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54 **Cathode protection in aluminium-smelting cells.**

57 An method of operating an aluminium smelting cell during the start-up phase of the cell comprising forming a layer of boron oxide on the exposed surface of the cathode of the cell, forming a layer of aluminium on the boron oxide layer, said boron oxide layer forming a barrier impervious to oxygen at temperature from 400 ° C to about 650 ° C, and said aluminium layer forming a barrier to oxygen at temperatures above about 600 ° C up to temperatures of about 1000 ° C thereby reducing the development of oxidation products in the cathode during cell start-up.

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## CATHODE PROTECTION

Field of the Invention:

This invention relates to the protection of refractory hard material cathodes used in aluminium smelting cells and to aluminium smelting systems incorporating such protected cathodes.

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Background of the Invention:

In conventional designs for the Hall-Heroult cell, the molten aluminium pool or pad formed during electrolysis itself acts as part of the cathode system. The life span of the carbon lining or cathode material may average three to eight years, but may be shorter under adverse conditions. The deterioration of the carbon lining material is due to erosion and penetration of electrolyte and liquid aluminium as well as intercalation by metallic sodium, which causes swelling and deformation of the carbon blocks and ramming mix. Penetration of cryolite through the carbon body has caused heaving of the cathode blocks. Aluminium penetration to the iron cathode bars results in excessive iron content in the aluminium metal, or in more serious cases, a tap-out.

Another serious drawback of the carbon cathode is its non-wetting by aluminium, necessitating the maintenance of a substantial height of pool or pad of metal in order to ensure an effective molten aluminium contact over the cathode surface. In conventional cell designs, a deep metal pad promotes the accumulation of undissolved material (sludge or muck) which forms insulating regions on the carbon cathode surface. Another problem of maintaining such an aluminium pool is that electromagnetic forces create movements and standing waves in the molten aluminium. To avoid shorting between the metal and the anode, the anode-to-cathode distance (ACD) must be kept at a safe 4 to 6 cm in most designs. For any given cell installation there is a minimum ACD below which there is a serious loss of current efficiency, due to shorting of the metal (aluminium) pad to the anode, resulting from instability of the metal pad, combined with increased back reaction under highly stirred conditions. The electrical resistance of the inter-electrode distance traversed by the current through the electrolyte causes a voltage drop in the range of 1.4. to 2.7 volts, which represents from 30 to 60 percent of the voltage drop in a cell, and is the largest single voltage drop in a given cell.

To reduce the ACD, and associated voltage drop, extensive research using Refractory Hard Materials (RHM), such as titanium diboride ( $TiB_2$ ), as cathode materials has been carried out since the 1950's. Because titanium diboride and similar Refractory Hard Materials which are wetted by aluminium, resist the corrosive environment of a reduction cell, and are excellent electrical conductors, numerous cell designs utilising Refractory Hard Materials have been proposed in an attempt to save energy, in part by reducing anode-to-cathode distance.

The use of titanium diboride current-conducting elements in electrolytic cells for the production or refining of aluminium is described in the following exemplary U.S. patents: U.S. Pat. Nos. 2,915,442, 3,028,324, 3,215,615, 3,314,876, 3,330,756, 3,156,639, 3,274,093, and 3,400,061. Despite the rather extensive effort expended in the past, as indicated by these and other patents, and the potential advantages of the use of titanium diboride as a current-conducting element, such compositions have not been commercially adopted on any significant scale by the aluminium industry.

Lack of acceptance of  $TiB_2$  or RHM current-conducting elements of the prior art is related to their lack of stability in service in electrolytic reduction cells. It has been reported that such current-conducting elements fail after relatively short periods in service. Such failure has been associated with the penetration of the self-bonded RHM structure by the electrolyte, and/or aluminium, thereby causing critical weakening with consequent cracking and failure. It is well known that liquid phases penetrating the grain boundaries of solids can have undesirable effects. For example, RHM tiles wherein oxygen impurities tend to segregate along grain boundaries are susceptible to rapid attack by aluminium metal and/or cryolite bath. Prior art techniques to combat  $TiB_2$  tile disintegration in aluminium cells have been to use highly refined  $TiB_2$  powder to make the tile, where commercially pure  $TiB_2$  powder contains about 3000 ppm oxygen.

Moreover, fabrication further increases the cost of such tiles substantially. However, no cell utilizing  $TiB_2$  tiles is known to have operated successfully for extended periods without loss of adhesion of the tiles to the cathode, or disintegration of the tiles. Other reasons proposed for failure of RHM tiles and coatings have been the solubility of the composition in molten aluminium or molten flux, or the lack of mechanical strength and resistance to thermal shock. Additionally, different types of  $TiB_2$  coating materials, applied to

carbon substrates, have failed due to differential thermal expansion between the titanium diboride materials and the carbon cathode block or chemical attack of the binder materials. To our knowledge no prior RHM-containing materials have been successfully operated as a commercially employed cathode substrate because of thermal expansion mismatch, bonding problems, chemical erosion, etc.

5 Titanium diboride tiles of high purity and density have been tested, but they generally exhibit poor thermal shock resistance and are difficult to bond to carbon substrates employed in conventional cells. Mechanisms of debonding are believed to involve high stresses generated by the thermal expansion mismatch between the titanium diboride and carbon, as well as aluminium penetration along the interface between the tiles and the adhesive holding the tiles in place, due to wetting of the bottom surface of the tile  
10 by aluminium. In addition to debonding, disintegration of even high purity tiles may occur due to aluminium penetration of grain boundaries. These problems, coupled with the high cost of the titanium diboride tiles, have discouraged extensive commercial use of titanium diboride elements in conventional electrolytic aluminium smelting cells, and limited their use in new cell design. To overcome the deficiencies of past attempts to utilize Refractory Hard Materials as a surface element for carbon cathode blocks, coating  
15 materials comprising Refractory Hard Materials in a carbonaceous matrix have been suggested.

In U.S. Pat. Nos. 4,526,911, 4,466,996 and 4,544,469 by Boxall et al, formulations, application methods, and cells employing  $TiB_2$ /carbon cathode coating materials were disclosed. This technology relates to spreading a mixture of Refractory Hard Material and carbon solids with thermosetting carbonaceous resin on the surface of a cathode block, followed by cure and bake cycles. Improved cell operations and energy  
20 savings result from the use of this cathode coating process in conventionally designed commercial aluminium reduction cells. Plant test data indicate that the energy savings attained and the coating life are sufficient to make this technology a commercially advantageous process.

Advantages of such composite coating formulations over hot pressed RHM tiles include much lower cost, less sensitivity to thermal shock, thermal expansion compatibility with the cathode block substrate, and  
25 less brittleness. In addition, oxide impurities are not a problem and a good bond to the carbon cathode block may be formed which is unaffected by temperature fluctuations and cell shutdown and restart. Pilot plant and operating cell short term data indicate that a coating life of from four to six years or more may be anticipated, depending upon coating thickness.

The aforesaid patents both teach that the baking process should be carried out in an inert atmosphere,  
30 coke bed or similar protective environment to prevent "excessive air burn". In laboratory studies it is possible to bake the test samples in a retort which maintains a high grade inert atmosphere and excludes air/oxygen ingress, however this is not practical for commercial use. Baking under a coke bed is reported to give satisfactory protection for the  $TiB_2$ /carbon composite material.

Composite coatings have been tested in plants using full scale aluminium reduction cells (U.S. Pat. No.  
35 4,624,766; Light Metals 1984, pp 573-588; A.V. Cooke et al., "Methods of Producing  $TiB_2$ /Carbon Composites for Aluminum Cell Cathodes", Proceedings 17th Biennial Conference on Carbon, Lexington, Kentucky (1985)). After curing, the coating is quite hard and the coated blocks may be stored indefinitely until baking. For baking, the coated blocks were placed in steel containers, covered with a protective coke bed, and baked using existing plant equipment such as homogenizing furnaces. Once baked, the blocks  
40 could be handled without further precautions during cell reline procedures. The integrity of the cured coating and substrate bond remained excellent after baking. No changes in cell start-up procedure were required for using the blocks coated with composite  $TiB_2$  material. No difficulties were encountered when the coated cathode cells were started-up using either a conventional coke resistor bake or hot metal start-up procedure. Core samples from the test cells demonstrated areas of good coating condition after 109 and  
45 310 days of service in the operating cell, but performance was non-uniform.

Extensive testing of  $TiB_2$ /carbon composite materials have been performed in both laboratory and plant tests. The improved laboratory tests and more detailed cell autopsies have shown a variability in material performance not observed in previously reported tests. X-Ray Diffraction (XRD) analysis was used to measure the trace impurities in the test samples. It was discovered that the poor performance of a test  
50 material had a direct correlation with the presence of oxidation products of Ti and B such as  $TiO$  and/or  $TiBO_3$ , within the structure of the material. A similar variation was detected in the RHM coating applied to a carbon cathode.

Laboratory tests demonstrated that none of the conventional methods (e.g. coke bed, inert gas, liquid metal, boron oxide coating on anodes) for preventing/controlling carbon oxidation was adequate to prevent  
55 the formation of  $TiBO_3$  or similar oxidation products during the bake operation and/or the cell start-up.

In addition to the above described problems associated with RHM cathodes, the start-up phase of operation of conventional cells can also result in oxidation damage leading to reduced operational life, and the present invention is not therefore limited to cells have RHM cathodes.

Brief Description of Invention and Objects:

It is the primary object of the present invention to provide a method of protecting aluminium smelter cathodes against deterioration in use, and more specifically to provide an improved start-up procedure by means of which the life of aluminium smelter cell cathodes may be extended.

In its broadest form, the invention provides an improved start-up procedure for aluminium smelting cells characterized by the creation or establishment of conditions which reduce the formation of oxides from external oxidant sources in cathode materials during the start-up period of the cell. This reduction in the formation of oxides will result in cathode materials having superior longevity when compared with Refractory Hard Materials and other cathode materials which have not been similarly protected against the development of oxide products.

In one currently preferred form of the invention, the desired conditions are established in the smelting cell by the formation of a barrier which is liquid or molten during the start-up temperatures above about 400 °C, which is in intimate contact with the exposed surfaces of the cathode, which is stable and effective at temperatures up to about 1000 °C and which is substantially impervious to oxygen throughout the start-up period of the cell.

One of the major advantages of the use of a barrier which is liquid or molten is that it allows outgassing from the refractory material during the start up procedure while preventing the return of such gases or other oxidants to the cathode material. This would not be the case where say a gaseous barrier is present since the outgasses and other oxidants may readily mix with the barrier gas and will therefore be free to react with the cathode material.

The barrier may be formed of two materials, one which is effective up to one temperature and the other effective from said one temperature to temperatures up to about 1000 °C.

In one form of the invention, this is achieved by the use of boron oxide ( $B_2O_3$ ), which melts at about 450 °-470 °C or lower due to impurities, or some other suitable material which is liquid or molten at temperatures above about 400 °C, which is substantially impervious to oxygen transport and which wets carbon. This material provides a barrier which substantially prevents the Refractory Hard Materials (or other cathode materials) of the cathode from being oxide contaminated. At temperatures above about 650 °-700 °C at which the boron oxide material is likely to be less effective, aluminium pellets or the like which are added to the cell with the boron oxide and form a molten aluminium barrier which functions during start up until the cell starts producing aluminium which functions as a barrier for the remainder of the operating life of the cell. Thus, by establishing a substantially oxygen impermeable barrier which essentially prevents formation of oxides during the start-up period, the cathode of the cell is protected against subsequent damage of the type outlined above.

The boron oxide can be used directly or alternatively can be formed in situ by controlled oxidation of a  $TiB_2$  containing material such as the refractory hard material coating or a commercially available product such as Graphi-Coat.

In another aspect, the invention provides a method of reducing the development of oxidation products in Refractory Hard Material or other cathodes during the cell start-up procedure, comprising the step of adding to the cell at least one material which is liquid or molten at temperatures above about 400 °C and which is stable at temperatures up to about 1000 °C, which covers the cathode of the cell and thereby forms a barrier to oxygen, and which does not materially affect the operation of the cell.

In one preferred form, the method includes adding a first material which is liquid or molten at temperatures above about 400 °C and which is substantially impervious to oxygen transport, as well as a second material which is liquid or molten at temperatures above about 600 °C and which forms a substantially impervious barrier to oxygen transport.

While a currently preferred first material is boron oxide ( $B_2O_3$ ), other materials which are liquid or molten at about 400 °C and which form a carbon wetting film substantially impervious to oxygen at temperatures above 400 °C may be used. For example, materials such as mixtures of chloride or fluoride salts or liquid melts such as lead tin alloys may be used, although they are currently considered to be less practical than boron oxide. The boron oxide can be used directly or alternatively can be formed in situ by controlled oxidation of a  $TiB_2$  containing material such as the refractory hard material coating or a commercially available product such as Graphi-Coat (trade mark). While use of this alternative method may result in an outer skin of oxide contaminated RHM, this skin may be regarded as a sacrificial layer which an operator is willing to lose in return for a protection system which is less complex and costly to operate. The effectiveness of this alternative protection method will be dependent on the porosity of the refractory hard material with lower porosities giving better results.

Clearly the most preferable second material, for practical reasons, is aluminium metal since this is

present in the cell in any event. However, other metals or compounds, which are fluid at about 600 ° C and above, which completely cover the carbon to create a substantially impervious barrier to oxygen transport may be used.

In the post-start-up phase of operation of the cell, it may be necessary or desirable to remove the viscous boron oxide layer, or other viscous layer derived from the boron oxide coating, which adhere to the surface of the cathode. While this removal may be achieved in a number of ways, such as flushing the cell with fresh metal to physically remove the layer, it is presently preferred to remove the layer chemically by converting the boron oxide into a more innocuous boron-containing phase such as by contacting the boron oxide phase with a Ti-containing species, leading to the precipitation of TiB<sub>2</sub>. For example, Ti-bearing additions such as TiO<sub>2</sub> may be added to the electrolyte or Ti-Al alloys may be added to the metal. Other transition metal species in the fourth to sixth groups of the periodic system which are able to form borides from the boron oxide layer may also be used with acceptable results, such as Zr, Hf, V, Nb, Ta, Cr, Mo and W.

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#### Description of Preferred Embodiments:

In the following description, the conditions under which RHM material can be heated above 400 ° C without degrading its consistency and service life in an aluminium cell will be out lined in greater detail. Two types of TiB<sub>2</sub>/carbon composite materials were evaluated in laboratory and plant exposure tests to determine their uniformity and service life when used to form an aluminium wetted cathode surface for the electrolytic winning of aluminium from a molten cryolite based bath. The cathode coating material was formulated, mixed, applied to the cathode block top surface and cured as taught in U.S. Pat. No. 4,526,911 to Boxall et al. The cured coating blocks were then baked under a fluid coke bed as described by Boxall et al. A nitrogen purge was maintained through the metal box containing the coated blocks and fluid coke to prevent any ingress of air during the bake procedure. After cooling to less than 200 ° C, the baked coated blocks were removed from the coke bed. Normal cell construction procedures were used to construct a conventional pre-bake cathode using the coated blocks.

The cathode tiles were moulded, cured and baked as taught in U.S. Pat. No. 4,582,553 by Buchta. A fluid coke bed with a nitrogen purge was used to protect the tiles from "excessive air burn". The tiles were attached to the top of the cathode blocks in a conventionally rammed cathode using UCAR C-34 cement as described by Buchta.

A conventional resistor coke bed start-up procedure was used to heat the coated lined cathode cell up to about 900 ° -950 ° C before fluxing with molten bath transferred from other cells in the potline. The test cells were operated as regular cells for approximately 6 weeks before the shut down for autopsy. Most of the bath and metal were tapped from the cell during the shutdown procedure. After cooling, the remaining bath and metal were removed from the cathode surface to expose the coated tiled surface. Visual inspection and photographs of the cathode surface were used to evaluate the condition of the exposed cathode coating tiles. Core samples were taken for metallurgical and chemical analysis.

The seven day laboratory exposure test was performed in a Hollingshead cell comprising an inconel pot, a graphite crucible, a variable height graphite stirrer driven by a 60 r.p.m. geared motor and insulating lid of pyrocrete.

Test samples of TiB<sub>2</sub>/C composite were glued to the bottom of the crucible with UCAR C-34 cement and were coated with boron oxide paste. Samples were then buried in synthetic cryolite (2kg) and about 2kg of aluminium metal granules were placed on top. The temperature was raised at 40 ° /hr to 980 ° C and the stirrer was immersed so that it mixed both metal and bath. After seven days operation at 980 ° C, the graphite crucible and contents were allowed to cool and then cross sectioned to enable visual and chemical analysis of the test samples. Test results confirmed that this long term dynamic exposure test can be used to screen RHM cathode materials, glues, formulations and baking rates in the laboratory prior to their use in industrial scale cells.

The following TiB<sub>2</sub> composite failure mechanisms observed in the industrial cells were reproduced in the test cell:

- (a) delamination cracking of tiles and coatings;
- (b) complete debonding of tiles due to stresses set up by sodium swelling;
- (c) partial debonding of tiles due to chemical attack of the glue, and
- (d) deformation of tiles.

Furthermore, the dynamic exposure testing of TiB<sub>2</sub> composite materials also confirmed the following observations made during cell autopsies and laboratory investigations:

- \* glued joints between tiles and cathode block are subject to chemical attack;
- \* coating produced and baked under laboratory conditions performs much better than that produced and baked in the plant;
- \* order of rank of laboratory performance is coated anthracite block > coated MLI block > tiled anthracite block > tiled graphite block;
- \* structural integrity of the laboratory baked coatings is better than the laboratory baked tiles and much better than the plant baked coatings;
- \* the bonding interface between coating and anthracite block is at least as resistant to bath and sodium as the coating itself.

10 A large variation in coating/tile quality was found on the cathode surface of the autopsied test cells. There appeared to be a random distribution of good, poor and missing coating/tile areas over the cathode surface. The presence of well bonded undeformed areas of coating/tile demonstrated that the material could survive the aluminium cell environment provided a more consistent material could be produced.

15 No correlation between the material test results and the mixing, spreading, moulding and curing process parameters could be established to explain the variability observed in the plant tests.

It was discovered that the condition of the exposed coating/tile material was related to the presence of oxides of titanium, including mixed oxides, in the material, the oxide content being determined using known X-Ray Diffraction (XRD) analysis.

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TABLE 1

TiB <sub>2</sub> /Carbon Composite Baking Tests			
Test Sample	Protection Systems	Where Baked	Oxides of Titanium Relative XRD Peak Height
Coatings			
BN1	Coke bed	Lab	10
BN1	B <sub>2</sub> O <sub>3</sub> only	Lab	6
BN1	B <sub>2</sub> O <sub>3</sub> only	Lab	5
BN1	Al powder	Lab	10
BN1	B <sub>2</sub> O <sub>3</sub> + Al	Lab	1
BN1	Graphicoat	Lab	6
BN1	TiB <sub>2</sub> /C icing	Lab	5
BN1	B <sub>2</sub> O <sub>3</sub>	Lab	7
BN1	Graphicoat	Lab	5
BN1	TiB <sub>2</sub> /C icing	Lab	7.5
BN1-2C	Coke bed	Plant-28/5/87	4
BN1-4C	Coke bed	Plant-28/5/87	10
BN1-6C	Coke bed	Plant-28/5/87	4
BN1-7C	Coke bed	Plant-28/5/87	10
BN1-8C	Coke bed	Plant-28/5/87	24
BN1-1C	B <sub>2</sub> O <sub>3</sub> + Al	Plant-4/8/87	1
BN1-3C	B <sub>2</sub> O <sub>3</sub> + Al	Plant-4/8/87	2
BN1-6C	B <sub>2</sub> O <sub>3</sub> + Al	Plant-4/8/87	2
Pitch Bonded	Coke bed + Ar	Lab	34
Pitch Bonded	Coke bed + Ar	Lab	34
BM1	Graphi-Coat + Al	Plant Test	2
BM1	TiB <sub>2</sub> /C icing + Al	Plant Test	2
Cast Tiles			
BR7	Coke bed + Ar	Lab	6
BR7	Coke bed	Lab	8
BR7	B <sub>2</sub> O <sub>3</sub> only	Lab	5
BR7	B <sub>2</sub> O <sub>3</sub> + Al	Lab	2

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The preferred  $B_2O_3/Al$  protection system was found to provide the best results, although the use of a sacrificial layer or coating, such as Graphi-Coat or  $TiB_2/C$  icing, in lieu of the  $B_2O_3$  component also produced acceptable results.

By preventing this low level oxidation of the  $TiB_2$ , the composite structure remains intact and a long service life is maintained.

The appreciable oxidation of  $TiB_2$  evident during unprotected start-up was not anticipated since data sheets for  $TiB_2$  indicate a high resistance to air oxidation at temperatures up to  $1100^\circ C$  (ICD Group Inc., New York, NY, technical bulletin dated 10/79). Based on this data, the prior art use of a coke bed to prevent air burn of the carbon matrix and the carbon matrix itself was relied upon to provide adequate oxidations protection for the  $TiB_2$ .

The data in Table 1 show that the conventional methods for protecting carbon from air burn are inadequate and that an unexpected synergism was found when a combination of  $B_2O_3$  (or a suitable 'sacrificial' layer) plus Al was used to protect the  $TiB_2$  material.

According to one practical embodiment, the  $B_2O_3/Al$  protection system and cell start up procedure according to one embodiment is as follows:

1.  $B_2O_3$  powder is evenly distributed over the cured composite surface of the cathode. About 80 kgs was used in the 100 K ampere test cell. For difficult or vertical surfaces a  $H_3BO_3$  powder added to water to form a viscous paste is used.

2. Cover the  $B_2O_3$  with aluminium foil to protect the powder against disturbance during subsequent operation. Overlapping strips of 1200mm wide heavy duty foil has been found to be sufficient.

3. Cover the foil with aluminium "pellets". The amount should be calculated to provide at least 20mm of molten metal over the highest part of the cathode. About 4 tonnes of pellets was found sufficient for the 100 K ampere test cell.

4. Baking is carried out by directing oil fired burners between the anodes and the pellets, and heating at a rate of about  $50^\circ C/hr$ . After the aluminium has melted, the anodes can be lowered, current applied and the baking process continued.

It will be evident from the above discussion that the improved start-up procedure embodying the invention provides the following advantages over the prior art practices:

1. Provides improved protection for materials from oxidation damage at temperatures in excess of  $400^\circ C$ .

2. Provides low oxygen activity environment required to prevent oxidation of RHM and RHM containing composites when heated above  $400^\circ C$ .

3. Provides a quality control test for vendor supplied RHM composite articles (XRD analysis procedure for critical oxide impurities).

4. Improves reliability, uniformity and service life for RHM type cathodes.

5. Enables the use of RHM cathode materials which were previously unacceptable due to poor service life.

The above described start-up procedure leaves a viscous boron oxide layer, or other layer derived from the boron oxide coating, on the surface of the cathode. The continued presence of the viscous boron oxide layer prevents a sloping cathode cell from operating in its desired manner. That is, the aluminium metal is restricted from draining to the metal sump. Other operational difficulties may also occur, as described elsewhere (E.N. KARNAUKIIOV et al, Soviet Journal of Non-Ferrous Metals Research, English version Vol. 6 No. 1 1978, p. 16). Our own experience has shown that metal pooling may occur on the cathode surface, leading to uneven anode burning and/or short-circuiting, low current efficiency and general cell instability. The transition from start-up conditions to normal stable cell operation may therefore become problematic unless the boron oxide layer can be effectively removed at the end of the start-up phase. We have found that the establishment of stable operating conditions can be accomplished more efficiently by accelerating the rate of removal of the boron oxide. A number of methods have been found successful for achieving this removal. For instance, by flushing the cell with fresh metal the removal of the boron oxide has been promoted. However, the transferring of large volumes of molten metal into and out of the cell, whilst effective, is inconvenient, hazardous and undesirable.

We have discovered that the removal of boron oxide can be most conveniently facilitated by the chemical conversion in situ to a separate and more innocuous boron-containing phase that does not interfere with the draining of the cathode metal to the sump. By contacting the  $B_2O_3$  phase with a Ti-containing species, chemical interaction between Ti and B is achieved leading to the conversion of  $B_2O_3$  to  $TiB_2$  and the precipitation thereof. Importantly this chemical conversion process provides for the removal of the potentially problematic boron oxide viscous phase, which in turn allows for a rapid transition to stable and efficient drained cathode cell operation, as evidenced by normal bath temperatures and the uninter-

rupted filling of the metal sump at a rate consistent with the expected metal production rate.

Alternatively, it may be possible to use Ti in the form of an alloy of aluminium (eg. Ti-Al) to provide close contact between the B and Ti species, respectively. Ti-Al alloys are a preferred form of Ti addition since they are readily available as master alloys in the aluminium foundry industry. Furthermore, it is well known in aluminium foundry practice (eg. AU 21393/83 "Removal of Impurities from Molten Aluminium") that the removal of metal impurities from molten aluminium can be achieved in a straightforward manner by contacting molten aluminium with a boron-containing material, thus leading to the generation of insoluble metal borides (eg. (Ti, V) B<sub>2</sub>). The formation and deposition of TiB<sub>2</sub> is therefore readily accomplished. However, the use of Ti-Al alloys for the removal of viscous boron-containing layers on the cathode surface, by the chemical conversion to another phase, has not been previously demonstrated.

While the use of Ti species is preferred for the above reasons, any RHM species, such as the metals in the fourth to sixth groups of the periodic system (Ti, Zr, Hf, V, Nb, Ta, Cr, Mo and W), which can form borides from the boron oxide layer may be used with acceptable results.

In one preferred form of the process, Ti-bearing additions, or other RHM boride forming species, such as those mentioned above, may be made directly to the electrolyte. Cryolite electrolytes are good solvents for oxide ores, so a convenient form of the Ti-containing species is as TiO<sub>2</sub>, although other additives may also be employed. The Ti-containing species reacts with the B<sub>2</sub>O<sub>3</sub> to form at least a TiB<sub>2</sub> precipitate, although other equally acceptable precipitates may form.

In each of the above cases, an aluminium-RHM diboride alloy phase is formed on the cathode surface, and this may offer additional restorative and other benefits to the cathode surface.

In laboratory tests it was observed that a 1.875g addition to the bath of TiO<sub>2</sub> effectively removed a 0.975g layer of B<sub>2</sub>O<sub>3</sub> originally located at the interface between the composite and the metal (ie. no B<sub>2</sub>O<sub>3</sub> could be detected at the interface by either visual or chemical microprobe methods). The mass of TiO<sub>2</sub> was chosen to be in excess of that needed for stoichiometric conversion to TiB<sub>2</sub> to ensure that all the B<sub>2</sub>O<sub>3</sub> was removed. The mass ratio of Ti/B in TiB<sub>2</sub> is 2.218:1 and the mass ratio of Ti/B actually used was 3.71:1, which equates to a Ti mass excess of 67%. Thus a TiO<sub>2</sub>/B<sub>2</sub>O<sub>3</sub> mass ratio of 1.875/0.975 = 1.92 (ie. ≈ 2) is effective for removing the B<sub>2</sub>O<sub>3</sub> layer at the cathode surface.

The TiB<sub>2</sub> precipitate is formed as randomly distributed and irregularly shaped fine particles ranging in size from less than 1 μm to about 10 μm. These particles sometimes aggregate as clusters consisting of from 3 or 4 to 30 or 40 particles. Because of the much higher density of TiB<sub>2</sub> compared to Al (ie. 4.5g/cm<sup>3</sup> vs 2.3g/cm<sup>3</sup>) the TiB<sub>2</sub> has been observed to form a sediment on the cathode surface and may therefore provide restorative and other benefits for cathodes containing RHM, such as TiB<sub>2</sub> (eg. reduces solubility of the RHM). Similar comments apply equally to the other RHM boride forming species referred to above.

The above described post-start-up operations provide the means for enhancing the removal of a major portion of the boron oxide phase that is potentially disruptive to normal cell operation. The enhanced rate of removal facilitates the smooth transition from the start-up phase in which the boron oxide layer performs a useful protective function-to cell operation.

#### 40 Claims

1. A method of operating an aluminium smelting cell having a cathode surface during the start-up phase of the cell, comprising the steps of forming on said cathode surface of the cell a barrier which is liquid or molten during start-up temperatures above about 400° C, which is in intimate contact with the exposed surfaces of the cathode, which is stable and effective at temperatures up to about 1000° C and which is substantially impervious to oxygen throughout the start-up phase of the cell.

2. The method of claim 1, wherein said barrier comprised a layer of boron oxide applied to the cathode and a layer of aluminium, said boron oxide forming a molten layer substantially impervious to oxygen at temperatures substantially falling in the range 400° C to about 650° C to 700° C, said aluminium layer forming a molten layer over the cathode surface at temperatures above about 600° C and which substantially excludes oxygen at temperatures up to about 1000° C.

3. A method of reducing the development of oxidation products in cathodes during the cell start-up procedure, comprising the step of adding to the cell at least one material which is liquid or molten at temperatures above about 400° C and which is stable at temperatures up to about 1000° C, which covers the cathode of the cell and thereby forms a barrier to oxygen, and which does not materially affect the operation of the cell.

4. The method of claim 3, comprising the steps of adding a first material which is molten or liquid at temperatures in excess of about 400° C and which is stable and substantially impervious to oxygen at



temperatures up to about 650 °C and a second material which is molten at temperatures above about 600 °C and which wets the cathode and is stable and substantially impervious to oxygen at temperatures up to about 1000 °C.

5 5. The method of claim 4, wherein the first material is boron oxide and the second material is aluminium.

6. A method of removing boron oxide derived substances from an aluminium smelting cell following the method of claim 2 or 5, comprising the step of contacting the boron oxide derived substance with a phase which causes conversion of the boron oxide derived substance and substantial removal of the boron oxide derived substance from the cell.

10 7. The method of claim 6 comprising the step of adding an RHM boride forming species to the cell in quantities sufficient to cause precipitation of an RHM diboride aluminium alloy.

8. The method of claim 7, wherein the species is selected from the transition metals Ti, Zr, Hf, V, Nb, Ta, Cr, Mo and W.

9. The method of claim 8, wherein the species is added to the electrolyte.

15 10. The method of claim 9, wherein the species is in the form of an oxide.

11. The method of claim 7, wherein the species is added to the melt in the form of a RHM boride forming species.

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DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	CHEMICAL ABSTRACTS, vol. 89, no. 22, November 1978, page 518, abstract no. 188073r, Columbus, Ohio, US; & US-A-621 805 (A.E. BAZHENOV et al.) 30-08-1978 ---	1	C 25 C 3/06
A	SU-A-1 331 906 (BRATSKII ALUMINIEVII ZAVOD) * Column 1, lines 20-29; columns 5,6; claims * -----	1,7,8, 10	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			C 25 C 3
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 31-05-1990	Examiner GROSEILLER PH. A.
<b>CATEGORY OF CITED DOCUMENTS</b> X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ..... & : member of the same patent family, corresponding document	