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Lubricating oil for plastic working and articles worked by using the same.

A lubricating oil for plastic working contains a powder of a compound having a urea bond incorporated therein. The lubricating oil forms a thick lubricating coating having excellent thermal resistance and loading resistance on the frictional surface during working by simply applying it on the surface of a material or a mold and, therefore, effectively prevents occurrence of seizing, even in the production of moldings having a high degree of working or complex shapes. The plastic worked product has a coating of the lubricating oil on its surface which provides an excellent anticorrosive effect for steel stocks.

The oil may also contain at least one extreme-pressure additive selected from:

- (1) condensed phosphoric acid,
- (2) phosphite and phosphate esters,
- (3) organic sulfur compounds, and
- (4) organic chlorine compounds.

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TITLE OF THE INVENTION

LUBRICATING OIL FOR PLASTIC WORKING AND ARTICLES WORKED BY USING THE SAME

5 BACKGROUND OF THE INVENTION

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This invention relates to lubricating oils for plastic working used in manufacturing machine parts by a method which comprises placing a steel stock or the like in a mold and pressing it with a hydraulic press, a machinery press or the like. More particularly, the present invention is concerned with lubricating oils for plastic working suitable particularly for use in backward extrusion working and composite extrusion working which cause a large area of a surface to be newly produced, leading to an increase in the surface area, and articles worked by using said oils.

As opposed to lubricating oils for bearings, lubricating oils for plastic working should exhibit lubricating capacities sufficient to withstand temperature rise attributable to heat generation accompanying deformation, friction, etc. during working, a pressure applied on a frictional surface and an increase in the area of a newly produced surface. In other words, mold life is directly influenced by lubricating capacities of a lubricating oil used.

The use of a lubricating oil which is not satisfactory in lubricating capacities brings a material

into direct contact with a mold, leading to seizing. If the seizing takes place over a large area, working pressure is increased to cause a local damage to or crack of the mold, which leads to not only a remarkable shortening in mold life but also occurrence of defective moldings and further makes it impossible to conduct working.

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Conventional lubricating oils for cold working of steel stocks include a mineral, synthetic oil, a mixture thereof (hereinafter referred to as "base oil") or a water-mixed base oil obtained by adding water to a base oil, each incorporating therein, for example, an oleaginous matter such as fatty acid or tallow, sulfur, phosphorus, chlorine-based extreme-pressure additive, an organometal-based extreme-pressure additive such as zinc dithiophosphate (Zn-DTP) or a solid lubricant such as graphite or molybdenum disulfide as described in "SEKIYU SEIHIN TENKAZAI (additives for oil products) " (edited by Toshio Sakurai, published on May 15, 1973 by Saiwai Shobo, Japan). These lubricating oils for plastic working can be used for deep draw working and roll working which are low in both degree of workingand deformation of the material. However, the use of the lubricating oils in working which is high in degree of working and brings about a high temperature and high pressure on the worked surface, or working for complex shapes causes seizing, because they are insufficient in capacity for forming a

lubricating coating having a satisfactory thermal resistance and loading resistance as well as for forming a lubricating coating on a newly produced surface.

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Conventional methods of lubrication for working which is high in degree of working include a method in which a lubricant prepared by dispersing a solid lubricant in a solution obtained by diluting or dissolving a synthetic resin in a solvent is applied on the surface of a material to form a lubricating coating and a method which comprises subjecting the surface of a material for plastic working to phosphate coating treatment, treating the surface of the resulting coating with a treating solution composed mainly of sodium stearate for forming a metal soap coatingand subjecting the material to plastic working. There is also known a method of lubrication in which the surface of the material is subjected to oxalate coating treatment in place of the phosphate coating treatment and the surface of the resulting coating is further subjected to metal soap coating treatment. These chemical coating treatments are excellent in prevention of seizing as compared with the lubrication by means of the abovementioned lubricating oils for plastic working. Therefore, in general, the chemical coating treatment is practically used for lubrication in cold working for steel stocks. However, the chemical coating treatment method in which a lubricating coating is formed on a material by synthetic resin coating or a combination of phosphate

coating or oxalate coating treatment with metal soap coating treatment require a sufficient pretreatment and a strict process control. For example, when metal soap coating treatment is conducted after phosphate coating treatment, a material such as steel stock is degreased before immersed in a phosphate bath having a predetermined phosphate concentration to form a coating. Thereafter, the material is washed with water, neutralized, immersed in a metal soap bath having a predetermined metal soap concentration and then dried. In other words, the above method requires complicated steps. Further, when the treating solutions are deteriorated, there arises difficulties related to disposal of the resulting wastes. As is apparent from the foregoing, the above-mentioned prior-art methods have some advantages but involve problems more or less.

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Lubricating oils for plastic working are extremely advantageous in that their use contributes to simplification of processing steps, because lubrication can be conducted by simply applying it to a material or a mold according to the customary method such as spraying or dropping. However, conventional lubricating oils for plastic working have not been used for a high degree of working which is conducted under severe working conditions, because they are unsatisfactory in formation of a lubricating coating and, therefore, tend to cause seizing.

In order to hold a large amount of a lubricant on the frictional surface for eliminating the above-mentioned drawbacks of the lubricating oils, there has been proposed the use of highly viscous liquid lubricants or greases having an excellent heat resistance, e.g., greases as described in U.S. Patent Nos. 4,065,395, 4,100.081 and 4,113,640, i.e., greases containing, as a thickener, a diurea or a polyurea obtained by reacting a monoamine or a diamine with an isocyanate in a base oil. When such greases are used for cold forging involving a high degree of working, a seizing preventing ability thereof is slightly improved to those of liquid lubricants but is considerably inferior to that of lubrication by the chemical coating treatment method.

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The above-mentioned prior-art methods have some advantages but involve problems. Specifically, with respect to liquid lubricants, there arose a problem related to seizing resistance under such working conditions to produce a largeamount of heat due to deformation as well as a large area of a new surface and to apply a high pressure on the surface. On the other hand, the chemical coating treatement method had drawbacks that it involved complicated treating steps and required much labor and cost because of occurrence of a number of accompanying operations such as waste water disposal.

SUMMARY OF THE INVENTION

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An object of the present invention is to provide a lubricating oil for plastic working which does not require any chemical coating treatment, but requires simply to be fed to the surface of a material or a mold according to the customary method by making use of an advantage of lubricating oils and exhibits a seizing resistance which may be comparable to that of the lubrication by the chemical coating treatment.

Conventional lubricating oils of this kind comprise a mineral oil or a synthetic oil as a base oil and, incorporated therein, an extreme-pressure additive comprising a sulfur-, chlorine- or phosphorus-containing organic compound and a solid lubricant such as graphite or molybdenum disulfide. However, such lubricating oils cannot be used for a high degree of working and complicated working, because mere application of such lubricating oils on a material etc. gives only a thin oil coating which easily leads to seizing as compared with chemical coating and synthetic resin coating. The present invention has at least partly eliminated such drawbacks.

The present inventors have made extensive and intensive studies to attain the above-mentioned object. As a result, the present inventors have found that a liquid lubricating oil comprising a base oil and a compound having a urea bond (hereinafter referred to as "urea lubricant") incorporated therein exhibits a

remarkably improved resistance to seizing and makes it possible to obtain highly worked moldings and moldings having complex shapes by means of cold forging by merely applying it on the surface of a metal stock or a mold.

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According to the present invention, there is provided a lubricating oil for plastic working comprising a lubricating oil (hereinafter referred to as "base oil") and, incorporated therein, a component A Comprising a compound having a urea bond and optionally a component B comprising at least one member selected from the group consisting of organic compounds containing phosphorus, sulfur or chlorine (hereinafter referred to as "phosphorus-, sulfur- or chlorine-based extreme-pressure additive") and condensed phosphoric acid. The invention also provides a plastic working method using such a lubricating oil.

The lubricating oil for plastic working according to the present invention forms a thick lubricating coating having excellent thermal resistance, lubricity and loading resistance between a material and a mold by simply applying it on the surface of a material or a mold by a customary method such as spraying, brushing or dropping and, therefore, exhibits a remarkably improved resistance to seizing even in manufacture of plastic working products having a high degree of working or complex shapes.

The urea lubricants, i.e., components A in the present invention include diurea, tetraurea and polyurea. These urea lubricants can easily be produced by reacting an amine with an isocyanate, which are starting materials,

in an inert organic solvent, e.g., toluene. Examples of monoamines which may be used in the reaction include pentylamine, hexylamine, heptylamine, octylamine, decylamine, dodecylamine, tetradecylamine, hexadecylamine, octadecylamine, eicosylamine, dodecinylamine, 5 hexadecinylamine, octadecinylamine, octadecanylamine, abietylamine, aniline, toluidine, naphthylamine, cumylamine, bornylamine, butylamine, benzylamine, phenethylamine, laurylamine, palmitylamine, methylamine, isoamylamine, cyclohexylamine, and 2-methyl-6-10 ethylaniline. Examples of diamines which may be used in the reaction include ethylenediamine, propanediamine, butanediamine, hexanediamine, dodecanediamine, octanediamine, hexadecanediamine, cyclohexanediamine, cyclooctanediamine, phenylenediamine, tolylenediamine, 15 xylylenediamine, dianilinomethane, ditoluidinomethane, bisaniline, bistoluidine, diaminoheptane, diaminononane, diaminodecane, diaminopentane, benzidine, diaminodiphenylmethane and methylenebis (2-chloroaniline). Examples of triamines which may be used in the reaction 20 include diethylenetriamine, dipropylenetriamine and Nmethyldiethylenetriamine. Examples of other polyamines which may be used in the reaction include triethylenetriamine, tetraethylenepentaamine and pentaethylenehexaamine. Examples of monoisocyanates which 25 may be used in the reaction include hexyl isocyanate, decyl isocyanate, dodecyl isocyanate, tetradecyl

isocyanate, hexadecyl isocyanate, phenyl isocyanate, cyclohexyl isocyanate, tolyl isocyanate, xylylisocyanate, cumenyl isocyanate, cyclooctyl isocyanate, butyl isocyanate, methyl isocyanate, ethyl isocyanate, isopropyl isocyanate, chloroethyl isocyanate, chlorophenyl 5 isocyanate, dichlorophenyl isocyanate, naphthyl isocyanate, octadecyl isocyanate, phenyl isocyanate and tolylisocyanate. Examples of diisocyanates which may be used in the reaction include xylylene diisocyanate, 10 hexylene diisocyanate, decylene diisocyanate, octadecylene diisocyanate, phenylene diisocyanate, tolidine diisocyanate, tolylene diisocyanate, methylenebisphenylene isocyanate, naphthylene diiscyanate and polymethylenepolyphenyl isocyanate.

The reaction product obtained by reacting the abovementioned raw materials in an organic solvent is filtered,
dried and pulverized to obtain a urea lubricant powder.

The particle diameter of the powder may arbitrarily be
selected taking into consideration working conditions,

dispersion stability of the powder, etc., and is generally
in the range of 0.5 to 500μm. In the case of backward
extrusion working, composite extrusion working or
manufacture of articles having complex shapes or a high
degree of working which produces a large area of a new

surface, a preferred particle diameter is in the range of
35 to 500μm.

When a further improvement in lubricity of the urea lubricant is required, a powder comprising a urea lubricant powder of which the surface is coated with, e.g., a synthetic wax may also be used.

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Examples of phosphorus-based extreme-pressure additive which is one of the component B incude phosphites, e.g., tertiary phosphites such as triphenyl phosphite, tris(nonylphenyl) phosphite, triisooctyl phosphite, diphenyl isodecyl phosphite, phenyl diisodecyl phosphite, tristearyl phosphite, trioleyl phosphite and trilauryl trithiophosphite and secondary phosphites such as di-2-ethylhexyl hydrogen phosphite, dilauryl hydrogen phosphite and dioleyl hydrogen phosphite and phosphates such as trimethyl phosphate, tributyl phosphate, triphenyl phosphate, tricresyl phosphate, octyl diphenyl phosphate, trilauryl phosphate, tristearyl phosphate, trioleyl phosphate, monobutyl phosphate, dibutyl phosphate, monoisodecyl phosphate, trichloroethyl phosphate, methyl acid phosphate, isopropyl acid phosphate, butyl acid phosphate, 2-ethylhexyl acid phosphate, lauryl acid 20 phosphate, stearyl acid phosphate and oleyl acid phosphate. Examples of sulfur-based extreme-pressure additivewhich is one of the component B include sulfurized fat and oil, dibenzyl sulfide disulfide, polysulfide, ditert-butyl sulfide, di-n-butyl disulfide and 25 polyoxyethylene polysulfide. Examples of chlorine-based extreme-pressure additive which is one of the component B

incude chlorinated paraffin, chlorinated fat and oil and pentachlorinated fatty acid. Examples of condensed phosphoric acid which is one of the component B include pyrophosphoric acid and polyphosphoric acid.

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Examples of the base oil to which the components A and B are added include mineral oil, dibasic acid diester oil, neopentyl polyol ester oil, α -olefin oil, fluoro ester, silicate ester oil, polyglycol oil, silicone oil, polyphenyl ether oil and polybutene oil. The properties of the above-mntioned base oils may properly be determined taking into consideration working conditions and operating conditions. In general, a preferred viscosity of the base oil is in the range of about 10 to 500 cSt at 40°C.

Although the amount of the urea lubricant powder or coated urea lubricant powder to be incorporated should properly be determined taking into consideration the degree of working of the intended molded parts and working conditions, said amount is 1 to 25 wt% in the case of ordinary extrusion working. However, a preferred amount of incorporation in the case of backward extrusion working and composite extrusion working which bring about a large area of a new born surface (nascent surface) and, therefore, brings about an increase in the surface area is 1.5 to 25 wt%. Therefore, the amount of the component A to be incorporated in the base oil may properly be determined taking into consideration the kind of material, degree of working, shapes of intended worked articles,

method of feeding the lubricating oil, etc. However, a preferred amout of the component A is generally in the range of 1.5 to 25 wt%.

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When the amount of the component A is below the above-mentioned range, the effect attained by its addition is small, leading to seizing. On the other hand, even if the component is excessively added, the effect exceeding a certain limit cannot be attained. Therefore, it is preferred that the component A be used in an amount in the above-mentioned range.

The urea lubricant which is incorporated in the base oil is in powdery form, and the diameter of the powder particles should properly be determined taking into consideration the degree of working, method of working, dispersion stability, etc. In the case of ordinary extrusion working, a powder having a particle diameter of 0.5 to 500µm is used. However, a preferred particle diameter of the powder used in backward extrusion working and composite extrusion working which bring about a large area of a new born surface and, therefore, brings about an increase in the surface area is 35 to 500µm. In general, it is preferred that the larger the incrase in the surface area of the moldings, the large the particle diameter of the powder to be incorporated.

The urea lubricant or coated urea lubricant is used in the form of a dispersion in the above-mentioned base oil. Although the dispersant used varies depending on

the kinds of base oil and urea lubricating oil, examples of such dispersants are polymethacrylate, ethylene-olefin copolymer and polyisobutylene. Another method for attaining effective dispersion is to adjust the specific gravity of the base oil to that of the urea lubricant.

The lubricating oil for plastic working of the present invention may contain known organic extreme-pressure additives containing chlorine, phosphorus or sulfur, antioxidants and anticorrosive agents.

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The lubricating oil for plastic working of the present invention is used by applying it on the surface of a material for plastic working or a mold by known methods such as spraying, dropping, immersion, roll coating, etc.

The article produced by plastic working according to the present invention has a coating on its surface and, therefore, has anticorrosive properties. The powder of the compound having a urea bond forms a coating on the worked article together with the lubricating oil after working.

Prior to the description on the function of the components of the lubricating oil for plastic working of the present invention, some description will be given on a lubrication mechanism of liquid lubricants in deep draw working, roll working, etc. With respect to the lubrication mechanism, reference may be made to Mitsugu Tokizawa, Lubrication in the Plastic Working of Metals

("JUNKATSU", Vol. 18, No. 3, (1973) pp. 193 - 201) and Yasuo Kasuga, Lubrication Mechanism in Plastic Working ("SOSEI TO KAKO", Vol. 9, No. 87, (1968) pp. 202 - 214). As is described in the above references, a liquid lubricant which has been brought into the space between 5 the face of a material ad a face of a mold is confined in the recessed portions present in the surface of the material during working. With the proceeding of plastic deformation, the protruded portions on the surface are pressed down to cause the liquid lubricant remaining in 10 the recessed portions to be forcibly discharged therefrom, which causes the discharged lubricant to be fed to the flat face formed by pressing to form a thin oil coating. When the liquid lubricant contains a phosphorus-, chlorine- or sulfur-based extreme-pressure additive, an 15 extreme-pressure coating is formed on the surface of the material due to the heat generated accompanying plastic deformation, which contributes to prevention of seizing. . Although lubrication is conducted based on the abovementioned mechanism also in the case of working which is 20 high in degree of working and large in an increase in the surface area, the formation of an extreme-pressure coating is insufficient at the frictional surfaces exposed to high temperature and high pressure, which leads to occurrence of seizing. 25

The lubrication mechanism of a liquid lubricant for plastic working containing a urea lubricant powder

dispersed therein according to the present invention is the same as that described above. However, in the case of the liquid lubricant of the present invention, the powdery urea lubricant is confined together with the base oil in the recessed portions present on the surface of the material. Since the protruded portions present on the surface of the material is pressed down at a high temperature under a high pressure, the powdery urea lubricant is allowed to dissolve to form a highly viscous oil or rolled and fed to the frictional surfaces in the form of a mixture with the base oil, with the proceeding of deformation of the material. A thick lubricating coating is formed on the frictional surface to prevent direct contact of the material with a mold. A coated urea lubricant for improving the lubricity of the urea lubricant functions in the same manner as mentioned above.

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When the urea lubricant and coated urea lubricant are incorporated in an amount below the above-mentioned range or small in particle diameter, any satisfactory lubricating coating cannot be formed. On the other hand, the incorporation thereof in excessive amounts leads to an increase in the viscosity, which not only causes lowering in applicability on the surface of a metal stock and a mold, but also gives no further improved effect. Therefore, it is preferred that the amounts of the urea lubricating oil and coated urea lubricating oil incorporated be in the above-mentioned range.

BRIEF DESCRIPTION OF THE DRAWINGS

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- FIG. 1 is a graph showing the relationship between the particle diameter of a diurea powder and the maximum allowable working temperature in a forward extrusion working;
- FIG. 2 is a graph showing the relationship between the particle diameter of a diurea powder and the maximum allowable working temperature in a backward extrusion working;
- 10 FIG. 3 is a graph showing the amount of a diurea powder incorporated and the maximum allowable working temperature in a forward extrusion working and a backward extrusion working;
- FIG. 4 is an illustrative view of a forward extrusion

 working method, in which FIG. 4(a) is a cross-sectional

 view illustrating a state in which a workpiece coated

 with a liquid lubricant has been inserted into a mold and

 FIG. 4(b) is a cross-sectional view illustrating a state

 in which a punch has been pressed down to extrude the

 workpiece from the mold;
 - FIG. 5 is an illustrative view of a backward extrusion working method, in which FIG. 5(a) is a cross-sectional view illustrating a state in which a workpiece coated with a liquid lubricant has been inserted into a mold and FIG. 5(b) is a cross-sectional view illustrating a state in which a punch has been pressed down for working of the workpiece;

Fig. 6 is a longitudinal sectional view of a workpiece used for forging;

FIG. 7 is a longitudinal sectional view of a cylinder for a video tape recorder produced by forging;

FIG. 8 is a longitudinal sectional view of a photosensitive drum for electrophotography produced by forging; and

FIG. 9 is a longitudinal sectional view of a pinion for automobiles produced by forging.

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EXAMPLES

The examples of the present invention will now be described together with comparative examples. The present invention should not be construed to be limited to these examples.

First, some description will be given with respect to criteria for evaluating working performance.

working performance of liquid lubricants was evaluated by the forward extrusion working method as shown in FIG. 4 and the backward extrusion working method as shown in FIG. 5. Specifically, a mold 3 was equipped with a band heater 4. The temperature of the mold 3 was stepwise raised by 5 to 10°C a time. At each temperature, a material 2 coated with a liquid lubricant was inserted into the mold 3, and 10 to 15 pieces of the material were worked at the same temperature at a press-down rate of a

punch 1 of 8 mm/s to determine a mold temperature at which the material could be worked without causing any seizing (maximum allowable working temperature). The higher the maximum allowable working temperature, the more excellent the thermal resistance and loading resistance of the lubricating coating.

- Working Conditions:
- 1.1 Forward Extrusion Working Method
- (a) Material and Dimensions

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material	outside dia. (mm)	length (mm)	surface roughness (µm)
SCM415	9.9	30	Ra 1.5

(b) Principal Dimensions of Mold

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material	land inside dia. (mm)	extrusion angle (°)	drawing dia. (mm)	degree of working (%)
hard metal V ₅	10	120	5	75

1.2 Backward Extrusion Working

(a) Material and Dimensions

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material	outside dia. (mm)	length (mm)	surface roughness (μm)
SCM415	20	30	Ra 2.0

(b) Principal Dimensions of Mold

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material	land inside dia. (mm)	punch dia. (mm)	depth of boring (mm)	degree of working (%)
hard metal V ₅	20.1	16.1	48	64

EXAMPLE 1

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of dried toluene, and the mixture was heated at 110 to 115°C to dissolve the o-tolidine in the toluene. To the resulting solution was dropwise added 67.3 g (0.565 mol) of phenyl isocyanate at 106°C over 15 min. The mixture was stirred at 110 to 113°C for 4 hr, allowed to cool at room temperature, filtered and dried to obtain 117.8 g of a white crystalline diurea [4,4'-(3,3'-

- dimethyldiphenylene)-diphenylurea]. The diurea thus obtained was pulverized and classified to obtain a diurea powder having a particle diameter of 63 to 88 µm. 10% by weight of the diurea powder was incorporated in a mineral oil (viscosity at 40°C: 150 mm²/s) at ordinary
- temperature, and the mixture was stirred at 130 rpm for 10 min to obtain a liquid lubricant of the present invention comprising a diurea powder dispersed in the oil. The results of evaluation on working performance of the liquid lubricant thus obtained are shown in Table 1.
- The compositions of the comparative lubricants are shown below.

COMPARATIVE EXAMPLE 1 (commercially available processing oil)

base oil: mineral oil the remainder (amount)
extreme-pressure additive: a fatty acid content of 43
wt%, a chlorine content of 12 wt%, and a sulfur content
of 6 wt%.

COMPARATIVE EXAMPLE 2 (urea grease obtained by reacting amine with isocyanate in a base oil)

base oil: mineral oil (88 wt%)

thickner: diurea (10 wt%)

5 additive: antioxidant (2 wt%)

The above grease is in the form of semi-solid to solid obtained by agglomeration of the finely divided powder thickener in a colloidal form.

10 EXAMPLE 2

90.8 g (0.84 mol) of p-phenylenediamine was added to 1400 ml of dried toluene. To the resulting mixture was dropwise added 200 g (1.68 mol) of phenyl isocyanate at 100 toll0°C over 1 hr. The mixture was stirred at 110 to 112°C for 4 hr, allowed to cool at room temperature, 15 filtered and dried to obtain 283.8 g of a white crystalline diurea [p-phenylenediphenylurea]. The diurea thus obtained was pulverized and classified to obtain a diurea powder having a particle diameter of 63 to 88 m. 10% by weight of the diurea powder was incorporated in a 20 mineral oil (viscosity at 40°C: 150 mm²/s (cSt)) at ordinary temperature, and the mixture was stirred at 130 rpm for 10 min to obtain a liquid lubricat of the present invention comprising a diurea powder dispersed in the oil. The results of evaluation on working performance of 25 the liquid lubricant thus obtained are shown in Table 1.

EXAMPLE 3

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13.9 g (0.080 mol) of tolylene diisocyanate was dissolved in dried toluene at 25 to 33°C. To the resultig solution was dropwise added 20.5 g (0.16 mol) of pchloroaniline. The mixture was stirred at 110°C for 5 hr, allowed to cool at room temperature, filtered and dried to obtain 33.6 g of a white crystalline diurea [1methyl-2,4-bis(4-chlorophenylureido)benzene]. The diurea thus obtained was pulverized and classified to obtain a diurea powder having a particle diameter of 63 to 88 m. 10% by weight of the urea powder was incorporated in a mineral oil (viscosity at 40° C: 150 mm²/s) at ordinary temperature, and the mixture was stirred at 300 rpm for 10 min to obtain a liquid lubricant of the present invention comprising a diurea powder dispersed in the The results of evaluation on working performance of the liquid lubricant thus obtained are shown in Table 1.

EXAMPLE 4

20 17.4 g (0.1 mol) of tolylene diisocyanate was
dissolved in 180 ml of dried toluene. To the resulting
solution was dropwise added 18.6 g (0.20 mol) of aniline
at 27 to 34°C while stirring. The mixture was stirred at
75 to 80°C for 5 hr, allowed to cool at room temperature,
filtered and dried to obtain 35.5 g of a white crystalline
diurea [1-methyl-2,4-diphenylureidobenzene]. The diurea
thus obtained was pulverized and classified to obtain a

diurea powder having a particle diameter of 63 to 88µm.

10% by weight of the urea powder was incorporated in a mineral oil (viscosity at 40°C: 150 mm²/s) at ordinary temperature, and the mixture was stirred at 130 rpm for 10 min to obtain a liquid lubricant of the present invention comprising a diurea powder dispersed in the oil. The results of evaluation on working performance of the liquid lubricant thus obtained are shown in Table 1.

10 EXAMPLE 5

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3 g (0.05 mol) of ethylenediamine and 26 g (0.10 mol) of oleylamine were added to 200 ml of dried toluene of 60 to 75°C. 50 ml of dried toluene containing 17.4 g (0.10 mol) of tolylene diisocyanate dissolved therein was dropwise added to the above-prepared amine solution while stirring over 1 hr. Subsequently, the mixture was heated at 110°C for 5 hr to obtain a print-like reaction product. The reaction product was vacuum dried to obtain 40.2 g of a light yellow crystalline polyurea [1,2-ethylenebis(2methyl-5'-octadecylureidophenyl)urea]. The polyurea thus obtained was pulverized and classified to obtain a polyurea powder having a particle diameter of 63 to $88\mu m$. 10% by weight of the urea powder was incorporated in a mineral oil (viscosity at 40°C: 150 mm²/s) at ordinary temperature, and the mixture was stirred at 300 rpm for 10 min to obtain a liquid lubricant of the present invention containing a polyurea powder dispersed therein.

The results of evaluation on working performance of the liquid lubricant thus obtained are shown in Table 1.

EXAMPLE 6

A mixture of 3.6 g (0.06 mol) of ethylenediamine 5 with octadecylamine (0.10 mol) is heated at 60°C to form a solution. Separately, 17.4 g of a mixture of 2,4tolylene diisocyanate with 2,6-tolylene diisocyanate in a ratio of 80: 20 was added to dried toluene. The mixture was subjected to dispersion at about 30°C. The resulting 10 dispersion was dropwise added to the above-prepared hot solution while stirring. The mixture was stirred at 80°C for 5 hr, allowed to cool at room temperature, filtered and dried to obtain 27.9 g of a white crystalline diurea. The diurea thus obtained was pulverized and classified to 15 obtain a diurea powder having a particle diameter of 63 to 88 μm . 10% by weight of the urea powder was incorporated in a mineral oil (viscosity at 40°C: mm²/s) at ordinary temperature, and the mixture was stirred at 130 rpm for 10 min to obtain a liquid lubricant 20 of the present invention containing a diurea dispersed The results of evaluation on working performance therein. of the liquid lubricant thus obtained are shown in Table 1.

As is apparent from Table 1, the liquid lubricants of the present invention are higher in the temperature of a mold at which seizing occurs than those of comparative

examples, i.e., are superior in working performance to the comparative lubricants.

Table 1

				oldenotte	
			amount or	llax. attowarte	
EX.	isocyanate	amine	urea incorp. (wt%)	forward extrusion working 1)	backward extrusion working 2)
			,	150	70
-	phenyl isocyanate	o-tolidine	10	OCT .	
		n-nhenvlenediamine	10	150	70
7	ditto	- F 4			20
	+olulene diisocvanate	p-chloroaniline	10	120	6
7	COTÀTEME CITALINA			C L	08
_	ditto	aniline	10	150	
r		other lonediamine		150	70
2	ditto	olevlamine	ОТ	007	
,		othylenediamine	,	150	70
9	2,4-tolylene diisocyanate		OT	207	
)	2,6-tolylene alisocyanace	outrome pressure		Co	serzing occurred
COMP.	processing oil containing extra	excrand american		000	at room temp.
EX. 1				Ç	30
COMP.	urea grease (diurea: 10 wt%)	8)		30	
EX. 2	_				

1) degree of working: 75%

degree of working: 64%

EXAMPLE 7

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The diureas as obtained in EXAMPLES 1 and 3 are separately incorporated in an amount of 10% by weight to a mineral oil having a viscosity of 150 mm^2/s (cSt) at 40°C. The relationship between the particle diameter of the powder and the maximum allowable working temperature was determined by the forward extrusion working method and the backward extrusion working method using the aboveprepared samples. FIG. 1 shows the results with respect to a degree of working of 75% in the forward extrusion, while FIG. 2 shows the results with respect to a degree of working of 64% in the backward extrusion. As is apparent from Fig. 1, the maximum allowable working temperature increases rapidly when the particle diameter of the powder exceeds about 0.5 μm . Further, as is apparent from FIG. 2, the maximum allowable working temperature increases rapidly when the particle diameter of the powder exceeds about 35µm.

20 EXAMPLE 8

The same diurea as obtained in EXAMPLE 3 was incorporated in an amount of 0.6 to 12 wt% to a mineral oil having a viscosity of 150 mm²/s (cSt) at 40°C. The relationship between the amount of the powder incorporated and the maximum allowable working temperature was determined by the forward extrusion working method and the backward extrusion working method. The results are

shown in FIG. 3, in that, curve 10 shows the relationship with respect to the forward extrusion working method, curve 20 the backward extrusion working method.

As is apparent from FIG. 3, the effect of addition is observed when the amount of incorporation is 1 wt% or larger in the forward extrusion working method and 1.5 wt% or larger in the backward extrusion working method.

EXAMPLE 9

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The diurea and polyrea respectively obtained in EXAMPLES 4 and 5 and comprising particles of which the diameters were adjusted to 63 to 88µm were separately added in an amount of 10 wt% to the synthetic oil as indicated in Table 2 and dispersed therein under the same stirring conditions as in EXAMPLES 4 and 5 to obtain liquid lubricants. Evaluations on the maximum allowable working temperature of the above-prepared liquid lubricants were conducted by the forward extrusion working method and the backward extrusion working method.

As is apparent from Table 2, the liquid lubricants of the present invention containing a diurea or polyurea incorporated therein are higher in the maximum allowable working temperature than those obtained in COMPARATIVE EXAMPLES 1 and 2 as indicated in Table 1, i.e., are superior in working performance to the comparative lubricants.

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(D°) cmo+ ~~:-1	max. allowable working cemp.	backward extrusion working 2)	70	09	UV	04	45	09	70	2	75		09	45	09		70	70	
	max. allowable	forward extrusion working 1)	150	140		06	100	155		160	150		135	100	001	D	110	150	
	viscosity	at 40°C mm ² /s (cSt)	100	56		100	230	200		105	00.5	TOO	56	100		230	200	105	
		synthetic oil	2010612	G-Oretin Cir	polyor ester off	polybutene oil	polyphenyl ether oil	fluorogilicone oil		mineral oil + polyol	ol .	α-olefin oil	polyol ester oil	colvintene oil		polyphenyl ether oil	fluorosilicone oil	mineral oil + polyol	ester oil (50 : 50)
		urea	-			diurea	obtained						,	r	polyurea obtained	in EX. 5			
									EX. 9				<u>.</u>	ĵ.					

1) degree of working: 75%

degree of working: 64%

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EXAMPLES 10 to 23

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60 g of o-tolidine was added to 600 ml of dried toluene, and the mixture was heated at 110 to 115°C to dissolve the o-tolidine in the toluene. To the resulting solution was dropwise added 67.3 g of phenyl isocyanate at 106°C. The mixture was stirred at 110 to 113°C for about 4 hr, allowed to cool at room temperature, filtered and dired to obtain a white crystalline diurea. The diurea thus obtained was pulverized to obtain a urea lubricant having an average particle diameter of $90\mu\,m$ which is the component A. In a mineral oil as a base oil having a viscosity of 150 cSt at 40°C were incorporated the above-obtained component A and phosphorus-, sulfur-or chlorine-based extreme-pressure additives as the component B in amounts as indicated in Table 3 to obtain lubricating oils for plastic working of the present invention. lubricating oils thus obtained were applied on the surface of a chromium-molybdenum steel (SCM415) material 2 having a diameter of 10 mm or 20.1 mm and a length of 30 mm by Thereafter, molds 3 (made of a hard metal, V₅) for the forward extrusion working method as shown in FIG. 4 and for backward extrusion working method as shown in FIG. 5 were equipped with a band heater 4. temperature of the molds 3 was stepwise raised by 5 to 10°C a time, and 10 pieces of the material 2 were worked with a punch I with the same condition for evaluating maximum allowable working temperature.

The forward extrusion working was conducted under the following conditions:

material: a diameter of 10 mm and a length of 30 mm extrusion angle: 120°

5 drawing diameter: 5 mm

degree of working (reduction of cross-sectional area):
75%

press-down rate of punch: 8 mm/s

The backward extrusion working was conducted under the following conditions:

material: a diameter of 20.1 mm and a length of 30 mm punch diameter: 16.1 mm

degree of working: 64%

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depth of bore in worked article: 48 mm

press-down rate of punch: 8 mm/s

The compositions of the processing oils which have conventionally been used are shown in Table 4. The maximum allowable working temperature on these processing oils were also determined under the above-mentioned conditions. The results are shown in Table 5. As can be seen from Table 5, the lubricating oils for plastic working of the present invention exhibit a high maximum allowable working temperature, i.e., exhibit an excellent resistance to seizing.

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		base oil		component A		urea lubricant powder	powder '	component B extreme-pressure	additive
No.	7	viscosity	amount of	raw materials paration of lu	ls for pre- lubricant	average	amount of	2	amount of
	KING	(cSt)	(wt%)	amine	lsocyanate	(hm)	(wt&)		(wt%)
93	mineral oil	150	80	o-tolidine	phenyl isocyanate	90	10	monobutyl phosphate	10
11	=	=	z	=	н	=	п	tributyl phosphate	ε
12	ı	=	=	=	z	=	=	triphenyl phosphite .	E
13	2	=	=	=	=	=	=	dioleyl hydrogen phosphite	Ξ
14	=	=	z	=	=	=	z	methyl acid phosphate	τ
15	z	=	=	z	=	=	=	oleyl acid phosphate	.
16	:	=	=	=		±	*	pyrophosphoric acid	=
17	=	z	=	z	=	z	=	sulfurized fat and oil	E
18	=	a a	=	=	=	=	=	chlorinated paraffin	r
ł	•	•	-	=	•	=	=	pyrophosphoric acid	5
.		:	:	:	:	:		dioleyl hydrogen phosphate	5
5		=	=	•	=		=	tributyl phosphate	5
		:			:			sulfurized fat and oil	5
1		=	=		=	=	=	tributyl phosphate	S
	•	•	:	:	:		:	chlorinated paraffin	ທົ
	•	=	:	=		=	=	sulfurized fat and oil	5
77		:	1					pentachlorinated fatty ester	5
								dioleyl hydrogen phosphite	5
23	=		75		=	:	=	sulfurized fat and oil	S
								chlorinated paraffin	S

rable 4

	ped	base oil		extreme-pressure	solid	solid lubricant	
				S. Ha Hand		average	40000
conventional lubricant	kind	viscosity at 40°C (cSt)	amount of incorp. (wt%)	kind	kind	n)	incorp. (wt%)
Æ	mineral oil	200	39	fatty oil content: 43 wt% chlorine content: 12 wt% sulfur content: 6 wt%	l	ſ	ı
					molybdenum	ď	10
ď	rapeseed oil	45	85	ı	disulfide	0	
נו	polybudene oil	205	80	sulfurized fat and oil: 10 wt%	polyethylene	10	10
).	7						

Table 5

 			
		maximum allowabl	e working temp.(°C)
group	No.	forward extrusion working (degree of working: 75%)	backward extrusion working (degree of working: 64%)
	10	350	240
	11	350	190
	12	330	195
	13	350 or higher	210
	14	350 or higher	220 ·
lubricating oil for	15	340	215
plastic working	16	350 or higher	- 180
of the present	17	340	200
invention	18	345	200
	19	350 or higher	240
	20	350	240
	. 21	350 .	235
	22	335	210
	23	350 or higher	245
conventional lubricating	A	80	30°C, seizing occurred in work-ing of single piece
oil	В	30	11
	С	60	11

EXAMPLES 24 to 39

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With respect to lubricating oils for plastic working of the present invention prepared by incorporating a urea lubricant powder as the component A and an extremepressure additive as the component B in base oils, i.e., α -olefin oil, neopentyl polyol ester oil, polyphenyl ether oil or fluorosilicone oil as indicated in Table 6, the maximum allowable working temperature was determined by the forward extrusion working method and the backward extrusion working method under the same conditions as in EXAMPLE 1. The results are shown in Table 7. The lubricating oils for plastic working containing a urea lubricant powder as the component A and at least one member selected from among phosphorus-, sulfur- and chlorine-based extreme-pressure additives as the component B exhibits an excellent resistance to seizing, regardless of the kind of the base oil.

EXAMPLES 40 to 70

20 A mineral oil having a viscosity of 150 cSt at 40°C was used as the base oil. A urea lubricant powder having an average particle diameter of 90 µm produced by using raw materials of the component A as indicated in Table 8 and extreme-pressure additives such as pyrophosphoric acid, dioleyl hydrogen phosphite as the component B were incorporated in various amounts in the base oil. The maximum allowable working temperature of the resulting

lubricating oils for plastic working was evaluated. The results are shown in Table 9.

Table 6

No 1 1 1 1 1 1 1 1 1		component A	4	base oil		component B extreme-pressure additive	e additive
obtained in α-olefin oil 100 75 Ex. 10 (10) (No.	urea lubricant power (wt%)	kind	viscosity at 40°C (cst)	amount of incorp. (wt%)	kind	amount of incorp. (wt%)
obtained in	24	-			80	monobutyl.phosphate	10.
obtained in	25				80	pyrophosphoric acid	10
cobtained in α-olefin oil 100 /5 (10) (α-olefin oil 100 /5 (10) (α-olefin oil 100 /5 γ5 γ5 γ6 β0		1			L	pyrophosphoric acid	5
(10) 75 76 neopentyl- golyol ester oil 77 75 75	5	obtained in Ex. 10	α-olefin oil	100	<u>.</u>	dioleyl hydrogen phosphate	10
ditto polyol 56 75 75 75 75 75 75 75 75 75 75 75 75 75	-	(10)				dioleyl hydrogen phosphate	5
### ### ### ### ### ### ### ### ### ##	27				75	sulfurized fat and oil	5
### ### ### ### ### ### ### ### ### ##		-				chlorinated paraffin	5
ditto polyol 56 75 ester oil	28	·			80	monobutyl phosphate	3
ditto polyol 56 75 ester oil	29	,			80	pyrophosphoric acid	5.
ditto polyol 56 75 87 75 75					L	pyrophosphoric acid	5
ester oil	90	ditto	neopentyl- polyol	56	n (dioleyl hydrogen phosphate	10
75 sulfurized chlorinated			ester oll	-		dioleyl hydrogen phosphate	Z.
	31				75		īC
				•			ស

Table 6 (cont'd)

No. 1		+ 4000	q	base oil		component B extreme-pressure additive	e additive
ditto polyphenyl 230 75 ether oil 75 75 ditto fluorosilicone 200 75 ditto oil	ON	component a urea lubricant power (wt%)	kind	viscosity at 40°C (cst)	amount of incorp. (wt%)	kind	<pre>amount of incorp. (wt%)</pre>
ditto polyphenyl 230 75 ether oil 75 75 76 80 80 80 81 61 61 61 75 75 75 75 75 75 75 75	32				80	monobutyl phosphate	5
ditto polyphenyl . 230	33				80	pyrophosphoric acid	īŲ
ditto polyphenyl 230 75 75 76 6110000011100000 200 75 775 775						pyrophosphoric acid	S
75 76 80 80 81 fluorosilicone 200 75 75 75	94	ditto	polyphenyl	. 230	/5	dioleyl hydrogen phosphate	10
75 Gitto oil 75 77 75 75 75			i i i i i			dioleyl hydrogen phosphate	5
## ## ## ## ## ## ## ## ## ## ## ## ##	35				75	fat	5
41tto fluorosilicone 200 75 75 75 75						chlorinated paraffin	5 .
ditto fluorosilicone 200 75 75 75 75	36				80	monobutyl phosphate	5
fluorosilicone 200 75 oil 75	37			•	80	pyrophosphoric acid	5
ditto fluorosilicone 200 /5 oil 75					1	pyrophosphoric acid	5
75	38	ditto	fluorosilicone	200	ç/	dioleyl hydrogen phosphate	10
75			1			dioleyl hydrogen phosphate	5
chlorinated paraffin	39				75	sulfurized fat and oil	5
						chlorinated paraffin	5

Table 7

	maximum allowable w	working temp. (°C)
No.	forward extrusion working (degree of working: 75%)	backward extrusion working (degree of working: 75%)
24	340	235
25	320	185
26	350 or higher	220
27	350 or higher	. 240
28	330	220
29	320	180 .
30	350	225
31	350	230
32	350	230
33	320 .	210
.34	350	235
35	350	240
36	340	235
37	325	215
38	. 350	245
39	350	235

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<u></u>	······	 1	 1	Т	- 1	T	ſ			1	1						
extreme-pressure additive (wt%)	dioleylhydrogen phosphite		H		2	г					10	20	25		20	15	10
component B	pyrophosphoric acid	0	П	2		г	2	2	2	2	10			20		J.	.3
component A	urea lubricant powder (wt%)	1	1	2	2	2	5	10	20	30	30	35	30	2	10	10	15
Lals for production	isocyanate	phenyl															
raw materials	amine									o-tolidine							
mineral	oil (wt%)	66	97	96	96	96	93	88	78	68	50	45	45	78	70	70	72
	No.	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55

(cont'd)

	200	raw materials	als for production	component A	component B	extreme-pressure additive (wt%)
NO.	oil (wt%)	amine	isocyanate	urea lubricant powder (wt%)	pyrophosphoric acid	dioleylhydrogen phosphite
56	96			2	2	
57	93	p-phenylene- diamine	phenyl isocvanate	5	2	
28	70		1	10	ស	1.5
59	96			2	2	
8	93	p-chloro-	tolylene diisocynate	ហ	2	
61	70		1	10	2	. 1.5
62	96			2	2	
63	93	aniline	:	ഹ	2	
64	70	- -		10	ហ	15
65	96			2	2	
99	93	ethylenediamine olevlamine	=	ഗ	2	
67	70	1		10	ъ	15
68	96		2.4-tolvlene	2	2	
69	93	=	dilsocyanate 2,6-tolylene	ហ	2	
70	70		dilsocyanate	10	້ທ	15

Table 9

	maximum allowable	working temp. (°C)
No.	forward extrusion working (degree of working: 75%)	backward extrusion working (degree of working: 64%)
40	55	. 30
41	60	30
42	105	45
43	105	40
44	100	45
45	280	110
46	340	230
47	350	240
48	350	245
49	350	245
50	350	245
51 ·	350	245
52	60	40
53	300	230
54	350	240
55	350	240
56	70	40
57	290	105
58	340	235
59	65	, , 40
60	295	70

Table 9 (cont'd)

	maximum allowable v	working temp. (°C)
No.	forward extrusion working (degree of working: 75%)	backward extrusion working (degree of working: 64%)
61	350	210
62	60	35
63	260	80
64	330	220
65	70	. 40
66	250	65
67	320	215
68	55	40
69	230	60
70	300	200

EXAMPLES 71 to 78

was used as the base oil. A urea lubricant powder, i.e., component A, produced by using the same raw materials as in EXAMPLE 1, i.e., o-tolidine and phenyl isocyanate was incorporated in the base oil in varied average particle diameter in the range of 0.2 to 800µm as indicated in Table 10. The maximum allowable working temperature of the resulting lubricating oil for plastic working was evaluated. The results are shown in Table 10.

Table 10

											U
maximum allowable working temp. (°C)	backward extrusion	working 64%)	זכ	7	40	55	70	205	245	245	245
	forward extrusion	working: 75%)	Cac	2	350	350	350	350	350	350	345
extreme -pres- sure additive	amount of	(wtw)	S	1.5	1	Ξ	Ξ	Ξ	#	=	:
component B extr		pyrophosphoric acid	dioleyl hydrogren phosphite	11		11	•	=	11	=	
component A urea lubricant powder	amount of incorp. (wt%)		Q.	Q.	н	H	U	£	=	=	=
	average particle	dia. (µm)	c c		€*0	5*0	0.2	50	200	500	800
	g g		pheny1	isocyanate	Ħ	ŧ	11	н	н	#	=
	raw materials for production lubricant	amine	Lne			11	H	()	н	11	=
·base oil	amount of incorp. (wt%)		,	2	=	=	=	и	=	п	
	viscosity	(cst)		er G	Ξ	=	=	ŗ	н	11	2
-		VIIII.	mineral	oi1	=	=	=	I	z	=	=
	ě		F	1	72	73	74	75	9/	77	78

EXAMPLE 79

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The lubricating oil as obtained in EXAMPLE 1 was applied on the surface of JIS A2218 aluminum alloy material having a shape as shown in FIG. 6 by spraying. The material was inserted into a mold and subjected to cold forging in such a state that the temperature of both the alloy and the mold were ordinary one to form 500 cylinders for a video tape recorder having a shape as shown in FIG. 7. A coating, i.e., a product of a reaction of the lubricant oil with the substrate, is formed on the surface of the material after working, and the surface was like a mirror.

In the present example, one or both of the internal and external peripheral surfaces 11, 12 on which a tape is traveled is often cut and polished. Alternatively, the cylinder may be used as it is without removing the coating formed by a reaction between the lubricating oil for plastic working and the substrate. When an oval through-hole is provided at the bottom of the internal peripheral surface 14, the external peripheral surface is cut and polished to attain roundness of the external peripheral surface. When a groove is provided at the step portion 13, the entire portion of the step is cut and polished.

However, the cylinder may be used as it is without removing the coating formed by a reaction between the lubricating oil for plastic working and the substrate. The worked material itself has a mirror surface.

EXAMPLE 80

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The lubricating oil as obtained in EXAMPLE 1 was applied on the surface of A3003 aluminum alloy material having a diameter of 50 mm and a length of 45 mm. The material was inserted into a mold and subjected to cold forging in such a state that the temperature of both the alloy and the mold were ordinary one to form a vessel as shown in FIG. 8 having an external diameter of 50 mm, an internal diameter of 40 mm and a length of 100 mm. A coating i.e., a product of a reaction of the lubricant oil with the substrate, is formed on the surface of the material after working, and the surface was like a mirror.

In the present invention, a cup-like article as shown in FIG. 8 was formed from a block. The article having the worked internal and external peripheral surfaces can be used as it is. Both of the internal and external peripheral surfaces were like a mirror. The bottom was cut to form a cylinder. A coating, i.e., a reaction product, is formed on the surface of the material after working. Only the external periperal surface may be cut and polished.

Further, it is possible to directly form a cylinder by subjecting a pipe shaped material to plastic working. Therefore, the formed product is used as it is after cutting only the edge face. The article can be formed by a single-step working or two-step working in which a further working is conducted in the smaller degree of

working than that in the first step. The two-step working leads to a further improved mirror surface. The second working is conducted without addition of the lubricating oil.

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EXAMPLE 81

The lubricating oil as obtained in EXAMPLE 1 was applied on the surface of A2218 aluminum alloy material having a diameter of 40.4 mm and a length of 20 mm by the immersion method. The material was inserted into a mold and subjected to cold forging in such a state that the temperature of both the alloy and the mold was ordinary one to form a pinion having a shape as shown in FIG. 9. A coating, i.e., a product of a reaction of the lubricant oil with the substrate, is formed on the surface of the material after working, and the surface was like a mirror.

In the present example, the coating which has been formed during the working of the curved portions of the teeth 22 remains on the article. However, the top of the teeth 22 may be cut and polished. The internal peripheral surface 21 is left intact. Numeral 24 designates a through-hole portion formed by cutting. The surface designated by numeral 25 may be left intact or may be subjected to cutting treatment. The bottom surface 23 is left as it is.

As is apparent from the foregoing, the lubricating oil of the present invention comprising a base oil such

as a mineral oil or synthetic oil or a mixture thereof and a diurea or polyurea incorporated therein forms a lubricating coating having excellent thermal resistance and loading resistance on the frictional surface during working by simply applying it on the surface of a material or a mold and, therefore, not only effectively prevent occurrence of seizing but also greatly contributes to an improvement in the service life of tools such as a mold, enhancement of productivity and reduction in production cost.

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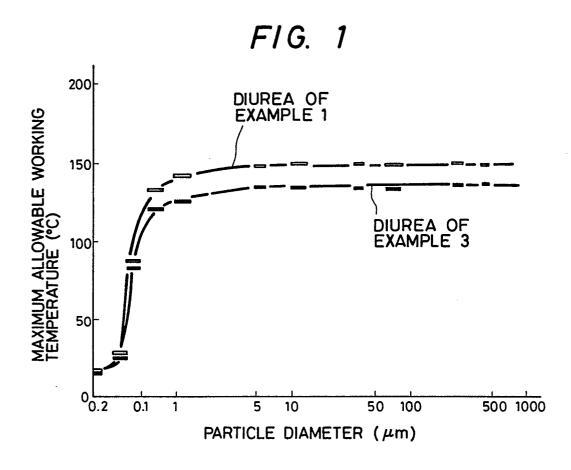
Further, the plastic working product of the present invention has a coating comprising the above-mentioned lubricating oil on its surface which particularly exhibits an excellent anticorrosive effect for steel stocks, so that a plastic working product having excellent corrosion resistance is advantageously provided.

CLAIMS

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- 1. A lubricating oil for plastic working comprising a lubricating oil and a powder of a compound having a urea bond dispersed and incorporated in said lubricating oil.
- 2. A lubricating oil for plastic working according to claim 1 wherein said powder has a particle diameter of 35 to 500 μm_{\bullet}
 - A lubricating oil for plastic working according to claim 1 or claim 2, wherein said powder is incorporated in said lubricating oil in an amount of 1.5 to 25% by weight.
- 4. A lubricating oil for plastic working according to any one of claims 1 to 3 which contains, as well as (A) said powder of a compound having a urea bond,
 - (B) at least one extreme-pressure additive
 selected from:
 - (1) condensed phosphoric acid,
 - (2) phosphite and phosphate esters,
- 20 (3) organic sulfur compounds, and
 - (4) organic chlorine compounds.

- 5. A lubricating oil for plastic working according to any one of claims 1 to 4 wherein said powder is coated with a wax.
- 6. A plastic working product comprising a molding, wherein said molding has on its surface a coating of a lubricating oil according to any one of the preceding claims.
- 7. A cylinder for a video tape recorder produced by plastic working using a lubricating oil for plastic working, wherein said cylinder has on its surface a coating of said lubricating oil which oil is according to any one of claims 1 to 5.
 - 8. A photosensitive drum for electrophotography produced by plastic working using a lubricating oil
 - for plastic working, wherein said photosensitive drum has on its surface a coating of said lubricating oil which oil is according to any one of claims 1 to 5.
 - 9. A pinion for an automobile or other machine produced by plastic working using a lubricating oil
- 20 for plastic working, wherein said pinion has on its surface a coating of said lubricating oil which oil is according to any one of claims 1 to 5.



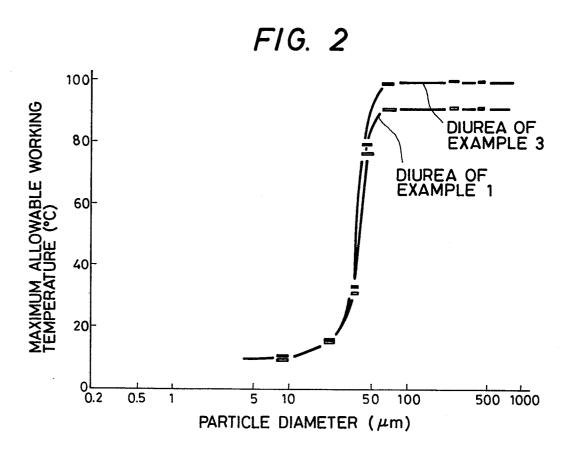


FIG. 3

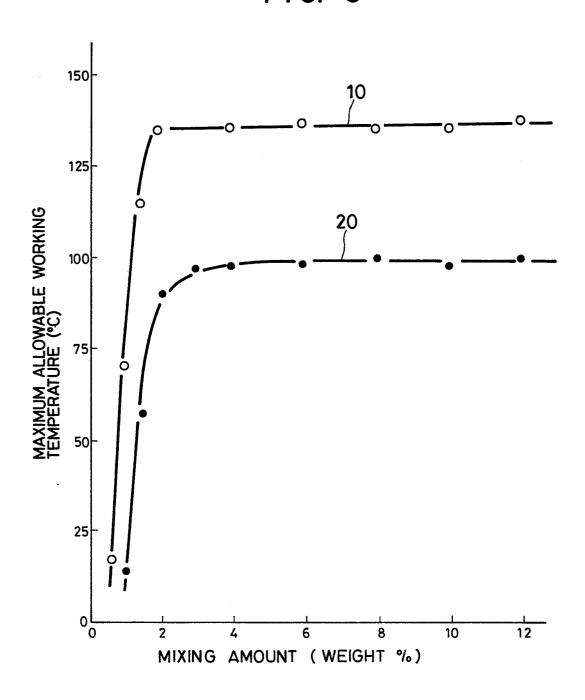


FIG. 4(a)

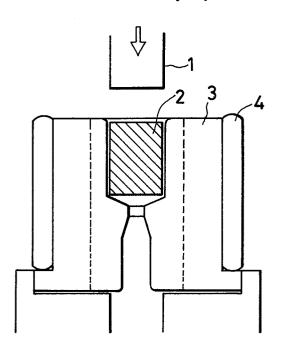


FIG. 4(b)

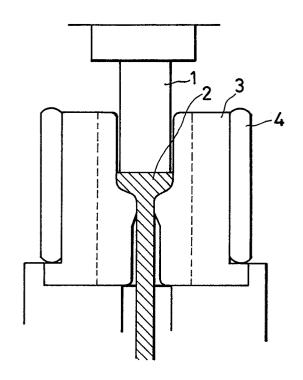
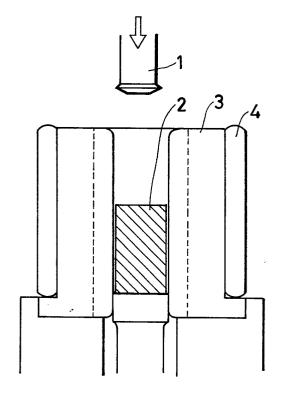
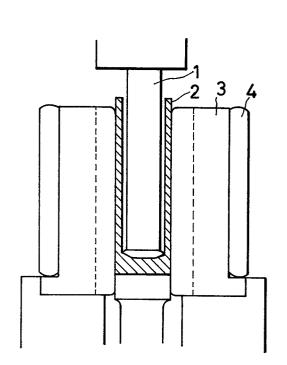


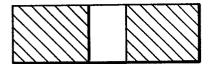
FIG. 5(a)



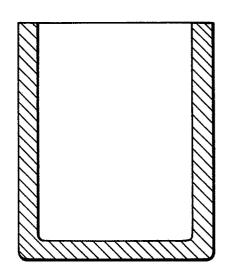




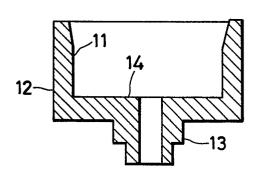
F1G. 6



F1G. 8



F1G. 7



F1G. 9

