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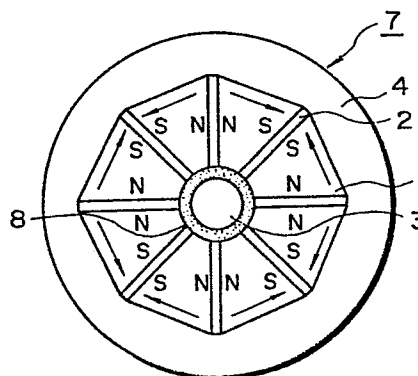
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54 **A method for manufacturing a continuous-length extruded bar of plastic magnet with circumferentially multipolar magnetization.**

57 A continuous-length extruded bar of plastic magnet with circumferentially multipolar magnetization is manufactured efficiently by extruding a plastic magnet composition (8) out of the discharge port of an extruder machine on which a multipolar orientating magnetizing member is constructed of an alternate radial arrangement of a plural number of sector-like permanent magnets (1) and a plural number of also sector-like magnetic pole plates (2) of a magnetic material having a saturation magnetization of at least 10 kG.

**FIG. 3**



A METHOD FOR MANUFACTURING A CONTINUOUS-LENGTH  
EXTRUDED BAR OF PLASTIC MAGNET WITH CIRCUMFERENTIALLY  
MULTIPOLAR MAGNETIZATION

BACKGROUND OF THE INVENTION

The present invention relates to a method for manufacturing a continuous-length extruded bar of plastic magnet with circumferentially multipolar magnetization by extrusion molding.

It is a trend in recent years that control of higher and higher precision is required for various types of magnetic heads for picking up electronic and magnetic signals in robots and numerically controlled machines for factory automatization as well as in computers, VTRs and the like. Such high-precision control of magnetic heads is performed in many cases by means of a servomechanism using a stepping motor so that demand for multipolar tubular permanent magnets is rapidly increasing as an important component of stepping motors.

Multipolar tubular permanent magnets can be manufactured by several different methods of magnetization of a bar material of a plastic magnet extruded without magnetization or extrusion molding through a multipolar magnetizer so that the extruded bar material of the plastic magnet is already magnetized. The methods include :

- (A) multipolar magnetization of an isotropic plastic magnet along the inner or outer circumference;
- (B) multipolar magnetization of a radially anisotropic magnet oriented in the radial direction along the inner or outer circumference; and
- (C) molding of a circumferentially anisotropic magnet under magnetic orientation through a multipolar magnetizer.

The magnetic force of these three types of the permanent magnets is, as a general trend, in the decreasing order of circumferentially anisotropic magnets, radially anisotropic magnets and isotropic magnets. It is of course that control of a servo motor is easier when the inertia thereof is smaller and a smaller servomotor is preferable to larger ones assuming that the output force is the same. Accordingly, preferable multipolar tubular permanent magnets are of the type of the circumferentially anisotropic magnets capable of generating a larger torque than the other types in order to design smaller and lighter motors.

One of the conventional methods for the manufacture of a circumferentially anisotropic magnet is to fill the space between a core and a metal mold having a coil of a multipolar magnetizer with a powder of a magnetic material which is compression-molded by means of a pair of upper and lower punches while the magnet particles are magnetized by energizing the coil of the magnetizer. Alternatively, a method is disclosed in Japanese Patent Kokai 60-

89717 by utilizing the techniques of injection molding. These prior art methods, however, are disadvantageous in respect of the efficiency of production because each metal mold can serve for molding of only one product in one shot.

#### SUMMARY OF THE INVENTION

Accordingly, the scope of the present invention consists in manufacturing a continuous-length extruded bar of a plastic magnet having a high degree of orientation and multipolar circumferential anisotropy by mounting a multipolar, circumferentially anisotropic magnetizing member on the discharge port of an extruder machine and cutting the thus extruded continuous-length bar in a desired product length.

Thus, the present invention provides a method for manufacturing a continuous-length extruded bar of a plastic magnet with circumferentially multipolar magnetization which comprises extruding a plastic magnet composition out of the discharge port of an extruder machine having a multipolar, circumferentially anisotropic magnetizing member which is constructed of a plural number of radially oriented sector-like magnetic pole plates formed of a magnetic material of a saturation magnetization of at least 10 kG and a plural number of radially oriented sector-like permanent magnets, each pair of adjacent two thereof sandwiching one of the magnetic pole plates therebetween with the poles of the respective

permanent magnets having the same polarity facing to each other, coaxially mounted thereon.

#### BRIEF DESCRIPTION OF THE DRAWING

FIGURES 1a and 1b are each an illustration of the direction of magnetization in a circumferentially and radially anisotropic, multipolar tubular magnets, respectively.

FIGURES 2a and 2b are a plan view and an axial cross sectional view of an assembly of a metal mold and a pair of punching dies used in the prior art method for the manufacture of a circumferentially anisotropic, multipolar tubular magnet.

FIGURE 3 is a schematic illustration of the structure of the multipolar, circumferentially anisotropic orientating magnetizing member used in the inventive method and magnetic orientation therein.

FIGURE 4a is a plan view of the circumferentially anisotropic orientating magnetizing member used in the Example showing the sector-wise arrangement of the magnetic pole plates and permanent magnets in part and FIGURE 4b is an axial cross sectional view thereof.

FIGURE 5 is a chart of the distribution of the magnetic open flux measured along the circumference of the circumferentially anisotropic, multipolar tubular magnet prepared in Example 1.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

In the accompanying drawing, FIGURES 1a and 1b are for the illustration of a multipolar tubular magnets magnetized either circumferential or radial direction, respectively. The present invention particularly relates to the former type of multipolar tubular magnet made of a plastic magnet composition.

Figures 2a and 2b are for the illustration of a molding die assembly used in the conventional compression molding method for the preparation of a circumferentially anisotropic multipolar tubular magnet. Namely, the space formed between the core 3 and the metal mold 10 having a plural number of magnetizing coils 9 as a multipolar magnetizer is filled with a powder of the magnetic material, e.g. a plastic magnet composition, 8 which is compression-molded by means of the upper and lower punches 11,11 while the powder is under magnetization by energizing the coils 9.

In the following, the method of the present invention is described in detail with reference to the other figures of the accompanying drawing. The method of the invention is practiced by using an extruder machine, which is provided with a sizing die having a multipolar, circumferentially anisotropic orientating

magnetizing member mounted on the discharge port. This sizing die includes the circumferentially anisotropic multipolar orientating magnetizing member constructed, as is shown in FIGURE 3, by the assembly of a plural number of the sector-like permanent magnets 1 and a plural number of the magnetic pole plates 2 to surround the extruded material out of the discharge port of the extruder machine in such a manner that each pair of two adjacent pole plates 2 sandwiches one of the permanent magnets 1 therebetween or vice versa. The orientating magnetizing member is mounted firmly on the holder frame 4 to form a sizing die 7. When the magnetic material 8, such as a plastic magnet composition, is extruded out of the discharge port of the extruder machine, the extruded bar material is subjected to anisotropic multipolar magnetization as it goes through the opening of the sizing die 7. Although FIGURE 3 illustrates an 8-polar member having eight permanent magnets 1 and eight pole plates 2, the number of the magnets is of course not limited thereto. The magnetic pole plates 2 should be made of a material of high saturation magnetization of, preferably, at least 10 kG or, more preferably, at least 15 kG such as iron and alloys of iron and cobalt. A pole plate 2 is sandwiched by two sector-like permanent magnets 1 having the same polarity in the radial direction. Namely, the N-poles or S-poles of the two adjacent permanent magnets 1 face to each other with the pole plate 2 intervening therebetween and the magnets 1 and pole plates 2 are adhesively bonded together.

As is shown by the arrows in FIGURE 3, the direction of magnetic orientation in the permanent magnets 1 should preferably be parallel to the base of the equilateral triangle formed by the two adjacent magnetic pole plates or perpendicular to the magnetic pole plates adjacent to each other by sandwiching the same. Each of the permanent magnets 1 should be so powerful that at least 15 kG of the magnetic flux is obtained at the circumferential surface of the extruded material at the magnetic poles. The permanent magnet should also have a coercive force of at least 6 KOe and residual density of magnetic flux of at least 6 kG with the coefficient of temperature dependency of the coercive force and magnetic flux of each 0.1%/°C or smaller.

A coercive force of the permanent magnet smaller than 6 KOe means greater demagnetization thereof while a larger permanent magnet must be used when the density of the residual magnetic flux is smaller than 6 kG resulting in an increase in the magnetic leakage along the magnetic circuit in each case. The coefficient of temperature dependency should be as small as possible because a magnetic material having a larger temperature dependency is subject to greater thermal demagnetization in the process of molding.

Recommendable permanent magnet materials for the permanent magnets 1 in view of the above mentioned requirements include those of a rare earth-based magnet alloy or, in particular,



samarium-cobalt magnet alloy though not particularly limitative thereto. When consideration is made of the minimum magnetic field of about 10 KOe required to effect full orientation of a melt of a plastic magnet composition in which the dispersed phase of the magnetic material is a rare earth-based magnet powder, the material of the magnetic pole plates 2 should have a saturation magnetization of at least 10 kG or, preferably, at least 18 kG. When the saturation magnetization of the material of the magnetic pole plates 2 is smaller than 10 kG, the magnetic leakage from the magnetic pole plates is increased so that the magnetic orientation in the extruded bar material may eventually be incomplete.

The magnetic material molded according to the invention is a plastic magnet composition compounded of a fine powder of a permanent magnet such as rare earth-based magnets, ferrites and the like and a thermoplastic polymer as the matrix together with optional additives. The magnet powder should have an average particle diameter in the range from 0.5 to 100  $\mu\text{m}$  or, preferably, from 1 to 40  $\mu\text{m}$ . Various kinds of polymers having thermoplasticity can be used as the matrix including polyethylenes, polypropylenes, polystyrenes, polyvinyl chlorides, acrylic resins, polyamides, polyphenylene sulfides, polyphenylene oxides, polyacetals, polyethylene terephthalates, polybutylene terephthalates, polycarbonates, polyester elastomers, polyurethane elastomers and the like. The plastic magnet composition should be compounded in such a proportion of 35 to 70% by volume or, preferably, 40 to 65%

by volume of the magnet powder and 70 to 25% by volume or, preferably, 60 to 35% by volume of the thermoplastic polymer.

Although the accompanying drawing and the Examples given below are directed to a manufacturing process of an extruded bar material having a circular or annular cross section, it is of course that the above described inventive method is applicable to the manufacturing process of any tubular bar materials having different cross sections such as tubes having a polygonal cross section. As is understood from the above given description, the present invention provides a very efficient method for manufacturing a continuous-length extruded bar of plastic magnet with circumferentially multipolar magnetization so that the inventive method is industrially very valuable. In the following, the method of the present invention is described in more detail by way of Examples.

#### Example 1.

A plastic magnet composition was prepared by uniformly milling a mixture composed of 91% by weight or 58% by volume of a powdered rare earth-based permanent magnet (R-30, a product by Shin-Etsu Chemical Co.) having an average particle diameter of about 3.5 $\mu$ m and 9% by weight or 42% by volume of a plasticized polyvinyl chloride resin compound (MF-200, a product by the same company, *supra*). The plastic magnet composition was shaped into a continuous-length tubular bar by extrusion molding using a 25 mm diameter extruder machine. The sizing die of the extruder

machine was equipped with a multipolar, circumferentially anisotropic orientating magnetizing member as illustrated in FIGURES 4a and 4b. The orientating magnetizing member was constructed of 24 pieces of permanent magnets 1 made of the same R-30 rare earth magnet and 24 magnetic pole plates 2 made of pure iron having saturation magnetization of 21 kG each in a sector-like form with a central angle of  $7.5^\circ$  and alternately arranged around the center axis as is illustrated in FIGURE 4a. The sizing die had dimensions of 18 mm of outer diameter, 16 mm of inner diameter and 50 mm of length as is shown in FIGURE 4b and the temperature thereof was controlled not to exceed  $50^\circ\text{C}$ . The extruder machine was run at  $150^\circ\text{C}$  with the screw rotated at a velocity of 60 rpm.

A piece of plastic magnet with circumferentially multipolar magnetization was taken from the thus prepared continuous-length extruded bar material by cutting in a plane perpendicular to the axis and the distribution of magnetic open flux around the circumference was measured by using a gaussmeter to give the results shown in FIGURE 5 indicating that the tubular plastic magnet with circumferentially multipolar magnetization had a very high open flux of almost 2 kG.

#### Comparative Example 1.

For comparison, the same plastic magnet composition as used in the above described experiment was extrusion-molded into

a continuous-length tube of the same dimensions as above without mounting the circumferentially orientating magnetizing member on the discharge port of the extruder machine. The thus obtained plastic magnet bar was subjected to circumferential multipolar magnetization using a 24-polar magnetization yoke having an inner diameter of 18.1 mm by energizing each magnetizing coil with discharge of a capacitor of 600  $\mu$ F capacity charged at 2000 volts. The thus prepared multipolar circumferentially magnetized plastic magnet was subjected to the measurement of the magnetic open flux around the circumference in the same manner as above to find that the maximum value of the peaks in a chart similar to FIGURE 5 was about 1 kG.

#### Example 2.

A plastic magnet composition was prepared by uniformly kneading, in a kneader at 220 °C, 45% by volume of a polyester elastomer having a hardness of 60 according to JIS K 6301 and 55% by volume of a powder of the same rare earth-based magnetic alloy as used in Example 1 having an average particle diameter of about 3.5  $\mu$ m. This plastic magnet composition was extrusion-molded into a continuous-length tubular form of the same dimensions as in Example 1 with the die of which the temperature was controlled not to exceed 50 °C. The same circumferentially orientating magnetizing member as in Example 1 was mounted on the discharge port of the extruder machine which was run at 250 °C.

The thus obtained circumferentially magnetized plastic magnet was subjected to the measurement of the magnetic open flux in the same manner as in Example 1 to find that the maximum value at the peaks in a chart similar to FIGURE 5 was 1.8 kG.

#### Comparative Example 2.

The experimental procedure was the same as in Comparative Example 1 excepting the replacement of the plastic magnet composition with the composition used in Example 2. The measurement of the magnetic open flux along the circumference of the tubular magnet gave a result that the maximum value at the peaks in a chart similar to FIGURE 5 was about 0.9 kG.

CLAIMS

1. A method for manufacturing a continuous-length extruded bar of plastic magnet with circumferentially multipolar magnetization which comprises extruding a plastic magnet composition composed of a powder of a permanent magnet and a thermoplastic polymer out of the discharge port of an extruder machine provided with a multipolar, circumferentially anisotropic orientating magnetizing member, which is constructed of a plural number of radially oriented magnetic pole plates formed of a magnetic material having a saturation magnetization of at least 10 kG and a plural number of radially oriented permanent magnets, each pair of adjacent two thereof sandwiching one of the magnetic pole plates therebetween with the poles of the respective permanent magnets having the same polarity facing to each other, coaxially mounted on the discharge port.
2. The method as claimed in claim 1 wherein the radially oriented permanent magnets are made of a rare earth-based permanent magnet alloy.

FIG. 1a

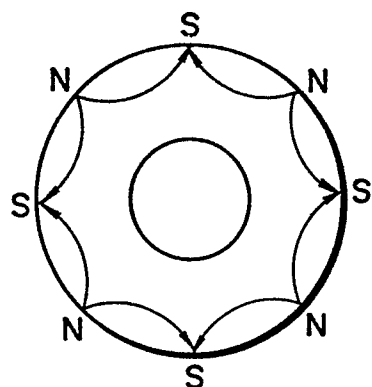


FIG. 1b

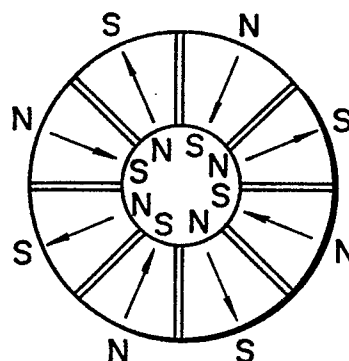


FIG. 2a

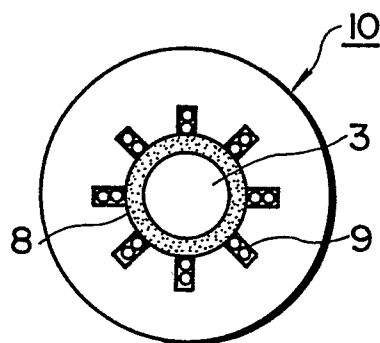


FIG. 2b

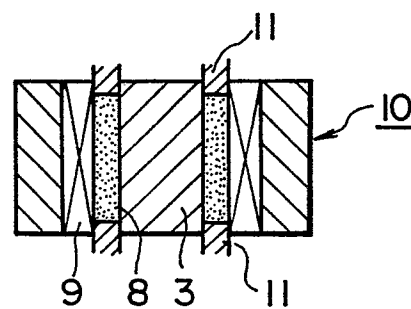
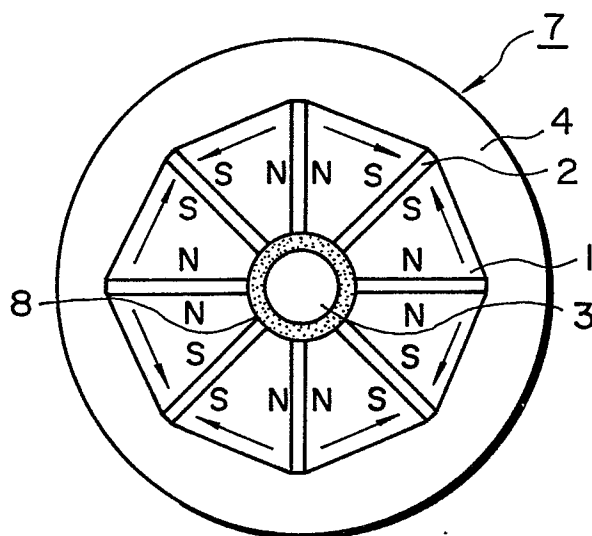


FIG. 3



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FIG. 4a

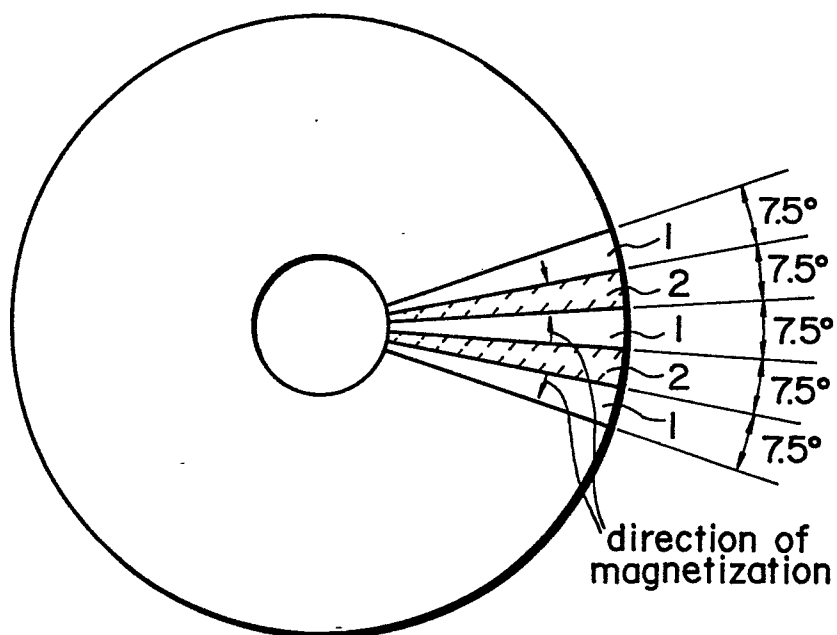
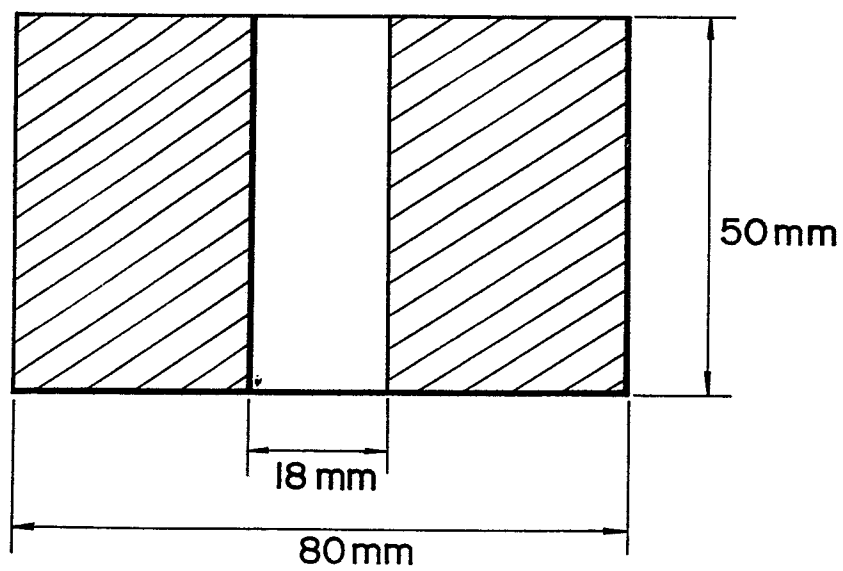


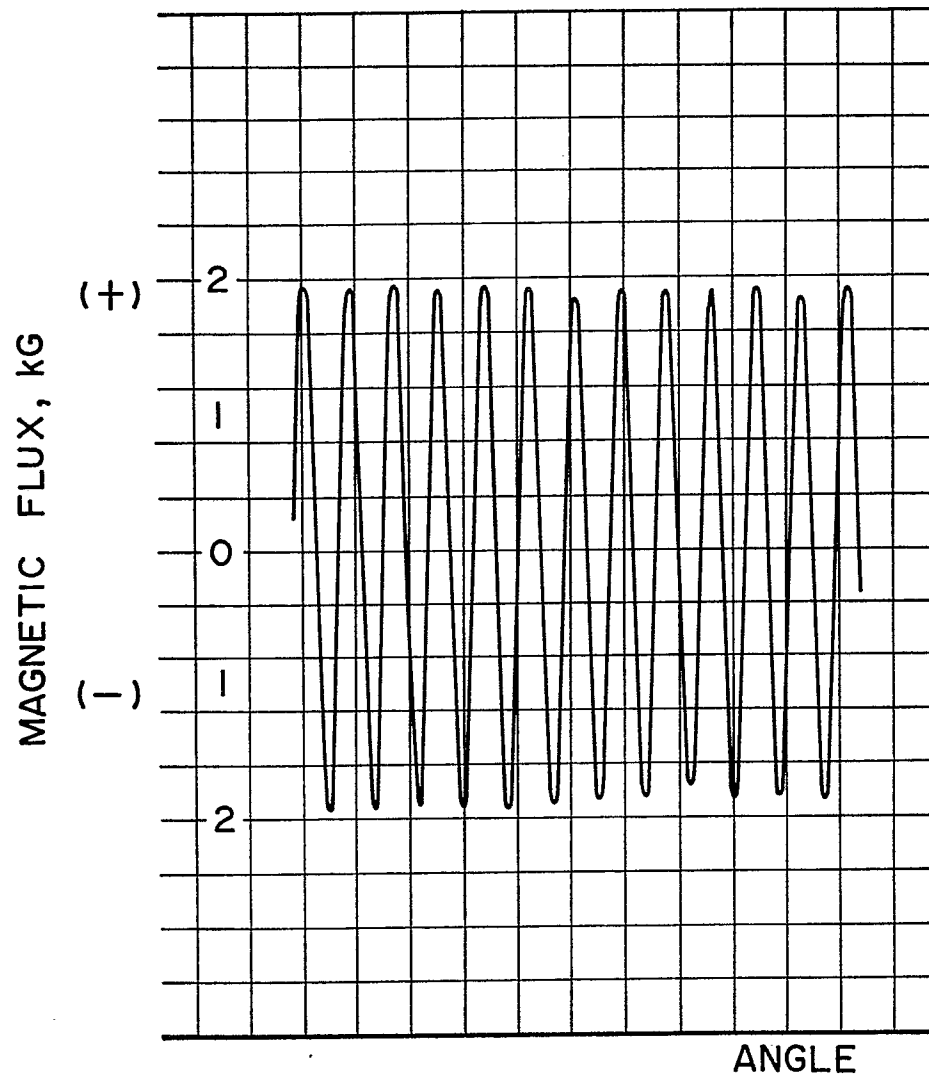
FIG. 4b





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FIG. 5





DOCUMENTS CONSIDERED TO BE RELEVANT			EP 87400682.8
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.4)
X	<p>US - A - 3 640 657 (ROWE et al.)</p> <p>* Claims 1-11; column 2, line 9 - column 3, line 53 *</p> <p>----</p>	1	<p>H 01 F 1/117</p>
			<p>TECHNICAL FIELDS SEARCHED (Int. Cl.4)</p>
			<p>H 01 F 1/00</p> <p>H 01 F 3/00</p> <p>H 01 F 13/00</p> <p>G 11 B 5/00</p> <p>H 02 K 1/00</p> <p>H 02 K 15/00</p>
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
VIENNA		06-07-1987	VAKIL
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone</p> <p>Y : particularly relevant if combined with another document of the same category</p> <p>A : technological background</p> <p>O : non-written disclosure</p> <p>P : intermediate document</p> <p>T : theory or principle underlying the invention</p> <p>E : earlier patent document, but published on, or after the filing date</p> <p>D : document cited in the application</p> <p>L : document cited for other reasons</p> <p>&amp; : member of the same patent family, corresponding document</p>			