bodies was measured and the results are shown in 5 Table 4 below.

From Table 4, it is understood that a sintered body having a volume ratio of cubic system boron nitride of 98 % or more has heat-conductivity as high as 4.0 W/(cm·°C) or above.

Table 4

Items No.	1	2	3	4	5	6
Sintering Pressure	55kb	→	→	→	→	→
Sintering Temperature	1400°C	→	→	→	→	→
Holding Time	2min.	5min.	10min.	15min.	20min.	30min.
Transformation Ratio	60 %	80 %	90 %	95 %	98 %	100 %
Heat-Conductivity	0.2	0.4	0.9	1.8	4.1	5.5

10 Example 5

As a raw material, a hexagonal system boron nitride body containing uniformly dispersed 0.8 0.9 mol % of $Mg_3B_2N_4$ was prepared, and the material thus prepared was put in a recipient of Mo. Then, it was subjected to

treatment under the conditions of 57 kb and 1450°C with the temperature being raised by two steps and sintered bodies were obtained. By changing the holding time in the first step, the lattice constants of the cubic system 5 boron nitride of the sintered bodies were made different.

Table 5 shows the results of measurement of the heat-conductivity values of the these sintered bodies.

From Table 5, it is understood that a high value of heat-conductivity of 4.0 W/(cm·°C) or above was exhibited 10 with the lattice constant of the cubic system boron nitride being in a range from 3.610 Å to 3.625 Å.

It is to be noted that the sintering time shown in Table 5 was 20 minutes in each case.

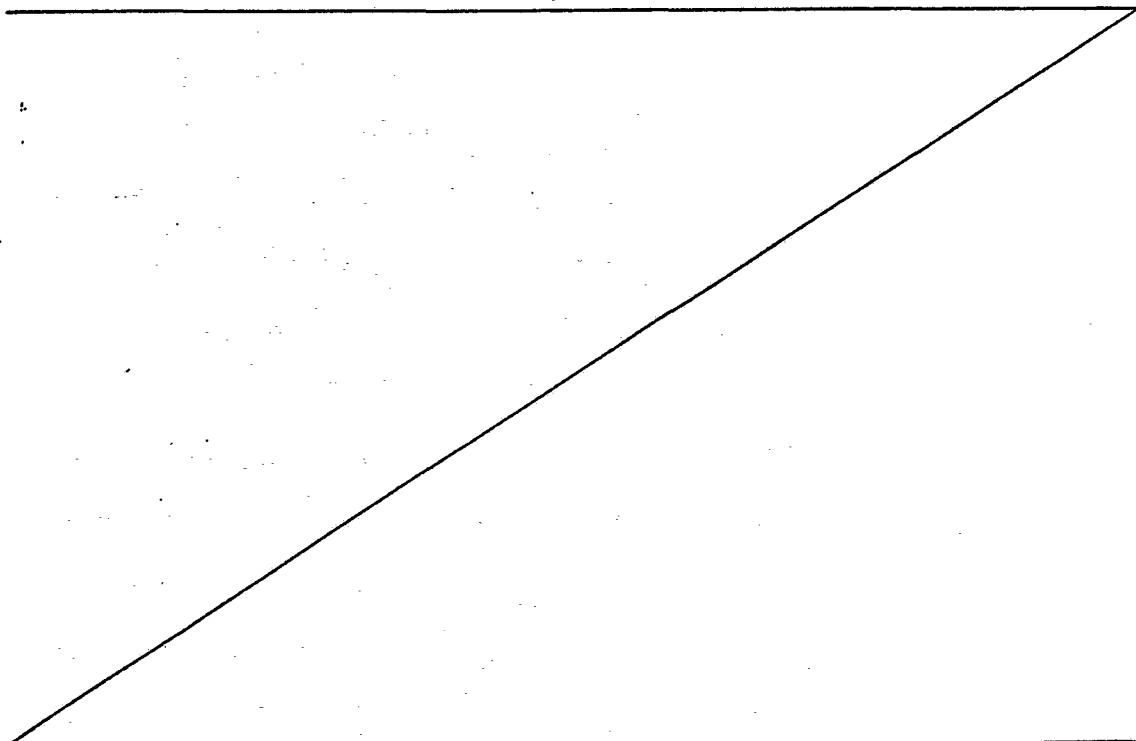


Table 5

Items	Specimen No.				
	1	2	3	4	5
Sintering Pressure	57kb	→	→	→	→
Sintering Temperature (in the second step)	1450°C	→	→	→	→
Raised Temperature in the first step	1250°C	→	→	→	→
Holding Time in the first step	1 min.	10 min.	20 min.	40 min.	60 min.
Lattice Constant Å	3.630	3.624	3.617	3.613	3.608
Heat-Conductivity W/cm.°C	2.0	4.3	5.9	6.0	3.4

Example 6

As a material, a hexagonal system boron nitride body containing uniformly dispersed 0.8~0.9 mol % of $Mg_3B_2N_4$ was prepared and this material was put in a recipient.

5 Then, using a belt-type device, the temperature was raised by two steps under the conditions of 55 kb and 1450°C, whereby sintered bodies were formed with the holding time in the second step being changed in this example. The sintered bodies thus obtained were wrapped with fine powder

10 of diamond and then, particle boundary was checked by using a scanning type electronic microscope. As a result, it was ascertained that the hexagonal system boron nitride

particles were substantially continuous with the surrounding adjacent particles and no particle boundary was observed.

In addition, a relation between an average value of 5 the surface proportion of continuity and the heat-conductivity was examined and the result is shown in Table 6 below.

Table 6

Items	Specimen No.				
	1	2	3	4	5
Proportion of continuity	40 %	50 %	60 %	80 %	85 %
Heat-conductivity W/cm·°C	2.3	2.9	4.0	4.5	6.1

As described previously, U.S. Patent No. 4,188,194 discloses a metallization technique in which the surface 10 of cubic system boron nitride is coated with Ni by sputtering and further coated with silver. However, such coating film has disadvantages that the adhesion to the cubic system boron nitride sintered body is insufficient and accordingly, they are liable to be detached at the 15 time of inserting the heat sink in a cooper substrate. By contrast, in a heat sink using a CBN sintered body of the

present invention, the above stated disadvantages have been dissolved and coating films having an excellent adhesion property can be provided. More specifically, a sintered body of the present invention may be provided 5 with on its surface, coating layers of one or more transition metals of the groups IVa, Va and VIa of the periodic table or the alloys thereof. In this case, boride, nitride or boron nitride of such metals is formed in the interface, which makes it possible to remarkable 10 increase the adhesion intensity of the coating films.

In addition, in the present invention, one or more coating layers of metals not oxidized at a temperature of 300°C or alloys thereof may be provided for purpose of preventing oxidation of the metal of the coating films. 15 As the metals not oxidized at a temperature of 300°C, Au, Ag, Cu, Pt, Al, Ni, Co and the like are preferred. The temperature of 300°C is based on the fact that the maximum temperature necessary for adhesion between a semiconductor device and lead wires, between the semiconductor device 20 and the sink, and between the heat sink and the substrate is approximately 300°C.

Example 7

The sintered body of specimen 4 in the example 5 was cut into 20 pieces each having a size of 1 mm² and 0.4 mm 25 thickness. After that, those pieces were heated to a high

temperature and Ti was coated to a thickness of 500 Å on the surface of each piece. Subsequently, was further coated to a thickness of 1 μ m on the Ti coating layer. Then, a semiconductor laser device was soldered on each 5 sintered body thus formed and leads were connected.

For comparison, a BeO body was cut into 20 pieces each having the same size as described above and in the same manner, coating was applied and semiconductor laser devices of the same kind were placed.

10 When electric current of 150 mA was made to flow, the surface temperature of each device was measured. As a result, it was observed that the temperature of the devices each provided with a heat sink comprising a cubic system boron nitride sintered body in accordance with the 15 present invention was lowered by approximately 15°C.

In addition, in a scratching test using a sapphire needle, some of the coating films of the heat sinks of BeO were detached, while the coating films on the sintered bodies, in accordance with the present invention were not 20 detached.

Furthermore, the face of contact between cBN sintered body and a coating film was examined by a TEM and there was found titanium borid.

Example 8

The sintered body of specimen 5 in the example 5 was cut into four pieces each having a size of 100 mm² and 0.5 mm in thickness. Then, those pieces were heated and Cr was coated on the surface of each piece and Ni and Ag 5 were further coated thereon. Each of the sintered bodies containing the coating films thus formed was attached to an IC substrate. As a result, it was observed that the IC operated more stably and the lifetime of the IC became remarkably long.

10 Now, in the following, a concrete structure of a heat sink for an IC using a sintered body in accordance with the present invention will be described.

In the below described case, for the purpose of improving the heat-radiation property, a sintered body is 15 shaped such that the area of the outer surface of the sintered body may be relatively larger than the surface thereof facing the semiconductor device. For the shaping, the following three manners are considered.

(a) The surface area of the heat sink on the side of an 20 envelope is made larger than the area of the portion of the heat sink contacting the IC device so that the heat content per unit area is lowered on the side of the envelope. Thus, the temperature of the heat sink material can be made close to the temperature of the external

atmosphere and accordingly, the temperature of the IC device can be lowered effectively.

(b) the surface area of the heat sink in the portion contacting the external gas or liquid is made large so 5 that the heat conduction to the exterior is improved.

(c) Radiation fins are provided in the portion of the heat sink contacting the external gas or liquid so that the heat radiation property is further improved.

The above described heat sink uses a CBN sintered 10 body having excellent heat-conductivity and is shaped such that the area of the outer surface thereof is relatively large compared with the surface thereof on the side facing the semiconductor device and in consequence, heat can be emitted efficiently from the inside of the device to the 15 exterior not only because of the good heat-conductivity of the material itself but also because of its structure.

Figs. 5A and 5B are respectively plane and side 20 sectional views of the first example of a heat sink in accordance with the present invention. Referring to Figs. 5A and 5B, a Si device or a compound semiconductor 2 as an IC devie is disposed in an envelope 1 and input and output pins 4 are provided through leads 3 connected to the Si device 2.

On the other hand, in the envelope 1 on the side of 25 the Si device 2, a tapered opening is formed, the diameter

thereof being small on the inner side and being increased toward the outer surface of the envelope 1. In the opening, a heat sink 5 for IC device in accordance with an embodiment of the present invention is placed. As is 5 clear from Fig. 5B, the heat sink 5 has a form corresponding to the tapered opening and accordingly the surface area thereof on the side of the Si device 2 as the semiconductor device is small and the surface of area thereof on the outer side of the envelope 1, that is on 10 the side contacting the external atmosphere is increased. Thus, as described previously, the heat content per unit area of the heat sink is smaller on the outer side than on the side of the Si device 2 and radiation of heat can be 15 made more efficiently.

15 Figs. 6A and 6B are respectively plane and side sectional views of an IC device where the second example of a heat sink in accordance with the present invention is applied. In this example, the envelope 1 and the heat sink 5 are formed in the direction in which the input and 20 output pins 4 extend. The other portions are the same as in the example shown in Figs. 5A and 5B. Accordingly, it is understood that heat is radiated efficiently also in the heat sink 5 of this example.

25 Figs. 7A and 7B are respectively plane and side sectional views of an IC device where the third example of

a heat sink in accordance with the the present invention is applied. In this third example, a through hole not tapered is formed in the envelope and the heat sink 5 for IC is placed in the through hole. However, the heat sink 5 in this example extends on the outer side of the envelope 1 over a range wider than the diameter of the through hole. More specifically, the heat sink 5 is provided over an area larger than the opening area so as to be in contact with the outer surface of the envelope 1.

Accordingly, also in this example, in the same manner as in the example shown in Figs. 5A and 5B, the surface area of the heat sink 5 on the external side is made larger than that on the side of the Si device 2 and the same radiation effect can be obtained.

Figs. 8A and 8B are respectively plane and side sectional views of a device where the fourth example of a heat sink in accordance with the present invention is applied. In this fourth example, in the same manner as in the heat sink 5 of the example shown in Figs. 6A and 6B, the envelope 1 and the heat sink 5 for IC are provided in the direction in which the input and output pins 4 extend. The structure of the envelope 1 and heat sink 5 are the same as those in the third example shown in Figs. 7A and 7B and therefore, the same effect can be obtained.

Figs. 9A and 9B are plane and side sectional views of a device where the fifth example of a heat sink in accordance with the present invention is applied. In this fifth example, radiation fins 6 are formed on the external 5 side of the heat sink 5. The other portions are the same as in the example shown in Figs. 7A and 7B. It is understood that the example shown in Figs. 9A and 9B has more excellent radiation characteristic compared with the third example since the radiation fins 6 are provided in 10 this fifth example.

The form of the radiation fins 6 is not limited to that shown in Figs. 9A and 9B. They may have any suitable form as shown in the sixth to eighth examples in Figs. 10A-10B, 11A-11B and 12A-12B. In any of the forms, the 15 area of the fins 6 can be made larger than the outer surface area of the heat sink 5 and accordingly, the heat radiation characteristic can be further improved.

Now, an example of a method of manufacturing a heat sink for IC in accordance with the present invention will 20 be described with reference to the partial front sectional views of Fig. 13. As shown in Fig. 13, in a girdle-type extra-high pressure generating apparatus, cBN bodies 11 containing diffused magnesium boron nitride are disposed respectively between the ultra-hard alloy plates 12 and 25 the Mo plates 13 of 0.1 mm in thickness shaped according

to the form of the radiation fins so that a multilayer structure is formed. The thus formed multilayer structure is placed in a recipient 14 of Mo. Then, under the pressure of 55 kb, the Mo recipient 14 is heated at a 5 temperature of 1450°C for 30 minutes. After that, the sintered bodies 11 are taken out from the Mo recipient 14. In advance, the respective surfaces of the Mo plates 13 disposed between the respective sintered bodies 11 have been coated with a peeling agent so that the multilayer 10 sintered bodies 11 may be easily separated from one another. Therefore, the sintered bodies 11 thus taken out are separated with the Mo plates 13 being attached thereto. The Mo plate 13 attached to the surface of each sintered body 11 is removed for example by treatment using 15 acid such as nitric acid, whereby the same form as that of the radiation fins 6 of the heat sink 5 in the example shown in Figs. 12A and 12B can be obtained.

On the face portion of contact between the thus obtained sintered body 11 and the IC device, a multilayer 20 coating film of Ti and Ni and Au is formed and this coating film is soldered by Au-Sn to the IC logic device, so that the structure thus formed is fixed to the envelope. Thus, the IC device shown in Figs. 12A and 12B can be obtained. For comparison, an IC device as shown in 25 Figs. 12A and 12B was manufactured using a heat sink of

BeO and the performances of the heat sinks of both IC devices were tested. In this test, the same electric power and the same electric current were applied and the temperatures on the surface of the envelopes of both IC 5 devices were measured. As a result, it was ascertained that the device using the heat sink of the present invention had a lower temperature and exhibited a more excellent characteristic when it was operated.

Although the present invention has been described and 10 illustrated in detail, it is clearly understood that the same is by way of illustration and example only and is not to be taken by way of limitation, the spirit and scope of the present invention being limited only by the terms of the appended claims.

WHAT IS CLAIMED IS:

1. A sintered body having high heat-conductivity comprised of substantially 100 % cubic system boron nitride (cBN), said sintered body being obtained by uniformly diffusing boron nitride of an alkaline earth metal or alkali metal in an amount of from 0.6 mol % to 5 1.2 mol % in a body of hexagonal system boron nitride and applying a sintering treatment to said body by a high pressure at a temperature of 1350°C and above under a thermodynamically stabilized condition of the cubic system 10 boron nitride, the heat-conductivity of said sintered body being 4 W/(cm·°C) and above at room temperature.
2. A sintered body having high heat-conductivity in accordance with claim 1, wherein said sintered body comprised of cubic system boron nitride contains cBN of 98 % by volume or more.
3. A sintered body having high heat-conductivity in accordance with claim 1, wherein an average unit particle diameter of said sintered body is 5 μm or more.

4. A sintered body having high heat-conductivity in accordance with claim 1, wherein the Vickers hardness of said sintered body is 5000 kg/mm² or more.
5. A sintered body having high heat-conductivity in accordance with claim 1, wherein the content of impurity in said sintered body is 0.5 % by weight or less.
6. A sintered body having high heat-conductivity in accordance with claim 1, wherein the lattice constant of the cBN in said sintered body comprised of cubic system boron nitride is in a range from 3.610 Å to 3.625 Å.
7. A heat sink using a sintered body having high heat-conductivity in accordance with claim 1.
8. A heat sink in accordance with claim 7, wherein a coating layer of 1μm or less comprised of one or more kinds of transition metal belonging to the groups IVa, Va and VIa of the periodic table or the alloys thereof is formed on the surface of said sintered body having high heat-conductivity, and on the face of contact between said sintered body of cBN and said coating layer, boride, nitride or

(continued)

10 boro-nitride is formed by reaction between the metal of
said coating layer and the cBN.

9. A heat sink in accordance with claim 8, wherein
one or more second coating layers comprised of a material
selected from the group consisting of Au, Ag, Cu, Pt, Al,
Ni and Co or the alloys thereof are further formed on the
5 outer surface of said coating layer.

10. A heat sink in accordance with claim 7, wherein
a coating layer comprised of copper or a copper alloy is
formed on the surface of said cBN sintered body.

11. A heat sink in accordance with claim 7 for use
as a heat sink for an intergrated circuit device, wherein
said heat sink is formed such that the area of the outer
surface thereof is relatively large as compared with
5 another surface thereof facing a semiconductor device.

12. A heat sink in accordance with claim 11 for use
as a heat sink for an intergrated circuit device, wherein
radiation fins are formed on said outer surface of said
heat sink.

13. A method of manufacturing of a sintered body having high heat-conductivity comprising the steps of: uniformly diffusing boron nitride of an alkaline earth metal or alkali metal in an amount of from 0.6 mol % to 1.2 mol % in a body of hexagonal system boron nitride and

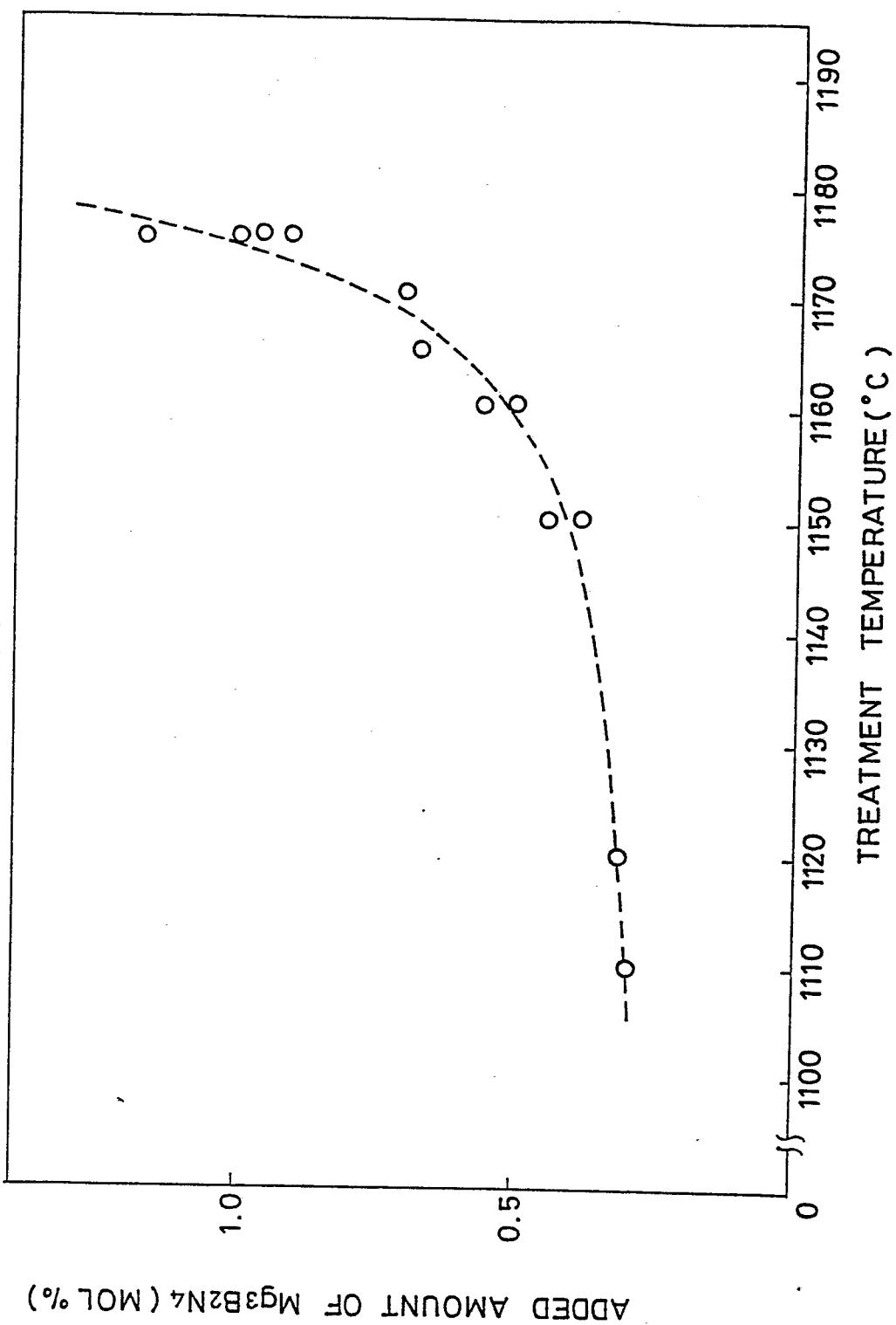
5 sintering said hexagonal system boron nitride body under a high pressure at a temperature of 1350°C and above under a thermodynamically stabilized condition of the

10 cubic system boron nitride.

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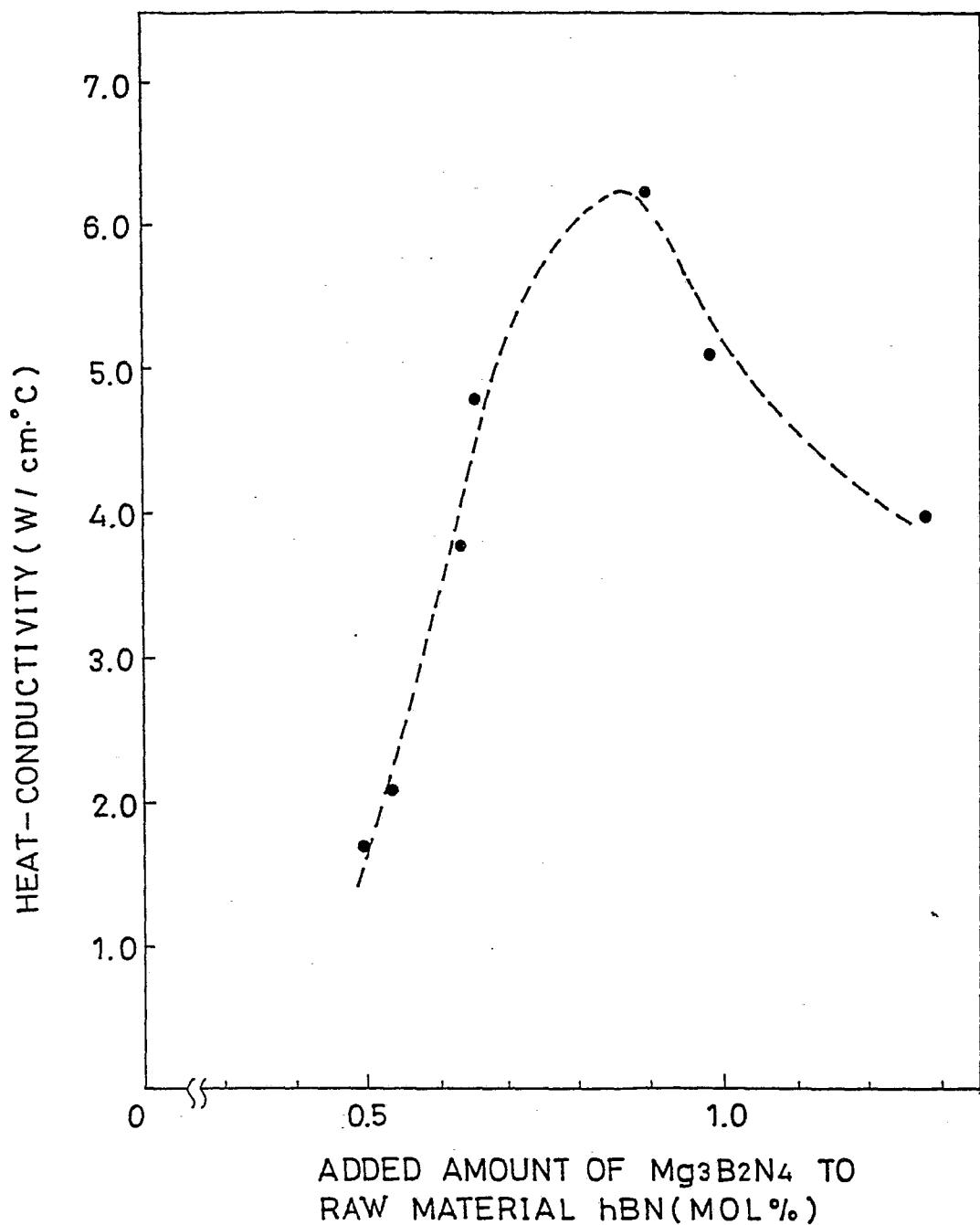
FIG. 1



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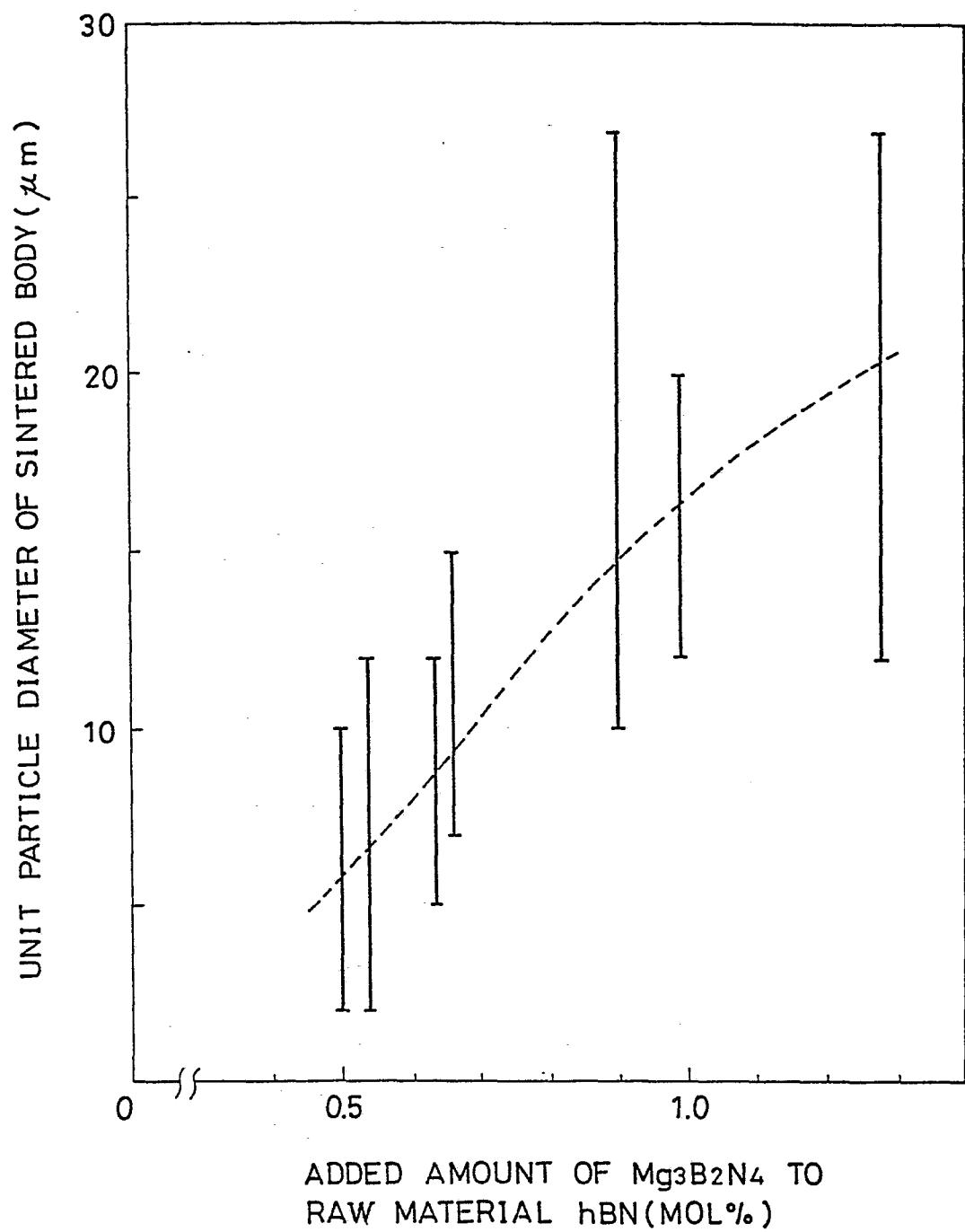
FIG. 2



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FIG. 3



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FIG. 4

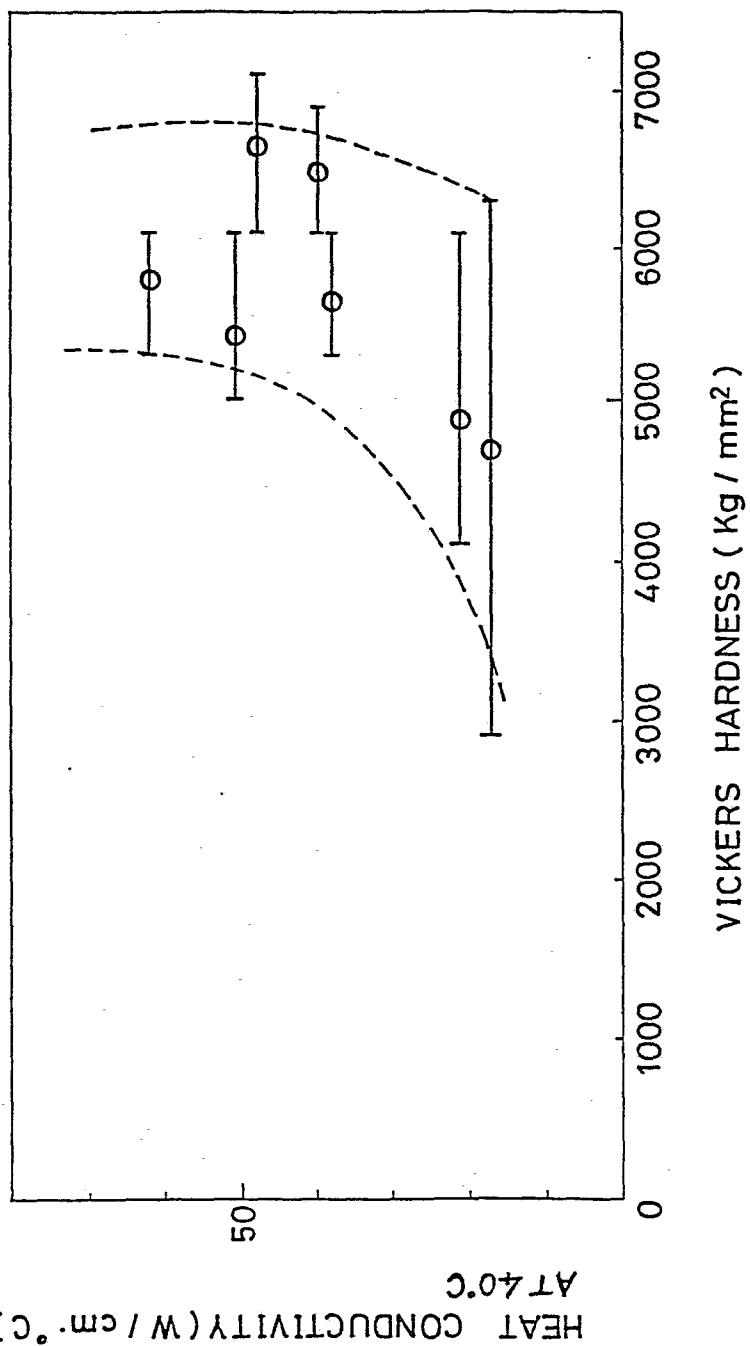


FIG. 5A

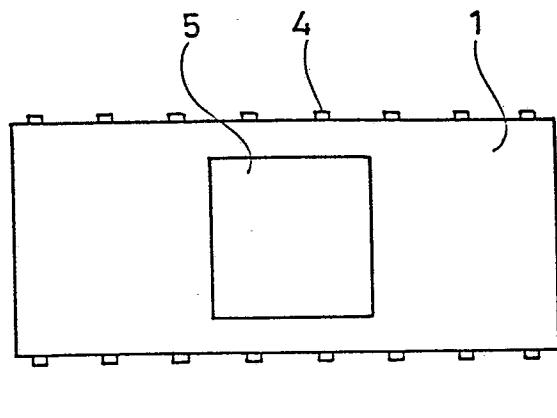


FIG. 5B

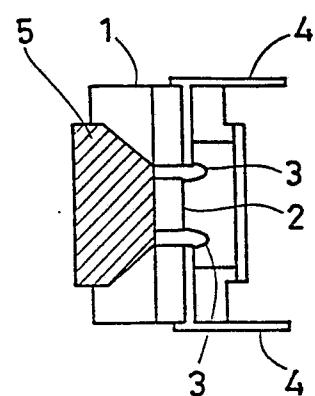


FIG. 6A

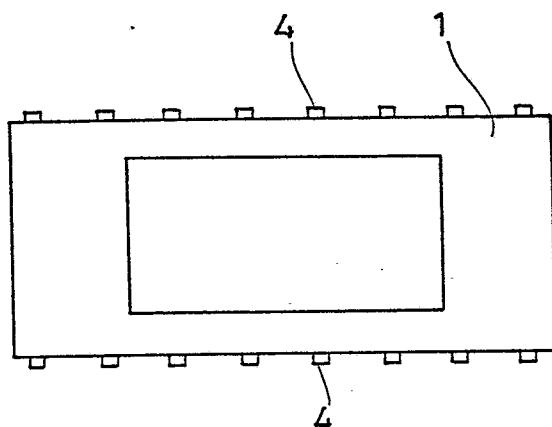


FIG. 6B

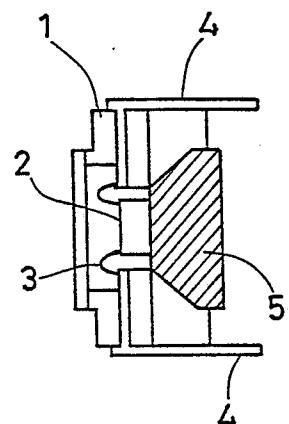


FIG. 7A

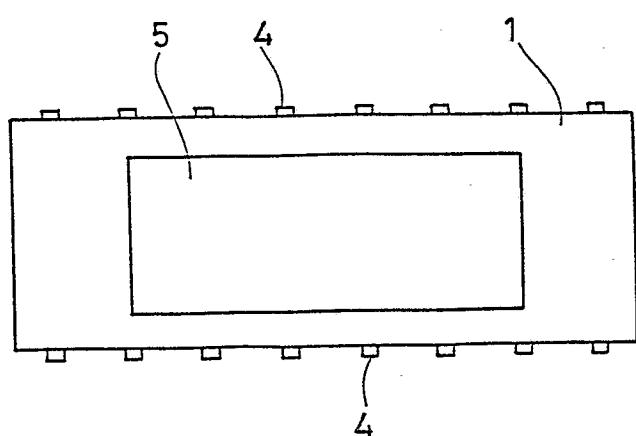


FIG. 7B

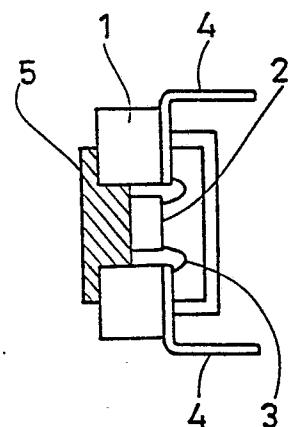


FIG. 8A

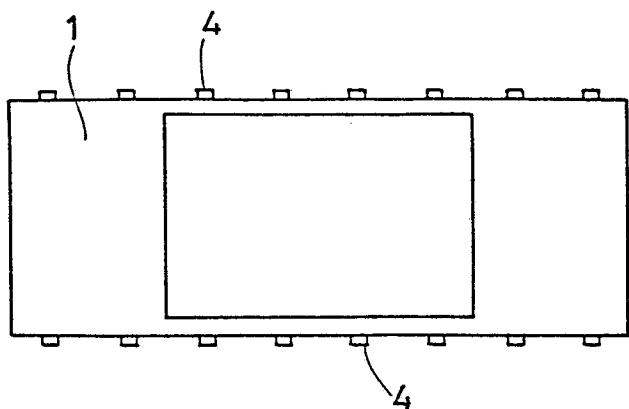


FIG. 8B

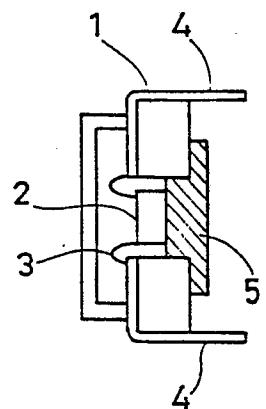


FIG. 9A

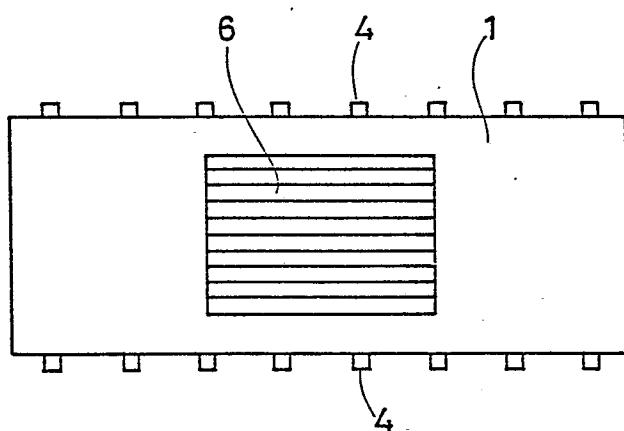


FIG. 9B

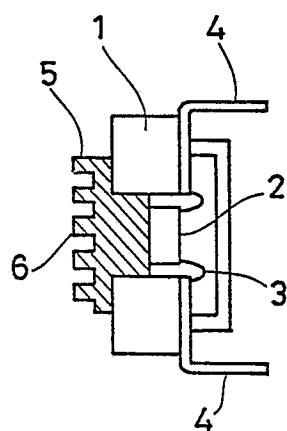


FIG. 10A

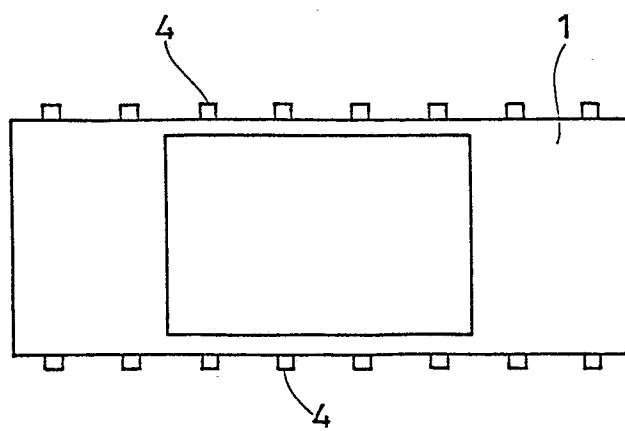


FIG. 10B

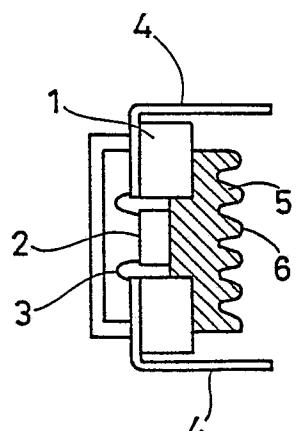


FIG. 11A

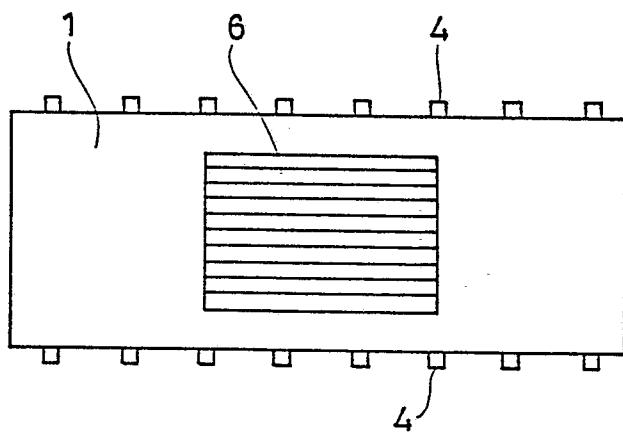


FIG. 11B

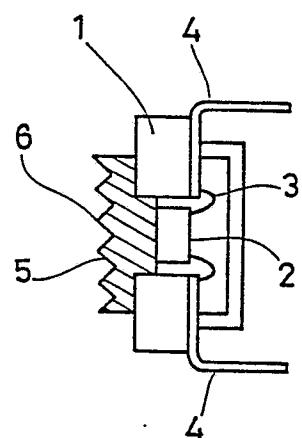


FIG. 12A

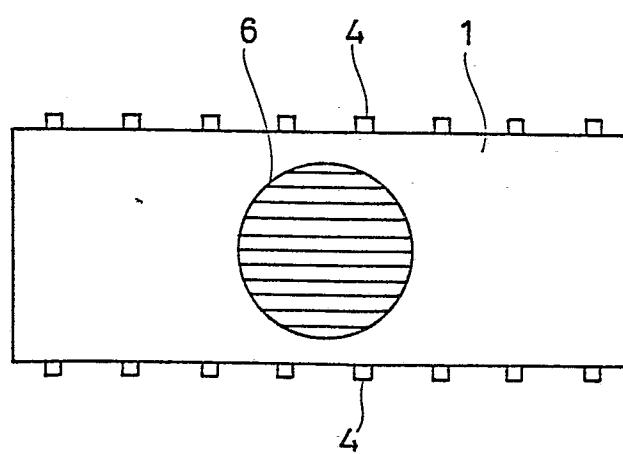
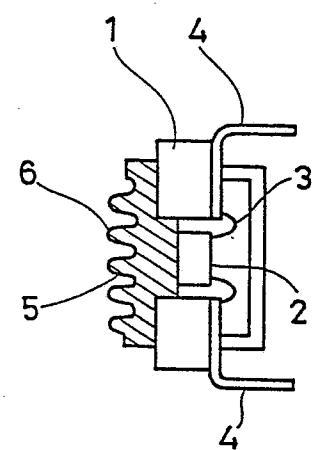


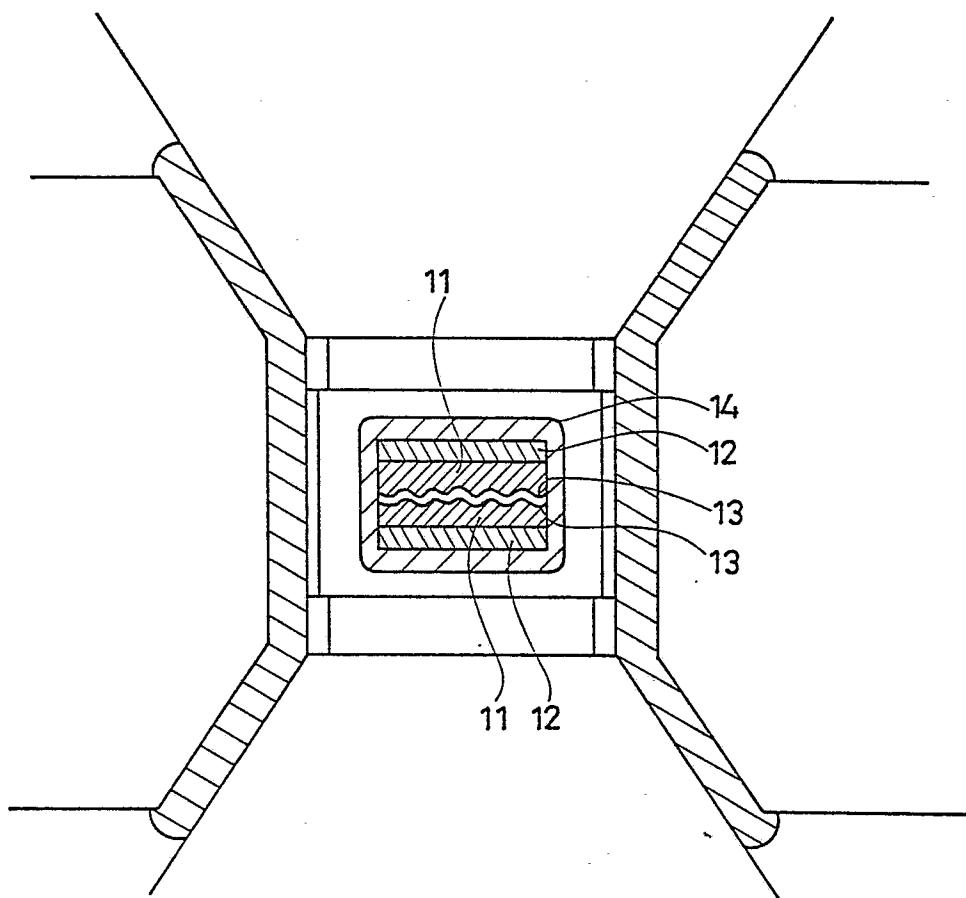
FIG. 12B



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FIG. 13





EUROPEAN SEARCH REPORT

0194358
Application number

EP 85 11 6660

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int Cl 4)
D, Y	US-A-4 469 802 (T. ENDO et al.) * whole document *	1-5, 13	C 04 B 35/58 C 04 B 41/90 H 01 L 23/36
Y	--- FR-A-2 395 948 (GENERAL ELECTRIC CO.) * claims 1, 9, 12, 14, 15, 19; figure 18; page 37, lines 21-33 *	1-5, 7-9, 11, 13	
Y	--- FR-A-2 344 642 (THOMSON-CSF) * claims 1, 6, 7; page 1, lines 1-12; page 3, line 32 - page 4, line 9 *	7-9	
A	* claim 6 *	10	
A	--- GB-A-2 051 474 (AEI SEMICONDUCTORS LTD.) * whole document *	7-10, 12	
Y	--- EP-A-0 019 003 (FUJITSU LTD.) * figure 4; abstract; page 9 *	11	C 04 B 35/58 C 04 B 41/88 C 04 B 41/90 H 01 L 23/36
A	* pages 8, 9; figures 3-5 *	7-10	
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
BERLIN	07-04-1986	STROUD J.G.	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
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Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
A	DE-B-2 111 180 (INSTITUT FISIKI TWOJORDOWO TELA I POLUPROWODNIKOW AKADEMII NAUK BELORUSSKOT) * example 2 *	2, 6	
P, A	--- EP-A-0 142 282 (PLESSEY OVERSEAS LTD.) * claims 1, 3, 4 *	9, 10	
A	--- PATENT ABSTRACTS OF JAPAN, vol. 7, no. 88 (E-170)[1233], 12th April 1983; & JP - A - 58 15241 (SUMITOMO DENKI KOGYO K.K.) 28-01-1983	7-11	
A	--- US-A-4 409 193 (T. SATO et al.) * claims 1, 3, 4, 10; comparative example in columns 5, 6 *	1, 3, 13	TECHNICAL FIELDS SEARCHED (Int. Cl.4)
A	--- US-A-4 287 164 (T. ENDO et al.) * claims 1-3, 7; abstract; column 1, lines 22-25; column 2, lines 5-20 *	1, 13	
D, A	--- US-A-4 188 194 (F.R. CORRIGAN) * abstract *	1, 7	
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The present search report has been drawn up for all claims			

Place of search BERLIN	Date of completion of the search 07-04-1986	Examiner STROUD J.G.
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Page 3

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A	U.S. DEPARTMENT OF COMMERCE - NATIONAL TECHNICAL INFORMATION SERVICE - NTIS FOREIGN TECHNOLOGY SERIES; T. ENDO "Production of cubic boron nitride"; NTN83-0288 (H) 1983 ---	1,3,13	
A	US-A-4 375 517 (M. WATANABE et al.) * whole document *		
A	US-A-3 894 850 (J.M. KOVALCHUK et al.) * example 6 *		
A	GB-A-1 005 425 (GENERAL ELECTRIC CO.) * claim 1; page 1, line 59 *	1,6	TECHNICAL FIELDS SEARCHED (Int. Cl.4)
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
BERLIN	07-04-1986	STROUD J.G.	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			