

12

EUROPEAN PATENT APPLICATION

21 Application number: 88119199.3

51 Int. Cl.⁴: **G11B 11/10**, **G11B 7/08**

22 Date of filing: 15.09.83

30 Priority: 25.01.83 JP 11037/83
18.04.83 JP 68770/83
19.04.83 JP 69619/83

43 Date of publication of application:
07.06.89 Bulletin 89/23

60 Publication number of the earlier application in
accordance with Art.76 EPC: 0 115 666

84 Designated Contracting States:
DE FR GB IT

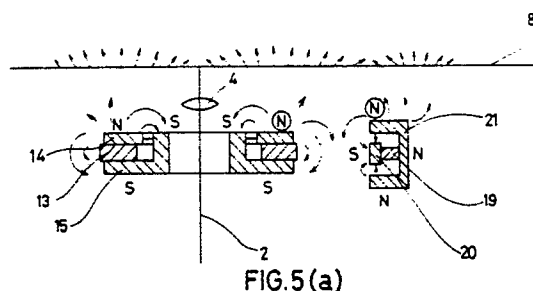
71 Applicant: **SHARP KABUSHIKI KAISHA**
22-22 Nagaike-cho Abeno-ku
Osaka 545(JP)

72 Inventor: **Fujii, Yoshikazu**
6-36 Chiyogaoka 2-chome
Nara-shi Nara-ken(JP)
Inventor: **Deguchi, Toshihisa**
2-200-5 Daiwa-cho Gakuen
Nara-shi Nara-ken(JP)
Inventor: **Inui, Tetsuya**
14 Inyo-cho
Nara-shi Nara-ken(JP)
Inventor: **Yamaoka, Hideyoshi**
2-5-21 Amaminishi
Matsubara-shi Osaka-fu(JP)

74 Representative: **Brown, Kenneth Richard et al**
R.G.C. Jenkins & Co. 26 Caxton Street
London SW1H 0RJ(GB)

54 **Optical focus position control device.**

57 This device has focussing (13 - 17) and tracking (19 - 24) controllers for moving the position of the optical focus of a light beam, such as a laser beam (2), respectively in focussing and tracking directions. Each controller has an electromagnetic drive means which comprises a closed magnetic circuit including a permanent magnet (13; 19), a yoke plate (14; 20), a yoke (15; 21), and a magnetic space (16; 22) between the yoke plate and yoke, and a drive coil (17; 23) arranged to move in the magnetic space. In order to minimise the magnetic field applied to the magnetic disc by the two electromagnetic drive means, the present invention is characterised in that respective portions of the closed magnetic circuits of the focussing and tracking electromagnetic drive means which are both closest to each other and disposed to be closest to the disc are of the same magnetic polarity.



EP 0 318 772 A1

OPTICAL FOCUS POSITION CONTROL IN OPTICAL DISC APPARATUS

Background of the Invention

The present invention relates to an optical focus position control device of an optical disc apparatus that records, plays back, and erases a variety of information by irradiating optical beams such as the laser beams onto a recording media composed of magnetic film.

Conventionally, any of the existing optical discs easily causes its surface to vibrate during rotation, and as a result, recording tracks on the disc are obliged to displace themselves in the direction of the optical axis of the incident laser beams that irradiate the disc surface. Also, being adversely affected by any deviation between the center position of the disc and the motor shaft that drives the disc, recording tracks of such a disc are then obliged to displace themselves in the direction of the disc radius (hereinafter called the radial direction). To prevent the recording tracks from any displacement, a device is provided so that the laser beam focus position can be correctly followed up within the optical head mechanism to enable the incident laser beam spot to correctly match the recording tracks of a disc. Such a device is called the optical focus position control in the following description.

Using any of the existing optical disc apparatus such as the one that only plays back information without containing any magnetic film recording media, or the other one that can record any additional information, in order to fine adjust the focus position of the incident laser beams (hereinafter called the focus controller) to deal with the disc displacement in the direction of the optical axis of the incident laser beams, a device that can vary the position of the objective lens by means of the electromagnetism is well known by now. On the other hand, to fine adjust the focus position of the incident laser beams (hereinafter called the tracking controller) to deal with the disc displacement in the radial direction, a variety of mechanism that can fine adjust the focus position of the incident laser beams via the rotary mirror that reflects the incident laser beams against any optimum direction have been introduced. On the other hand, a new proposal has been introduced quite recently, which provides a mechanism capable of jointly performing both the focus and tracking controls mentioned above, by varying the position of the objective lens via the electromegnetic force. Basically, said mechanism comprises a coil that can be moved integrally with an objective lens and a stationary

permanent magnet, thus causing the objective lens to be displaced by the current flowing through said coil.

If such an already known mechanism capable of jointly performing both the focus and tracking controls by varying the position of the objective lens via the electromagnetic force is actually applied to an optical disc apparatus, it will easily create problems described below.

Since the proposed mechanism uses magnetism generated by a permanent magnet, a leakage magnetism or flux will be generated in portions peripheral to the disc. Nevertheless, since the disc uses the magnetic film for the recording media, if such a leakage mechanism adversely affects said magnetic film, the following problems will arise.

(1) When the laser beams are irradiated onto an optical magnetic disc to cause temperature to rise, and simultaneously an information is recorded on said disc via an external magnetism, if a leakage magnetism out from said optical focus position control affects the disc, then the quality of the recorded information will be degraded significantly.

(2) When playing back the recorded information via the magnetic-optical effect by irradiating laser beams onto the optical magnetic disc, any leakage flux from said optical focus position control may adversely affect the disc, thus causing the recorded information to be easily erased.

In the light of these potential disadvantages, if an optical disc apparatus is used, it is quite necessary to completely prevent even the slightest leakage flux out of the optical focus position control from seriously affecting the optical disc. In addition, there are still further problems to solve. For example, using a mechanism incorporating an objective lens-mirror cylinder which is supported by rubber material whose one end is secured to a stationary holder, while said objective lens-mirror cylinder can be driven by electromagnetic force existing between the coil secured to said objective lens-mirror cylinder and the magnetic circuit secured to said stationary cylinder. Since said rubber-elastic material supports the objective lens-mirror cylinder, it cannot fully resist the tilting force of the objective lens-mirror cylinder, and as a result, any accidental force may be generated when the drive force generated by said electromagnetic force cannot be applied to the gravity center of the objective lens-mirror cylinder, thus causing said cylinder to eventually generate a rotary movement. This will cause the optical axis of beams to tilt against the center axis of the objective lens, and so either the off-axis astigmatism or coma aberration will adversely affect

the disc tracks containing information, causing beams to poorly focus on them, and as a result, quality of the recorded information will be degraded significantly.

Summary of the Invention

The present invention provides an improved mechanism for the optical focus position control device by minimizing any adverse effect of the leakage magnetism against the optical disc.

A still further object of the present invention is to securely achieve a mechanism that stably drives the objective lens in dual directions, i.e., either in the vertical (up/down) or horizontal (left/right) direction without causing the objective lens to incline by using an optical focus position controller capable of controlling both the tracking and focussing of an optical disc apparatus, and yet, the present invention aims at achieving such a mechanical device featuring a significantly compact dimension.

Brief Description of the Drawings

Figure 1 shows a simplified block diagram of an optical disc apparatus as a preferred embodiment of the present invention.

Figure 2 shows a sectional view of an optical focus position controller as a preferred embodiment of the present invention.

Figure 3 shows sectional views of a focussing controller as a preferred embodiment of the present invention.

Figure 4 shows sectional views of a tracking controller as a preferred embodiment of the present invention.

Figure 5 shows sectional views of the combined focussing and tracking controller.

Figure 6 shows a plane view of an optical focus position control device as a preferred embodiment of the present invention.

Figure 7 shows a sectional view of an optical focus position control device incorporating the first means for properly dealing with the damping characteristics as a preferred embodiment of the present invention.

Figure 8 shows a plane view of an optical focus position control device incorporating the second means for properly dealing with the damping characteristics related to the present invention.

Figure 9 also shows a plane view of an optical focus position control device incorporating the third means for properly dealing with the damping characteristics related to the present invention, and

Figure 10 also shows a plane view of an optical focus position control device incorporating the fourth means for properly dealing with the damping characteristics related to the present invention.

Detailed Description of the Invention

Figure 1 shows a simplified block diagram of an optical disc apparatus as a preferred embodiment of the present invention. In Figure 1, symbol 1 denotes a laser beam source that emits laser beams 2. Symbol 3 denotes a mirror, and symbol 4 denotes an objective lens that causes the laser beams 2 to be focussed onto the recording media surface of a disc. Symbol 5 denotes an optical focus position control device that causes the optical focus position to be accurately followed onto the tracks of the recording media of a disc by driving an objective lens 4 either in the vertical (up/down) or horizontal (left/right) direction. Symbol 6 denotes an optical head that contains all the optical devices mentioned above. Symbol 7 denotes a recording/erasing coil that provides the surface of the disc recording media with magnetism while either recording or erasing any information. Symbol 8 denotes an optical disc incorporating a disc recording media 8, and symbol 9 denotes a motor that drives said optical disc to rotate.

The focus control to be performed by said optical focus position control device 5, i.e., a fine adjustment of the incident laser beam focus position against the disc displacement made in the direction of the incident laser beam axis can be achieved by causing the objective lens 4 to move in the direction of the thickness of said optical disc 8. On the other hand, the tracking control to be performed by said optical focus position control device 5, i.e., a fine adjustment of the incidental laser beam focus position in dealing with the disc displacement in the radial direction can be performed by causing the objective lens 4 to move in the radial direction of the optical disc 8.

Figure 2 shows a detailed sectional view of the optical focus position control device as a preferred embodiment of the present invention. First, the focus controller is described below. Symbol 10 denotes a lens-mirror cylinder containing and supporting an objective lens 4, where said lens-mirror cylinder 10 is installed to a holder 11 so that it can

be vertically moved by the elastic material 12 movable in the direction of the focus.

Symbol 13 denotes the focussing permanent magnet, while symbol 14 denotes the focussing yoke plate, and symbol 15 denotes the focussing yoke, and so they make up a closed magnetic circuit, while each is securely installed to the holder 11. Magnetic space 16 is provided between said focussing yoke plate 14 and focussing yoke 15, which is available for the focussing operation. Symbol 17 denotes the focus driving coil, which is installed to the lens-mirror cylinder across said magnetic space 16. If the focus control current is fed to said focus driving coil 17, magnetism will be generated in said coil 17, and as a result, due to a combined effect with the other magnetism generated by said focussing permanent magnet 13, all the focus driving coil 17, lens-mirror cylinder 10, and the objective lens 4, will displace themselves in the direction of the incident laser beam axis. These make up the focus controller 18. Structure of the tracking controller is described below.

Symbol 19 denotes a permanent magnet available for the tracking operation, while symbol 20 denotes a yoke plate and symbol 21 denotes a yoke available for the tracking operation, respectively. These make up a closed magnetic circuit. These units are securely installed to a holder (not illustrated) that fully supports the optical focus position control device.

Magnetic space 22 available for the tracking operation is provided between said yoke plate 20 and yoke 21. These units are securely installed to a holder (not illustrated) that fully supports the optical focus position control device. Magnetic space 22 available for the tracking operation is provided between said yoke plate 20 and yoke 21. Symbol 23 denotes a radial driving coil, which is securely installed across said magnetic space 22 onto the radial drive coil holder 24. As shown in the drawing, said radial drive coil holder 24 is connected to the focus controller 18. Since the focus controller 18 can be moved by the elastic material (not illustrated) that is movable in the radial direction, if the tracking control current is fed to said radial drive coil 23, magnetism will be generated by said coil 23, and as a result, due to a combined effect with the other magnetism generated by the permanent magnet 19 that is used for the tracking operation, the focus controller 18 will displace its position in the radial direction. These make up the tracking controller 25.

The present invention provides a variety of means for effectively preventing the optical focus position control device comprising said focus controller 18 and tracking controller 25 from causing its leakage magnetism to adversely affect the recording media 8 of an optical disc. Such effective

means are described below.

(1) Details of means related to the focus controller.

Figure 3-a shows a sectional view of a focus controller incorporating an improved means as a preferred embodiment of the present invention, whereas Figure 3-b shows a sectional view of the other focus controller without incorporating any improved means. Symbols N and S respectively denote the north and south poles. As shown in Figure 3-a, the focus controller incorporating an improved means related to the present invention provides magnetic space 16 available for the focussing operation in an area close to the optical disc. This construction minimizes leakage magnetism that otherwise adversely affects the recording media 8 of the optical disc. In other words, leakage magnetism will significantly affect the surface of the recording media 8 of the optical disc if said magnetic space 16 for the focussing operation is provided in an area remote from the optical disc as shown in Figure 3-b. Length of each arrow in Figures 3-a and 3-b respectively denotes the intensity of the leakage magnetism at the position where the focussing operation just starts, while the direction of the leakage magnetism is shown in the arrowed direction.

(2) Details of means related to the tracking controller

Figure 4-a shows a sectional view of the tracking controller incorporating an improved means as a preferred embodiment of the present invention, whereas Figure 4-b shows a sectional view of the other tracking controller without incorporating any improved means. The tracking controller incorporating an improved means related to the present invention provides the permanent magnet 19 available for the tracking operation in the center position of the closed magnetic circuit. This construction minimizes leakage magnetism that otherwise adversely affects the recording media 8 of the optical disc. In other words, in such a construction where permanent magnets 19 available for the tracking operation are provided encircling the closed magnetic circuit, if the magnitude of magnetism that functions in the magnetic space 22 is designed to be equal to said magnetic space 22 of Figure 4-a available for the tracking operation, leakage magnetism will significantly affect the surface of the recording media 8 of the optical disc.

(3) Details of means related to both the focussing

and tracking controllers

Figure 5-a shows sectional views of both the focussing and tracking controllers incorporating improved means as preferred embodiments of the present invention, whereas Figure 5-b shows sectional views of both the focussing and tracking controllers without incorporating any improved means related to the present invention. As shown in Figure 5-a, both the focussing and tracking controllers with the improved means are set in positions being close to each other, while the magnetic poles of the yoke plate 14 available for the focussing operation set in positions close to the optical disc and the yoke 21 available for the tracking operation are of the same polarity, i.e., poles N and N face each other, as shown in Figure 5-a. On the other hand, an example denoted in Figure 5-b shows that the magnetic poles of the focussing and tracking controllers without incorporating any improved means related to the present invention are set in positions being close to each other, while the magnetic poles of the yoke plate 14 available for the focussing operation being set in positions close to the optical disc and the yoke 21 available for the tracking operation are of the opposite polarity, i.e., poles N and S face each other. In this case, magnitude of the leakage magnetism adversely affecting the surface of the recording media 8' of the optical disc doubles the other leakage magnetism affecting the device shown in Figure 5-a.

In addition to the improved constructions described above, any adverse effect of the leakage magnetism against the surface of the recording media 8' of the optical disc can be minimized furthermore by additionally providing said improved constructions with the following means including (a) a construction that provides a highly permeable magnetic substance such as permalloy in a position facing the optical disc of the optical focus position control device, (b) a construction that includes the entire optical focus position control device in said highly permeable magnetic substance, (c) a construction that includes a holder made of said highly permeable magnetic substance for supporting the entire optical focus position control device, and (d) a construction that includes both the focussing and tracking controllers within said highly permeable magnetic substance.

Figure 6 shows a plane view of the optical focus position control device shown in Figure 2. As shown in the drawing, an objective lens mirror cylinder 10 is provided so that it can be moved only in the dual axes directions, i.e., either in the vertical (up/down) or horizontal (left/right) directions by being supported by the vertically workable elastic material 12 that moves in the focussing direction and by the horizontally workable elastic material 26

that moves in the radial direction. This construction prevents the objective lens from even the slightest incline. A focussing drive coil 17 is provided so that it can only move in the direction across the focusing magnetic space 16, while a radial drive coil 23 is provided so that it can only move in the direction across the tracking magnetic space 22. As a result, magnetic space available for both the focussing and tracking operations can be extremely narrowed, and so electromagnetic force can be used very effectively. This permits the permanent magnet size to be significantly minimized, and as a result, an extremely compact size of the optical focus control device can be achieved.

Next, the movement characteristics of both the focussing and tracking controllers of the objective lens 10 are described below.

(1) Movement characteristics of the focussing controller

As shown in Figures 2 and 6, the focussing controller is driven by the electromagnetic effect that interacts between the focussing closed magnetic circuit secured to the interim holder 11 and the focussing drive coil 17 secured to the objective lens mirror cylinder 10. Said interim holder 11 and the objective lens mirror cylinder 10 are connected to each other via the elastic material that is workable only in the vertical direction by moving in the direction of focussing, i.e., via a parallel spring 12 that can be moved in the direction of focussing.

Assuming that the weight of the movable part in the direction of focussing including the objective lens 4, objective lens mirror cylinder 10, and the driving coil 17 for focusing operation is Mf , whereas the vertical spring constant of the parallel spring 12 moving in the direction of focussing is Kf , and then the objective lens mirror cylinder 10 will be provided with a resonance frequency which is represented by a formula

$$fF = \frac{1}{2\pi} \sqrt{\frac{KF}{MF}}$$

when performing vertical (up/down) movements. As soon as a driving force for the focussing operation is given by the interacting electromagnetic force, the movement phase delay in the displacement XF caused by the objective lens mirror 10 in the focussing direction can be represented to be 0° through 90° when $0 < f < fF$, where f (Hz) represents a frequency, whereas such a delay in the movement phase can be represented to be 90° through 180° when $fF < f$, and it will be exactly at 180° when $fF \ll f$. As a result, if the focussing

target position is Y_f , by advancing the phase of the signal representing the focussing drive force FF via the phase advancing compensation circuit, the movement phase delay in the displacement XF caused by the focus direction moving part can be adjusted to any desired level below 18° . This ensures a very stable focus control operation.

(2) Movement characteristics of the tracking controller

As shown in Figures 2 and 6, the tracking controller is driven by the electromagnetic effect that interacts between the closed magnetic circuit secured to the tracking closed magnetic circuit that is secured to the stationary holder 27 and the tracking drive coil 23 on the tracking drive coil holder 24 being secured to the interim holder 11. Said stationary holder 27 and the interim holder 11 are connected to each other via the elastic material that is workable only to the left and to the right by moving in the radial direction, i.e., via a parallel spring 26 that moves in the direction of the disc radius. Assuming that the weight of the focussing controller 18 is MT and the spring constant of the parallel spring 26 moving in the direction of the disc radius is KT , and then the objective lens mirror cylinder 10 will have a resonance frequency (hereinafter called the primary resonance frequency) f_T which is represented by a formula

$$f_T = \frac{1}{2\pi} \sqrt{\frac{KT}{MT}}$$

when the focussing controller 18 moves to the left and to the right. The interim holder 11 and the objective lens mirror cylinder 10 are connected to each other via the parallel spring 12 moving in the direction of focussing. while said parallel spring 12 moves to the left and to the right due to a certain amount of elasticity. Thus, assuming that the spring constant of the focus-direction parallel spring 12 is KF' , when it moves to the left and to the right and the objective lens mirror cylinder 10 also moves to the left and to the right, the spring constant will have a resonance frequency (hereinafter called the secondary resonance frequency) represented to be

$$f'T = \frac{1}{2\pi} \sqrt{\frac{KF'}{MF'}}$$

As described above, whenever the objective lens mirror cylinder 10 moves to the left and to the right, both the primary and secondary resonance

frequencies exist. Note that the spring constant KF' of the parallel spring that moves in the focussing direction increases significantly when the spring moves to the left and to the right, which is denoted by $KF' \gg KT$. This means that the secondary resonance frequency $f'T$ is significantly higher than the primary resonance frequency f_T , the relationship of which is denoted by $f'T > f_T$. When the tracking drive force FT is generated by the interacting electromagnetic force mentioned above with a frequency denoted by f , the movement phase delay caused by the displacement XT of the objective lens mirror cylinder 10 in the tracking direction is 0° through 90° when $0 < f < f_T$, or 90° through 270° when $f_T < f < f'T$, or 270° through 360° when $f'T < f$.

When the tracking drive force FT is generated, the delay in the movement phase caused by the displacement XT of the objective lens mirror cylinder 10 moving to the tracking target position YT should remain below 180° throughout the frequency bands of the tracking control signal. As described earlier, even if the phase advancing compensation circuit is used to advance the phase of the tracking drive signal FT , since there is a certain limit for advancing the phase amount, the phase cannot be compensated for in order that it can exceed 180° significantly.

To properly compensate for the phase delay, the second resonance frequency $f'T$ should be set at an optimum level higher than the frequency band of the tracking control signal. Although frequency bands available for the tracking control signal are variable according to uses, generally, an optical disc apparatus uses 1 through 4KHz of the frequency bands. As a result, it was made clear that the secondary resonance frequency $f'T$ should be set at a level above 8KHz. Means for designing a construction that fully satisfies the above conditions are described below.

As described above, the secondary resonance frequency $f'T$ can be determined by the spring constant KF' of the parallel spring 12 moving in the focussing direction when it moves to the left and to the right and by the weight MF of the moving parts in the focussing direction, where the greater the spring constant KF' , the greater the secondary resonance frequency $f'T$. Nevertheless, since there is a certain limit in the means for decreasing the weight MF of the objective lens 4 and the lens mirror cylinder 10, the weight MF of the part moving in the focussing direction cannot be decreased significantly. (Normally, said weight MF is designed in a range from 0.5 to 10 grams.) The inventors followed up trials for increasing the spring constant KF' of the parallel spring 12 movable in the focussing direction during its movement to the left and to the right.

The spring constant KF' was found to be

$KF'/KF = (XY/YF)^2$ when the parallel spring 12 had a width XF and a thickness YF . As a result, it is clear that the spring constant KF' in the horizontal direction (left/right) can be increased by expanding the width XF and decreasing the thickness YF of said parallel spring 12. In the light of the relationship denoted by

$$\frac{f'T}{fT} = \sqrt{\frac{KF'}{KF}},$$

the secondary resonance frequency $f'T$ can be obtained by an equation $f'T = \frac{XF}{YF} \cdot fF$. It was eventually made clear that the parallel spring 12 moving in the horizontal direction (left/right) should be designed so that it can be provided with 20 through 50 micron meter of the thickness and an actual width that is 50 up to 100 times the reference width YF . If the parallel spring 12 movable in the focussing direction can be correctly designed in accordance with the findings described above, the delay in the movement phase caused by the displacement XT of the objective lens 4 against the tracking target position can be decreased below 180° within the frequency bands available for the tracking control signal. It is important that the phase advancing compensation circuit be used for correctly compensating for the movement phase.

According to the results of the trials followed up by the inventors, very stable focussing and tracking controls were actually achieved by using a parallel spring 12 made from beryllium-copper alloy having 30 through 50 micron meters of the thickness. Nevertheless, since there are two kinds of the resonance frequencies; fF and fT , if the damping characteristics in the directions of focussing and tracking control remain negligible, the resonance multiple factor in said resonance frequencies fF and fT will grow, thus causing any interference vibration to easily occur during either the focussing or tracking control operation. Also, when a certain frequency above the resonance frequency level is fed, the phase in responding to the displacement of the movable parts will be extremely delayed to a point very close to 180° , which will result in an extremely unstable optical focus position control operation. To prevent this and ensure satisfactory amount of the damping characteristics, the present invention effectively provides the following means.

(1) Structure of the primary means

Figure 7 shows a sectional view of the optical focus position control device incorporating the primary means embodied by the present invention.

As shown in the drawing, a damping material 28 is held in a space A between the objective lens mirror cylinder 10 and the focussing yoke 15, thus increasing the damping characteristics in the direction of the focus. The other damping material 28 is held in a space B between the tracking drive coil holder 24 and the stationary holder 27, thus increasing the damping characteristics in the direction of the tracking. To make up said damping material 28, viscose-elastic materials such as silicon rubber, butyl rubber, silicon-butyl rubber, and acrylic-ethylene rubber, foaming synthetic resin such as foamed polyurethane, and viscose fluid such as silicon grease, can be made available.

(2) Structure of the second means

Figure 8 shows a plane view of the optical focus position control device incorporating the second means embodied by the present invention. Parallel spring 12 that moves in the direction of focus has a structure that connects two concentric circles, where two flat sheet springs, each being connected to four arms at the edges, are provided in the upper and lower positions (See Figure 2). Said parallel spring 12 moving in the direction of focus causes the objective lens mirror cylinder 10 to move only in the vertical direction relative to the position of the interim holder 11. Damping material 29 is bonded to the portion C of the surface of said parallel spring 12, where the largest amount of the relative displacement exists, thus resulting in greater damping characteristics in the direction of focus. To make up said damping material 29, viscose-elastic materials such as silicon-rubber, butyl rubber, silicon-butyl rubber, and acrylic-ethylene rubber, and foaming synthetic resin such as foamed polyurethane, can be made available.

(3) Structure of the third means

Figure 9 shows a plane view of the optical focus position control device incorporating the third means embodied by the present invention. Said damping material 29 is bonded to the portion C of the surface of the parallel spring 12, where the largest amount of the relative displacement exists. Said damping material 29 is connected to the parallel spring 12 via the edges C1 and C2. Viscose fluid such as silicon grease is charged in the portion C3 located between the edges C1 and C2, thus increasing the damping characteristics in the direction of focus.

(4) Structure of the fourth means

Figure 10 shows a plane view of the optical focus position control device incorporating the fourth means embodied by the present invention. The parallel spring 26 moving in the tracking direction is secured to the interim holder 11 (See Figure 2) in the center position, while said spring 26 is also secured to the stationary holder 27 in both ends. First, one end D is secured to the stationary holder 27, and then the other end E is inserted into a slit 30 of the stationary holder 27, and finally viscose fluid 31 such as silicon grease is charged into said slit 30 to complete the installation of said parallel spring 26 that moves in the tracking direction.

In addition to these means described above, there are a variety of useful means for effectively making up either the focus-direction or tracking-direction movable parallel springs by using vibration-proof alloy such as manganese-copper alloy, ferro-aluminum alloy, nickel-titanium alloy, magnesium alloy, etc. It is also useful to make up said springs by coating latexed acrylic-ethylene rubber over both surfaces of either the focus-direction or tracking direction moving parallel spring. (Note that, if a sheet rubber is bonded to a metal spring by any adhesive agent such as primer, it will disadvantageously cause the spring to become stiff and the spring constant to increase.)

A wide variety of useful means for effectively increasing the damping characteristics have been described above, however, it will be quite useful if such effective means as described above are mutually combined so that the damping characteristics can be improved furthermore.

The embodiments of the invention thus described with reference to the accompanying drawings will obviously be suggestive of derivations and modifications. For example, the focusing and/or tracking means can be applied to any head positioning device for a recording disc, the head being used for recording, playing back or erasing information or for performing any combination of these functions.

There are thus described above novel features which the skilled man will appreciate give rise to advantages. These are each independent aspects of the invention to be covered by the present application, irrespective of whether they are included within the scope of the following claims. Reference is hereby directed to copending European patent application No. 83305435.6 from which this present application is divided and to copending European patent application No. 83305435.6.

Claims

1. An optical focus position control device for an optical disc apparatus that records, plays back, and/or erases information on a recording medium (8) which includes a magnetic film by irradiation of said magnetic film with an optical beam, such as a laser beam (2), said optical focus position control device comprising a focussing controller operable to move the position of the optical focus of the beam in the focussing direction, that is in a direction transverse the film, and a tracking controller (19 - 24) operable to move said position of the optical focus of the beam in the tracking direction, that is in a direction parallel to the film;
the focussing controller having focussing electromagnetic drive means (13 - 17) which comprises:
a closed magnetic circuit which includes a permanent magnet (13), a yoke plate (14), a yoke (15) and a magnetic space (16) between said yoke plate (14) and yoke (15), and;
a drive coil (17) arranged to move in said magnetic space;
and said tracking controller having tracking electromagnetic drive means which comprises:
a closed magnetic circuit which includes a permanent magnet (19), a yoke plate (20), a yoke (21) and a magnetic space (22) between said yoke plate (20) and yoke (21), and;
a drive coil (23) arranged to move in said magnetic space (22);
characterised in that respective portions of the closed magnetic circuits of the focussing and tracking electromagnetic drive means which are both closest to each other and disposed to be closest to the film are of the same magnetic polarity.

2. An optical focus position controlling device according to claim 1 wherein said respective portions are portions of the focussing controller yoke plate (14) and of the tracking controller yoke (21), respectively.

3. An optical focus controlling device according to claim 1 or claim 2 wherein said focussing controller includes an intermediate holder (11) and is mounted with respect to a stationary holder (27) by way of a first parallel spring coupling (26) arranged to allow movement of the focussing controller relative to the stationary holder in the tracking direction and wherein there is provided an objective lens (4) by which the optical beam is focussed and a cylindrical holder (10) in which the objective lens is mounted, said cylindrical holder being coupled to the intermediate holder (11) by way of a second parallel spring coupling (12) arranged to allow movement of the cylindrical holder relative to the intermediate holder in the focussing direction, said focussing electromagnetic drive means being coupled to drive the cylindrical holder in the focussing

direction relative to the intermediate holder and said tracking electromagnetic drive means being coupled to drive the intermediate holder in the tracking direction relative to the stationary holder.

4. An optical focus position controlling device according to claim 3, further including elastic material (29) bonded to said first and/or second parallel spring coupling(s) for improving the damping characteristics thereof.

5

10

15

20

25

30

35

40

45

50

55

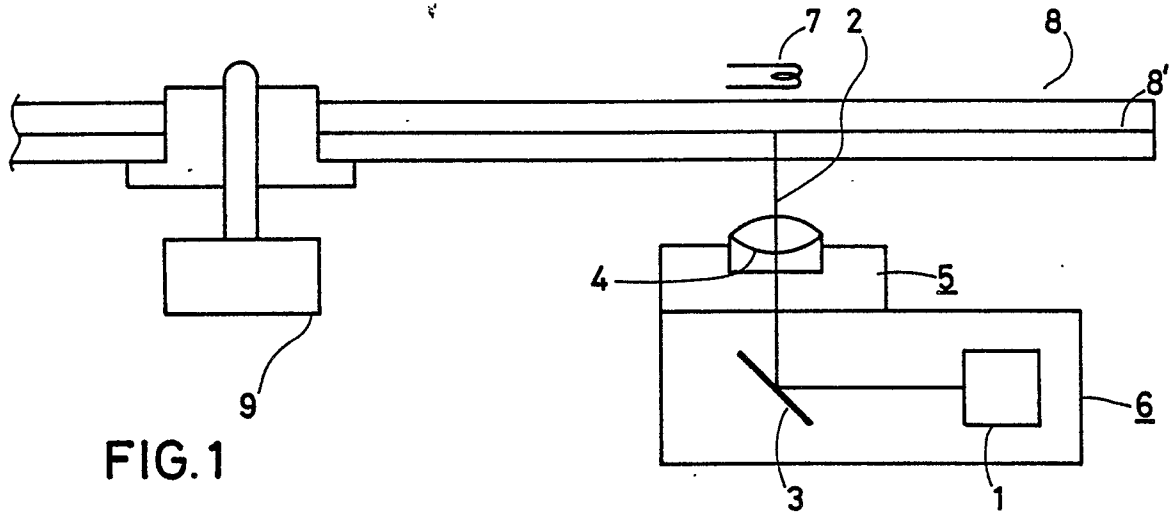


FIG. 1

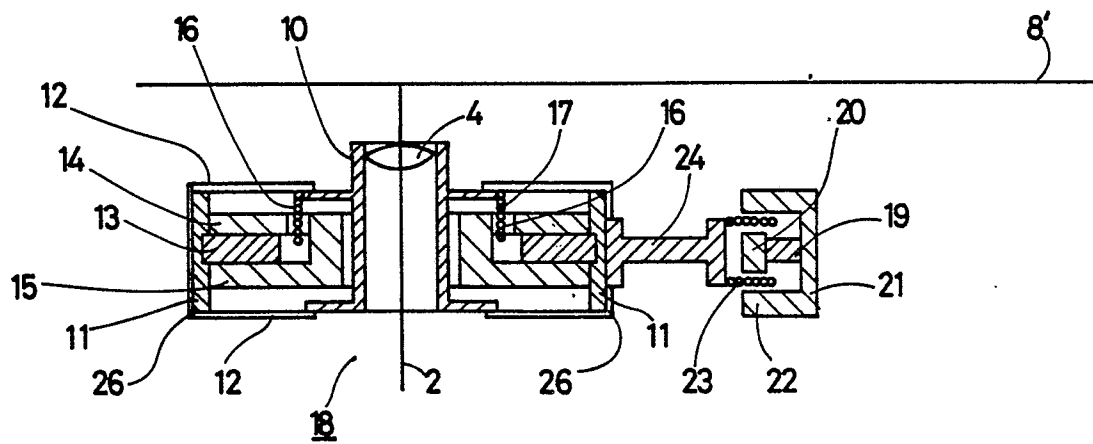


FIG.2

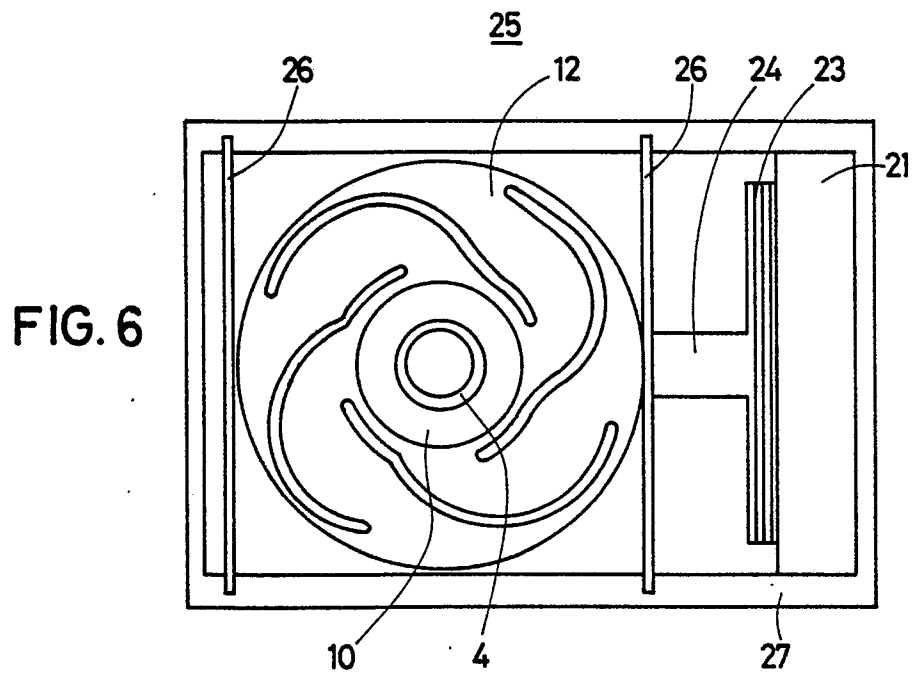


FIG. 6

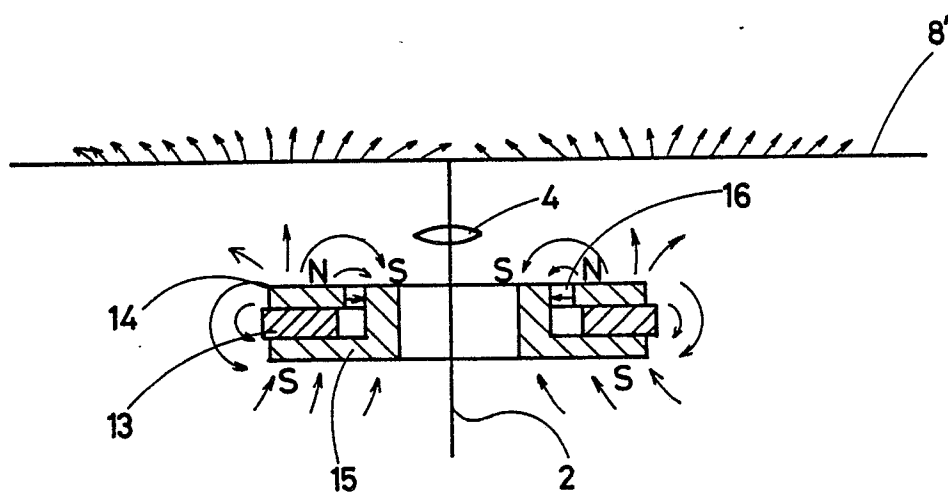


FIG. 3(a)

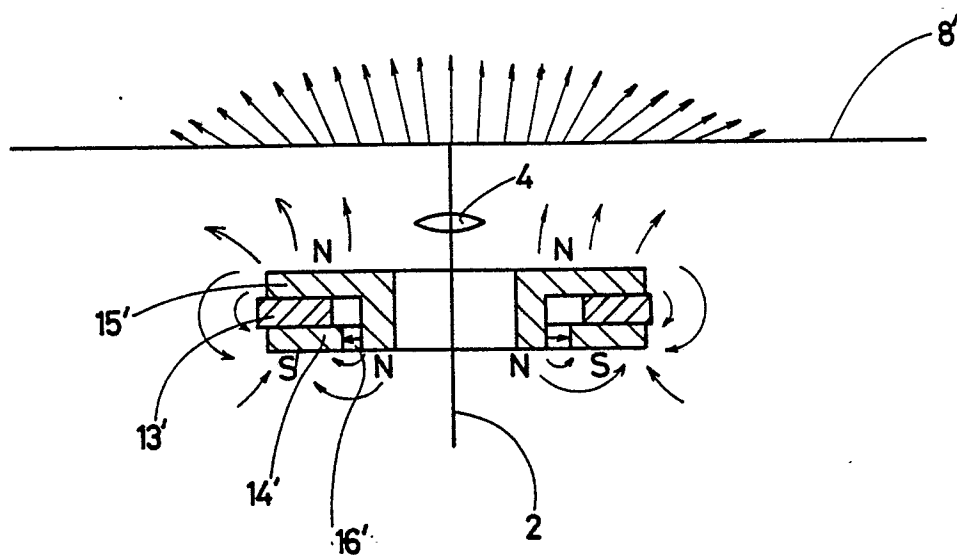


FIG. 3(b)

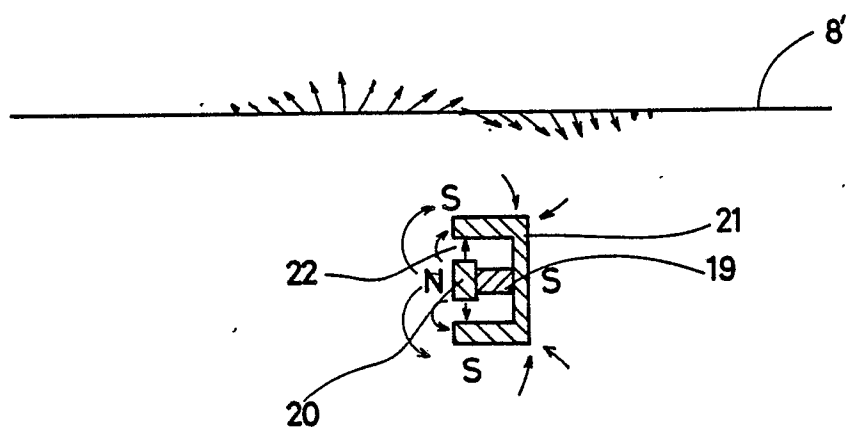


FIG. 4(a)

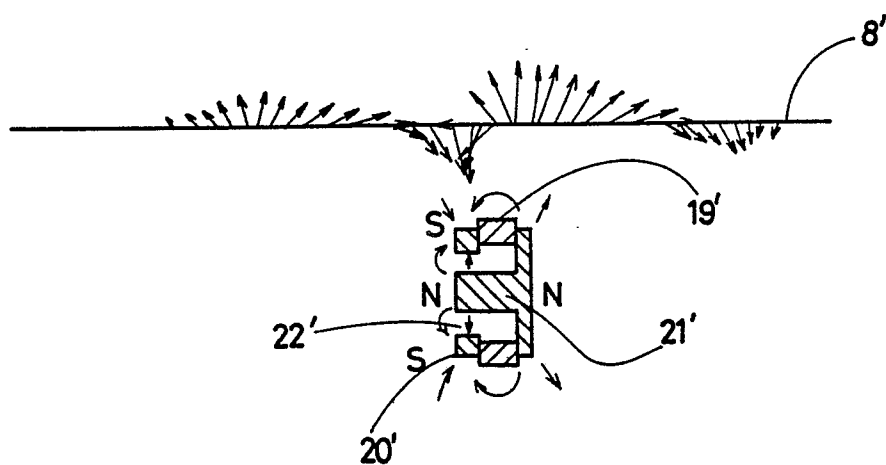


FIG. 4(b)

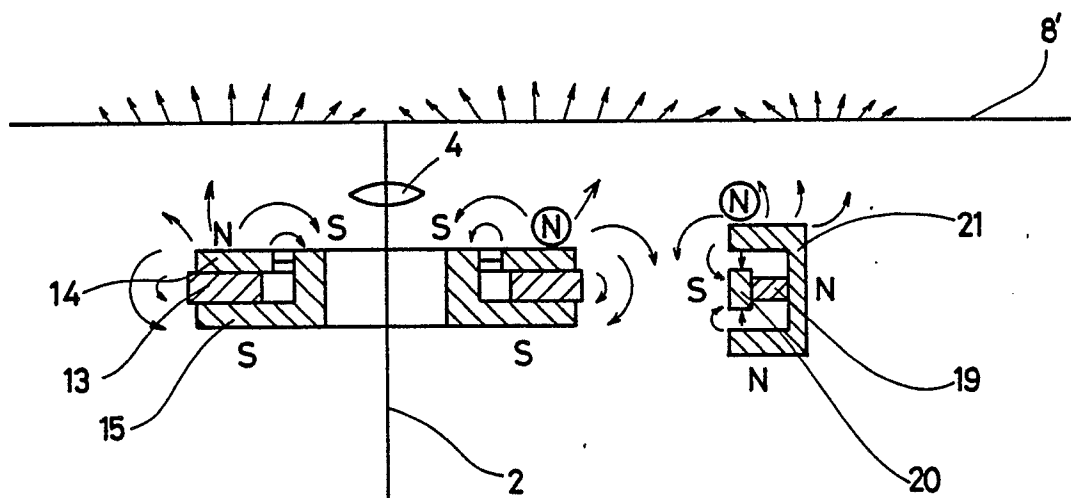


FIG. 5(a)

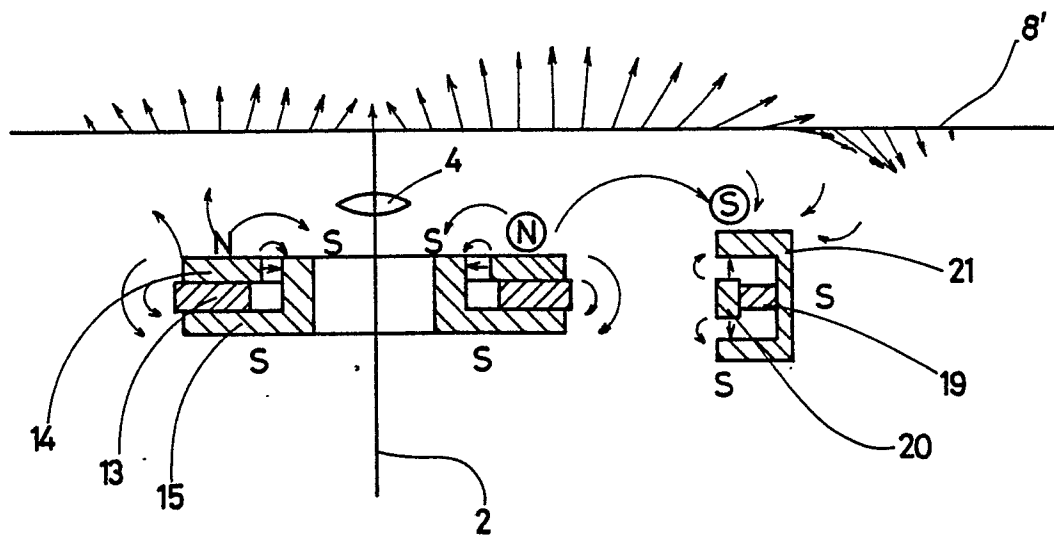


FIG. 5(b)

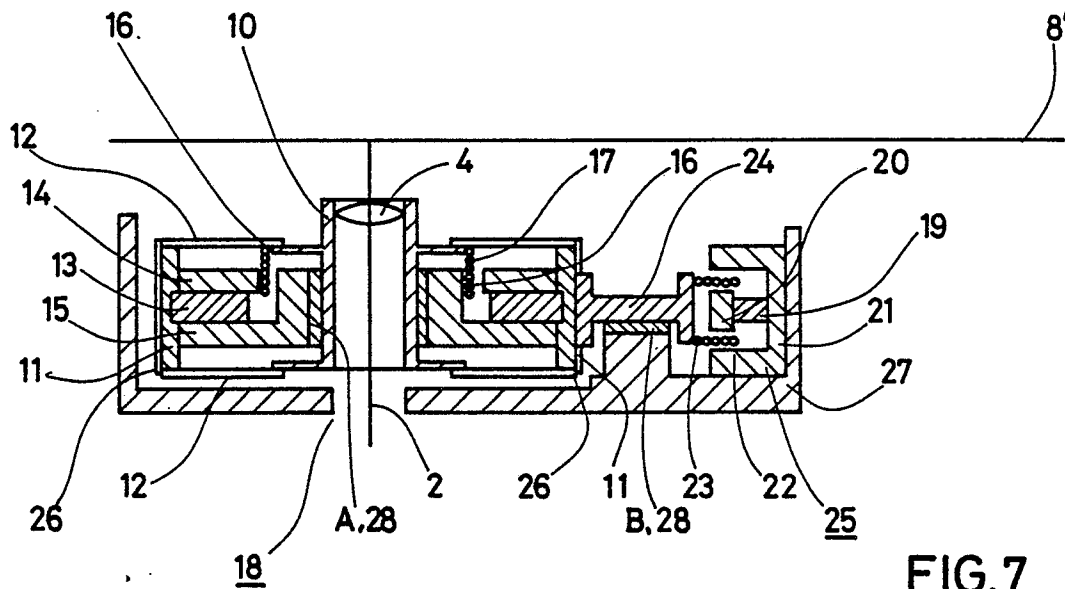


FIG.7

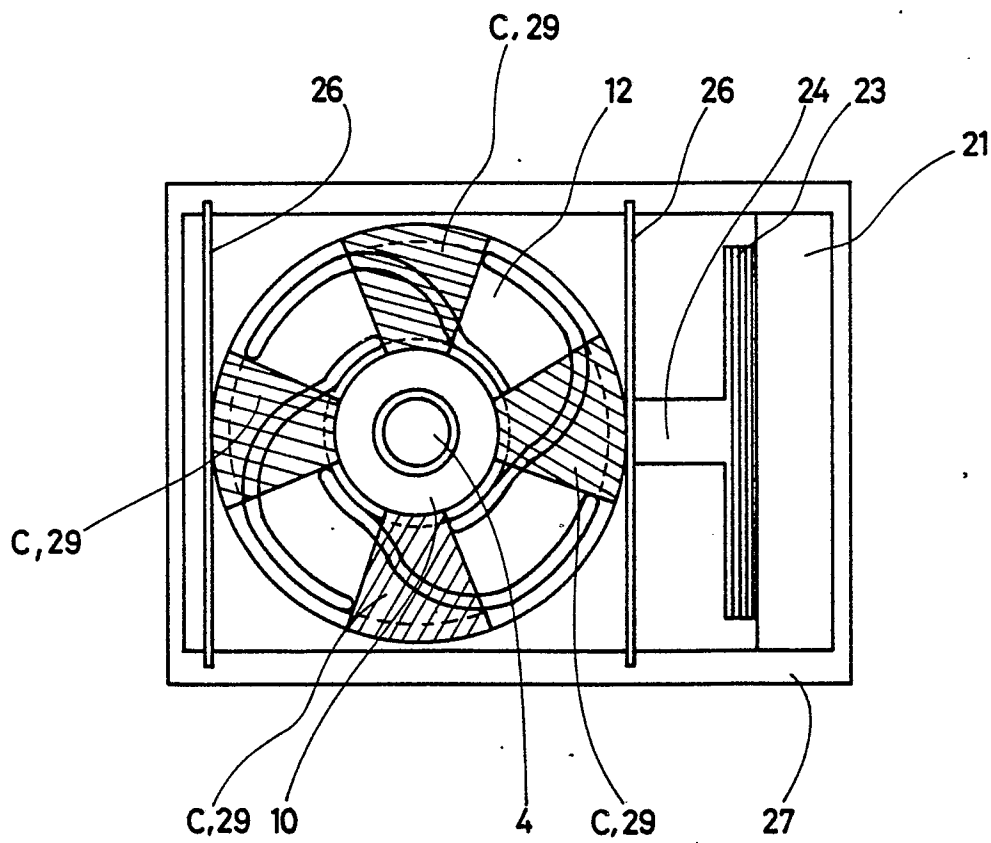


FIG. 8

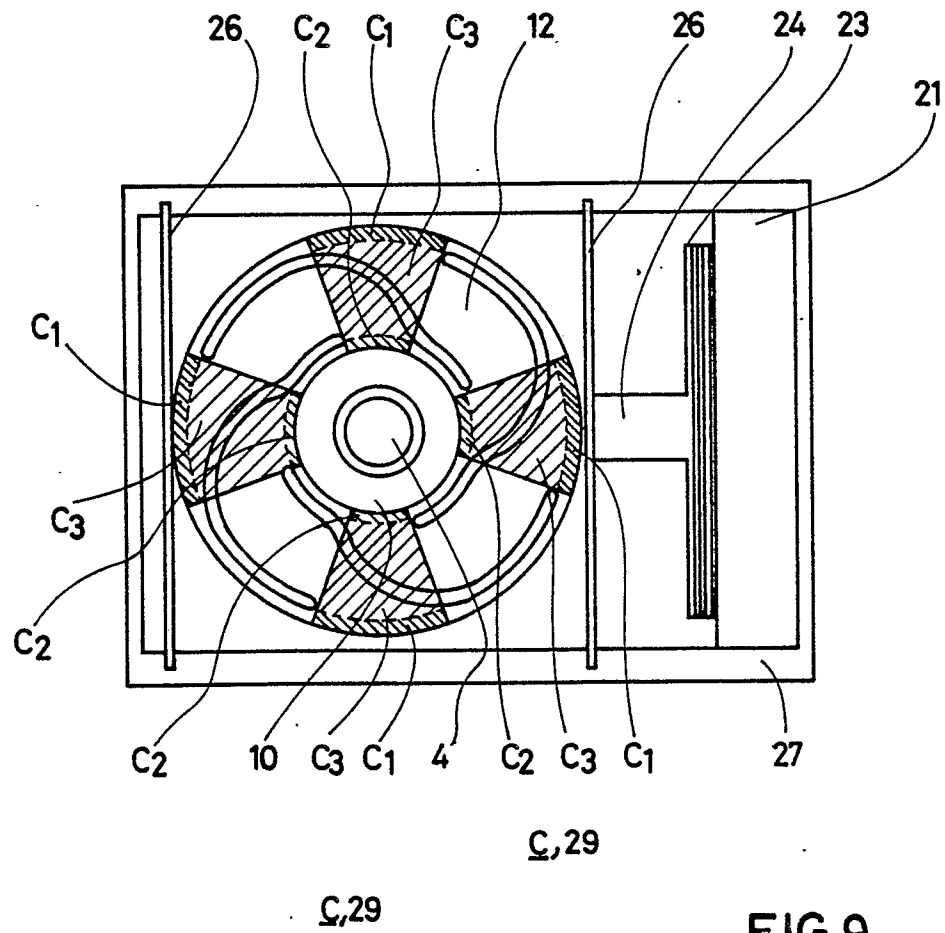


FIG.9

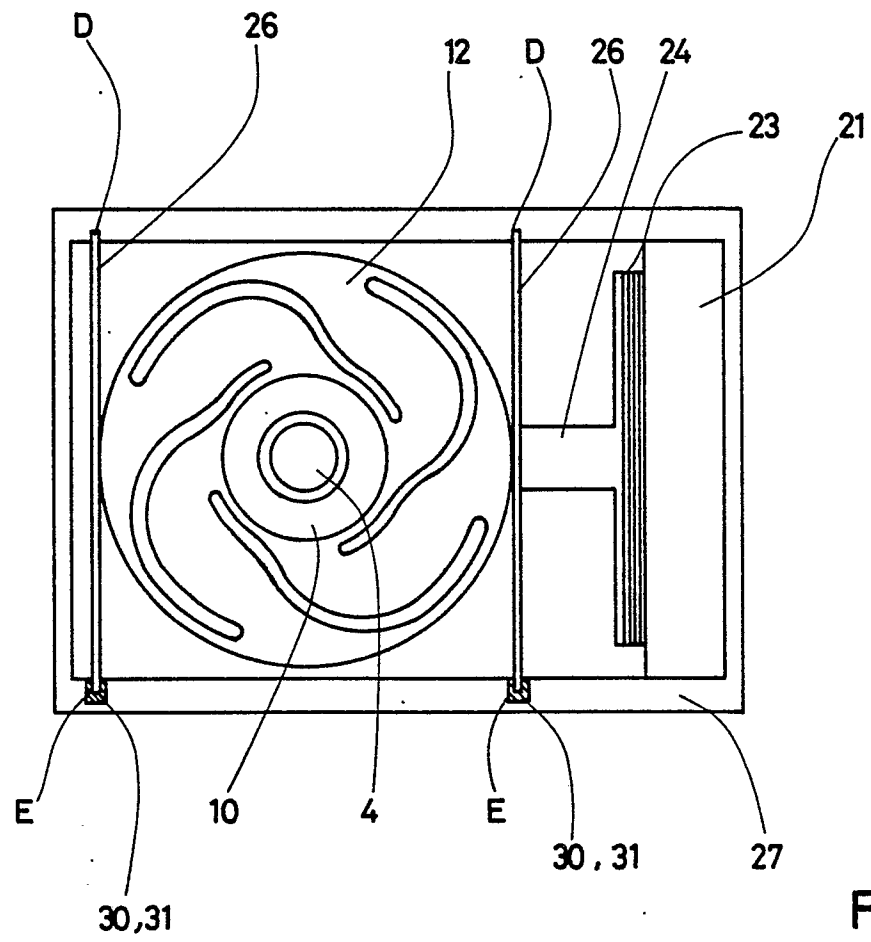


FIG.10



DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.4)
A	JAPANESE JOURNAL OF APPLIED PHYSICS, vol. 19, no. 12, December 1980, pages L731-L734, Tokyo, JP; NOBUTAKE IMAMURA et al.: "Experimental study on magneto-optical disk exerciser with the laser diode and amorphous magnetic thin films" * Page L733, right-hand column, line 29 - page L734, left-hand column, line 1 *	1	G 11 B 11/10 G 11 B 7/08
A	WO-A-8 001 016 (HITACHI LTD)(Publ. 15-05-1980) * Figure 14 * & US-A-4 410 277 (Publ. 18-10-1983) Column 9, line 35 - column 10, line 59; figure 14	1	
A	GB-A-2 064 848 (NIPPON TELEGRAPH & TELEPHONE PUBLIC, CORP.) * Page 2, line 64 - page 3, line 10; figures 3,4 *	1,3	
A	PATENT ABSTRACTS OF JAPAN, vol. 7, no. 18 (P-170)[1163], 25th January 1983; & JP-A-57 172 535 (HITACHI SEISAKUSHO K.K.) 23-10-1982 * Abstract *	1,2	TECHNICAL FIELDS SEARCHED (Int. Cl.4) G 11 B
A	DE-A-3 027 950 (UNIVERSAL PIONEER CORP.) * Whole document *	1,3	
A	PATENT ABSTRACTS OF JAPAN, vol. 6, no. 206 (P-149)[1084], 19th October 1982; & JP-A-57 113 431 (OLYMPUS KOGAKU KOGYO K.K.) 14-07-1982 * Abstract *	1,3,4	
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 22-02-1989	Examiner DAALMANS F.J.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			