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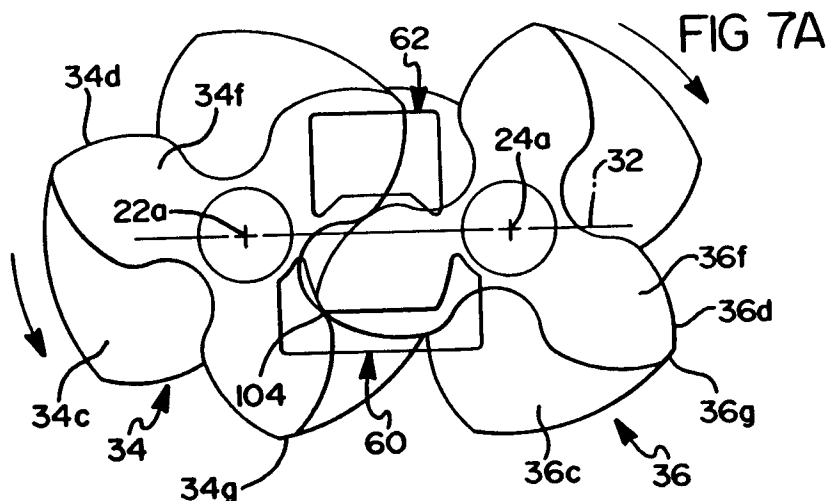
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(54) **Supercharger carry-over venting means.**

(57) A rotary positive displacement blower (10) of the Roots-type having inlet and outlet vents recess (60,62) for reducing fluid pressure build up in spaces

between meshing, helical lobes (34a,36a) on rotating rotors of the blower.

**EP 0 519 276 A1**

Field of the Invention

This invention relates to rotary compressors or pumps, particularly to pumps of the backflow type. More specifically, the present invention relates to improving efficiency and reducing airborne noise associated with compression of volumes of air trapped between meshing teeth or lobes of Roots-type blowers employed as superchargers for internal combustion engines.

Background of the Invention

As is known, Roots-type blowers are similar to gear pumps in that both employ toothed or lobed rotors meshingly disposed in transversely overlapping cylindrical chambers. Adjacent nonmeshing lobes of each rotor transfer volumes of inlet port fluid to the outlet port. When the lobes remesh, outlet port fluid is trapped in contracting spaces between the meshing lobes and compressed unless venting is provided. When the rotor lobes are straight, i.e., parallel to the rotor axis, outlet vents have been provided for returning a portion of the trapped fluid to the outlet port and inlet vents have been provided for returning the remainder of the trapped fluid to the inlet port. However, when helical lobes are employed, known outlet vents have not been provided since such outlet vents would provide a leak path from the outlet port to the inlet port via expanding spaces between the meshing lobes. Examples of gear pumps with outlet and inlet vents may be seen by reference to U.S. Patents 3,113,524; 3,303,792; and 4,130,383, which are incorporated herein by reference. Examples of Roots-type blowers with helical lobes and inlet vents may be seen by reference to U.S. Patent 4,556,373 and 4,569,646, which are incorporated herein by reference.

Summary of the Invention

An object of the present invention is to provide inlet and outlet vents for trapped volumes between meshing teeth of a backflow blower having helical lobes.

According to an object of the present invention, a rotary pump of the backflow type with helical lobes, as disclosed in U.S. 4,556,373, is provided with vent means for relieving pressure build-up in trapped volumes between meshing lobes of the rotors.

The vent means are characterized by inlet and outlet recesses formed in an end wall surface sealingly related with rotor and lobe end surfaces at trailing ends of the lobes. The outlet and inlet recess means are respectively disposed on opposite sides of a plane defined by axes of the

rotors. The outlet recess means communicates the fluid in the trapped volumes to the pump outlet and the inlet recess means communicates the fluid in the trapped volumes to the pump inlet. The outlet recess means includes first and second recess fingers in continuous communication with the outlet fluid. The first and second recess fingers are disposed such that contracting trapped volumes defined by contracting spaces between the meshing lobes move from positions communicating with the associated recess finger to positions sealed from such communication while expanding spaces between the meshing lobes are sealed from such communication with the associated recess finger. Thereafter, the trapped volumes move from positions sealed from communication with the inlet recess means to positions communicating therewith as the trapped volume move to positions sealed from communication with the associated recess fingers of the outlet vent means.

Brief Description of the Drawings

A Roots-type blower intended for use as a supercharger is illustrated in the accompanying drawings in which:

Figures 1-3 are relief views of the Roots-type blower with Figure 1 being a top view, Figure 2 being a bottom view and Figure 3 being a side view;

Figure 4 is a longitudinal cross-sectional view of a housing member in Figures 1-3 looking along line 4-4 in Figure 1;

Figure 5 is a cross-sectional view of the blower looking along line 5-5 in Figure 3;

Figure 6 is a relief view of one blower rotor in free space;

Figures 7A-7G illustrate seven meshing positions of the blower rotors in free space;

Figure 8 is a cross-sectional view of the blower looking along line 6-6 of Figure 3; and

Figures 9-12 illustrate two alternative embodiments of features in Figures 7A-7G and 8.

Detailed Description of the Drawings

The drawing figures illustrate a rotary pump or blower 10 of the Roots-type. Such blowers are used almost exclusively to pump or transfer volumes of compressible fluid, such as air, from an inlet port opening to an outlet port opening without compressing the air in the transfer volumes prior to exposure to higher pressure air at the outlet port opening. The rotors operate somewhat like gear-type pumps, i.e., as the rotor teeth or lobes move out of mesh, air flows into volumes or spaces defined by adjacent lobes on each rotor. The air in the volumes is then trapped between the adjacent

unmeshed lobes as the rear lobe thereof moves into a sealing relation with the wall surfaces of the chambers. The volumes of air are transferred or directly exposed to air at the outlet port opening when the front lobe of each transfer volume traverses the boundaries of the outlet port opening or boundaries of passages for preflowing or backflowing outlet port air at a controlled rate into the upcoming transfer volume.

Blower 10 comprises a housing assembly 12 including a main housing member 14, a bearing plate member 16, and a drive housing member 18. The three members are secured together by a plurality of screws 20. The main housing member 14 is an unitary member defining cylindrical wall surfaces 14a,14b and a flat end surface 14c of an end wall 14d of first and second transversely overlapping cylindrical chambers 22,24. Member 14 also defines an outlet port opening 26, an inlet port opening 28 in end wall 14d, a main inlet duct 30, and a bypass duct 31.

The other end wall of chambers 22,24 is defined by a flat surface 16a of bearing plate member 16. Chambers 22,24 respectively have parallel, longitudinal axes 22a,24a lying in a common plane 32. With reference to position in the drawings, the upper part of wall surfaces 14a,14b intersect to define a cusp 14e extending parallel to the chamber axes. As disclosed herein, the lower part of the surfaces 14a,14b do not actually intersect and are joined by a plane 33 parallel to plane 32. Chambers 22,24 respectively have rotors 34,36 mounted therein for counter rotation on shafts 38,40 having axes substantially coincident with the respective chamber axes. Shafts 38,40 are mounted at their opposite ends in known and unshown manner in antifriction bearings supported by bearing plate 16 and end wall 14d. The rotors are driven in the direction of arrows A and B by a drive pulley 41 fixed to a drive shaft which in turn drives unshown timing gears affixed to the rotor shafts. Details of mounting and driving the rotors, which form no part of the invention herein, may be obtained by reference to U.S. Patent Numbers 4,595,349; 4,828,467; and 4,844,044, all of which are incorporated herein by reference.

Rotors 34,36 respectively include three lobes 34a,36a of modified involute profile having an end-to-end helical twist of 60 rotational degrees. The lobes are circumferentially spaced apart by bottom lands or root surfaces 34b,36b at the lobe roots or radially inner extents. Each lobe includes fore-and-aft flank surfaces 34c,36c and 34d,36d respectively facing in the direction of rotor rotation, oppositely facing end surfaces 34e,34f and 36e,36f which sealingly cooperate with end wall surfaces 14c,16a, and top lands or outer surfaces 34g,36g which sealingly cooperate with the cylindrical wall sur-

faces 14a,14b of the respective chamber and when meshing with the roots surfaces of the other rotor. With respect to the direction of rotor rotation, end surfaces 34e,36e define lead ends of the lobes and end surfaces 34f,36f define trailing end of the lobes. Radially inward extents of the flank surfaces merge or blend into radially outward extents of the roots surfaces along the length of the lobes in the area designated by action lines 34h,36h in Figure 5. The action lines are omitted in Figures 7A-7G to avoid undue clutter therein. The helical lobes preferably, but not necessarily, have a twist defined by the relation $360^\circ/2n$, wherein n equals the number of lobes per rotor.

Outlet port opening 26 has a somewhat triangular shape disposed intermediate chambers 22,24 and skewed toward the ends of the chambers defined by flat surface 16a of the bearing plate member, and completely below common plane 32. Air from opening 26 flows into a rectangular recess 42 in the bottom or base of housing member 14. Preflow or backflow slots 44,46 disposed on opposite sides of the outlet port opening respectively provide for backflow of outlet air in recess 42 to transfer volumes of air trapped by adjacent unmeshed lobes of the rotor prior to traversal of the outlet port boundaries 26a,26b by the outer surface of the front lobe of each transfer volume. Further detail of the outlet port and backflow slots may be obtained by reference to previously mentioned U.S. Patent Number 4,768,934 which is incorporated herein by reference. The base of housing member 14 is adapted to be affixed to an unshown manifold, such as an engine manifold, which directs outlet port air from recess 42 to engine combustion chambers and to bypass duct 31.

Inlet port opening 28 extends through end wall 14d at a position completely above common plane 32 and adjacent end surfaces 34e,36e at the lead ends of the lobes. The opening includes radially inner and outer boundaries 28a,28b with respect to axes 22a,24a and first and second lateral boundaries 28c,28d.

Boundaries 28a,28b are positioned to maximize axial and minimize radial flow of inlet air into the spaces between adjacent lobes of each rotor. Such flow of inlet air mitigates negative effects of centrifugal forces imparted to the inlet air by the rotating lobes even at moderate rotor speeds. Further, since the inlet opening is at the lead ends of the helical lobes, the lobe helix angles impart axial forces on the inlet air which improves or assists flow into the spaces rather than opposes such flow as do centrifugal forces. Radially inner boundary 28a is positioned for substantial alignment with the radially inner most extent of root surfaces 34b,36b of the lobes and radial outer boundary 28b is slightly outward of a tangent across the crest or

uppermost arc of cylindrical surfaces 14a,14b. Housing 14 includes a surface 14f beginning at outer boundary 28b and smoothly tapering into cylindrical surfaces 14a,14b over an axial distance less than 25% of the axial length of chamber 22,24.

Boundaries 28c,28d are positioned in circumferentially opposite directions from cusp 14e distances sufficient to be substantially untraversed by the aft lobe lead end surface of each transfer volume until the top land at the trailing end of the aft lobe traverses cusp 14e. This prior traversal of the cusp prevents a net air loss from substantially mature transfer volumes due to airflow across the top land to emerging transfer volumes at lower pressure.

Lateral boundaries 28c,28d may be, and in many applications, such as high rotor speed applications, are preferably, positioned for traversal as long after cusp traversal as possible, thereby increasing the number of rotational degrees each transfer volume is connected to inlet air. For example, with rotors having three 60 degree twist lobes each, lateral boundaries 28c,28d may be a minimum of about 60 degrees from cusp 14e. However, by extending the lateral boundaries to about 85 degrees, as shown in Figure 5, volumetric efficiency at high rotor speeds improved substantially while low speed volumetric efficiency was substantially unaffected.

Inlet duct 30 includes an end 30a adapted to be connected to a source of air in known manner and an end 30b defined by inlet port opening 28. Duct 30 has a mean flow path represented by phantom line 30c which is disposed below plane 32 at end 30a, curves upward across plane 32, and curves slightly downward for smooth transition into inlet port opening 28. Bypass duct 31 includes an inlet 31a adapted to receive blower discharge air as previously mentioned, a butterfly valve 48 for controlling bypass air flow in known manner, and an outlet 31b which directs the bypass air into inlet duct 30 at an acute angle with respect to the air flow in the inlet duct. This blending of inlet and bypass air reduces air turbulence in passage 30 and therefore mitigates inefficiencies associated with bypass air flow into an inlet duct of a supercharger. The butterfly is affixed to a shaft 50 which is rotated by a link 52. The link is spring loaded in a direction closing the butterfly and moved toward positions opening the butterfly by a vacuum motor 54 or the like in known manner.

Rotation of rotors 34,36 effects alternate meshes of the lobes wherein one lobe 34a or 36a of one rotor moves into and out of space between the front and rear adjacent lobes of the other rotor. Each mesh includes arcs-of-action defining sealing relation between the outer surface 34g or 36g of the one lobe of the one rotor and the root surface

36b or 34b between the front and rear adjacent lobes of the other rotor. The arcs-of-action start at the lobe lead ends 34e,36e and progress to the lobe trailing ends 34f,36f in response to continued rotation of the rotors.

With reference to Figure 6 and as viewed from axis 24a, therein rotor 34 is illustrated in free space with arcs-of-action 101-110 of an infinite family of arcs-of-action extending diagonally across root surface 34b as would occur with rotor 34 rotation about axis 22a in the direction of arrow B and with rotor 36 rotating about its axis 24a in the opposite direction during a mesh cycle. Each family of arcs-of-action for each mesh starts at an intersection 56 of action line 34h and lobe lead end 34e and progresses incrementally to termination at an intersection 58 of action line 34h and lobe trailing ends 34f. Each arc-of-action 101-104 has a beginning 101a-104a and each arc-of-action 102-110 has an ending 102b-110b. Each beginning arc-of-action is in response to rotor rotation moving successive increments of the outer surface 36g of lobe 36a into sealing relation with successive incremental portions of root surface 34b juxtaposed the radially inner extent of fore surface 34c of rear adjacent lobe 34a in the area of action line 36h. Each incremental beginning of each arc-of-action occurs while a sealing relation exists between the fore surface 36c of lobe 36a and the aft surface 34d of the front adjacent lobe 34a. Each ending arc-of-action is in response to rotor rotation moving successive increments of the outer surface 36g of lobe 36a out of sealing relation with successive incremental portions of root surface 34b juxtaposed the radially inner extent of aft surface 34d of adjacent lobe 34a in the area of action line 34h. Each incremental ending arc-of-action occurs while a sealing relation exists between the aft surface 36d of lobe 36a and the fore surface 34c of the rear adjacent lobe 34a. Arcs-of-action 102, 103 and 104 are fully developed in that each has a beginning 102a, 103a and 104a and each has an ending 102b, 103b and 104b as previously mentioned. Arc-of-action 101, which has just started to develop has a beginning arc-of-action 101a and no ending arc-of-action. Arcs-of-action 105-110, which are moving toward termination, have ending arcs-of-action 105b-110b and no beginning arcs-of action. With continued reference to Figure 6 and additional reference to Figures 7A-7G, arcs-of-action 104-110 and intersection 58 of Figure 6 correspond respectively to the rotor lobe positions of Figures 7A-7G with each successive figure representing lobe positions after five rotational degrees of rotor rotation.

Each arc-of-action and the concurrent sealing relations between the fore-and-aft surfaces of the meshing lobes defines first and second pockets extending along the meshed lobes and sealingly

separated by the diagonal sealing relation between outer surface 36g and root surface 34b. The first pockets are formed between fore surface 36c of lobe 36a and root surface 34b between the adjacent front and rear lobes. The volume of each of the first pockets is defined by a maximum spacing between the fore surface 36c and root surface 34b at the beginning of each arc-of-action; the spacing decreases to a minimum as each ending arc-of-action is approached. In an analogous manner, the volume of each second pocket is defined by a maximum spacing between the aft surface 36d and root surface 34b at the ending of each arc-of-action; the spacing decreases to a minimum as each beginning arc-of-action is approached. The first pockets open toward the trailing ends of the lobe; and the second pockets open toward the lead ends of the lobes. Between intersection 56 and arc-of-action 104, the first pockets are open to the gaseous fluid in outlet 26, thereafter the first pockets become trapped volumes with outlet fluid therein trapped against direct communication with outlet 26 due to the sealing relations between the lobe meshing surfaces, and the sealing relation between lobe trailing end surfaces and end wall surface 16a of bearing plate member 16.

Each trapped volume progressively decreases from a maximum size at arc-of-action 104 and the corresponding lobe position of Figure 7A to a minimum size just prior to intersection 58 and corresponding lobe position of Figure 7G. Figures 7A-7G illustrate rotors 34,36 in free space and in mesh for rotation about their respective axes 22a,24a. As the meshing lobes progress through arcs-of-action 104-110 and intersection 58, the foot print of the spacing between fore spaces 36c and root surface 34b at end wall surface 16a decreases while the foot print of the spacing between the aft surface 36d and root surface 34b increases.

With reference to Figure 8, end wall surface 16a of bearing plate member 16 is provided with outlet and inlet vent recesses 60,62 respectively disposed on opposite sides of plane 32 defined by the rotor axes. The outlet recess communicates fluid in the trapped volumes to housing outlet 26 and the inlet recess communicates the remainder of the fluid in the trapped volumes to the housing inlet 26. Both recesses diminish pressure build up in the trapped volumes as they decrease in size. The outlet recess also increases pump efficiency by retaining a portion of the trapped outlet fluid back to the pump outlet. Both vent recesses are shown superimposed on the trailing ends 34f,36f of rotors 34,36 in Figures 7A-7G.

The outlet vent recess 60 includes an elongated recess portion 60a extending parallel to plane 32 and in continuous communication with outlet 26, and first and second recess fingers

60b,60c extending from the ends of recess portion 60a toward position wherein portions of fingers 60b,60c are respectively traversed and communicated with alternately formed contracting trapped volumes respectively associated with root surfaces 34b,36b. Fingers 60b,60c respectively have converging boundary limits 60d,60e and 60f,60g. Boundary limits 60d,60f are positioned such that the expanding second pockets are sealed from direct communication with the outlet vent recess, thereby preventing a leak path from housing outlet 26 to housing inlet 28. Boundaries limits 60e,60g are spaced relatively small distances radially outward of the outer edges of bores 16b,16c in bearing plate member 16 that shafts 38,40 extend through. Such positioning allows traversal of boundary limits 60e,60g by the radially innermost extend of root surfaces 34b,36b to increase the flow area and the time that the trapped volumes are communicated with the outlet vent recess prior to communication with the inlet vent recess.

The inlet vent recess 62 includes a rectangular recess portion 62a in communication with inlet 28, and first and second recess fingers 62b,62c extending from corners thereof toward plane 32 a distance sufficient to establish alternate communication with the alternately formed trapped volumes as they move out of communication with outlet vent recess fingers 60b,60c.

Figures 9,10 and 11,12 illustrate two alternative embodiments of vents 60,62 in Figures 7A-7G and 8. The embodiment of Figures 9,10 include a primary outlet vent recess 64, primary inlet vent recesses 66,68 which together are equivalent to inlet vent recess 62, and secondary vent grooves 70,72 intercommunicating the primary outlet and inlet vent recesses. Outlet and inlet vent recesses 64 and 66,68 provide, as do vent recesses 60,62, relatively unrestricted flow paths to the outlet 28 and inlet 26. Outlet vent recess 64 includes an elongated recess portion 64a extending parallel to the plane 32 and in continuous substantially unrestricted communication with outlet 26 in a manner analogous to outlet vent recess 60. Outlet vent recess 64 also includes first and second recess fingers 64b,64c extending from the ends of recess portion 64a toward positions wherein portions thereof are respectively traversed and communicated with the alternately formed contracting trapped volumes respectively associated with root surfaces 34b,36b. Figures 64b,64c, in a manner somewhat analogous to fingers 60b,60c, include converging boundary limits 64d,64e and 64f,64g. Boundary limits 64d,64f are positioned substantially the same as boundary limits 60d,60f. Boundary limits 64e,64f are positioned further radially outward of the outer edges of bores 16b,16c than are boundary limits 60e,60g, thereby increasing or

maintaining structural strength in the area of the land between the bores and boundary limits 64e,64g. However, such positioning of boundary limits 64e,64g decreases the flow area and time that the trapped volumes are communicated with the outlet recess.

The effects of such decreased communication are mitigated by secondary vent grooves 70,72 having a rather narrow width W and shallow depth D relative to the recesses. Accordingly, each groove provides a restricted flow path along its length between the outlet and inlet grooves. The restricted flow paths provided by the grooves of course appear to provide a continuous leak path from outlet 26 to inlet 28. However, leakage of outlet fluid to the inlet is substantially mitigated relative to the vents of Figure 8 due to position of the grooves, due to cyclic pressure in the trapped volumes being greater than the fluid pressure in outlet 28, and due to flow restriction of the grooves. By way of example only, the restricted flow paths of the grooves may be one-tenth the flow paths of the recesses. More specifically, during each mesh cycle, the pressure in the grooves from the trapped volumes is substantially greater than the fluid pressure in outlet 26 and; accordingly, there is no leakage from outlet 26 to inlet 28 during the mesh cycle periods of the grooves. Further, since the foot print of the trapped volumes initially overlies portions of the grooves contiguous to boundary limits 64d,64f, a greater portion of the trapped volume fluid flows to the outlet vent recess than to the inlet recesses. As the rotors continue to rotate and the second pockets or spaces between the meshing lobes are formed sufficiently to provide an effective flow path therethrough to inlet 28, the pockets though overlying the grooves are spaced sufficient distances from the groove ends contiguous to the outlet boundary limits 64d,64f such that there is little or no leakage of fluid from outlet 28 due to flow restriction in the grooves and the trapped volume fluid pressure therein.

With reference now to the alternative embodiment of Figures 11,12, therein are outlet and inlet vent recesses 74 and 76,78, as in Figures 9,10, and secondary vent grooves 80,82 extending from fingers 74a,74b of the outlet vent recess, and secondary vent grooves 84,86 extending from the inlet vent recesses. Grooves 80,84 and 82,86 are discontinuous but functionally the same as grooves 70,72 in that they are sufficiently shallow to provide flow restrictions in the manner of grooves 70,72. However, tests indicate that grooves 80,84 and 82,86 should provide somewhat greater restricted flow paths than do grooves 70,72,

A preferred embodiment of the invention has been disclosed in detail for illustrative purposes. Many variations of the disclosed embodiments are

believed to be within the spirit of the invention. The following claims are intended to cover inventive portions of the disclosed embodiment and modifications believed to be within the spirit of the invention.

Claims

1. A rotary pump (10) including a housing (12) defining an inlet and an outlet (28,26) and first and second parallel, transversely overlapping cylindrical chambers (22,24) having cylindrical (14a,14b) and end wall surfaces (14c,16a);
first and second meshed lobed rotors (34,36) respectively disposed in the first and second chambers for transferring volumes of substantially gaseous fluid from the inlet to the outlet via spaces between front and rear adjacent and unmeshed lobes (34a,36a) of each rotor in response to rotation of the rotors about their respective axes, the rotors and lobes having end surfaces (34e,34f and 36e,36f) disposed for sealing relation with the end wall surfaces, the lobes having an end-to-end helical twist such that each lobe has a lead end (34e,36e) and a trailing end (34f,36f) in the direction of rotor rotation, the lobes of each rotor having a radially outer surface (34g,36g) disposed for sealing relation with the cylindrical wall surface (14a,14b) of the associated chamber and fore-and-aft surfaces (34c,34d and 36c,36d) in the direction of rotor rotation and a root surface (34b,36b) extending between radially inner extents (34h,36h) of the fore-and-aft surfaces of adjacent lobes;
rotation of the rotors effecting alternate meshes of the lobes (34a,36a) wherein one lobe of one rotor moves into and out of the spaces between front and rear adjacent lobes of the other rotor, each mesh forming first and second pockets extending along the meshed lobes, the pockets sealingly separated by a sealing relation of the one lobe outer surface extending diagonally across the root surface, the pockets initially formed at the lead ends (34e,36e) of the meshing lobes and progressing toward the trailing ends (34f,36f) in response to continued rotation of the rotors, the first and second pockets respectively open to the housing outlet and inlet when opposite ends of the diagonal sealing relations are spaced from the lead and trailing ends of the meshing lobes, the first pocket becoming a trapped volume contracting in cross-section and sealed from direct communication with the housing outlet in response to the diagonal sealing relation of the one lobe outer surface initially reaching the trailing ends (34f,36f) of

the meshing lobes and due to the sealing relation with the associated end wall surface (16a), each trapped volume containing outlet fluid and the volume decreasing from a maximum to a minimum size in response to continued rotation of the rotors, and the second pockets expanding in cross-section in response to the diagonal sealing relation of the one lobe outer surface initially reaching the trailing ends of the meshing lobes;

vent means (60,62) for relieving pressure build-up in the trapped volumes; characterized by:

the vent means (60,62) including outlet and inlet recess means (60,62) formed in the end wall surface (16a) sealingly related with the rotor and lobe end surfaces at the lobe trailing ends (34f,36f), the outlet and inlet recess means respectively disposed on opposite sides of a plane (32) defined by the rotor axes (22a,24a), the outlet recess means (60) for communicating a portion of the fluid in the trapped volumes to the housing outlet (26), the inlet recess (62) means for communicating another portion of the fluid in the trapped volumes to the housing inlet (28), the outlet recess means including first and second recess fingers (60b,60c) having a substantially unrestricted flow area in continuous communication with the outlet fluid in the housing outlet (26), the first and second recess fingers (60b,60c) disposed such that the trapped volumes of the first pockets move from positions communicating directly with the associated recess finger to positions sealed from such direct communication while the expanding second pockets are sealed from communication with the associated recess finger, and the trapped volumes move from positions sealed from direct communication with the inlet recess means (62) to positions directly communicating therewith as the trapped volumes move to positions sealed from direct communication with the associated recess fingers.

2. The rotary pump of claim 1, further including:

fluid flow restriction grooves (70,72 or 80,82,84,86) formed in the end wall surface sealingly related with the rotor and lobe end surfaces (34f,36f) at the lobe trailing ends, and the first and second recess (64b,64c) fingers having boundary (64d,64e,64f,64g) limits disposed such that the trapped volumes of the first pockets respective disposed between the root surfaces (34b,36b) of the first and second rotors (34,36) and the fore surface (34c,36c) of the one lobe (34a,36a) moves from the positions communicating directly with the asso-

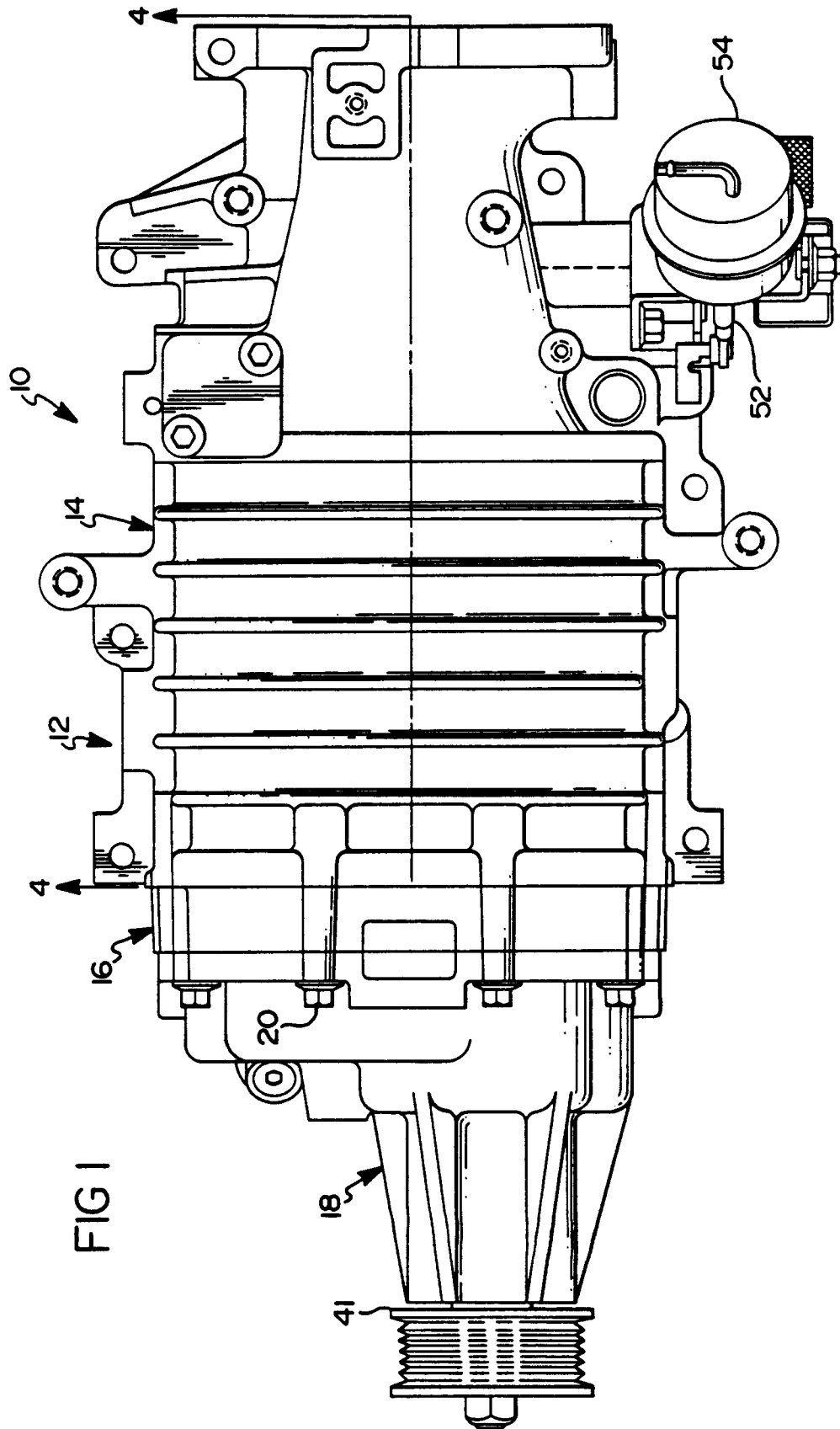
ciated finger (64b,64c) to positions wherein the trapped volumes and the expanding second pockets disposed between the root surfaces (34b or 36b) and the aft surfaces (34d or 36d) of the one lobe (34a or 36a) communicate with the associated finger (60b or 60c) via the flow restriction grooves (70,72 or 80,82,84,86).

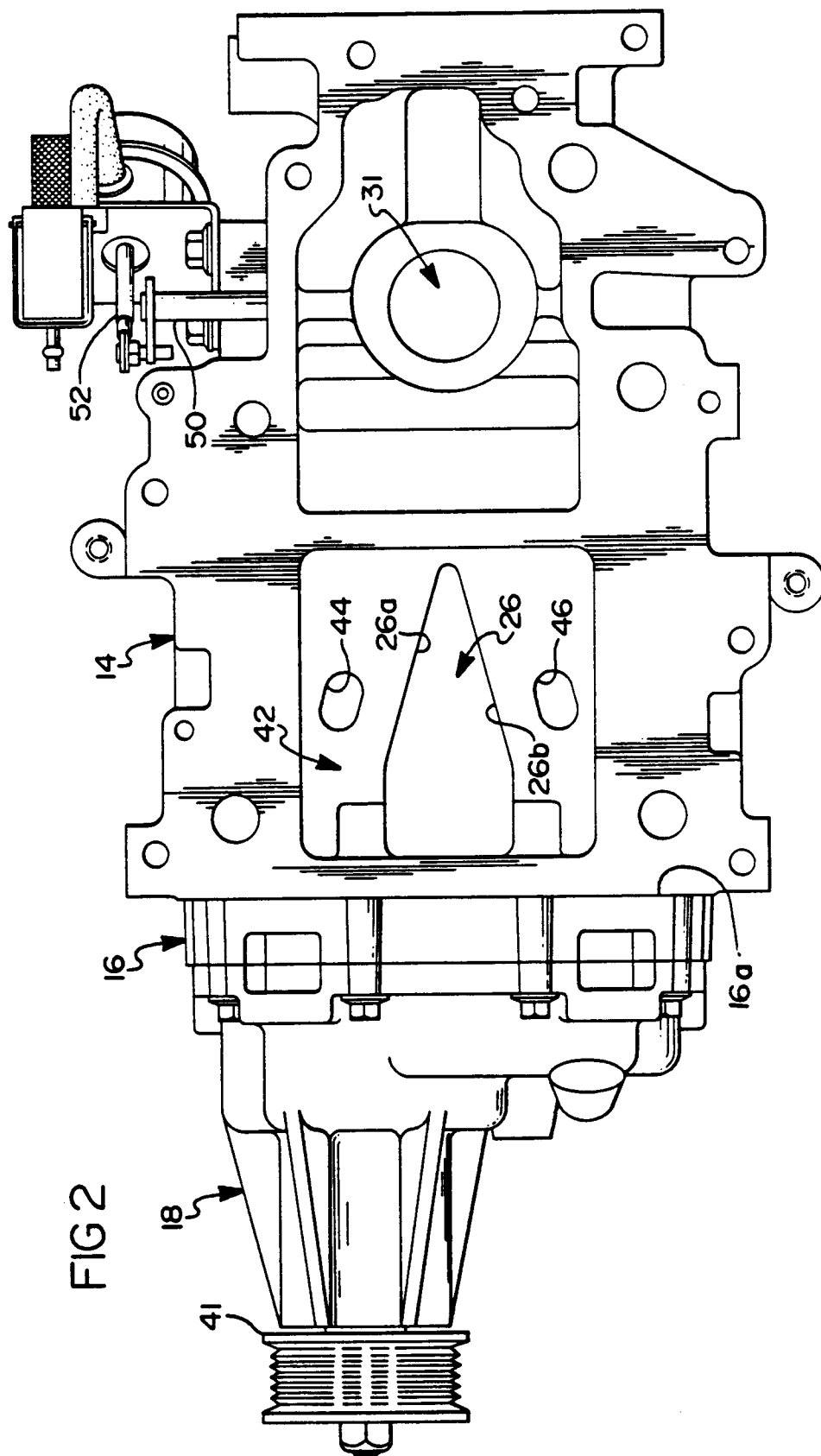
3. The rotary pump of claim 2, wherein the restricted grooves (70,72) include first and second grooves (70,72) extending respectively from direct communication with the first and second fingers (64b,64c) to direct communication with the inlet recess means (66,68).

4. The rotary pump of claim 3, wherein the fluid flow restricted grooves (70,72) have a flow area less than one-tenth the flow area of the outlet vent recess (64).

5. The rotary pump of claim 2, wherein the restricted grooves (80,82,84,86) include first and second grooves (80,82) extending respectively from direct communication with the first and second fingers (74a,74b) to positions spaced from the plane (32) and third and fourth grooves (84,86) extending respectively from the inlet recess means (76,78) toward the first and second grooves (80,82) to positions spaced therefrom and adjacent the plane (32).

6. The rotary pump of claim 5, wherein the fluid flow restricted grooves (80,82,84,86) have a flow area less than one-tenth the flow area of the outlet vent recess (74).





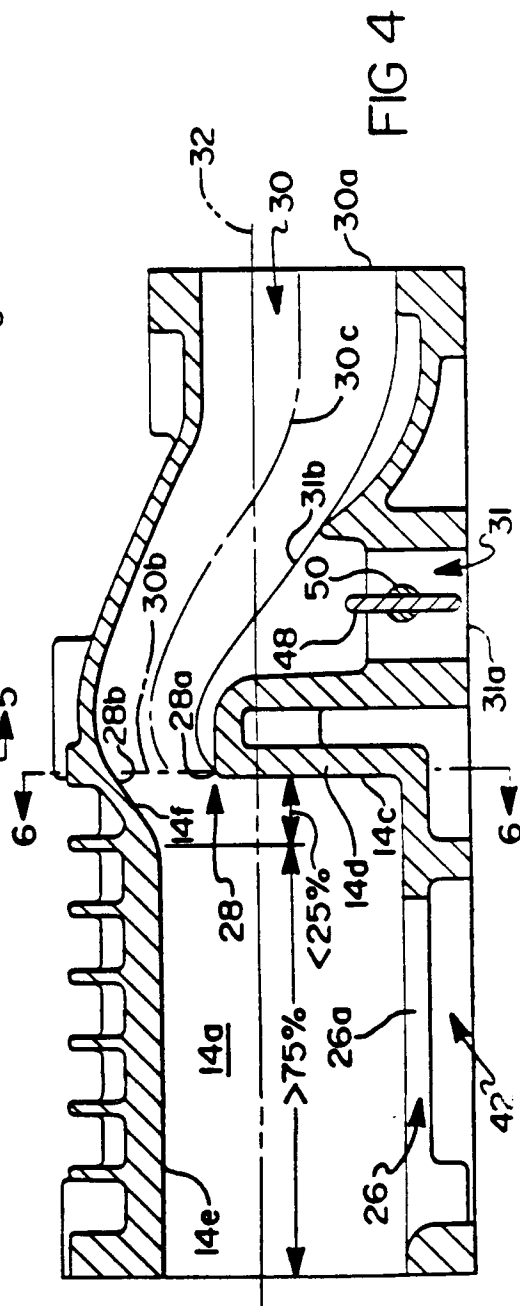
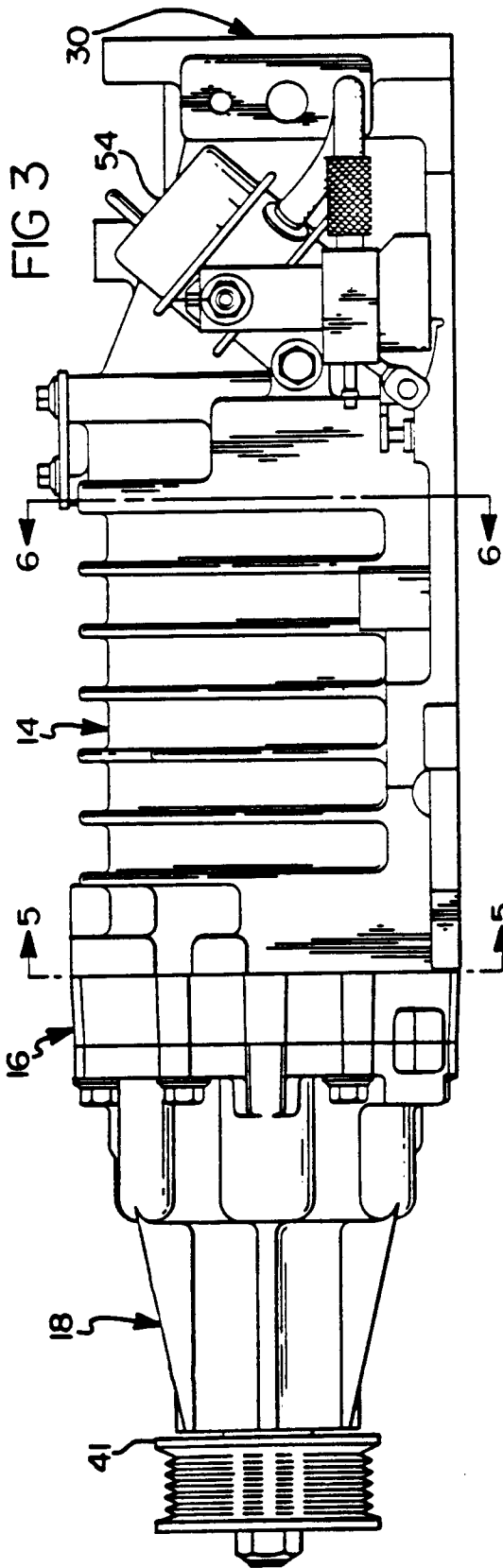
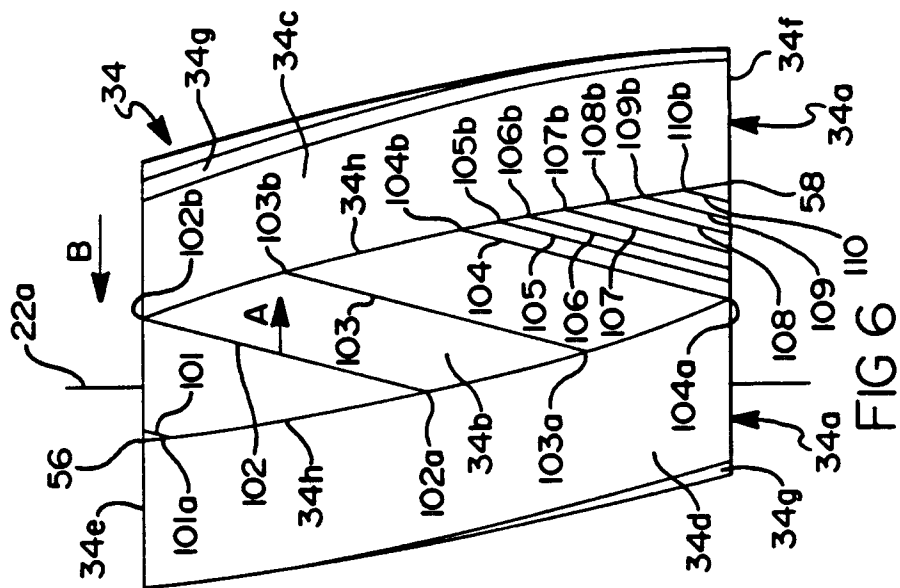
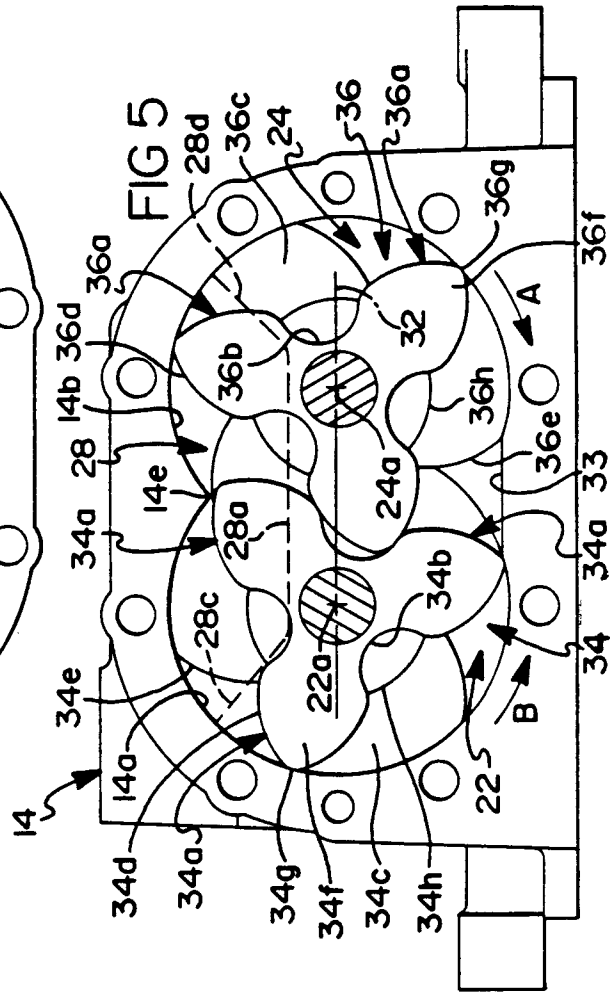
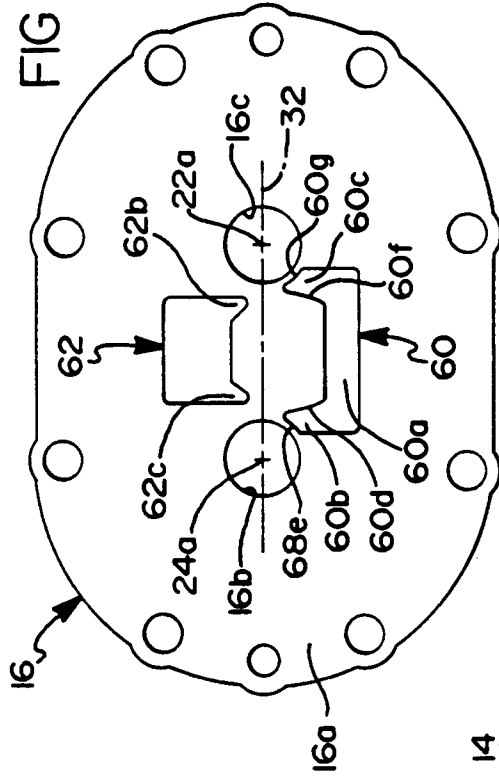
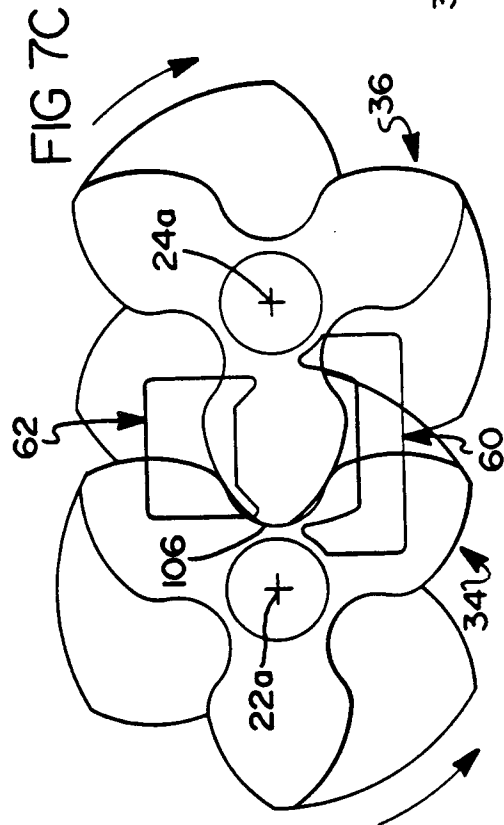
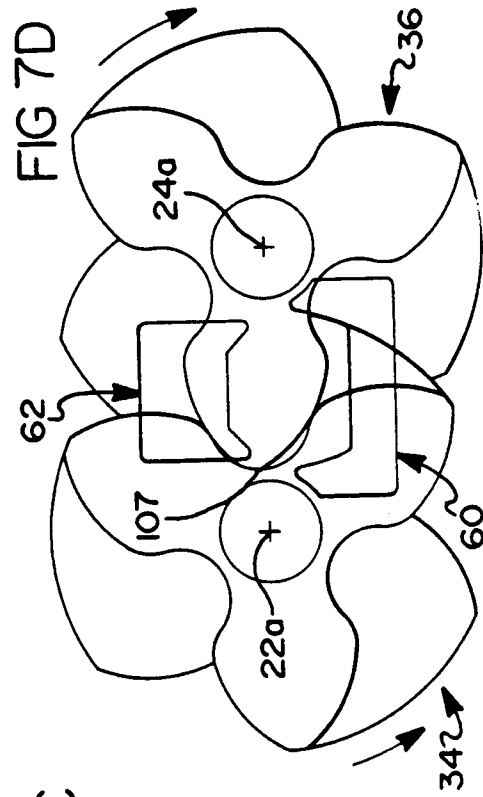
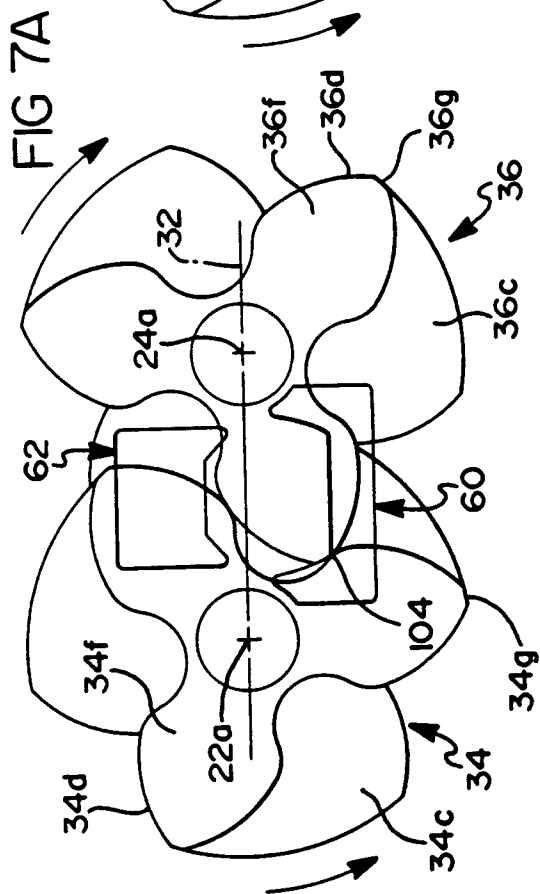
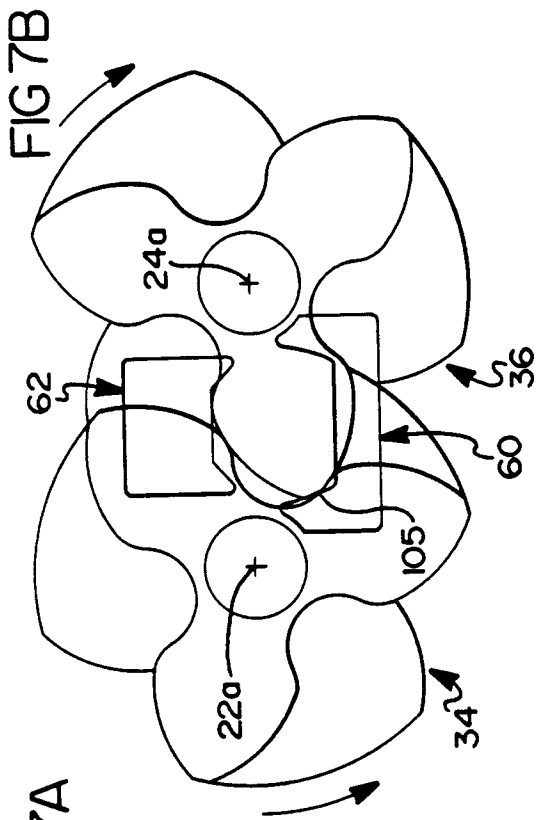
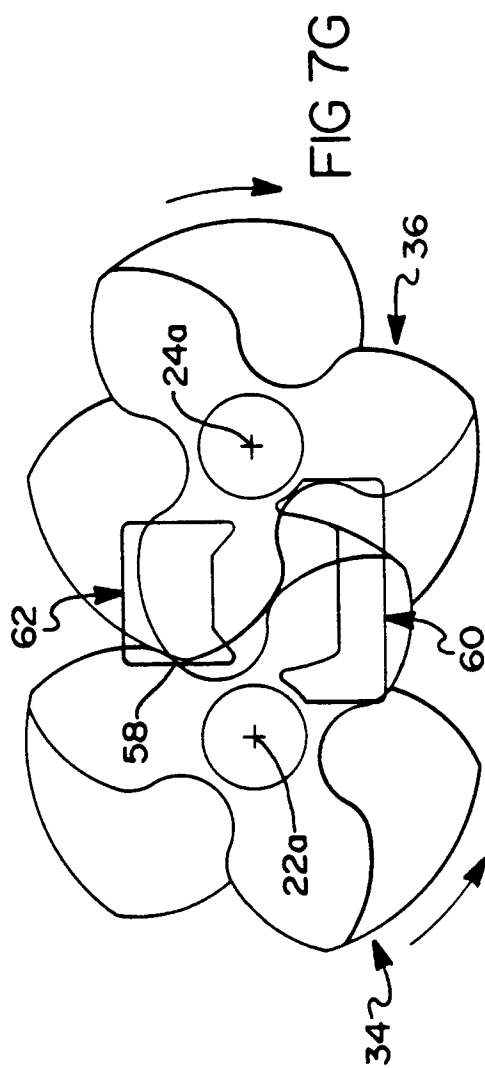
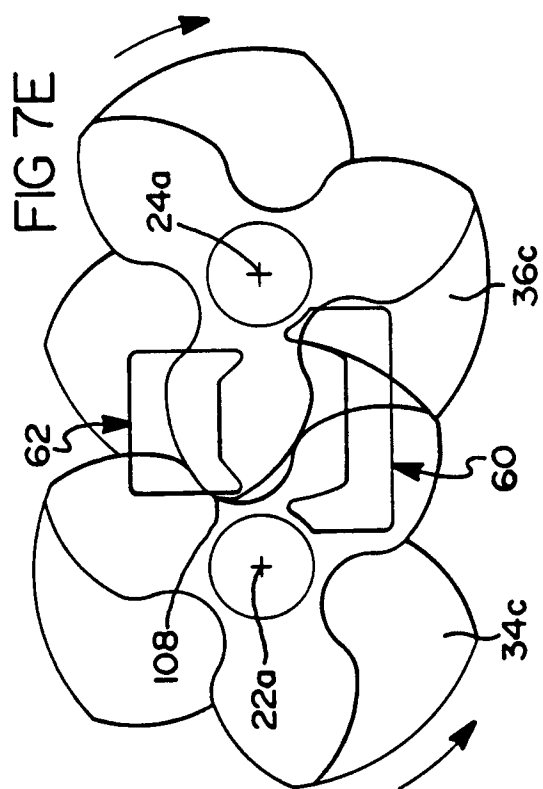
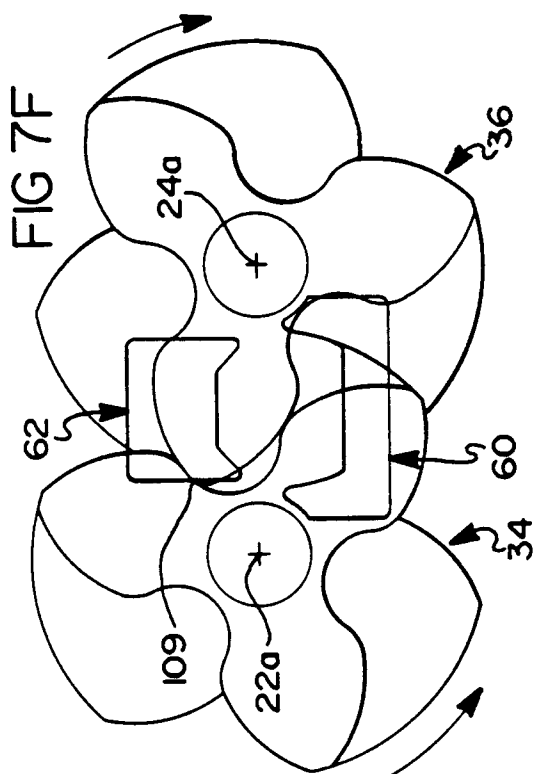
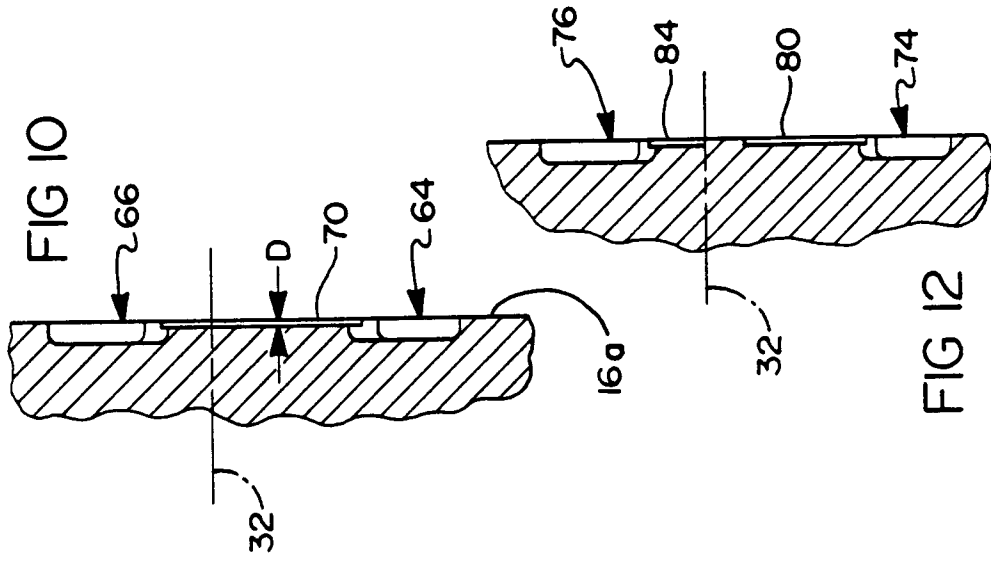
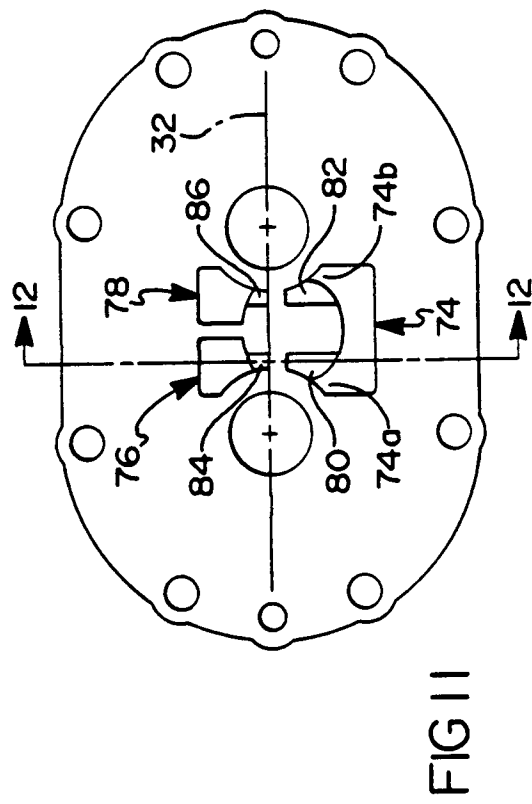
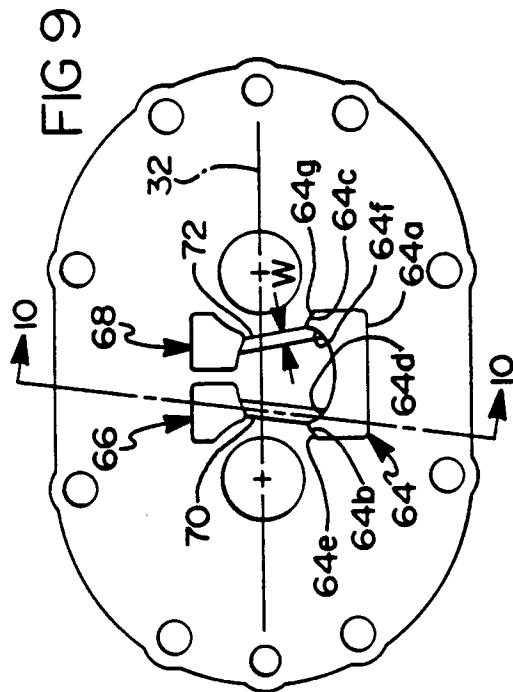


FIG 8











European Patent
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EUROPEAN SEARCH REPORT

Application Number

EP 92 10 9479

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
D,A	US-A-4 556 373 (SOETERS) * the whole document * ---	1	F04C18/12 F04C18/08
D,A	US-A-4 569 646 (SOETERS) * the whole document * ---	1	
P,A	EP-A-0 455 059 (FIATGEOTECH - TECNOLOGIE PER LA TERRA S.P.A.) * the whole document * ---	1	
A	US-A-3 817 665 (MYERS) -----		
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			F04C
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 29 SEPTEMBER 1992	Examiner DIMITROULAS P.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			