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54 **Conductive composite filament and process for producing the same.**

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## Description

### BACKGROUND OF THE INVENTION

#### 5 1. Field of the invention

This invention relates to a composite filament having excellent antistatic properties, and more particularly to a white, highly oriented, undrawn, conductive filament having excellent filament properties and antistatic properties which are durable when the clothing made thereof is placed in actual service of being  
10 worn.

More specifically, the present invention relates to a white, sheath-core composite filament having excellent antistatic properties, which comprises a sheath component of a fiber-forming thermoplastic polymer (A) selected from polyethylene terephthalate and polybutylene terephthalate and a core component of a thermoplastic polyamide (B) containing a compound comprising a conductive material which comprises  
15 a metal oxide(s). Addition in an amount of only 0.01 to 10% by weight of this composite filament to a usual nonconductive fiber can provide the fabrics containing them with excellent antistatic properties, which do not deteriorate even after being worn for one year.

#### 20 2. Description of the prior art

Various conductive filaments have been proposed as having excellent antistatic properties. For example, there has been proposed a conductive filament comprising a conductive component which comprises a polymer containing a conductive carbon black mixed therein and a protective component which comprises a fiber-forming polymer.

25 However, such composite filaments utilizing a carbon black has a disadvantage that they are black or grey, and hence their use is limited.

Conductive filaments utilizing a white or colorless conductive metal oxide have recently been proposed to eliminate the above disadvantage. For example, Japanese Patent Application Laid-Open No. 6762/1982, Japanese Patent Publication No. 29526/1987 and GB-A-2 077 182 proposed a process of preparing a  
30 conductive composite filament comprising a mixture (conductive layer) of a conductive metal oxide and a thermoplastic resin and a fiber-forming thermoplastic polymer, said process comprising first preparing a composite filament as spun and drawing it and then further heat-treating the drawn filament to thereby restore the conductive layer. Where a thermoplastic resin is used as a binder for a conductive metal oxide, the obtained conductive layer is broken at the drawing process and as such the drawn filament cannot act  
35 as a conductive filament. Heat treatment is thus necessary when a thermoplastic resin, particularly a thermoplastic resin having high crystallinity, is used as the protective component for a conductive metal oxide. The process of the above patents however has a drawback of low productivity due to the presence of the heat treatment process after the heat drawing; and further the composite filament obtained by the process has a large drawback of insufficient durability when an article of clothing made thereof is actually  
40 worn. The "durability" of a composite filament herein is judged by whether the antistatic properties are still exhibited or not after a fabric comprising the conductive filament to be evaluated woven therein in an amount of 0.1 to 10% by weight has actually been worn for about 1 year. The standard of upper limit of the static charge specified in "Recommended Practice for Protection against Hazards Arising out of Electricity" in "Technical Recommendations" issued by Research Institute of Industrial Safety of Labor Ministry is  $7\mu$   
45 Coulomb/m<sup>2</sup>. This standard for the durability has not been cleared by conventional white or colorless conductive composite filaments. It has become clear from a study made by the present inventors that a thermoplastic polymer of for example polyethylene cannot give a conductive filament having a sufficient durability and that a fabric comprising such filament is hence not suited for use in work wears used for dangerous jobs. In the case where a crystalline thermoplastic resin is used as the thermoplastic polymer,  
50 the obtained conductive composite filament just after being produced has an electric resistance of less than  $9 \times 10^{10} \Omega/\text{cm} \cdot \text{filament}$  which satisfies the static charge standard for fabrics. The filament however has a poor durability, and the fabric obtained therefrom hence has low antistatic properties and is difficult to put in practical use.

The present inventors have made a detailed study to obtain a conductive filament without above  
55 drawbacks, and, particularly, have intensively studied the relationship between the filament structure and the antistatic properties and the durability thereof, and found a composite filament having excellent anti static properties and durability to accomplish the invention.

## SUMMARY OF THE INVENTION

The present invention provides a highly oriented, undrawn, conductive, composite filament which is a sheath-core composite filament comprising a sheath of a fiber-forming thermoplastic polymer (A) selected from polyethylene terephthalate and polybutylene terephthalate and a core of a composition (B) comprising a conductive material which comprises a conductive metal oxide(s) and a thermoplastic polymer, and maintaining a critical elongation of at least 5% and a shrinkage in hot water at 100 °C of not higher than 20%, said thermoplastic polymer for the core being a polyamide, said core having an electric resistance at a D.C. voltage of 1 kV of less than  $9 \times 10^{10} \Omega/\text{cm}\cdot\text{filament}$ .

## BRIEF DESCRIPTION OF THE DRAWINGS

A more complete appreciation of the invention and many of the attendant advantages thereof will be readily obtained as the same become better understood by reference to the following detailed description when considered in connection with the accompanying drawings, wherein:

FIG. 1 is a graph showing the relationship between the elongation and the electric resistance (resistance of filament core) of a composite filament with the moisture content of the composition of the core component of the filament as a parameter, and

FIG. 2 is a schematic diagram showing the apparatus for measuring the critical elongation in the present invention.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

As is well known, the term "antistatic properties" herein means a function of eliminating the static charge from a charged article by a non-contacting process. While a composite filament having a core resistance of less than  $10^{11} \Omega/\text{cm}\cdot\text{filament}$  can form a nonuniform electric field to thereby eliminate static charge by corona discharging, one having a core resistance of at least  $10^{11} \Omega/\text{cm}\cdot\text{filament}$  cannot eliminate static charge by corona discharging and hence does not exhibit effective antistatic properties.

The present inventors have intensively studied the relationship between the critical elongation and the constituents of a filament and the durability of antistatic properties of a fabric comprising the filament. The "critical elongation" herein means an elongation reached in the course of extending a filament at which the core resistance exceeds  $1 \times 10^{11} \Omega/\text{cm}\cdot\text{filament}$  at a D.C. voltage of 1 kV, that is, an elongation at which the filament loses its antistatic properties. As a result of the study, it was found that the durability is largely affected by the critical elongation and the type of the thermoplastic resin containing a conductive substance. The critical elongation varies from 0 to 15% in the case of white, conductive, composite filaments. It has been found, surprisingly, that a conductive composite filament with a critical elongation maintained at and above 5% can have a sufficient durability of antistatic properties.

The present inventors have pursued how to make a white or colorless composite filament containing a conductive metal oxide(s) have a critical elongation of at least 5%, and found that such filament can be obtained when the fiber-forming thermoplastic polymer (A) is selected from polyethylene terephthalate and polyethylene terephthalate, a polyamide is employed as the thermoplastic polymer for the core component and the moisture content of the core component at the spinning is in a specific range.

FIG. 1 is a graph showing the relationship between the elongation and the electric resistance (resistance of filament core) when the moisture content of the core component is (I) 90 ppm, (II) 200 ppm, (III) 800 ppm, (IV) 1,100 ppm or (V) 1,300 ppm respectively. Where the moisture content is out of the range of from 100 to 1,200 ppm, that is, in the cases of (I) and (V), if the filament is elongated by at least 5% in the processing or in the actual service, i.e. in the region of elongation exceeding 5%, the core resistance will not fall below  $1 \times 10^{11} \Omega/\text{cm}\cdot\text{filament}$  which can eliminate static charge by corona discharging. On the other hand, in the case of (IV) and (II), in which the moisture content of the core component falls in the range of from 100 to 1,200 ppm, even when the filament is elongated in the course of processing or in the actual service by 5% the core resistance is of an order of  $1 \times 10^{10} \Omega/\text{cm}\cdot\text{filament}$  thereby being capable of eliminating static charge by corona discharging. Further in the case of (III), the core resistance remains below  $10^{10} \Omega/\text{cm}\cdot\text{filament}$  even when the filament is subjected to elongation of 15% and thus has excellent durability.

FIG. 1 further shows that there is a large difference between the core resistance of filaments utilizing white conductive particles and that of conventional ones utilizing carbon black as the conductive material. From the FIGURE it will be understood that a filament utilizing a white particulate conductive material has a conducting structure markedly unstable than that of a carbon-black conductive filament. The present

invention has made it clear that the former can exhibit antistatic properties applicable to practice only within a limited region inside the unstable region, i.e. within a limited region of the moisture content of the core component.

As stated heretofore, the present inventors have succeeded in markedly improving the durability of the antistatic properties of a white conductive filament by providing the filament with a core resistance at a D.C. voltage of less than 1 kV of  $9 \times 10^{10} \Omega/\text{cm}$  filament and a critical elongation of at least 5%.

Though the reason of the phenomena discovered in the present invention is not quite clear at the moment, it is estimated to be as follows. If the moisture content of a polyamide resin is as low as 100 ppm or below when it is formed into a filament, the resin will tend to be fragile to thereby render the conducting structure unstable. On the other hand, if the moisture content is as much as 1,200 ppm or higher, there will readily generate bubbles, voids or the like to thereby form minute defectives in the conductive layer.

Hereinbelow a more concrete and detailed explanation will be given on the production conditions for obtaining such filaments.

The thermoplastic polymer constituting the core component must be a polyamide. It has been found that polyamides, e.g. nylon 6 give higher conductive characteristics than those obtained by polyethylene, which is generally employed.

When obtaining a conductive composite filament comprising as a component a conductive metal oxide(s) dispersed in a polymer, important points are as follows.

(1) To assure a high conducting property by dispersing the metal oxide;

(2) to assure a good dispersion of the metal oxide in the obtained conductive polymer to thereby cause no unusual filter clogging at the spinning;

(3) to assure a good fluidity of the obtained conductive polymer;

(4) to assure good mechanical properties of the obtained conductive polymer; and the like.

From the above points of view, the present inventors have studied various polymers while dispersing a metal oxide(s) therein, and found that polyamides are the most suited. This is because that: since polyamides have appropriate polar groups, they are good in compatibility and adhesiveness with metal oxides and hence their fluidity does not decrease so much when a metal oxide(s) is incorporated in them in a high concentration, so that they have both high conducting property and good fluidity. Furthermore, perhaps because of a firm adhesion between the metal oxide and polyamides, the obtained conductive polymer has very high mechanical properties. On the other hand, polyesters incorporating a metal oxide kneaded thereinto give, for some reason or another, a sharp viscosity increase and lose the fluidity even in a low incorporation ratio, and thus they hardly give a fiber-forming conductive polymer having the desired conducting property and hardly compete with polyamides. Polyolefins such as polyethylene can, upon incorporation of a metal oxide, give conductive polymers having a fluidity to some extent and at the same time a good conducting property. However, it has been found that the polyolefin conductive polymers rapidly lose their static eliminating performance in a short period of actual service and thus have no durability, perhaps because they have only a small adhesiveness with metal oxides, thereby rendering fragile the mechanical properties of the obtained conductive polymer as compared to the case with polyamides. To summarize, polyamides are the best suited, among general-purpose polymers, for producing the conductive polymers to be used for conductive composite filaments.

Examples of preferred polyamides are nylon 6 and metaxylylenediamine nylon or polyamides comprising the foregoing as a principal component.

As for the polymer to be used as the fiber-forming polymer constituting the sheath of the conductive composite filament of the present invention, it is necessary that the intrinsic viscosity of the sheath-component polymer be at least 0.55. If a polymer having an intrinsic viscosity less than 0.55 is used as the sheath component, the melt viscosity at the spinning will be too low to keep a good balance with that of the conductive polymer layer, thereby rendering the composite structure unstable in the longitudinal direction. In such case, spinnability becomes worse particularly at a high speed of not less than 2,500 m/min and frequent filament breakages occurs, which is not preferred. The thermoplastic polymers constituting the sheath are polyesters selected from polyethylene terephthalate and polybutylene terephthalate. Such polymers give a markedly improved durability against processing or when actually worn.

The conductive filament of the present invention is generally used while being mixed in a fabric in an amount of 0.1 to 10% by weight, which is the same as in the case of other conductive filaments. Such fabrics are naturally finished by dyeing and finishing process, and, then, the core component of the conductive filament readily suffers damage since it is fragile because of high content of a conductive metal oxide. Particularly, where fabrics comprising a conductive filament undergo high-temperature dyeing or high-temperature setting, the core component is markedly affected through such treatments. In this case the filament decreases its strength and will hence readily break by the bending in the practical service, leading

to a drop-off or deterioration of the conductive layer. Employment of a polyester, e.g. polyethylene terephthalate not only maintains the mechanical properties of the sheath component, but causes no decrease in the performance.

5 The conductive material to be incorporated into core component is a white or colorless particulate metal oxide(s) or a particulate inorganic material with the metal oxide(s) coating the surface thereof. Preferred example of the latter is fine particles having an average diameter of 0.01 to 0.3 $\mu$  of titanium dioxide or barium sulfate coated on the surface thereof with stannic oxide or zinc oxide containing antimony oxide.

10 Majority of metal oxides are semiconductors close to non-conductors which do not exhibit sufficient conductive property. However, addition of a small amount of a second component to a metal oxide or the like methods can increase the conductive property and give a sufficiently conductive material. Antimony oxide and the like oxides are known as such conductivity increasing agents or "doping agents" for stannic oxide or zinc oxide. For example, while particulate stannic oxide having an average particle diameter of 0.1 $\mu$  has a specific resistance of about 10<sup>3</sup> $\Omega$ ·cm, solid solutions of antimony oxide in stannic oxide have specific resistances of from 1 to 10 $\Omega$ ·cm. The ratio by weight of antimony oxide contained in a  
15 particulate conductive material is required to be 0.01 to 0.10 in view of overall performance. The ratio by weight of stannic oxide or zinc oxide contained in a particulate conductive material is preferably in the range from 0.05 to 0.20. Too small a coating amount leads to insufficient conductivity, while too much amount will deviate the obtained particulate material from white color.

20 The particulate conductive material is contained in the core of the composite filament of the invention in an amount of 60 to 75% by weight. While a content of less than 60% by weight cannot give a sufficient conductivity to exhibit the desired antistatic properties; one exceeding 75% by weight is not preferred since it will not further increase the conductivity and will markedly decrease the fluidity of the core component, whereby the spinnability is extremely worsened and, particularly, the life of the spinneret pack is strikingly shortened due to filter clogging or the like, thus rendering unstable the spinning operation.

25 For the filaments of the present invention, it is further important that the ratio by weight of the fiber-forming thermoplastic polymer constituting the sheath (A) and the composition of a thermoplastic polyamide and a conductive material constituting the core (B) be: (B)/(A) = 8/92 to 22/78. If the sheath component (A) exceeds 92% by weight and the conductive core component (B) is not more than 8% by weight, the composite filament with a stable sheath-core structure cannot be spun stably and, particularly, it becomes  
30 difficult to obtain longitudinally continuous core component to thereby render the stable spinning of the sheath-core composite filament itself difficult to achieve. On the other hand, if the core component (B) exceeds 22% by weight, the spinnability of the composite filament will, even when the sheath component (A) has a sufficient fiber-forming capability, decrease and further the obtained filament will have extremely low filament properties and be of no practical value. The reason of this is estimate to be that such large  
35 content of the core component (B) actualize the characteristic of the core component, i.e. a very low spinnability due to the incorporation of a conductive metal oxide. Accordingly, the ratio by weight of the sheath component (A) to the core component (B) is: (A) : (B) = 78 : 22 to 92 : 8, preferably 80 : 20 to 90 : 10.

40 The conductive composite filament of the present invention can be obtained by a process for producing the sheath-core composite filament comprising the above-described sheath component and core component, which comprises extruding a fiber-forming thermoplastic polymer selected from polyethylene terephthalate and polybutylene terephthalate and having an intrinsic viscosity,  $[\eta]$ , after spinning of at least 0.55 which constitutes the sheath component and the composition constituting the core component having a moisture content adjusted by drying to 100 to 1,200 ppm separately through different extruders, and  
45 conducting high-speed spinning using a composite spinning apparatus. The high-speed spinning herein means melt-spinning at at least 2,500 m/min so that the filaments thus spun will be highly oriented and have a shrinkage in hot water of 100 °C, W<sub>Sr</sub>, of not more than 20%.

50 If the core component (B) having a moisture content of less than 100 ppm is spun into a composite filament, filaments having a core resistance exceeding 10<sup>11</sup> $\Omega$ /cm·filament will frequently be formed though the spinnability is good. If the core component (B) having a moisture content exceeding 1,200 ppm is spun into a composite filament, the spinnability will be low (frequent filament breakages) and further many of the obtained conductive filaments will have critical elongations not more than 5%. Accordingly, the moisture content of the core component (B) is very important and preferably in the range of from 200 to 1,000 ppm, more preferably 300 to 800 ppm.

55 The wet shrinkage, W<sub>Sr</sub>, of conductive filaments is also important. Generally, it is essential that textile fabrics be subject to after-processing, after the weaving, in a high-temperature hot water, such as scouring and relaxation, dyeing or the like. If the filament constituting the fabric has a too large wet shrinkage, the fabric will shrink by such processing to thereby become hard, which is not preferred. Fibers for textile

fabrics in general therefore must have wet shrinkages lower than about 20%. In addition, in the case of the conductive filament of the present invention, such filament is most frequently used while being mixed in a small amount into conventional fibers in view of economy. For example a single filament each of the conductive filament may be inserted at  $2.54 \times 10^{-2}$ m (1-inch) intervals among a plurality of conventional warps for a fabric. In this case if the conductive filament has a much larger wet shrinkage than that of neighbouring warps, the conductive filament will be put under a high tension after the fabric has been wet treated, to thereby readily break when the fabric is loaded with an external force, which is often the case when clothes made of the fabric are actually put on.

The present invention conducts melt-spinning at a rate of at least 2,500 m/min to obtain highly oriented composite filaments as spun having a shrinkage in hot water at 100 °C of not more than 20%. Therefore, in the present invention, since a high orientation melt spinning is conducted with the drawing process omitted, there can be eliminated troubles arising from the drawing process, such as cracks or breakages of the core component, and cut-off of the conducting circuit by drawing can be avoided.

Other features of the invention will become apparent in the course of the following descriptions of exemplary embodiments which are given for illustration of the invention and are not intended to be limiting thereof.

## EXAMPLES

In the present invention, the electric resistance of the filament core is measured as follows.

### Measurement of electric resistance of the filament core

Both ends of a 10-cm specimen of a composite filament are immersed in a pair of pot-shape electrodes filled with a conductive resin. Electric current at a voltage of 1 kV is measured. The electric resistance is calculated by Ohm's law and then divided by 10 (cm) and the number of filaments constituting the specimen to give a filament core resistance in  $\Omega/\text{cm}\cdot\text{filament}$ .

The critical elongation was measured in the present invention, by application of the above-described measurement of filament core resistance, according to the method described below. It may however be also measured by measuring an electric resistance of a specimen when elongated by using a tensile tester combinedly with an electrode and resistance tester.

### Measurement of critical elongation

FIG. 2 shows an example of the measuring apparatus. As seen from the FIGURE, an apparatus comprising a pair of electrodes (1) and a dial (4) for extending the specimen are used for measurement.

The both ends of a specimen (3) are each set on a pair of the electrodes (1) at a gauge length of 3 cm. A conductive paint is applied to the both ends including the exposed core tip so that electric current can send therethrough, then the both ends are fixed. Then the dial (4) is turned to elongate the specimen until it breaks while its electric resistance is being measured. The obtained values of electric resistance are converted to ones per unit cm and the elongation (%) at which the electric resistance exceeds  $1 \times 10^{11}\Omega/\text{cm}\cdot\text{filament}$  is obtained therefrom as the critical elongation.

The intrinsic viscosity,  $[\eta]$ , of polyethylene terephthalate is measured at 30 °C in a 1/1 mixed solvent of phenol/tetrachloroethane. The intrinsic viscosity of nylon 6 is measured on its solution in 96%  $\text{H}_2\text{SO}_4$ . The melt index of polyethylene is measured according to JIS-K6760.

### Example 1

Particle-incorporating chips having a volume specific resistance of  $9 \times 10^2\Omega\cdot\text{cm}$  were obtained by melting and mixing 60 parts of a particulate titanium oxide having an average particle diameter of not more than  $0.2\mu$  coated on the surface thereof with 15% by weight of stannic oxide containing 2% by weight of antimonium oxide (hereinafter this conductive material is referred to as  $W_1$ ) and 40 parts of nylon 6 chips ( $T_{m1} = 218^\circ\text{C}$ ) at  $270^\circ\text{C}$ . The thus obtained chips were vacuum dried at  $80^\circ\text{C}$  to a chip moisture content of 400 ppm (B). The chips (B) and conventional polyethylene terephthalate chips (A) ( $T_{m2} = 256^\circ\text{C}$  and  $[\eta]$  after spinning = 0.63) were separately melted in two extruders and, using a composite-spinning apparatus, extruded through a spinneret having 4 holes at  $295^\circ\text{C}$  into sheath-core composite filaments so that (B) and (A) formed the core and the sheath respectively in a (A)/(B) ratio by weight of 87/13, and the filaments were wound at a rate of 4,500 m/min while being divided into two to give two highly oriented conductive

composite yarns of each  $27.7 \times 10^{-7}$  kg/m (25 deniers)/2 filaments. The obtained yarns had a core resistance of  $5 \times 10^{10} \Omega/\text{cm} \cdot \text{filament}$  and a critical elongation of 15%.

The thus obtained yarn was covered with a blended yarn of polyester (polyethylene terephthalate)-/cotton = 65/35 to give a core yarn. The core yarn was inserted into warps of a blended yarn of polyester (polyethylene terephthalate) fiber/cotton = 65/35 having a cotton count of 20s/2 at an interval of 1 core yarn per 80 warps and woven into a 2/1 twill of 80 warps/in  $\times$  50 wefts/in (1 in =  $2.54 \times 10^{-2}$ m). The twill thus woven was dyed and finished under the usual finishing conditions for conventional polyester/cotton blended yarn fabric. The fabric thus obtained had a static charge of  $4.5 \mu$  Coulomb/m<sup>2</sup>. A suit was tailored from the fabric and actually worn by a man for 1 year, while being washed 250 times during the period, and measured again for the static charge to give  $5.5 \mu$  Coulomb/m<sup>2</sup>, which clears the standard of "Recommended Practice for Protection Against Hazards Arising out of Electricity" in "Technical Recommendations" issued by Research Institute of Industrial Safety of Labor Ministry, proving the excellent antistatic properties with superior durability of the conductive filament

#### 15 Examples 2 and 3 and Comparative Examples 1 and 2

Example 1 was repeated except for changing the parts by weight of  $W_1$  and the results are shown in Table 1 as Examples 2 and 3 and Comparative Examples 1 and 2.

In Examples 2 and 3, 65 parts by weight and 70 parts by weight of  $W_1$  were respectively used to obtain 20 conductive polymers having a volume specific resistance of both  $4.1 \times 10^2 \Omega \cdot \text{cm}$ , which were further formed under the same spinning conditions as in Example 1 into conductive composite filaments. These filaments both had critical elongations of at least 10% and a core resistance of  $6 \times 10^9 \Omega/\text{cm} \cdot \text{filament}$ , thus having excellent antistatic properties. The conductive composite filaments were woven into 2/1 twill fabrics, which were then dyed and finished, in the same manner as in Example 1. The fabrics thus obtained showed a 25 static charge of both  $35 \mu$  Coulomb/m<sup>2</sup>, and that after 250 times of washings of 4 to  $4.3 \mu$  Coulomb/m<sup>2</sup>, which clears the standard, i.e. not more than  $7 \mu$  Coulomb/m<sup>2</sup>, proving their excellent durability.

In Comparative Example 1, Example 1 was repeated except for changing the amount of  $W_1$  to 55 parts by weight to obtain a composite filament. The obtained filament had a core resistance of  $8 \times 10^{12} \Omega/\text{cm} \cdot \text{filament}$  and was not a filament having antistatic properties.

In Comparative Example 2, Example 1 was repeated except for changing the amount of  $W_1$  to 80 parts 30 by weight to obtain a conductive composite filament. Though the obtained filament had antistatic properties, the spinning operation was unstable because the life of the spinneret pack was very short due to filter clogging and the like.

#### 35 Examples 4 and 5 and Comparative Examples 3 through 5

The influence of the moisture content of conductive polymer was studied herein.

In Examples 4 and 5, Example 1 was repeated except for changing the moisture content of the polymer to 800 ppm and 1,100 ppm respectively to obtain conductive composite filaments under the same spinning 40 conditions as in Example 1. These filaments had core resistances of  $5 \times 10^9 \Omega/\text{cm} \cdot \text{filament}$  and  $6 \times 10^9 \Omega/\text{cm} \cdot \text{filament}$  respectively and critical elongations of 15% and 5% respectively. The obtained conductive composite filaments were woven into 2/1 twill fabrics, which were then dyed and finished, in the same manner as in Example 1. The fabrics thus obtained showed static charges of from 3.5 to  $4.0 \mu$  Coulomb/m<sup>2</sup>, and those after 250 times of washings of from 4.1 to  $4.5 \mu$  Coulomb/m<sup>2</sup>, which clears the standard, proving their excellent durability. 45

In Comparative Examples 3 and 4, Example 1 was repeated except for changing the moisture content of the conductive polymer to 1,500 ppm and 2,000 ppm respectively under the same spinning conditions as in Example 1, where frequent filament breakages occurred. The obtained conductive composite filaments had a core resistance of both  $8 \times 10^9 \Omega/\text{cm} \cdot \text{filament}$ , which proved their high antistatic properties, but they 50 had critical elongations as small as 1 to 2%. These filaments were woven into 2/1 twill fabrics, which were then dyed and finished, in the same manner as in Example 1. The filaments contained in the fabrics thus obtained showed core resistances after 250 times of washings of from  $10^{10}$  to more than  $10^{13} \Omega/\text{cm} \cdot \text{filament}$ , with cracks being observed in some portions of the conductive layer, thus being of inferior durability.

In Comparative Example 5, Example 1 was repeated except for changing the moisture content of the 55 conductive polymer to 80 ppm under the same spinning conditions as in Example 1. Though the spinnability was good, many of the obtained conductive composite filaments showed a core resistance exceeding  $10^{11} \Omega/\text{cm} \cdot \text{filament}$ , and further after the fabric incorporating the composite filament had been washed 250 times cracks were observed in the conductive layer of the filament, thus proving its inferior

durability.

#### Example 6

5 A conductive composite filament was obtained by extruding the conductive polymer used in Example 1 and a polybutylene terephthalate (Novadur 5008® made by Mitsubishi Chemical Industries Limited;  $T_m = 226^\circ\text{C}$ ) such that the former formed the core and the latter the sheath through a spinneret having 4 holes at  $265^\circ\text{C}$  and the extruded filaments were divided into two and then wound at a rate of 3,750 m/min to give two  $27.7 \times 10^{-7}$  kg/m (25 deniers)/2 filament yarns (core resistance:  $5 \times 10^9 \Omega/\text{cm}\cdot\text{filament}$ ; critical  
10 elongation: 12%). The obtained conductive composite filament was woven into a 2/1 twill fabric, which was then dyed and finished, in the same manner as in Example 1. The fabric thus obtained showed a static charge of from  $4.0\mu$  Coulomb/m<sup>2</sup>, and that after 250 times of washings of  $4.5\mu$  Coulomb/m<sup>2</sup>, proving the excellent durability of its antistatic properties.

#### 15 Examples 7 and 8

Particle-incorporating chips having a volume specific resistance of  $3 \times 10^2 \Omega\cdot\text{cm}$  were obtained by melting at  $270^\circ\text{C}$  and mixing 64 parts of the same particulate conductive material,  $W_1$ , as in Example 1, 1 part of particulate stannic oxide containing antimony oxide having an average particle diameter of  $0.1\mu$   
20 and 35 parts of nylon 6 chips. The thus obtained chips were vacuum dried at  $80^\circ\text{C}$  to a chip moisture content of 400 ppm (B). Two types of conductive composite filaments were obtained with the thus obtained conductive polymer used for the core under the same spinning conditions as in Examples 1 and 6 respectively. These filaments had core resistances and critical elongations of  $3 \times 10^9 \Omega/\text{cm}\cdot\text{filament}$  and 10% and  $4 \times 10^9 \Omega/\text{cm}\cdot\text{filament}$  and 10%, respectively. The obtained conductive composite filaments were  
25 woven into 2/1 twill fabrics, which were then dyed and finished, in the same manner as in Example 1. The fabrics thus obtained both showed a static charge after 250 times of washings of  $4.6\mu$  Coulomb/m<sup>2</sup>, proving their excellent antistatic properties with durability.

#### Comparative Example 6

30 A composite filament as spun was obtained under the same spinning conditions as in Example 4 except that the spinning speed was changed to 1,500 m/min. The as spun yarn, which had a maximum drawability of 4.53 times, was drawn by roller-plate system, at a hot roller temperature and a hot plate temperature of  $75^\circ\text{C}$  and  $120^\circ\text{C}$  respectively by 3.1 times to give a composite filament. Observation with a transmission-type electron microscope revealed that the conductive layer of the core had been torn to pieces. The  
35 filament had a core resistance of at least  $10^{13} \Omega/\text{cm}\cdot\text{filament}$  and was not a filament having antistatic properties. No heat drawing conditions with the temperature and the drawing ratio varied while maintaining stable drawing could give a composite filament in which the conductive core layer was not broken and which had antistatic properties.

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#### Comparative Example 7

A conductive polymer was obtained by melting and mixing parts of the conductive fine particles,  $W_1$ , used in Example 1, and 35 parts of polyethylene chips having a melt index of 50 g/10 min. A composite  
45 filament as spun was obtained using this polymer for the core under the same conditions as in Example 1 except for changing the spinning speed to 1,500 m/min. The thus obtained filament as spun was drawn by 3.0 times at a hot roller temperature and a hot plate temperature of  $75^\circ\text{C}$  and  $120^\circ\text{C}$  respectively to yield a conductive composite filament having a core resistance of  $9 \times 10^9 \Omega/\text{cm}\cdot\text{filament}$  and a critical elongation of 10%. The obtained conductive composite filament was woven into a 2/1 twill fabric, which was then dyed  
50 and finished, in the same manner as in Example 1. The fabric thus obtained showed a static charge of  $4.2\mu$  Coulomb/m<sup>2</sup>, which cleared the standard, but had a static charge after 250 times of washings of  $7.8\mu$  Coulomb/m<sup>2</sup>, thus being of no durability.

#### Comparative Example 8

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A composite filament having a low wet shrinkage was obtained under the same spinning conditions as in Example 1 (i.e. spinning speed: 4,500 m/min; no heat drawing) except for using the conductive polymer prepared in Comparative Example 7 as the core. Though the obtained filament had antistatic properties, it

did not have the durability, similar to the one in Comparative Example 7.

#### Example 9 and Comparative Examples 9 and 10

5 The influence of the sheath-core composite ratio was studied herein.

In Example 9, the same conductive component as in Example 2 was used as the core component and Example 1 was repeated except for changing the sheath-core composite ratio to 17/83. The spinnability and the durability of antistatic properties of the obtained fabric were both excellent as shown in Table 1.

10 In Comparative Examples 9, the ratio of the conductive component to the sheath was further increased to 30/70. Frequent filament breakages occurred in the spinning process and no stable spinning was thus accomplished.

In Comparative Example 10, the ratio of the conductive component to the sheath component was 4/96. Though the spinnability was good, no conductive filament having antistatic properties was obtained.

#### 15 Example 10 and Comparative Example 11

The influence of the intrinsic viscosity,  $[\eta]$ , after spinning of polyethylene terephthalate used for the sheath was studied.

20 Spinning operation of Example 1 was repeated except that the  $[\eta]$  after spinning were 0.58 (Example 10) and 0.52 (Comparative Example 11). While the filament obtained in Example 10 had excellent antistatic properties with durability, in Comparative Example 11 frequent filament breakages occurred and stable spinning was not attained.

#### Example 11

25 Particle-incorporating chips having a volume specific resistance of  $4 \times 10^2 \Omega \cdot \text{cm}$  were obtained by melting and mixing 65 parts of the same particulate conductive material,  $W_1$ , as in Example 1, and 35 parts of metaxylylenediamine nylon chips made by Mitsubishi Gas Chemical Company, Inc. The thus obtained chips were dried to a moisture content of 400 ppm and then formed into a conductive composite filament  
30 under the same spinning conditions as in Example 1. The filament had a core resistance and a critical elongation of  $2 \times 10^{10} \Omega/\text{cm} \cdot \text{filament}$  and 15% respectively. The fabric incorporating the thus obtained filament showed a static charge after 250 times of washings of  $6.5 \mu \text{ Coulomb}/\text{m}^2$ , proving its excellent antistatic properties with durability.

#### 35 Example 12

Particle-incorporating chips having a volume specific resistance of  $4 \times 10^2 \Omega \cdot \text{cm}$  were obtained by melting and mixing 73 parts of the same particulate conductive material,  $W_1$ , as in Example 1, and 35 parts  
40 of nylon 12 chips made by Ube Industries, Ltd. The thus obtained chips were dried to a moisture content of 400 ppm. A conductive composite filament was obtained with the thus prepared chips as the core and polybutylene terephthalate as the sheath under the same spinning conditions as in Example 6. The filament had a core resistance and a critical elongation of  $8 \times 10^9 \Omega/\text{cm} \cdot \text{filament}$  and 15% respectively and thus had antistatic properties. The fabric incorporating the thus obtained filament in the same manner as in Example  
45 1 showed a static charge of  $3.7 \mu \text{ Coulomb}/\text{m}^2$ , and that after 250 times of washings of  $5.0 \mu \text{ Coulomb}/\text{m}^2$ , which cleared the standard and proved its excellent durability of antistatic properties.

#### Comparative Example 12

50 Example 1 was repeated except for changing the spinning speed to 2,000 m/min. The obtained filament had a shrinkage in hot water at  $100^\circ \text{C}$  of 28%. The finished fabric contained the composite filament under high tension. Though the fabric initially showed good antistatic properties, it completely lost the properties after being worn actually for some period.

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Table 1 (1)

	Core component (B)				Sheath component (A)			Spinning conditions			
	Polymer	T <sub>m</sub> (°C)	Mixing ratio by weight of conductive particles (%) W <sub>1</sub> T <sub>1</sub>	Moisture content of polymer (ppm)	Polymer	T <sub>m</sub> (°C)	[ $\eta$ ] after spinning	Core- sheath ratio B/A	Spin- ning speed (m/ min)	Spinna- bility	Remarks
Ex. 1	Nylon 6	218	60 0	400	polyethylene terephthalate	256	0.63	13/87	4500	⊙	
" 2	"	"	65 0	"	"	"	"	"	"	⊙	
" 3	"	"	70 0	"	"	"	"	"	"	⊙	
Comp. Ex. 1	"	"	55 0	"	"	"	"	"	"	⊙	
" 2	"	"	80 0	"	"	"	"	"	"	X	Unstable spinning due to filter clogging and the like
Ex. 4	"	"	65 0	800	"	"	"	"	"	⊙	
" 5	"	"	"	1100	"	"	"	"	"	○	
Comp. Ex. 3	"	"	"	1500	"	"	"	"	"	X	Frequent filament breakage
" 4	"	"	"	2000	"	"	"	"	"	X	
" 5	"	"	"	80	"	"	"	"	"	⊙	
Ex. 6	"	"	"	400	polybutylene terephthalate	226	0.82	"	3750	⊙	
" 7	"	"	64 1	"	"	"	"	"	"	⊙	
" 8	"	"	"	"	polyethylene terephthalate	256	0.63	"	4500	⊙	

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Table 1 (2)

	Antistatic property and its durability							Overall evaluation
	Heat drawing	Core resistance ( $\Omega / \text{cm} \cdot \text{f}$ )	Antistatic property	Critical elongation (%)	Static charge ( $\mu \text{C} / \text{m}^2$ )	Performance after one-year service (washed 250 times)		
						Core resistance ( $\Omega / \text{cm} \cdot \text{f}$ )	Static charge ( $\mu \text{C} / \text{m}^2$ )	
Ex. 1	No	$5 \times 10^{10}$	◎	15	4.5	$7 \times 10^{10}$	5.5	◎
" 2	"	$6 \times 10^9$	◎	15	3.5	$8 \times 10^9$	4.0	◎
" 3	"	$6 \times 10^9$	◎	10	3.5	$1 \times 10^{10}$	4.3	◎
Comp. Ex. 1	"	$8 \times 10^{12}$	×	17	—	—	—	×
" 2	"	$6 \times 10^9$	◎	10	—	—	—	×
Ex. 4	"	$5 \times 10^9$	◎	15	3.5	$9 \times 10^9$	4.1	◎
" 5	"	$6 \times 10^9$	◎	5	4.0	$2 \times 10^{10}$	4.5	◎ ~ ◎
Comp. Ex. 3	"	$8 \times 10^9$	◎	2	3.7	$10^{10} \sim 10^{13} <$	7.2	$\Delta \sim \times$
" 4	"	$8 \times 10^9$	◎	0	—	—	—	×
" 5	"	$10^{10} \sim 10^{13}$	◎	0	6.8	$10^{13} <$	8.7	×
Ex. 6	"	$5 \times 10^9$	◎	12	4.0	$1 \times 10^{10}$	4.5	◎
" 7	"	$3 \times 10^9$	◎	10	3.1	$8 \times 10^9$	4.6	◎
" 8	"	$4 \times 10^9$	◎	10	4.0	$8 \times 10^9$	4.6	◎

Table 1 (3)

	Core component (B)				Sheath component (A)			Spinning conditions			
	Polymer	T <sub>m</sub> (°C)	Mixing ratio by weight of conductive particles (%) W, T <sub>i</sub>	Moisture content of conductive polymer (ppm)	Polymer	T <sub>m</sub> (°C)	[ $\eta$ ] after spin- ning	Core- sheath ratio B/A	Spin- ning speed (m/ min)	Spinna- bility	Remarks
Comp. Ex. 6	nylon 6	218	65 0	800	polyethylene terephthalate	255	0.63	13/87	1500	⊙	
" 7	polyethylene	127	"	-	"	"	"	"	"	⊙	
" 8	"	"	"	-	"	256	"	"	4500	⊙	
Ex. 9	nylon 6	218	"	400	"	"	"	17/83	"	○	
Comp. Ex. 9	"	"	"	"	"	"	"	30/70	"	×	Frequent filament breakage
" 10	"	"	"	"	"	"	"	4/96	"	⊙	
Ex. 10	"	"	"	"	"	"	0.58	13/87	"	⊙	
Comp. Ex. 11	"	"	"	"	"	"	0.52	"	"	×	Frequent filament breakage
Ex. 11	metaxyllylene- diamine nylon	223	65 0	"	polyethylene terephthalate	256	0.63	"	4500	⊙	
" 12	nylon 12	180	"	"	polybutylene terephthalate	226	0.82	"	3750	⊙	
Comp. Ex. 12	"	"	60 0	"	polyethylene terephthalate	256	0.63	"	2000	⊙	

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Table 1 (4)

	Antistatic property and its durability								Overall evaluation
	Heat drawing	Core resistance ( $\Omega / \text{cm} \cdot \text{f}$ )	Antistatic-property	Critical elongation (%)	Static charge ( $\mu \text{C} / \text{m}^2$ )	Performance after one-year service (washed 250 times)			
						Core resistance ( $\Omega / \text{cm} \cdot \text{f}$ )	( $\mu \text{C} / \text{m}^2$ )		
Comp. Ex. 6	Yes	$10^{12} <$	X	-	-	-	-	-	X
" 7	"	$9 \times 10^9$	⊙	10	4.2	$10^{13} <$	7.8		X
" 8	No	$5 \times 10^9$	⊙	10	3.5	$10^{13} <$	7.6		X
Ex. 9	"	$3 \times 10^9$	⊙	10	3.5	$9 \times 10^9$	4.4		○ ~ ⊙
Comp. Ex. 9	"	-	-	-	-	-	-		X
" 10	"	$5 \times 10^{11}$	X	-	-	-	-		X
Ex. 10	"	$9 \times 10^9$	⊙	10	4.0	$2 \times 10^{10}$	5.2		⊙
Comp. Ex. 11	"	-	-	-	-	-	-		X
Ex. 11	No	$2 \times 10^{10}$	⊙	15	5.5	$7 \times 10^{10}$	6.5		⊙
" 12	"	$8 \times 10^9$	⊙	15	3.7	$5 \times 10^{10}$	5.0		⊙
Comp. Ex. 12	"	$8 \times 10^9$	⊙	15	4.5	$10^{13} <$	10.0		X

55 **Claims**

1. A highly oriented, undrawn, conductive, composite filament which is a sheath-core composite filament comprising a sheath of a fiber-forming thermoplastic polymer (A) selected from polyethylene tereph-

thalate and polybutylene terephthalate and a core of a composition (B) comprising a conductive material which comprises conductive metal oxide(s) particles and a thermoplastic polyamide, said filament having a critical elongation of at least 5% and a shrinkage in hot water at 100 °C of not higher than 20%, said core having a core resistance at a D.C. voltage of 1 kV of less than  $9 \times 10^{10} \Omega/\text{cm} \cdot \text{filament}$ ; wherein the critical elongation means an elongation reached in the course of extending a composite filament at which the core resistance exceeds  $1 \times 10^{11} \Omega/\text{cm} \cdot \text{filament}$  at a D.C. voltage of 1 kV.

2. The highly oriented, undrawn, conductive, composite filament of Claim 1, wherein said conductive material is a particulate conductive material ( $W_1$ ) having an average particle diameter of 0.01 to  $0.3 \mu\text{m}$  comprising titanium dioxide or barium sulfate coated on the surface thereof with a metal oxide (D) selected from stannic oxide and zinc oxide, said metal oxide (D) containing antimonium oxide (C), the ratios by weight of said antimonium oxide (C) and said metal oxide (D) to said particulate conductive material ( $W_1$ ) satisfying the following formulae (1) and (2)

$$C/W_1 = 0.01 \text{ to } 0.10 \quad (1)$$

$$D/W_1 = 0.05 \text{ to } 0.25 \quad (2).$$

3. The highly oriented, undrawn, conductive, composite filament of Claim 1, wherein said conductive material is incorporated in said polyamide in an amount of 60 to 75% by weight.

4. The highly oriented, undrawn, conductive, composite filament of Claim 1, wherein the ratio by weight of said fiber-forming thermoplastic polymer (A) selected from polyethylene terephthalate and polybutylene terephthalate and said composition (B) comprising a conductive material and a polyamide is:  
 $(B)/(A) = 8/92 \text{ to } 22/78$ .

5. A process for producing a highly oriented, undrawn, conductive, composite filament which is a sheath-core composite filament comprising a sheath component of a fiber-forming thermoplastic polymer (A) selected from polyethylene terephthalate and polybutylene terephthalate and a core component of a composition (B) comprising a conductive material which comprises a conductive metal oxide(s) and a thermoplastic polyamide, which comprises extruding said fiber-forming thermoplastic polymer (A) having an intrinsic viscosity,  $[\eta]$ , after spinning of at least 0.55 and said composition (B) having a moisture content adjusted by drying to 100 to 1,200 ppm separately through different extruders, and conducting high orientation melt spinning using a composite spinning apparatus at at least 2,500 m/min so that the filaments thus spun will have a shrinkage in hot water at 100 °C of not more than 20%.

### Patentansprüche

1. Hochorientiertes, nicht-verstrecktes, leitfähiges Verbundfilament, das ein Mantel-Kern-Verbundfilament ist, welches einen Mantel aus einem unter Polyethylenterephthalat und Polybutylenterephthalat ausgewählten, faserbildenden thermoplastischen Polymer (A) und einen Kern aus einer Zusammensetzung (B) enthält, die ein leitfähiges Material umfaßt, das leitfähige Metalloxydteilchen und ein thermoplastisches Polyamid enthält, wobei das Filament eine kritische Dehnung von mindestens 5% und eine Schrumpfung in heißem Wasser bei 100 °C von nicht mehr als 20% aufweist, wobei der Kern bei einer Gleichspannung von 1 kV einen Widerstand von weniger als  $9 \times 10^{10} \Omega/\text{cm}$  Filament aufweist, worin die kritische Dehnung eine im Laufe des Streckens eines Verbundfilaments erreichte Dehnung bezeichnet, bei der bei einer Gleichspannung von 1 kV der Kernwiderstand  $1 \times 10^{11} \Omega/\text{cm}$  Filament übersteigt.

2. Hochorientiertes, nicht-verstrecktes, leitfähiges Verbundfilament nach Anspruch 1, worin das leitfähige Material ein als Teilchen vorliegendes leitfähiges Material ( $W_1$ ) mit einem durchschnittlichen Teilchendurchmesser von 0,01 bis  $0,3 \mu\text{m}$  ist, welches Titandioxid oder Bariumsulfat umfaßt, das auf der Oberfläche mit einem unter Zinndioxid und Zinkoxid ausgewählten Metalloxyd (D) beschichtet ist, wobei das Metalloxyd (D) Antimonoxid (C) enthält, wobei das jeweilige Gewichtsverhältnis des Antimonoxids (C) und des Metalloxyds (D) zu dem als Teilchen vorliegenden, leitfähigen Material ( $W_1$ ) den folgenden Formeln (1) und (2) genügt:

$$C/W_1 = 0,01 \text{ bis } 0,10 \quad (1)$$

$$D/W_1 = 0,05 \text{ bis } 0,25 \quad (2).$$

3. Hochorientiertes, nicht-verstrecktes, leitfähiges Verbundfilament nach Anspruch 1, worin das leitfähige Material in dem Polyamid in einer Menge von 60 bis 75 Gew.-% enthalten ist.
4. Hochorientiertes, nicht-verstrecktes, leitfähiges Verbundfilament nach Anspruch 1, worin das Gewichtsverhältnis des unter Polyethylenterephthalat und Polybutylenterephthalat ausgewählten, faserbildenden thermoplastischen Polymer (A) und der Zusammensetzung (B), die ein leitfähiges Material und ein Polyamid enthält:  
(B)/(A) = 8/92 bis 22/78 ist.
5. Verfahren zur Herstellung eines hochorientierten, nichtverstreckten, leitfähigen Verbundfilaments, das ein MantelKern-Verbundfilament ist, welches eine Mantel-Komponente aus einem unter Polyethylenterephthalat und Polybutylenterephthalat ausgewählten, faserbildenden thermoplastischen Polymer (A) und eine Kernkomponente aus einer Zusammensetzung (B) enthält, die ein leitfähiges Material umfaßt, das ein leitfähiges Metalloxid/leitfähige Metalloxide und ein thermoplastisches Polyamid enthält, umfassend:  
getrenntes Extrudieren des faserbildenden thermoplastischen Polymers (A), das nach Verspinnen eine Grenzviskositätszahl ( $\eta$ ) von mindestens 0,55 besitzt, und der Zusammensetzung (B), die einen durch Trocknen auf 100 bis 1200 ppm eingestellten Feuchtigkeitsgehalt aufweist, durch unterschiedliche Extruder und Hochorientierungs-Schmelzspinnen unter Verwendung einer Verbund-Spinnvorrichtung bei mindestens 2500 m/min, wobei die so gesponnenen Filamente eine Schrumpfung in heißem Wasser bei 100 °C von nicht mehr als 20% zeigen.

## 25 Revendications

1. Filament composite, conducteur, non étiré, fortement orienté, qui est un filament composite à gaine et âme, comportant une gaine en un polymère thermoplastique (A) formant des fibres, choisi parmi le téréphtalate de polyéthylène et le téréphtalate de polybutylène et une âme d'une composition (B) comportant un matériau conducteur qui comprend des particules d'oxyde(s) métallique(s) conducteur(s) et un polyamide thermoplastique, ledit filament possédant un allongement critique d'au moins 5% et un retrait dans l'eau chaude à 100 °C non supérieur à 20%, ladite âme possédant une résistance à une tension continue de 1 kv inférieure à  $9 \times 10^{10} \Omega/\text{cm}.\text{filament}$  ; dans lequel l'allongement critique signifie un allongement atteint au cours de l'extension d'un filament composite pour lequel la résistance de l'âme excède  $1 \times 10^{11} \Omega/\text{cm}.\text{filament}$  à une tension continue de 1 kv.
2. Filament composite, conducteur, non étiré, fortement orienté selon la revendication 1, dans lequel ledit matériau conducteur est un matériau conducteur particulière ( $W_1$ ) ayant un diamètre de particule moyen de 0,01 à 0,3  $\mu$  comportant du dioxyde de titane ou du sulfate de baryum revêtu sur sa surface avec un oxyde métallique (D) choisi parmi l'oxyde stannique et l'oxyde de zinc, ledit oxyde (D) contenant de l'oxyde d'antimoine (C), les rapports en poids dudit oxyde d'antimoine (C) et dudit oxyde métallique (D) audit matériau conducteur particulière ( $W_1$ ) satisfaisant aux formules suivantes (1) et (2)  
 $C/W_1 = 0,01 \text{ à } 0,10 \quad (1)$   
 $D/W_1 = 0,05 \text{ à } 0,25 \quad (2)$
3. Filament composite, conducteur, non étiré, fortement orienté, selon la revendication 1, dans lequel ledit matériau conducteur est incorporé audit polyamide selon une quantité de 60 à 75% en poids.
4. Filament composite, conducteur, non étiré, fortement orienté, selon la revendication 1, dans lequel le rapport en poids dudit polymère thermoplastique (A) formant des fibres choisi parmi le téréphtalate de polyéthylène et le téréphtalate de polybutylène et ladite composition (B) comportant un matériau conducteur et un polyamide est :  
(B)/(A) = 8/92 à 22/78.
5. Procédé de fabrication d'un filament composite, conducteur, non étiré, fortement orienté, qui est un filament composite à gaine et âme comportant une gaine d'un polymère thermoplastique (A) formant

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des fibres, choisi parmi le téréphthalate de polyéthylène et le téréphthalate de polybutylène, et une  
âme d'une composition (B) comprenant un matériau conducteur qui comporte un ou des oxydes  
métalliques et un polyamide thermoplastique, comportant les étapes consistant à extruder ledit  
polymère thermoplastique (A) formant des fibres possédant une viscosité intrinsèque,  $[\eta]$ , après filage  
5 d'au moins 0,55 et ladite composition (B) ayant une teneur en humidité réglée par séchage à 100 à  
1200 ppm séparément à travers différentes extrudeuses, et à effectuer un filage par fusion à forte  
orientation en utilisant un dispositif de filage composite à au moins 2500 m/min. de sorte que les  
filaments ainsi filés possèdent un retrait dans l'eau chaude à 100 ° C non supérieur à 20%.

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Fig. 1

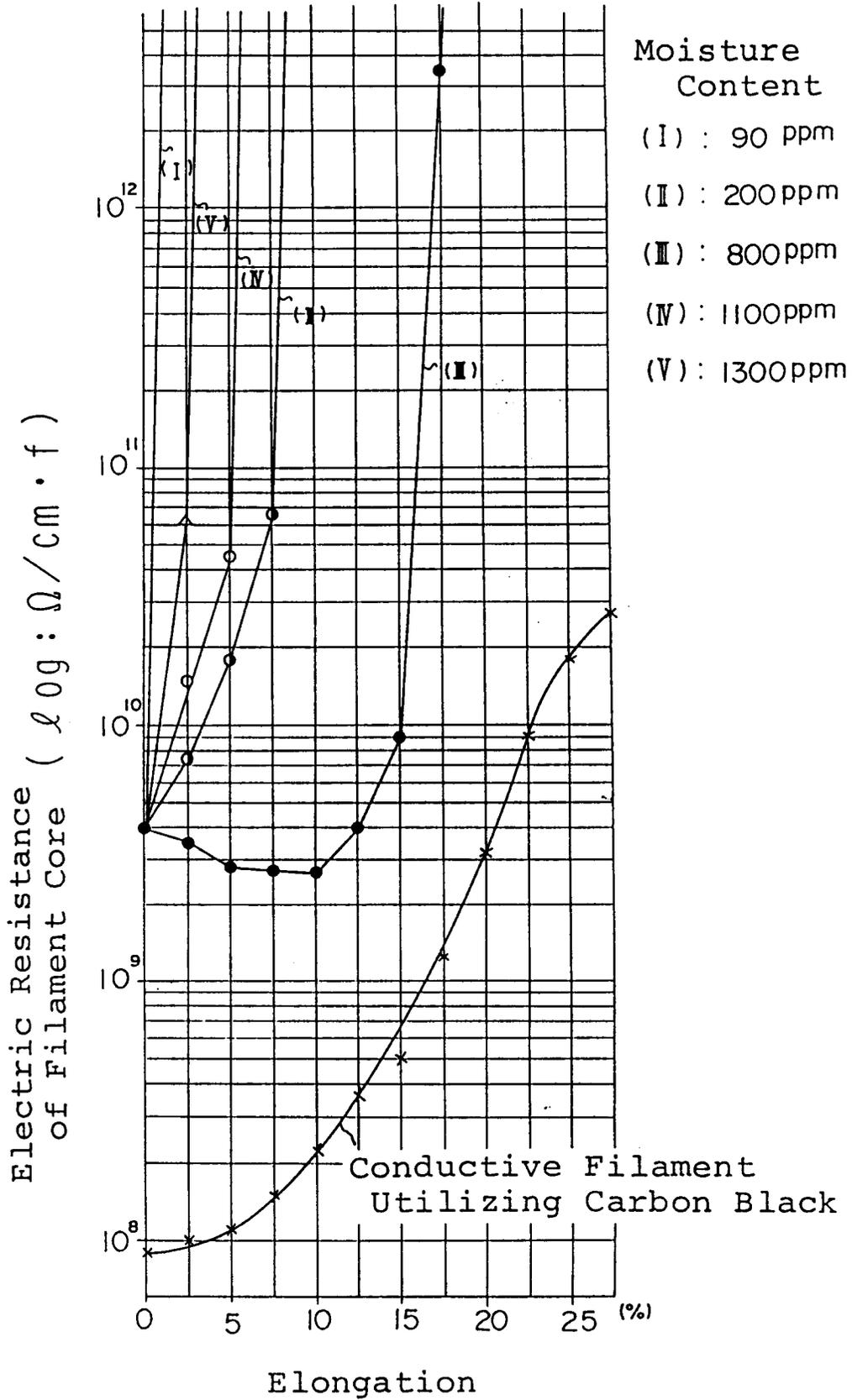


Fig. 2

