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(54) **Microwave plasma treating apparatus**

Mikrowellen-Plasma-Bearbeitungsgerät

Appareil de traitement par plasma de micro-ondes

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Description

The present invention relates to a microwave plasma treating apparatus. More specifically, it relates to an improved microwave plasma treating apparatus suitable for forming a deposited film and etching an object.

There are known a number of plasma chemical vapor deposition methods (hereinafter referred to as "plasma CVD method") and a number of apparatuses for practicing those plasma CVD methods (hereinafter referred to as "plasma CVD apparatus").

As for the plasma CVD methods, as they have advantages such as (i) capable of forming a deposited film at a low temperature of from 200 to 400°C, (ii) requiring no heat resistance for a substrate, etc. In view of this, they have been applied for the formation of a silicon dioxide film or a silicon nitride film which is usable as an insulating film in semiconductor systems, an amorphous silicon (a-Si) film which is usable in solar cells, close-contact type image sensors or photosensitive drums, a diamond thin film, etc. As for the plasma CVD apparatuses, there has been predominantly used a radiowave (RF) plasma CVD apparatus that RF is introduced between two flat plate type electrodes opposed in parallel with each other, thereby forming a plasma. And for such RF plasma CVD apparatus, it has a merit that its size may be easily modified because of their simple structure.

However, the conventional RF plasma CVD method involves the following drawbacks on the other hand. That is, ion sheath is apt to form on the side of a substrate to develop a negative self-bias, by which ion species in the plasma is drawn to the cathode to moderate the incident impact shock of the ion species to the anode on which the substrate is disposed. However, the ion species is still applied to the surface of the substrate and mixed into the deposited film to bring about internal stresses or increase the defect density, failing to obtain a deposited film of good quality. In addition, since the electron density is as low as from 10^8 to 10^{10} , the decomposing efficiency of the starting material gas is not so high and the deposition rate is low. Further in addition, since the electron temperature is as low as - 4 eV, starting material gas of high bonding energy such as silicon halide compound is less decomposable.

For improving the above-mentioned drawbacks of the RF plasma CVD method, there have been proposed, in recent years, several plasma treating methods and apparatuses used therefor using a microwave of about 2.45 MHz capable of efficiently forming a high density plasma and, at the same time, heating an object to be treated. And studies have been made on the method of depositing a thin film such as of silicon dioxide, silicon nitride, a-Si, diamond, etc. as well as an etching method for the silicon film.

Incidentally, conventional microwave plasma treating apparatuses are classified roughly into two types.

One of them is of a type as disclosed in Japanese Patent Publication Nos. 58-49295 and 59-43991 and Japanese Utility Model Publication No. 62-36240, in which a gas pipe is inserted through or placed in contact with a rectangular or coaxial waveguide to form a plasma (hereinafter referred to as "type 1 MW-plasma treating apparatus").

The other one is of a type as disclosed in Japanese Patent Laid-Open No. 57-133636, in which electron cyclotron resonance (ECR) is established within a cavity resonator and a plasma is drawn out by a divergent magnetic field (hereinafter referred to as "type 2 MW-plasma treating apparatus").

Fig. 3 shows a typical type 1-MW-plasma treating apparatus (refer to Japanese Utility Model Publication No. 62-36240).

That is, the type 1 MW-plasma treating apparatus comprises a vacuum system, an exhaust system and a microwave introducing system as shown in Fig. 3.

Referring to Fig. 3, the vacuum system comprises a reactor 307, and a microwave transmissive tube or a window (for example, made of quartz tube) having an inside diameter on the order of 40 mm and connected by a gas introducing pipe 307a. The quartz tube (or the window) is connected to a first gas introducing pipe and is arranged perpendicularly to a microwave waveguide. A second gas introducing pipe is connected to the inside of the reactor 307 and a gas (silane gas) supplied is exhausted through an exhaust system (307b and 308). In the apparatus, the gas introduced through the first gas introducing pipe (O_2 gas or N_2 gas) is converted into a plasma by microwave discharge. During microwave discharge caused by microwave energy, microwave input impedance can be matched by moving a sliding short-circuit plate, i.e., a plunger 305. Radicals of the plasma thus produced react with the silane gas supplied through the second gas introducing pipe, whereby a silicon dioxide film or a silicon nitride film is formed over the surface of a substrate 309.

Fig. 4 shows a typical type 2 MW-plasma treating apparatus (refer to Japanese Patent Laid-Open No. 57-133636). The system and configuration of this apparatus are the same as those of the foregoing type 1 MW-plasma treating apparatus except for the discharging space for which an electromagnet 407 is used. That is, the vacuum system comprises a cylindrical plasma producing vessel 401 and a reactor 402 connected thereto, in which a microwave introducing window 403 is attached hermetically to the plasma producing vessel. A first gas introducing pipe 406 and a microwave waveguide 404 are connected to the plasma producing vessel 401. The plasma producing vessel 401 is water-cooled by means of a water-cooling pipe 405 disposed at the outer circumference thereof. The apparatus shown in Fig. 4 is provided with an electromagnet 407 disposed coaxially with the plasma producing vessel 401. The direction of lines of magnetic force from the electromagnet 407 is the same as the travelling direction of the microwave. Electrons

move for a magnetron motion by the combination of a magnetic field and an electric field formed by the microwave in the perpendicular direction. Therefore, the plasma producing vessel 401 is designed as a cavity resonator of a TE_{11t} mode ($t =$ a natural number). A second gas introducing pipe and the exhaust system are connected to the reactor 402, and gases within the deposition vessel are exhausted by the exhaust system.

When the typical type 2 MW-plasma treating apparatus shown in Fig. 4 is used, for example, as a deposition apparatus a gas (H_2 gas) introduced through the first gas introducing pipe 406 is formed into a plasma by electric discharge caused by the microwave energy. When the magnetic flux density of the magnetic field is 875 gauss, the reflected wave of the microwave energy is almost zero. In this apparatus, the end plate 411 of the cavity resonator having the construction of a choke is moved under vacuum depending on the type of the gas, the pressure of the gas and the microwave power applied, so that the cavity resonator meets required conditions. Radicals in the plasma are transported under an electron cyclotron motion in the direction of the lines of magnetic force, and the radicals in the plasma react with the gas (silane gas) introduced through the second gas introducing pipe to form an a-Si film over the surface of a substrate 408.

However, both the type 1 MW-plasma treating apparatus and the type 2 MW-plasma treating apparatus have the following problems to be solved.

That is, the type 1 MW-plasma treating apparatus involves the following drawbacks; (i) it is necessary to control the pressure during electric discharge to an order of about 6.65 Pa (0.05 Torr) or higher, or to a gas of such a type as having a large ionizing cross sectional area easily causing electric discharge in order to attain stable discharge; and (ii) in the case where the apparatus is used for the film deposition, when the charged microwave power is increased in order to increase the film deposition rate, an electric field is concentrated to the junction between the quartz tube and the waveguide to cause sputtering to the quartz tube, by which impurities formed by the sputtering are mixed into the deposited film, failing to obtain a deposited film of satisfactory property.

On the other hand, the type 1 MW-plasma treating apparatus is free from the sputtering problem as described above and discharge even in a low pressure region of about 0.0133 Pa (10^{-4} Torr) is possible. However, there are the following problems upon forming, for example, an a-Si film by using a H_2 gas and a silane gas (SiH_4); (iii) a a-Si film is deposited on the microwave introducing window along with the progress of the depositing reaction making it difficult for impedance matching and maintenance of electric discharge; (iv) since the microwave introducing window 403 and the waveguide 404 are fastened and fixed, the end plate 411 has to be moved in vacuum for changing the axial length of the cavity resonator, thereby making the operation difficult; and (v) the weight of the apparatus is heavy and the cost is expensive since the apparatus uses coils for generating electric field under ECR conditions.

According to the disclosure of the documents EP-A-0 236 998 and EP-A-0 334 000 representing earlier patent applications, there is known a microwave plasma treating apparatus comprising a vacuum vessel, means for introducing a microwave to the inside of the vacuum vessel by a way of a microwave transmission circuit, means for supplying a starting gas to the inside of the vacuum vessel, means for evacuating the inside of the vacuum vessel and a specimen holder for maintaining a specimen substrate inside the vacuum vessel. The microwave transmission circuit has a cavity resonator, integrated with two matching circuits comprising an axial length running plunger for the cavity resonator and a sliding type is disposed at the portion of the cavity resonator where the microwave is introduced.

According to the document US-A-4 507 588, there is disclosed a generic microwave plasma treating apparatus from which the invention starts, said apparatus comprising a vacuum vessel, means for introducing a microwave to the inside of the vacuum vessel by the way of a microwave transmission circuit, means for supplying the starting gas to be inside of the vacuum vessel, means for evacuating the inside of the vacuum vessel and a specimen holder for maintaining a specimen substrate inside the vacuum vessel, wherein a cavity resonator integrated with a sliding short serving as an axial length varying means is disposed in the microwave transmission circuit and the magnetic field generator for generating the magnetic field in the discharging space disposed inside the cavity resonator is disposed outside the cavity resonator. The microwave power is introduced into the cavity resonator by means of an adjustable excitation probe while the reflection of the microwave power is controlled by means of the probe.

Accordingly, it is a principal object of the present invention to provide an improved microwave plasma treating apparatus having satisfactory operationability and productivity and capable of efficiently producing desired thin film semiconductors such as of a-Si.

An aim of the present invention is to overcome the foregoing problems in the conventional microwave plasma treating apparatus and provide a microwave plasma treating apparatus capable of conducting dry etching to an object to be treated at good operationability and productivity.

A further aim of the present invention is to provide a microwave plasma treating apparatus capable of stable electric discharge without using a large electromagnet as in the ECR system, in a low pressure region irrespective of the type of gas with small ionizing cross sectional area, while suppressing the reflected power, and at a low electric power.

The object of the invention is achieved by means of the combination of the features defined in claim 1. According to these features the invention is characterized over the above mentioned generic microwave plasma treating apparatus thereby that instead of the conventional means for introducing a microwave, the cavity resonator is integrated with a

sliding type iris matching with the axial length varying plunger.

Preferable embodiments of the invention are defined in claims 2 to 5.

The microwave plasma treating apparatus according to the present invention have the following constitutions.

The main features of the apparatus according to the present invention resides in the following points (a) through (c). Specifically, (a) matching is facilitated by a plunger for adjusting the axial length of the cavity resonator and a matching circuit by a cylindrical sliding type iris disposed at the portion of the cylindrical cavity resonator where the microwave is introduced, (b) a bell jar is penetrated into the cavity resonator to excite TM mode and (c) a magnetic field generator is disposed to the outside of the cavity resonator to prepare a region of a high magnetic flux density in the electric discharging space at the inside of the cavity resonator.

According to the present invention, various problems in the conventional microwave plasma treating apparatus are dissolved and stable electric discharge can be made with effective utilization of the microwave power, free from the effect of the ionizing cross sectional area of the gas and the pressure of the gas.

In addition, the apparatus according to the present invention can be desirably used for effectively forming a desired functional deposited thin film or for dry etching an object, which enables one to form semiconductor films or insulating films respectively of good quality, or to produce various etched materials, with good productivity and at a reduced cost.

In the following the invention is further illustrated by an embodiment with reference to the enclosed figures.

Fig. 1 is a schematic perspective view for a typical embodiment of a microwave plasma treating apparatus according to the present invention.

Fig. 2(A) through Fig. 2(H) are schematic constitutional views, respectively, for the magnetic field generating device in the apparatus according to the present invention.

Fig. 3 and Fig. 4 are, respectively, schematic constitutional views of conventional microwave plasma treating apparatus.

Fig. 5 is a chart collectively illustrating the results of electric discharge test for the apparatus according to the present invention.

The microwave plasma treating apparatus having the foregoing constitutions according to the present invention is to be explained below while mainly referring to the above-mentioned features (a), (b) and (c).

A constitution of the apparatus regarding the feature (a) can be attained by providing two matching circuits capable of being adjusted properly according to the phase and amplitude of a microwave. Since the energy of a standing wave is accumulated between the matching circuits and the cavity resonator, it is desirable that the distance between the matching circuits and the cavity resonator is reduced to the least possible extent. Most desirably, the matching circuits and the cavity resonator are integrated and at least one of the matching circuits is used as a plunger for varying the cavity length.

Incidentally, the phase and amplitude of the reflected microwave are dependent primarily on the plasma density and the morphology of a microwave feed circuit.

That is, the plasma density changes dependent on the kind of the gas, gas pressure or microwave power introduced and the complex refractive index $n-ik$ ($0 < n < 1$; k is absorption coefficient) also changes correspondingly. Accordingly, for always maintaining the function of the cavity resonator, the effects of n and k has to be nullified.

Since it is difficult to nullify the effect of n by varying the inside diameter of the cavity, the cavity length (L) of the cavity resonator may be increased by a length equivalent to the reduction of the inside diameter of the cavity to n times ($0 < n < 1$) the original length.

When the resonator frequency f (2.45 GHz), the resonance rst mode (TM_{rst}) and the inside diameter nD) of the cavity are known, the air equivalent value (L') of a new cavity length can be determined by the equation:

$$(2L')^2 = t^2/(f/c)^2 - (y_{rs}/nD)^2 \quad (1)$$

where y_{rs} is the root of the Bessel function: $J_r(y) = 0$, and c is the velocity of light.

As is obvious from the equation (1), the effect of n can be nullified by varying the length (L) of the cavity resonator according to the variation of n .

The effect of k , namely, the effects of the amplitude and phase lag δ of the reflected wave, can be nullified by adjusting the two matching circuits.

Practically, since n and k are dependent on each other, the length (L) of the cavity resonator and the position of sliding matching irises may be adjusted for one set of (n and k).

On the other hand, the reflected wave, which are dependent on the morphology of the microwave feed circuit, can be matched efficiently by using the two matching circuits.

A constitution relating to the aforesaid feature (b) can be attained by connecting a rectangular waveguide and a cylindrical cavity resonator with the axes thereof intersecting each other at a right angle as shown in Fig. 1. When the waveguide and the cavity resonator are thus connected, an operation for varying the length of the cavity resonator is not obstructed by the waveguide. In the cylindrical cavity resonator, the microwave is driven in TM_{01n} (n is a natural

number), and the length of the cavity resonator can be changed even in the atmosphere, thereby facilitating the efficiency of operation.

A constitution regarding the aforesaid feature (c) can be attained by disposing a tubular cylindrical magnetic field generator to the outside of the cavity resonator, by which a region of high magnetic flux density can be formed in the electric discharging space at the inside of the cavity resonator. The magnetic field generator is generally classified into a permanent magnet and an electromagnet. Specifically, there are permanent magnets disposed in a coaxial manner as shown in Figs. 2 (A) through (D), ring-like permanent magnets disposed as shown in Figs. 2(E) and (F), and electromagnets comprising air-cored solenoid coils as shown in Figs. 2(G) and (H). In each of Figs. 2, the upper view is a side elevational view and the lower view is a top plan view each in a schematic manner, in which N and S mean magnetic poles. As the permanent magnet those having great coercive force and residual magnetic flux density are suitable and, among all, rare earth or ferrite series magnets are preferred. As the electromagnets, those having central magnetic flux density of greater than 50 gauss and, more preferably, greater than 100 gauss are desirable. Electromagnets are combined by one set in Fig. 2(G) and by two sets in Fig. 2(H). Particularly, in the embodiment shown in Fig. 2(H), it is possible to change the magnetic poles by changing the polarity of current for the two sets of electromagnets, thereby obtaining a mirror type or cusped type magnetic field.

It is not always necessary that the magnetic flux density in the electric discharging space of the magnetic field generator used for the microwave plasma treating apparatus according to the present invention is such a magnetic flux density as capable of obtaining electron cyclotron resonance relative to the frequency of the microwave. In the case of using the electromagnet, while it is necessary to increase the number of turns for the coils for increasing the maximum magnetic flux density produced, desired magnetic flux density can be obtained by controlling the electric current supplied thereto. In view of the above, it is more preferred to use a combination of permanent magnets if the importance is attached to the compactness and the cost reduction, and to use an electromagnet in the case where the importance is attached to the control of the magnetic flux density as the magnetic field generator of the microwave plasma treating apparatus.

In the present invention, using the magnetic field generator as described above, the performance of the microwave plasma treating apparatus is improved remarkably thereby enabling to lower the pressure during electric discharge, reduce the reflected power and save in the electric power for maintaining the electric discharge.

The illustrated embodiment for the microwave plasma treating apparatus according to the present invention is to be explained more in details, but the present invention is no way restricted only thereto. For the sake of simplicity, although the explanation is made only to the case of using the cylindrical cavity resonator, the present invention is no way limited only thereto.

One embodiment for the apparatus according to the present invention is shown as a schematic perspective view in Fig. 1.

In Fig. 1, are shown a rectangular waveguide 101, a cylindrical cavity resonator 102, a plunger 103 for varying the length of the cavity resonator, cylindrical sliding matching irises 104, a microwave transmissive bell jar 105, a microwave reflector 106, a reaction vessel (or film-forming vessel) 107, a substrate 108, a substrate holder 109, gas introducing pipes 110, 111, a gas outlet 112, a driving device 113 for the plunger 103 for varying the axial length connected with a feedback control circuit from a power monitor, and a magnetic field generator 114, respectively.

Essentially, the apparatus shown in Fig. 1 is a microwave plasma treating apparatus of a cavity resonator type according to the present invention comprises a microwave oscillator (not shown), a microwave transmission circuit (not shown), a cavity resonator, and a reaction vessel provided with a microwave transmissive bell jar defining a plasma producing chamber, gas introducing pipes (110, 111) and a gas outlet 112.

In Fig. 1, the cylindrical cavity resonator 102 is preferably made of material having a low electric resistivity in order to decrease ohmic loss attributable to the surface current of a microwave. In addition, since the plunger for varying the length of the cavity moves under fitting with the cavity resonator, it has to be abrasion resistant. Accordingly, the cavity resonator is desirably made of material such as copper, brass and a silver-plated, copper-plated or gold-plated stainless steel. Among all, a silver-plated stainless steel is most suitable.

The cylindrical cavity resonator 102 and the rectangular waveguide 101 are joined together with the axes thereof intersecting each other at right angle to convert the H_{10} (TE_{10}) mode of the rectangular waveguide 101 into the E_{01} (TM_{01}) mode of a circular waveguide. The cavity resonator 102 is provided integrally with two matching circuits, namely, the plunger 103 for varying the length of the cavity resonator 102, and the cylindrical sliding matching irises 104.

The plunger 103 for varying the length of the cavity resonator 102 is movable along the axis of the cavity resonator 102. The plunger 103 may be driven, for example, by a motor 113. To prevent abnormal electric discharge between the cavity resonator 102 and the plunger 103, spring members made of phosphor bronze are used so that stable contact can be maintained.

A pair of right and left cylindrical sliding matching irises 104 are disposed respectively at the junction of the rectangular waveguide 101 and the cavity resonator 102. As indicated by an arrow in the figure, the irises are moved in the longitudinal direction of the rectangular waveguide 101 and the two irises are individually slidable along the cylin-

dricial surface of the cavity resonator 102. The irises and the cavity resonator 102 are put into contact in a manner similar to that of the plunger.

To the outside of the cavity resonator 102, a magnetic field generator 114 selected from the embodiments shown in Figs. 2(A) through (H) is disposed for forming a magnetic field in the discharging space of the bell jar.

The microwave transmissive bell jar 105 is disposed within the cavity resonator 102 (for example, 120 mm in inside diameter). The bell jar 105 is connected to the reaction vessel 107. An O-ring or a metallic sealing member for vacuum seal and the microwave reflector 106 are provided at the flange surface of the bell jar 105. A microwave is reflected by the microwave reflector 106, and the gas can flow between the interior of the bell jar 105 and that of the film-forming vessel 107.

The bell jar 105 is made of material such as quartz (SiO_2), alumina (Al_2O_3), boron nitride (BN) or silicon nitride (SiN).

The microwave reflector 106 is a perforated silver-, copper- or gold-plated metallic plate (a silver-plated metallic plate is particularly suitable) provided with a plurality of through holes, such as a perforated aluminum plate of 0.8 mm thickness having a plurality of circular holes of 6 mm in diameter and a ratio of hole area of 60 %, namely, a so-called punched board. The perforated plate is screwed to the reaction vessel 107 to suppress abnormal electric discharge.

The microwave reflector may be made of an expanded metal instead of the perforated plate.

Disposed within the reaction vessel 107, are the substrate 108, the substrate holder 109 and the two gas introducing pipes 110 and 111. The extremity of the gas introducing pipe 110 penetrates through the microwave reflector 106 and opens into the interior of the bell jar 105. The other gas introducing pipe 111 has an annular extremity provided with a plurality of nozzle holes for jetting a gas. The pipe 111 is disposed between the bell jar 105 and the substrate holder 109.

The reaction vessel 107 is connected to a vacuum pump, not shown, for evacuating the reaction vessel.

Prior to the start of operation of the microwave plasma treating apparatus thus constructed in accordance with the present invention, the length of the cavity resonator is adjusted to a value slightly shorter than $m/2 \times \lambda$ (m: natural number) for easy starting of initial electric discharge. Concretely, the length of the cavity resonator is decided so that the cavity resonator functions with the bell jar 105 being disposed therein by previously measuring the network by a network analyzer (manufactured by Hewlett Packard Co.).

For example, when the bell jar is 3 mm in wall thickness, 70 mm in diameter and 100 mm in height, the decrement in the length of the cavity resonator is 3 mm and the length of the cavity resonator is 192 mm and, when the bell jar is 3 mm in wall thickness, 100 mm in diameter and 100 mm in height, the decrement in the length of the cavity resonator is 4 mm and the length of the cavity resonator is 290 mm.

In the microwave plasma treating apparatus according to the present invention, the following advantageous effects can be obtained. That is, in a low pressure region of less than 1.33 Pa (10^{-2} Torr) without using a magnetic field of great magnetic flux density as in ECR conditions, (i) stable electric discharge can be attained solely with such a type of gas as having relatively small ionizing cross sectional area, for example, H_2 or H, (ii) the electric power for maintaining the electric discharge can be reduced and (iii) the reflection power can be decreased.

Explanation is to be made for the method of operating the microwave plasma treating apparatus shown in Fig. 1, which illustrates one embodiment of the present invention.

At first, after evacuating the inside of the bell jar 105 and the film-forming chamber by way of a vacuum pump not illustrated to less than a predetermined pressure, the gas used for forming a plasma is introduced from the gas introduction pipe 110 or 111 into the bell jar 105, while a magnetic field is applied from the plasma forming device 114 (Figs. 2(A) through (H)) and the microwave power applied from a microwave generator not illustrated is introduced by way of the waveguide 101 to the inside of the cavity resonator 102. Successively, the axial length varying plunger and the cylindrical irises for the cavity resonator are controlled by the reflection power feedback control mechanism for restricting the reflection power of the power monitor for the microwave and causing stable electric discharge (E-H tuner or three-stub tuner may be used instead of the cylindrical irises). After operating for a certain period of time under this state, supply of the microwave power is interrupted and the operation is ended.

The microwave plasma treating apparatus according to the present invention can be used suitably as a thin film depositing apparatus and dry etching apparatus.

In the case of using the apparatus according to the present invention for the dry etching of an object to be treated, an etching gas is introduced from the gas introducing pipe 110 in the above-mentioned operating method to conduct etching. As the etching gas, CF_4 , C_2F_6 , C_3F_8 , C_4F_{10} (octafluorocyclobutane), C_5F_{12} , CHF_3 , CBrF_3 , CCl_4 , CCl_3F , CCl_2F_2 , CClF_3 , SF_6 , NF_3 , BCl_3 , F_2 , Cl_2 , Br_2 , HF or HCl, or a gas mixture of the above-mentioned etching gas and H_2 , O_2 , N_2 , He, Ne, Ar, Kr or Xe is used depending on the material to be etched. For example, there are generally used $\text{CF}_3 + \text{O}_2$ for etching Si and CF_4 for SiO_2 etching. The inner pressure for the dry etching is preferably from 0.0133 to 13.3 Pa (10^{-4} to 10^{-1} Torr).

In the case of using the apparatus according to the present invention for thin film deposition, there are two methods (a) and (b) in the above-mentioned operating method, that is, (a) a method of introducing film-forming starting gas from the gas introduction pipe 110 thereby forming a deposited film and (b) a method of introducing a plasma-forming starting gas from the gas introducing pipe 110 into the reaction vessel (film-forming vessel) 107 and introducing the film-forming

starting gas from the gas introduction pipe 111 into the film-forming vessel 107, thereby forming a deposited film. The method for forming the deposited film is properly selected depending on the desired deposited film or the starting gas employed.

When the microwave treating apparatus according to the present invention is applied to the deposition of thin films, it is possible to form thin films of satisfactory quality such as of amorphous silicon, crystalline silicon, amorphous silicon germanium, silicon nitride, silicon oxide, amorphous silicon carbide, diamond and various kinds of organic high molecular compounds.

The gas used in the above-mentioned cases can be selected depending on the kind of deposited film as shown below.

That is, as the starting material gas for depositing a thin film of amorphous silicon or crystalline silicon, there can be mentioned those gases containing silicon atoms, for example, SiH_4 , Si_2H_6 , SiF_4 , SiHF_3 , SiH_2F_2 , SiH_3F , Si_2F_6 , SiCl_4 , SiH_2Cl_2 , SiH_3Cl . Liquid material such as SiCl_4 is used after gasifying by the bubbling of an inert gas. As the gas used for forming plasma, there can be mentioned, for example, H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe in addition to the starting gas described above.

As the starting gas in the case of depositing a thin film of amorphous silicon germanium, a gas mixture of the silicon atom-containing starting gas used for depositing the amorphous silicon as described above and germanium atom-containing gas, for example, GeH_4 or GeF_4 is used. As the gas used for forming the plasma, there can be mentioned H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe in addition to the gas mixture of the silicon atom-containing gas and the germanium atom-containing gas.

As the starting gas for depositing the silicon nitride thin film, there may be used the silicon atom-containing gas used for depositing the amorphous silicon as described above, or a gas mixture of at least one of gases containing nitrogen atoms, for example, N_2 , HN_3 , HF_3 and a silicon atom-containing gas. The gas used for forming the plasma can include, in addition to the starting gas as described above, N_2 , NH_3 , HF_3 , H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe . In the case of forming silicon nitride, it is necessary that the starting gas or plasma-generating gas contains at least nitrogen-containing gas and silicon-containing gas.

As the starting gas for depositing a silicon oxide thin film, there can be used the silicon atom-containing gas used for depositing amorphous silicon as described above, or a gas containing oxygen O_2 and silicon atoms. The gas used for forming the plasma can include, in addition to the starting material gas as described above, O_2 , H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe . In the case of forming silicon oxide, the starting gas or the plasma forming gas has to contain at least O_2 and silicon atom-containing gas. As the starting gas in the case of depositing the amorphous silicon carbide thin film, there may be used the silicon atom-containing gas used for depositing amorphous silicon as described above, silicon atom- and carbon atom-containing gas such as $\text{Si}(\text{CH}_3)_4$, or a gas mixture comprising at least one of carbon atom-containing gases selected from CH_4 , C_2H_2 , C_2H_4 or C_2H_6 , and the silicon atom-containing gas as described above. The gas used for forming the plasma can also include, in addition to the starting gas described above, carbon atom-containing gas, H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe . In the case of forming amorphous silicon carbide, it is necessary that the starting gas or plasma-forming gas contains at least a carbon atom-containing gas and a silicon atom-containing gas.

As the starting gas for depositing a diamond thin film, there can be mentioned, CH_4 , C_2H_2 , C_2H_4 , C_2H_6 , CH_3COCH_3 , CH_3OH , CH_3COCH_3 or CH_3OH is used after gasifying by the bubbling of an inert gas. Further, as the gas for forming plasma, there may be mentioned, in addition to the carbon atom-containing gas described above, H_2 , F_2 , Cl_2 , HF , HCl , He , Ne , Ar , Kr or Xe .

The starting gas used for forming the film described above may be used also as a gas for generating the plasma. Further, the film-forming starting gas may be diluted with an inert gas such as He or Ar . In the case of adding impurity into the deposited film, a gas such as PH_3 , PF_5 , PF_3 , PCl_3 , PCl_5 , B_2H_6 , BF_3 , BCl_3 , BBr_3 , AsF_5 , AsCl_3 , AsH_3 , I_2 , SbH_3 or SbF_5 is mixed into the film-forming starting gas or plasma-forming gas. The pressure upon reaction for forming a thin film of amorphous silicon, crystalline silicon, amorphous silicon germanium, silicon nitride, silicon oxide or amorphous silicon carbide is preferably from 0.00133 to 133 Pa (10^{-5} to 10^{-1} Torr).

The reaction pressure upon forming the diamond thin film is preferably from 0.133 to 13300 Pa (10^{-3} to 10^2 Torr).

Further, in the formation of the deposited film and etching by using the microwave plasma treating apparatus according to the present invention, heat energy or light energy may be applied to the surface of the substrate in order to promote the reaction.

Electric Discharge Test

An electric discharge test was conducted by using the microwave plasma treating apparatus according to the present invention shown in Fig. 1, while varying the kind of the gas and the pressure region in a case where the bell jar 105 had 100 mm diameter ϕ , taking notice on the maintenance of the electric discharge, reflection power and incident power. As a comparison, electric discharge test by detaching the magnetic field generator and TE mode electric dis-

charge test by detaching the electromagnet in the microwave plasma apparatus shown in Fig. 4 were also conducted. H_2 , Ar, SiH_2Cl_2 was used as the gas and introduced through the gas introduction pipe 110. The magnetic field generator of the type shown in Fig. 2 (B) having a central magnetic flux density at 150 gauss was used. The results of the electric discharge test are collectively shown in Table 1.

Further, in Fig. 1, by using the microwave plasma treating apparatus with the diameter ϕ of the bell jar 105 of 70 mm and the central magnetic flux density at 100 gauss, H_2 and Ar discharge was conducted to determine the relationship between the pressure and the electric power for maintaining the discharge. The results are shown in Fig. 5 (1 Torr = 133 Pa).

It can be seen from the results of Table 1 and Fig. 5 that the reflection power can be restricted and electric discharge could be caused in a lower pressure region and with a lower electric power by using the microwave plasma treating apparatus according to the present invention disposed with the magnetic field generator.

When the same electric discharge test as above was conducted for the magnetic generator with the type other than that shown in Fig. 2(B), similar results with those for the type shown in Fig.2(B) were obtained.

Deposited Film Forming Example 1

Using the apparatus shown in Fig. 1 used for electric discharge test and the magnetic field generator of a type shown in Fig. 2(G), formation of the amorphous silicon (a-Si) film was investigated.

At first, a cleaned #7059 glass substrate manufactured by Corning Glass Works and a high resistance silicon single crystal substrate were attached to the specimen holder 109, the inside of the vessel was evacuated to a high vacuum degree of 0.000133 Pa (1×10^{-6} Torr) and the substrate temperature was controlled to 250°C by a substrate heater not illustrated in Fig. 1. Then, 5 SCCM of SiH_2Cl_2 and 50 SCCM of H_2 were introduced from the gas introducing pipe 110, the pressure in the reaction vessel 107 was controlled to 6.65 Pa (0.05 Torr), the current for the magnetic field generator was controlled such that the magnetic flux density at the center of the discharging space in the bell jar 105 200 gauss. Then, a microwave at a frequency of 2.45 GHz was applied at 250 W power to conduct reaction for one hour to obtain an a-Si film of 1.2 μm thickness (the reflection power was minimized during reaction by the power feedback mechanism).

The deposition rate was 3.3 Å/sec and the ratio $\delta P/\delta d$ between the photoconductivity (δp) under light irradiation of AMI (100 mw/cm²) and the dark conductivity (δd) was 1.1×10^5 .

Separately, when an a-Si film is deposited by the same method as in the experimental method described above while detaching the magnetic field generator, the deposition rate was reduced to 1/3, that is, 1.5 Å/sec, the ratio $\delta p/\delta d$ was 1.4×10^3 and broad absorption peak was observed near 1100 cm⁻¹ based on IR absorption spectrum for a-Si film formed on silicon single crystals.

It is assumed that since SiH_2Cl_2 as the starting gas was not completely decomposed and reacted in the case not using the magnetic field generator, Cl atoms remained in the deposited film, which were hydrolyzed when exposed to air thereby forming Si-O-bonds.

Deposited Film Forming Example 2

In the apparatus shown in Fig. 1, forming for polysilicon (poly-Si) film was studied by using a mirror type magnetic field generator of a type illustrated in Fig. 2(H), in which identical magnetic poles are formed from first and second solenoid coils. In the same method as in the deposited film forming example, a # 7059 glass substrate and a silicon single crystal substrate were attached to the specimen holder 109. The inside of the vessel was evacuated to a high vacuum degree of 0.000133 Pa (1×10^{-6} Torr). The substrate temperature was controlled to 300°C, the pressure in the reaction vessel 107 was maintained at 0.665 Pa (0.005 Torr) and the current for the magnetic field generator was controlled to attain the magnetic flux density to 200 gauss at the center of the discharging space in the bell jar 105. Then, 100 SCCM of H_2 was introduced from the gas introducing pipe 110 and 10 SCCM of Si_2F_6 after heated to 700°C was introduced from the gas introducing pipe 111, a microwave of 2.45 GHz was charged at 300 W power and reaction was conducted for one hour. The thickness of the resultant silicon film was 6000 Å and, as a result of the evaluation for the crystallinity according to RHEED (reflection high speed electron rate diffraction). It was found that an epitaxial film was grown on the (110) silicon single crystal substrate and < 110 > oriented poly-crystalline film was grown on the #7050 glass substrate.

Deposited Film Forming Example 3

Deposition of a silicon nitride film was investigated by using the apparatus shown in Fig. 1 provided with magnetic field generator of a type illustrated in Fig. 2(A) having the 1000 gauss of central magnetic flux density.

At first, a cleaned single crystal silicon substrate was attached to the specimen holder 109 and the inside of the

vessel was evacuated to a high vacuum degree of 0.000133 Pa (1×10^{-6} Torr). The substrate temperature was controlled to 250°C, 100 SCCM of N_2 and 10 SCCM of NH_3 were introduced from the gas introducing pipe 110, while 5 SCCM of SiH_4 was introduced from the gas introducing pipe 111, the pressure in the reaction vessel 107 was controlled to 2.66 Pa (0.02 Torr) and a microwave of 2.45 GHz was applied at 250 W of electric power. After reaction for 30 min, the thickness of the resultant silicon nitride film was 6800 Å. The etching rate with a fluoric acid buffer solution (50% HF: 40% $NH_4F = 15 : 85$) was 92 Å/min and a silicon nitride film having a film quality substantially equal to that formed by the thermal CVD method was obtained.

Etching Example 1

Using the same apparatus as that used for the electric discharge test, dry etching for the silicon nitride film was investigated.

Photoresist (OFPR-800, manufactured by Tokyo Ohka Co.) was coated on a silicon nitride film formed on a single crystal silicon wafer and a resist pattern was formed by photolithography. A silicon nitride substrate masked with the resist pattern was attached to the specimen holder 109, the vessel was evacuated to 0.00133 Pa (1×10^{-5} Torr), 50 SCCM of CF_4 was introduced from the gas introduction pipe 110, the pressure in the reaction vessel 107 was controlled to 0.665 Pa (0.005 Torr) and a microwave of 0.45 GHz was charged at 3000 W of electric power. The etching reaction was conducted for 5 min, the nitride silicon substrate was taken out and, after removing the resist, the step in the silicon nitride film was measured to calculate the etching rate as 1100 Å/min.

As the result of the etching reaction conducted in the same procedure as described above except for detaching the magnetic field generator, the etching rate was 470 Å/min and the effect of attaching the magnetic field generator was recognized.

In the Deposition Film Forming Examples 1, 2 and 3, examples for forming amorphous silicon, polysilicon and silicon nitride were shown, respectively, and an example for etching silicon nitride was shown in Etching Example 1. However, the present invention is not restricted to them but also effective to the formation of silicon oxide, amorphous silicon carbide and diamond or various etching for metals.

Table 1 (to be continued)
(1 Torr = 133Pa)

			TE mode		
No.	Gas used/ flow rate (SCCM)	Inner pressure (Torr)	$\frac{\text{Incident power (W)}}{\text{Reflection power (W)}}$	Electric discharge (○) (×)	$1 - \frac{\text{Reflection power (W)}}{\text{Incident power (W)}}$
1	Ar/50	0.005	182/90	○	0.51
		0.002	—	×	—
2	H ₂ /50	0.020	—	×	—
		0.005	—	×	—
3	He/50	0.070			
		0.020			
4	H ₂ /50 He/40 Ar/10	0.020			
		0.010			
5	SiH ₂ Cl ₂ /10 H ₂ /50	0.020			
		0.005			

Table 1 (to be continued)

Without magnetic field generator					
No.	Gas used/ flow rate (SCCM)	Inner pressure (Torr)	Incident power (W) — Reflection power (W)	Electric discharge (○) (×)	1 — Reflection power (W) Incident power (W)
1	Ar/50	0.005	178/33	○	0.81
		0.002	190/22	○	0.88
2	H ₂ /50	0.020	430/150	○	0.65
		0.005	—	×	—
3	He/50	0.070	335/75	○	0.78
		0.020	—	×	—
4	H ₂ /50 He/40 Ar/10	0.020	320/150	○	0.54
		0.010	325/200	instable discharge	0.38
5	SiH ₂ Cl ₂ /10 H ₂ /50	0.020	380/100	○	0.74
		0.005	—	×	—

Table 1 (continued)

No.	Gas used/ flow rate (SCCM)	Inner pressure (Torr)	With magnetic field generator (present invention)		
			$\frac{\text{Incident power (W)}}{\text{Reflection power (W)}}$	Electric discharge (○) (×)	$1 - \frac{\text{Reflection power (W)}}{\text{Incident power (W)}}$
1	Ar/50	0.005	172/26	○	0.85
		0.002	183/18	○	0.90
2	H ₂ /50	0.020	450/30	○	0.93
		0.005	340/160	○	0.53
3	He/50	0.070	320/40	○	0.88
		0.020	330/175	○	0.47
4	H ₂ /50 He/40 Ar/10	0.020	280/85	○	0.70
		0.010	145/35	○	0.76
5	SiH ₂ Cl ₂ /10 H ₂ /50	0.020	370/55	○	0.85
		0.005	280/115	○	0.59

Claims

1. A microwave plasma treating apparatus comprising a vacuum vessel (107), means (101-106) for introducing a microwave to the inside of said vacuum vessel by way of a microwave transmission circuit, means (110, 111) for supplying a starting gas to the inside of said vacuum vessel, means for evacuating the inside of said vacuum vessel and a specimen holder (109) for maintaining a specimen substrate (108) inside said vacuum vessel, wherein a cavity resonator (102), integrated with two matching circuits (103, 104) comprising an axial length varying plunger (103) for said cavity resonator and a sliding type iris (104) disposed at the portion of the cavity resonator where the microwave is introduced, is disposed in said microwave transmission circuit, and a magnetic field generator (114; 200; 201) for generating a magnetic field in the discharging space disposed inside said cavity resonator is

disposed outside said cavity resonator.

2. A microwave plasma treating apparatus according to claim 1, **characterized in that** said cavity resonator (102) is cylindrical and said sliding type iris (104) constitutes a cylindrical sliding type iris.
3. A microwave plasma treating apparatus according to claim 1, **characterized in that** said cavity resonator (102) is rectangular and said sliding type iris (104) comprises a planar sliding type iris.
4. A microwave plasma treating apparatus according to claim 1, **characterized in that** said means for introducing the microwave comprises a continuously oscillating microwave generator and a microwave transmissive bell jar (105) for forming the discharging space disposed within said cavity resonator.
5. A microwave plasma treating apparatus according to claim 1, which further comprises a power monitor means disposed in the microwave transmission circuit, a feedback control mechanism (113) provided for applying coarse control by said plunger (103) for varying the length of said cavity resonator (102), and means for applying fine control by a matching circuit disposed separately in order to reduce the value: (reflection power) / (incident power) based on the signal from said power monitor means.

Patentansprüche

1. Mikrowellenplasmabehandlungsvorrichtung, umfassend einen Vakuumbehälter (107), eine Einrichtung (101 bis 106) zum Einleiten einer Mikrowelle ins Innere des Vakuumbehälters mit Hilfe eines Mikrowellenübertragungsschaltkreises, eine Einrichtung (110 und 111) zum Einleiten eines Ausgangsgases ins Innere des Vakuumbehälters, eine Einrichtung zum Evakuieren des Inneren des Vakuumbehälters und einen Probenhalter (109) zum Aufnehmen eines Probesubstrates (108) im Inneren des Vakuumbehälters, worin ein Hohlraumresonator (102), in den zwei Abgleichschaltkreise (103 und 104) integriert sind, die einen Stempel (103) zum Verändern der axialen Länge des Hohlraumresonators und eine Blende (104) vom Gleittyp umfassen und in einem Bereich des Hohlraumresonators angeordnet sind, und in den die Mikrowelle eingeleitet wird, in dem genannten Mikrowellenübertragungsschaltkreis angeordnet ist und eine Erzeugungsvorrichtung für ein magnetisches Feld (114, 200 und 201) zum Erzeugen eines magnetischen Feldes im Entladungsraum, der im Inneren des Hohlraumresonators angeordnet ist, außerhalb des Hohlraumresonators angebracht ist.
2. Mikrowellenplasmabehandlungsvorrichtung nach Anspruch 1, dadurch gekennzeichnet, daß der Hohlraumresonator (102) zylindrisch ist und die Blende vom Gleittyp (104) eine zylindrische Blende vom Gleittyp darstellt.
3. Mikrowellenplasmabehandlungsvorrichtung nach Anspruch 1, dadurch gekennzeichnet, daß der Hohlraumresonator (102) rechteckig ist und die Blende vom Gleittyp (104) eine planare Blende vom Gleittyp darstellt.
4. Mikrowellenplasmabehandlungsvorrichtung nach Anspruch 1, dadurch gekennzeichnet, daß die Einrichtung zum Einleiten der Mikrowelle eine ununterbrochen schwingende Erzeugungsvorrichtung für Mikrowellen und eine mikrowellendurchlässige Glasglocke (105) zur Bildung des Entladungsraumes, die im Hohlraumresonator angeordnet ist, umfaßt.
5. Mikrowellenplasmabehandlungsvorrichtung nach Anspruch 1, die weiter eine Energieüberwachungseinrichtung, die in den Mikrowellenübertragungsschaltkreis eingebaut ist, einen Rückmeldesteuermechanismus (113), der bereitgestellt ist zur Durchführung einer Grobsteuerung durch den Stempel (103) zur Veränderung der Länge des Hohlraumresonators (102), und eine Einrichtung zur Durchführung einer Feinkontrolle durch einen Abgleichschaltkreis, der getrennt angeordnet ist, um den Wert:
(reflektierte Energie)/(eingestrahlte Energie)
auf Grundlage des Signals von der Energieüberwachungseinrichtung zu verringern, umfaßt.

Revendications

1. Appareil de traitement de plasma par micro-ondes comprenant un récipient à vide (107), des moyens (101 à 106) pour introduire des micro-ondes à l'intérieur dudit récipient à vide au moyen d'un circuit de transmission de micro-ondes, des moyens (110, 111) pour fournir un gaz de démarrage à l'intérieur dudit récipient à vide, des moyens

pour évacuer l'intérieur dudit récipient à vide et un porte-échantillons (109) pour maintenir un substrat d'échantillon (108) à l'intérieur dudit récipient à vide, dans lequel une cavité résonnante (102), intégrée avec deux circuits d'adaptation (103, 104) comprenant un piston variant en longueur axiale (103) pour ladite cavité résonnante et un iris de type coulissant (104) disposé à la partie de la cavité résonnante où les micro-ondes sont introduites, est disposé dans ledit circuit de transmission de micro-ondes, et un générateur de champ magnétique (114 ; 200 ; 201), pour générer un champ magnétique dans l'espace de décharge situé à l'intérieur de ladite cavité résonnante, est disposé à l'extérieur de ladite cavité résonnante.

2. Appareil de traitement de plasma par micro-ondes selon la revendication 1, caractérisé en ce que ladite cavité résonnante (102) est cylindrique et ledit iris de type coulissant (104) constitue un iris de type coulissant cylindrique.

3. Appareil de traitement de plasma par micro-ondes selon la revendication 1, caractérisé en ce que ladite cavité résonnante (102) est rectangulaire et en ce que ledit iris de type coulissant (104) constitue un iris de type coulissant plan.

4. Appareil de traitement de plasma par micro-ondes selon la revendication 1, caractérisé en ce que lesdits moyens destinés à introduire les micro-ondes comprennent un générateur de micro-ondes en oscillation continue et une cloche de transmission de micro-ondes (105) pour former l'espace de décharge disposé à l'intérieur de ladite cavité résonnante.

5. Appareil de traitement de plasma par micro-ondes selon la revendication 1, qui comprend en outre des moyens de contrôle de puissance disposés dans le circuit de transmission des micro-ondes, un mécanisme d'asservissement (113) prévu pour appliquer un contrôle approximatif à l'aide dudit piston (103) pour modifier la longueur de ladite cavité résonnante (102), et des moyens pour appliquer un contrôle fin au moyen d'un circuit d'adaptation disposé séparément afin de réduire la valeur (puissance de réflexion)/(puissance incidente) sur la base du signal provenant desdits moyens de contrôle de puissance.

FIG. 1

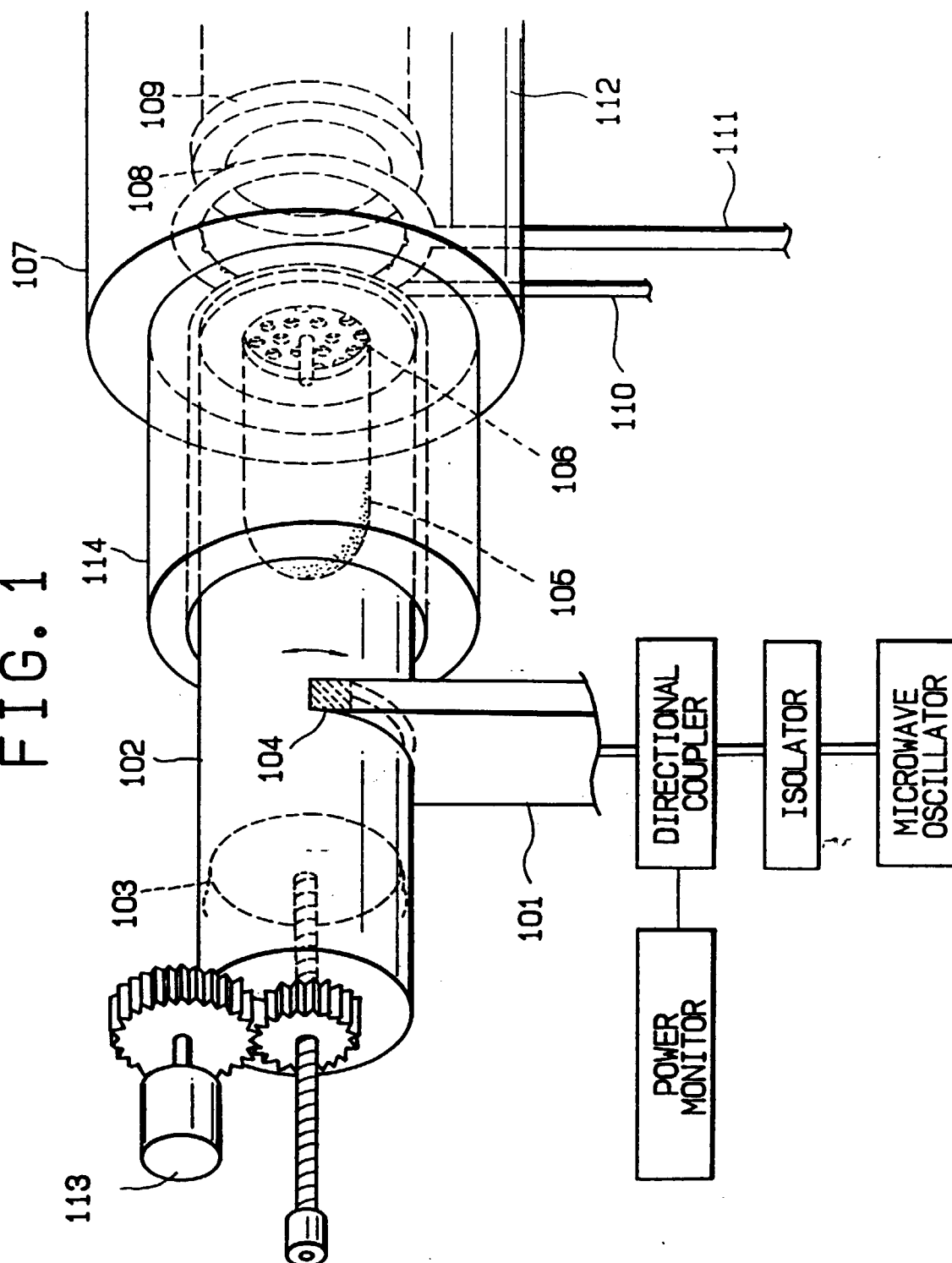


FIG. 2(A)

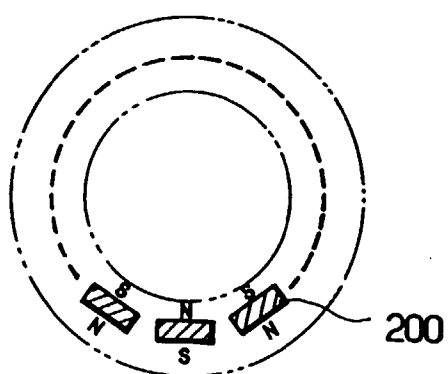
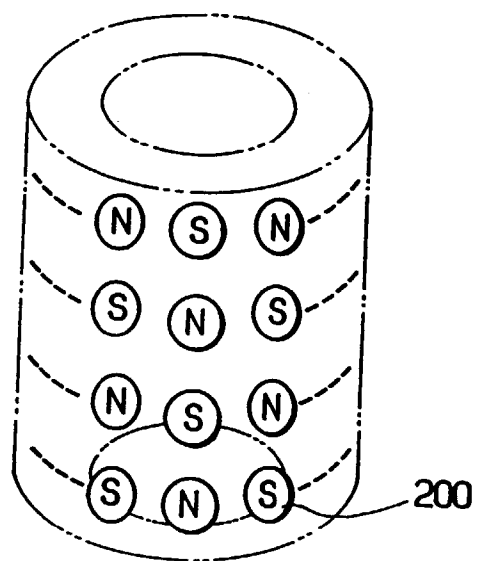


FIG. 2(B)

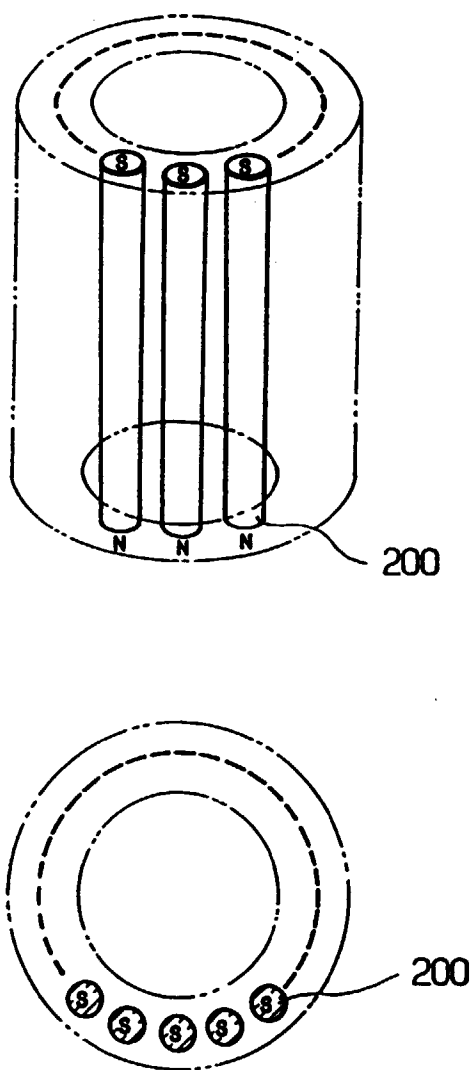


FIG. 2(C)

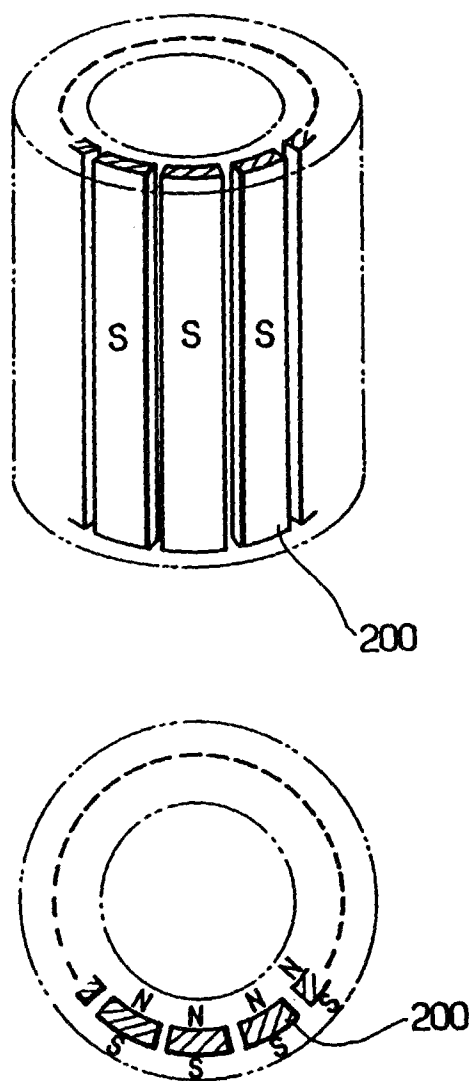


FIG. 2(D)

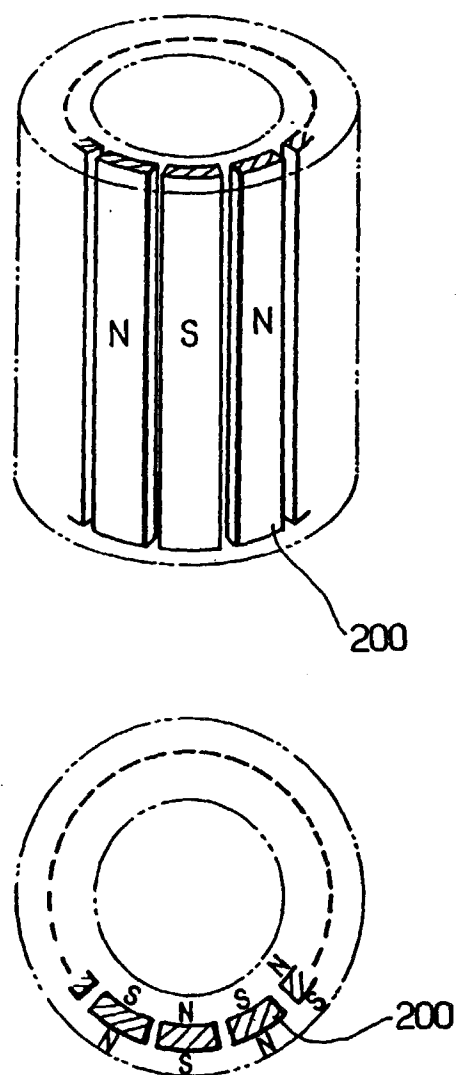


FIG. 2(E)

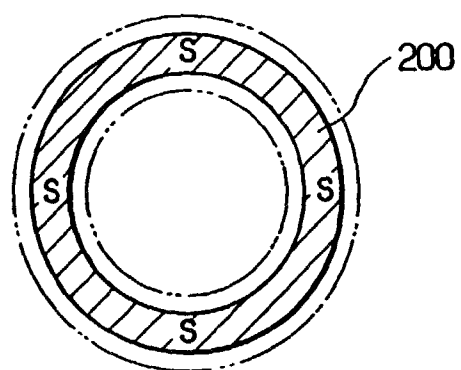
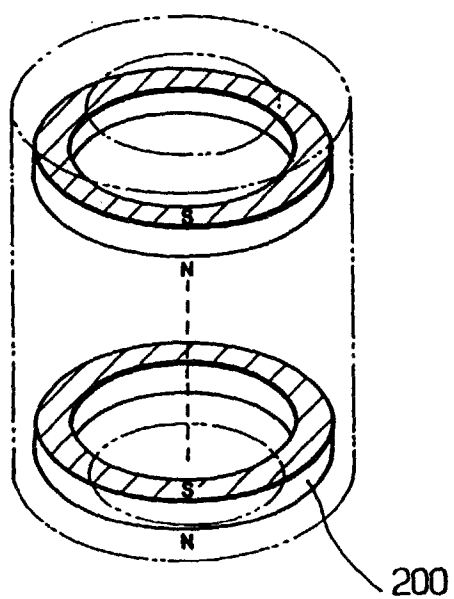


FIG. 2(F)

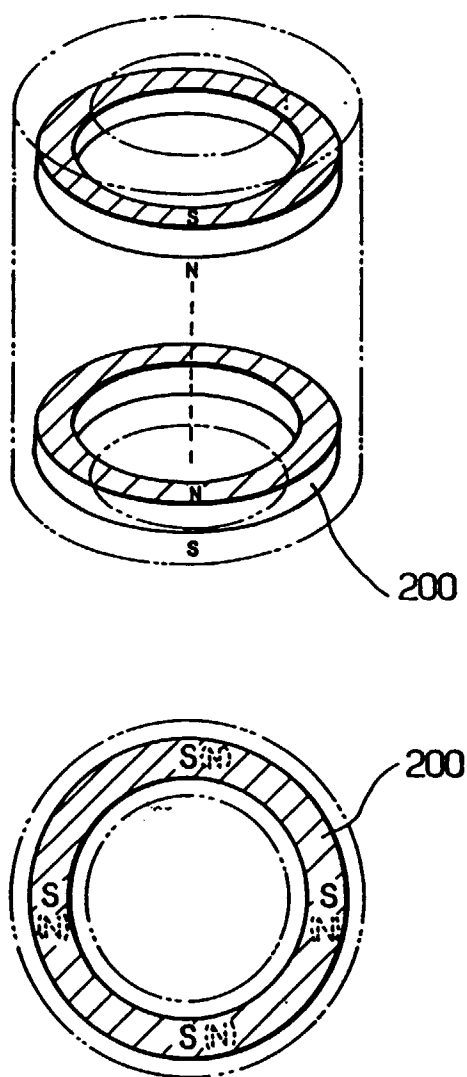


FIG. 2(G)

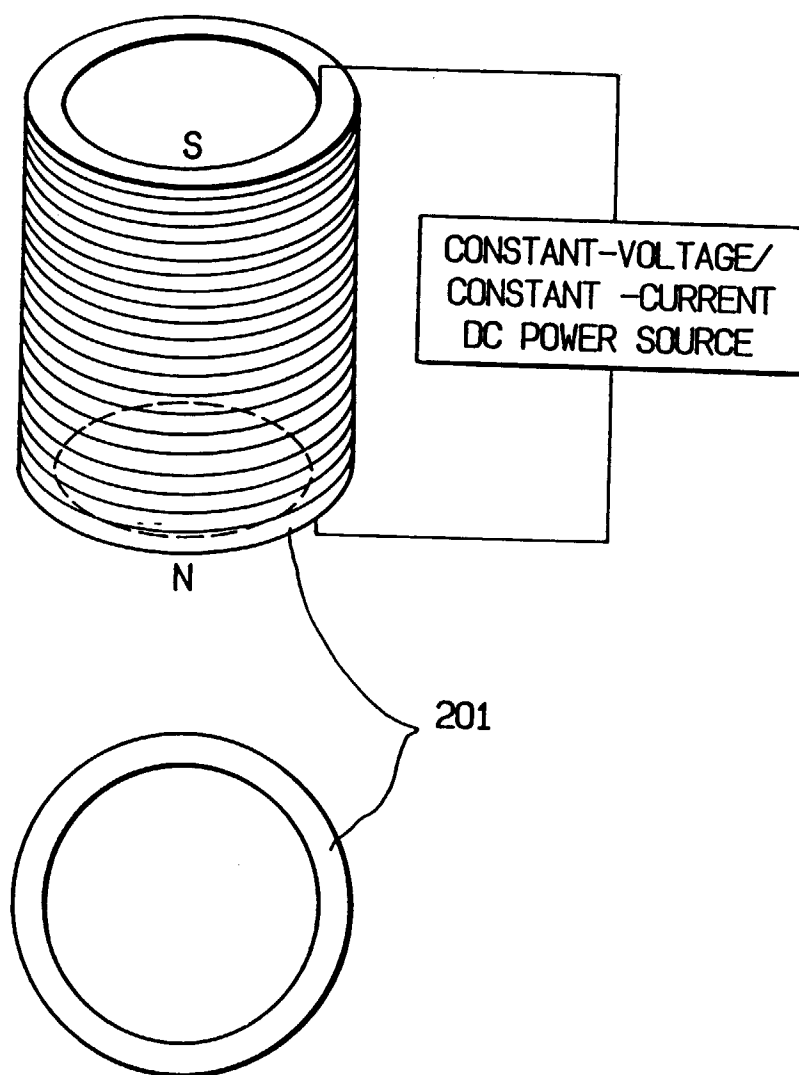


FIG. 2(H)

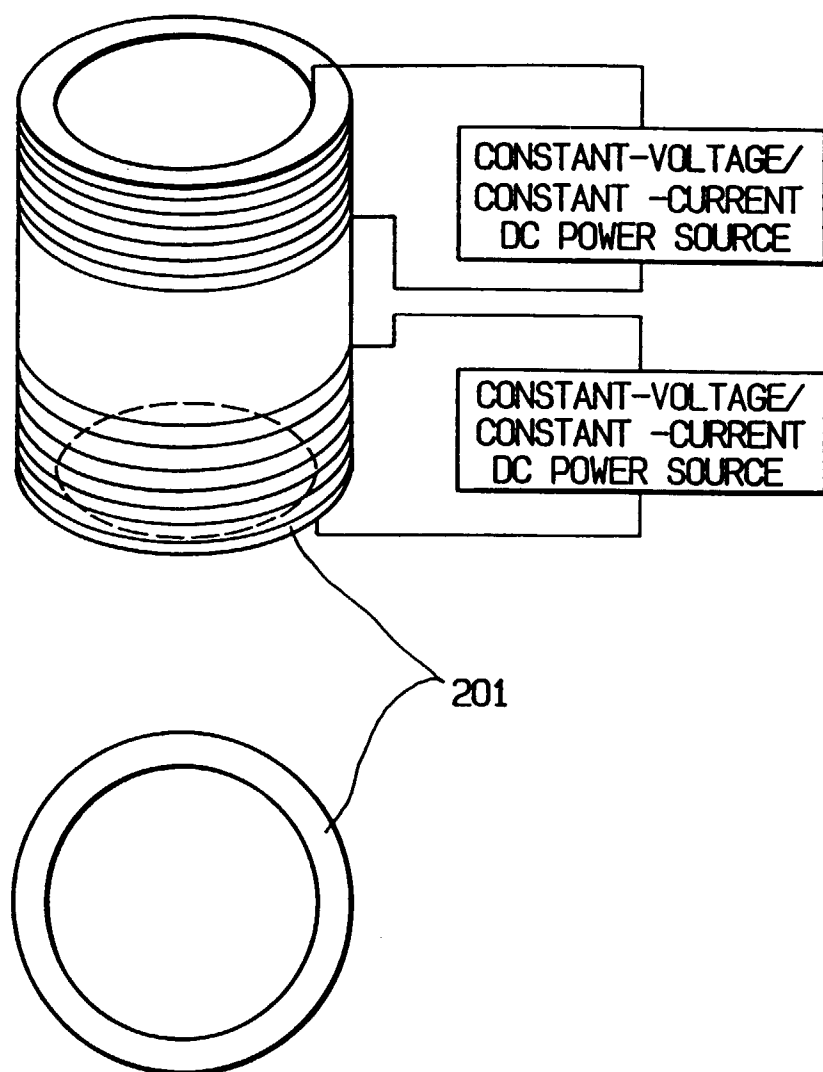


FIG. 3

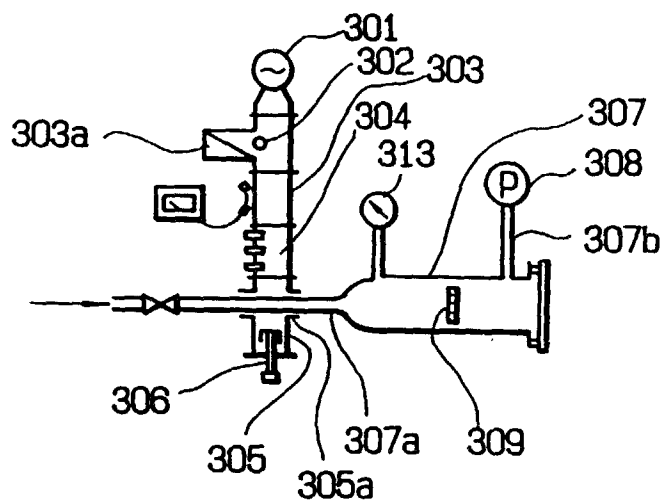


FIG. 4

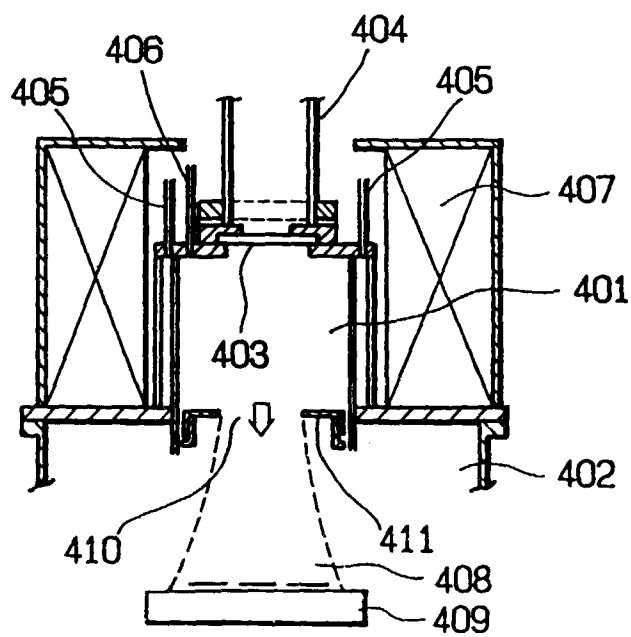


FIG. 5

