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## 54) Press section of a paper or board machine.

The invention concerns a press section of a paper or board machine, comprising a number of rolls (1,11,22,32,44,70) which form press nips  $(N_1,N_2,N_3,N_4)$  that dewater the web (in) with each other, the web being arranged to run through said nips. Of the rolls at least one roll (1;70) is a smooth-faced so-called centre roll, which forms a press nip  $(N_2,N_3;N_4)$  with at least one other press roll (11,32;44), over which a press felt (10,30;40), which has been formed as an endless loop, is passed to absorb water out of the web (in) into said press felt

(10,30;40). The centre roll (1;70) in accordance with the invention is a variable-crown roll, which comprises a metallic roll mantle (2;71) arranged revolving on a stationary roll axle (3;72). The roll includes at least one set of crown-variation means (4,5;73), which are arranged to load the roll mantle (2;71) in the direction of the nip plane ( $K_2,K_3;K_4$ ) of the centre roll (1;70) and the roll (11,32;44) that forms a press nip ( $N_2,N_3;N_4$ ) with said centre roll so as to regulate the profile of linear load in said nip ( $N_2,N_3;N_4$ ).



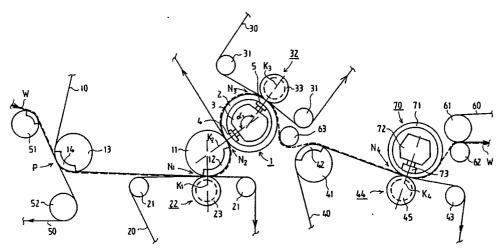


FIG. 1

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The invention concerns a press section of a paper or board machine, comprising a number of rolls which form press nips that dewater the web with each other, the web being arranged to run through said nips, and of which said rolls at least one roll is a smooth-faced so-called centre roll, which forms a press nip with at least one other press roll, over which a press felt, which has been formed as an endless loop, is passed to absorb water out of the web into said press felt.

In a paper machine, out of fibre pulp, a web is formed in the former of the paper machine, whereupon the formed web is passed, being supported and carried by the felts in the paper machine, into the press section of the paper machine, wherein both the web and the felts that support it are passed through nips formed by the rolls in the press section to absorb water out of the web into the felts. From the press section the web is passed further into the drying section of the paper machine. A conventional solution in a press section comprises a large and massive centre roll as well as wire or felt loops grouped around it, the rolls placed inside said loops forming press nips either with one another or together with the centre roll, and when the web runs through said press nips, water is drained out of the web by the effect of compression, said water being absorbed into the felts. In the drying section, water is removed out of the web by means of evaporation, which is highly energy-consuming and therefore expensive and uneconomical. This is why attempts are made to remove a maximal proportion of water out of the web before the drying section, in the press section, by mechanical means. It is known in prior art that water is removed out of the web considerably more readily at a raised temperature, because the viscosity of water and the springback coefficient of the web are thereby lowered together with the surface tension. Owing to this, it has been possible already to raise the temperature of the web in the press section. Based on earlier experience, it can be established that, e.g., an increase in thetemperature by 6...10°C in the press section produces an increase of an order of 1 or more in the dry solids content of the web. An increased dry solids content in the press section produces considerable economies of costs. For example, in paper machines it can be considered a rough rule that, if the moisture content in the web in the press section can be lowered by 1 %, the consumption of steam in the drying section is lowered by about 5 %.

One drawback, which has been recognized for quite a long time, in the press sections which are used commonly to-day consists of the centre roll in the press section, as whose material, as a rule, some suitable rock, such as granite, is used. As is well known, rock rolls are quite sensitive to large

and sudden changes in temperature, and the effects of such changes may be quite fatal. This is why attempts have been made to develop suitable substitutes for granite rolls. As substitutes for rock rolls, e.g., such metal rolls have been used as are coated, e.g., with a mixture of polyurethane and rock dust to make the surface properties of the roll similar to those of a rock roll. Advantages of metal rolls compared with rock rolls include their considerably better ability to tolerate variations in temperature. Moreover, owing to this, they can be run as considerably hotter than rock rolls. Moreover, a metal roll tolerates considerably higher running speeds than rock rolls do.

A conventional construction in the press section of a paper machine wherein a centre roll and press rolls grouped around it are employed constitutes three press nips. In such a construction, the first press nip is formed between a grooved roll and a press-suction roll. On the other hand, the second press nips is formed between a presssuction roll and the centre roll, and the third press nip is formed between the centre roll and a second grooved roll. Since, in the nips in the press section, it must be possible to make the linear loads as uniform as possible, in such a solution, as a rule, said grooved rolls have been formed as variablecrown rolls, preferably as rolls adjustable in zones. Thus, owing to the crown variation of the grooved rolls, in the first nip and in the third nip in the press section, a uniform linear load is achieved. In order that a linear load as uniform as possible could also be obtained for the second press nip, the mantles of the press-suction roll and the centre roll, which form the second press nip, are, as a rule, cam bered. By means of the camber, a uniform linear load is, however, never obtained for a nip and, moreover, it is a further drawback of the cambering that the camber is always "fixed". If the camber has to be changed, the roll must always be ground. This is again quite a costly and laborious operation. Since cambering alone does not bring the profile of linear load under full control, for example, a problem of the metallic centre rolls in use at present has been uneven heating. This has caused distortions of the profile of linear load. Since the grooved rolls are provided with crown-variation means, the grooved rolls have been highly expensive. In this respect, the high cost has also been contributed to by the fact that it has been difficult to fit the crownvariation means inside a grooved roll, because the diameters of the grooved rolls are relatively small. If a fourth, separate press has been added to such a press section, in this press a variable-crown grooved roll has also been used.

Thus, as a summary of the drawbacks related to prior art, it is possible to mention the high cost of the construction, the problems of temperature

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related to the construction, as well as the difficulties in providing uniform and, if necessary, adjustable profiles of linear loads.

The object of the present invention is to provide a press section by means of which the drawbacks described above are minimized and by means of which an essential improvement is obtained in respect of increased dry solids content and increased running speed. A further object is to provide a construction to substitute for the rock rolls employed in presses. In view of achieving these objectives, the solution in accordance with the invention is mainly characterized in that the centre roll is a variable-crown roll, which comprises a metallic roll mantle arranged revolving on a stationary roll axle as well as at least one set of crown-variation means, which are arranged to load the roll mantle in the direction of the nip plane of the centre roll and the roll that forms a press nip with said centre roll so asto regulate the profile of linear load in said nip.

Compared with prior art, by means of the invention, a number of advantages are obtained, which were partly already discussed above. Of the differences, for example, the following should be mentioned additionally. With the use of the solution in accordance with the invention, if necessary, two variable-crown rolls can be substituted for by one variable-crown roll. This results in considerable economies. Since the crown-variation means are used expressly in connection with the centre roll, it is considerably easier to construct these means in the interior of the roll, because the available space is larger. With the use of the present invention, if desirable, it is also possible to control the profile of linear loads in the nip between a press-suction roll and the centre roll.

Moreover, by means of the solution in accordance with the invention, those problems are avoided that are related to the uneven heating of the prior-art metallic centre rolls. When a solution in accordance with the invention is used, the mantle of the centre roll can be made thinner than in prior art, whereby it has an improved thermal conductivity. If desired, the roll can also be used for heating the web. Nor is it necessary to grind any camber on a roll in accordance with the invention. An additional advantage obtainable by means of the invention is related to the construction of the grooved rolls that are used to-day. Currently, the grooved rolls are made so that they are provided with a suitable coating, e.g. of polyurethane. It results from this that they have a limited ability to tolerate heat. Variable-crown rolls, and in particular rolls adjustable in zones, however, develop a considerable amount of heat. Since, when a solution in accordance with the invention is used, the grooved rolls do not have to be variable-crown rolls, if

necessary, they can be provided with cooling in a simple way. As a further, additional advantage can be stated that the invention can be applied as such as an after-installation to existing presses. The further advantages and characteristic features of the invention come out from the following detailed description of the invention.

In the following, the invention will be described in detail with reference to the figures in the accompanying drawing.

Figure 1 is a schematical side view of the press section of a paper or board machine wherein a solution of the invention is applied.

Figure 2 is a corresponding view of an embodiment alternative of the solution shown in Fig. 1.

Figure 3 is a corresponding view of a further embodiment alternative of the solutions shown in Figs. 1 and 2.

Figure 4 shows a further alternative embodiment of the solution in accordance with the invention.

As is shown in Figs. 1,2 and 3, the web W in is formed on the wire 50, which is either a fourdrinier wire or the carrying wire of a twin-wire former. On the downwards inclined run of the wire 50 between the wire suction roll 51 and the wire draw roll 52, the web in is transferred on the detaching line P on the suction zone 14 of the pick-up roll 13 onto the first press felt 10, which, thus, also acts as the pick-up felt. The first press felt 10 carries the web in on its lower face into the first press nip N<sub>1</sub>, which is formed between two press rolls, i.e. a press-suction roll 11 and a grooved roll 22 or an equivalent roll provided with a hollow face 23. The first press felt 10 forms an endless loop by means of guide and alignment rolls (not shown), which also keep said first press felt 10 appropriately tensioned. The first nip N<sub>1</sub> is provided with two press felts, i.e. said first press felt 10 and a second press felt 20, the latter felt also forming an endless loop by means of guide and alignment rolls 21, which keep said second press felt 20 appropriately tensioned. The nip plane of the first nip  $N_1$  is denoted with the reference denotation K<sub>1</sub>.

After the first nip  $N_1$  the web in is sucked by means of the suction zone 12 of the press-suction roll 11 out of contact with the second press felt 20 onto the face of the first press felt 10 and, being guided by the press-suction roll 11, into the second nip  $N_2$ . For this purpose, a so-called pick-up felt is used as said first press felt, and the press-suction roll is provided with a suction zone 12 of appropriate length, which ensures the detaching of the web in from the second press felt 20 onto the face of the first press felt 10. The second nip  $N_2$  is formed between the press-suction roll 11 and the centre roll 1 in the press section. After the second nip  $N_2$ , said first press felt 10 is passed away from

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the centre roll 1. Owing to the surface properties of the centre roll 1 (smooth-faced roll), the web in is detached after the second nip  $N_2$  from the first press felt and adheres to the face of said centre roll, under whose guidance the web in is hereupon transferred into the third nip  $N_3$  in the press section. The third nip  $N_3$  is formed between the centre roll 1 and an opposite grooved roll 32 or an equivalent roll provided with a hollow face 33. Over said grooved roll 32, a third press felt 30 is passed, which is formed as an endless loop by means of guide and alignment rolls 31.

In the embodiments shown in Figs. 1,2 and 3, the press section further includes a fourth, separate press, in which case the fourth nip N4 in the press is formed between a second centre roll 70, corresponding to the centre roll 1, and an opposite grooved roll 44 or an equivalent roll provided with a hollow face 45. After the third nip N<sub>3</sub> the web in is detached from the third press felt 30 onto the face of the centre roll 1, from which it is detached by means of a transfer-suction roll 63. Thus, an open draw is formed between the centre roll 1 and said transfer-suction roll 63. From the transfer-suction roll 63 the web in is transferred onto the fourth press felt 40 on the suction zone 42 of the suction roll 41, which acts as a pick-up roll. Between the transfer-suction roll 63 and the suction roll 41, there is also an open draw. The fourth press felt 40 is also a so-called pick-up felt. The fourth press felt 40 is formed as an endless loop by. means of guide and alignment rolls 43. Said fourth press felt 40 transfers the web in into the fourth press nip N4, after which, owing to the surface properties of the second centre roll 70, the web in is detached from the fourth press felt 40 onto the face of the second centre roll 70. The nip plane of the fourth nip N4 is denoted with the reference denotation K4. From the second centre roll 70, the web in is transferred onto the drying wire 60 by means of transfersuction rolls 61 and 62, while the drying wire 60 transfers the web in further into the drying section (not shown).

Fig. 1 shows a first preferred embodiment of a press section in accordance with the invention. As is shown in Fig. 1, the centre roll 1 in the press section is a variable-crown roll, which comprises a metallic roll mantle 2 which is arranged as revolving on a stationary roll axle 3. In the embodiment shown in Fig. 1, inside the centre roll 1, crownvariation means 4 and 5 are. fitted which act in the nip plane  $K_2$  of the second nip  $N_2$  as well as in the nip plane  $K_3$  of the third nip  $N_3$ , by means of which said means the roll mantle 2 is loaded in said nip planes  $K_2$  and  $K_3$  to produce the desired profile of linear load. In the embodiment of Fig. 1, said crown-variation means comprise loading shoes supported on the roll axle 3 and acting upon the

inner face of the roll mantle 2. Thus, in the embodiment of Fig. 1, the centre roll 1 is a roll adjustable in zones, wherein the crown variation is provided in two directions, which form an angle a with each other. Thus, in the embodiment shown in Fig. 1, regulation of the profile of linear loads is accomplished both in the second and in the third nip No and N<sub>3</sub> in the press section. Since, in the centre roll in accordance with Fig. 1, there are two directions of crown variation, as the crown-variation means 4 and 5 it is necessary to employ exactly the above loading-shoe constructions. If crown variation were provided in the centre roll 1 in one direction only, either in the nip plane K2 of the second nip  $N_2$  or in the nip plane  $K_3$  of the third nip N<sub>3</sub>, in this direction it would be possible to employ any crown-variation means accomplished by means of the present-day technique as the crown-variation means. In Fig. 1 this has not been shown, but, if necessary, it would also be possible to provide crown-variation means in the grooved roll 22, in which case the profile of linear loads could also be brought under control in the first part  $N_1$  of the press section.

As was already mentioned in the description above, the press section shown in Fig. 1 also includes a fourth press nip N4 constituted by a separate press. Thus, in the embodiment of Fig. 1, the second centre roll 70 is arranged as a variablecrown roll, so that the second centre roll 70 comprises a hollow, metallic roll mantle 71, which is arranged revolving on a stationary roll axle 72. In the interior of the roll mantle 71, crown-variation means 73 are provided, by whose means the fourth nip N<sub>4</sub> is loaded in the direction of the nip plane k4 to produce the desired profile of linear loads. In Fig. 1 it is shown that in the second centre roll 70, as the crown-variation means 73, a loading-shoe construction similar to that described above, in relation to the centre roll 1 is used. However, since in the fourth, separate press it is necessary to control one regulation direction only, as the crownvariation means 73 it is possible to use any construction whatsoever that can be accomplished by means of the present-day technique. Thus, if necessary, in the embodiment shown in Fig. 1, it is possible to bring the profiles of linear load under control in all the press nips in the press section.

The second embodiment of the invention shown in Fig. 2 differs from that shown in Fig. 1 in the respect that, in the centre roll 1, crown-variation means 4 are provided in the nip plane  $K_2$  of the second nip  $N_2$  only. Owing to this, in the embodiment shown in Fig. 2, as crown-variation means 4 it is possible to use any construction whatsoever that can be accomplished by means of the present-day technique. In Fig. 2, it is shown additionally that in this embodiment the profile of linear loads is also

regulated in the first nip  $N_1$  in the direction of the nip plane  $K_1$  so that the grooved roll 22 is formed as a variable-crown roll. Thus, the grooved roll 22 comprises a tubular roll mantle 24, which is mounted as revolving on the stationary roll axle 25. Inside the roll mantle 24, the necessary crown-variation means 26 are provided to regulate the profile of linear loads in the nip  $N_1$ . Since herein one direction of regulation only is concerned, as crown-variation means it is possible to use any regulation means that can be accomplished, e.g., by means of the present-day technique.

In view of regulating the profile of linear loads also in the third nip N<sub>3</sub> in the press section, in the embodiment shown in Fig. 2, the grooved roll 32 in said third nip N<sub>3</sub> is formed as a variable-crown roll, whose construction corresponds to that of the grooved roll 22 in the first nip N<sub>1</sub> described above. Thus, the grooved roll 32 comprises a tubular roll mantle 34, which is arranged revolving on the roll axle 35. Further, inside the roll mantle 34, crownvariation means 36 are provided, which act in the nip plane K<sub>3</sub> of the third nip N<sub>3</sub> to regulate the profile of linear loads. Since, in this case as well, regulation is required in one direction only, the crown-variation means 36 can be accomplished in any desired way. As the crown-variation means 36. it is possible to employ, for example, the loading shoes shown in Fig. 2, but in their place it is also possible to use, for example, a chamber of pressure fluid or a series of chambers provided between the roll axle 35 and the roll mantle 34. In the fourth, separate nip N<sub>4</sub> in the press section, in the embodiment shown in Fig. 2, the regulation of the profile of linear loads is arranged in a way differing from Fig. 1. In the embodiment shown in Fig. 2, the grooved roll 44 in the fourth nip N4 is arranged as a variable-crown roll so that the roll 44 comprises a tubular roll mantle 46, which is arranged revolving on the axle 47 of the roll mantle. Inside the roll mantle 46, crown-variation means 48 similar to those described above in connection with the crown-variation means 26 and 36 of the grooved rolls 22 and 32 in the first nip N1 and in the third nip N<sub>3</sub> are provided. Thus, in this embodiment, in the fourth nip N<sub>41</sub> it is possible to employ a fully conventional metal roll or even a rock roll as the centre roll 70.

The third embodiment of the invention, shown in Fig. 3, is in a way a combination of the embodiments shown in Figs. 1 and 2. In the solution shown in Fig. 3, the regulations of the profiles of linear loads in the first, second and third nip  $N_1,N_2,N_3$  in the press section are accomplished in the same ways as in the solution shown in Fig. 2, and in the fourth nip  $N_4$  in the same way as is shown in Fig. 1. Thus, in respect of the embodiment shown in Fig. 3, reference is made to the

description given above.

The embodiment shown in Fig. 4 differs from the above embodiments as follows. In respect of the first nip N<sub>1</sub> in the press section, the solution is similar to that described in the above embodiments. On the contrary, in Fig. 4, the second nip N<sub>2</sub> in the press section is not formed between the press-suction roll 11 and the centre roll 1, but in this embodiment, on the run of the first press felt 10 after the press-suction roll 11, a grooved roll 15 or an equivalent roll provided with a hollow face 16 is provided, which forms the second nip N2 in the press section with the centre roll 1. The first press felt 10 is formed as an endless loop, as is the case in the above embodiments, by means of guide and alignment rolls 17. In the embodiment of Fig. 4, the construction and the operation of the centre roll 1 are identical with that shown in Fig. 1. The grooved roll 32 in the third nip N<sub>3</sub> and the related constructions are also, in this embodiment, identical with those shown in Fig. 1. In the solution of Fig. 4, a fourth, separate press is not shown at all, but in this solution the web in can be transferred by means of the transfer-suction roll 63 directly onto the drying wire (not shown). It is, however, fully obvious that this embodiment may also be provided with a fourth, separate press similar to that described in relation to the embodiments described above. In a corresponding way, it is fully obvious that the embodiments of Figs. 1,2 and 3 may also be accomplished without a fourth, separate press.

Above, the invention has been described by way of example with reference to the exemplifying embodiments shown in the figures in the accompanying drawing. This is, however, not supposed to confine the invention to the examples given only, but many variations are possible within the scope of the inventive idea defined in the accompanying patent claims.

## **Claims**

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1. Press section of a paper or board machine, comprising a number of rolls (1,11,15,22,32,44,70) which form press nips  $(N_1,N_2,N_3,N_4)$  that dewater the web (in) with each other, the web being arranged to run through said nips, and of which said rolls at least one roll (1;70) is a smooth-faced so-called centre roll, which forms a press nip  $(N_2,N_3;N_4)$  with at least one other press roll (11,15,32;44), over which a press felt (10,30;40), which has been formed as an endless loop, is passed to absorb water out of the web (in) into said press felt (10,30;40), characterized in that the centre roll (1;70) is a variable-crown roll, which comprises a metallic roll mantle (2;71) arranged revolving on a stationary roll axle (3;72) as well as at

least one set of crown-variation means (4,5;73), which are arranged to load the roll mantle (2;71) in the direction of the nip plane  $(K_2,K_3;K_4)$  of the centre roll (1;70) and the roll (11,15,32;44) that forms a press nip  $(N_2,N_3;N_4)$  with said centre roll so as to regulate the profile of linear load in said nip  $(N_2,N_3;N_4)$ .

- 2. Press section as claimed in claim 1, **characterized** in that the crown-variation means (4;73) in the centre roll (1;70) comprise a chamber of pressure fluid or a series of chambers, which is in itself known and which is fitted between the roll mantle (2;71) and the roll axle (3;72).
- 3. Press section as claimed in claim 1, wherein the centre roll (1) forms press nips  $(N_2,N_3)$  with two other press rolls (11 or 15,32), **characterized** in that, in the centre roll (1), crown-variation means (4,5) are provided to load the roll mantle (2) in the directions of the nip planes  $(K_2,K_3)$  of both of the nips  $(N_2,N_3)$  so as to regulate the profiles of linear loads in both nips  $(N_2,N_3)$ .
- 4. Press section as claimed in claim 3, **characterized** in that the nip planes  $(K_2,K_3)$  form an angle  $\alpha$  with each other, which angle is different from 180°.
- 5. Press section as claimed in claim 3 or 4, characterized in that the crown-variation means (4,5) comprise loading-shoe constructions which are known in themselves, which are supported on the axle of the roll, and which act upon the inner face of the roll mantle (2).

