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- (54) Refrigeration lubricants.
- © Use of a lubricant for compressors using a hydrofluorocarbon refrigerant containing no chlorine, comprising as a main component an ester(s) obtained by reacting (a) neopentyl glycol with (b) at least one branched-chain monovalent saturated fatty acid having a carbon number of 3-18, wherein said ester has a total acid value of not more than 3 mg KOH/g and a hydroxyl value of not more than 50 mg KOH/g.

This invention relates to lubricants used with refrigerants, and more particularly to lubricants suitable for use in the compression of refrigerants containing no chlorine such as hydroflorocarbons (HFC), preferably HFC-134a (1,1,1,2-tetrafluoroethane) and the like.

Heretofore, compounds containing fluorine and chlorine as a constituent element such as R-11 (trichloromonofluoromethane), R-12 (dichlorodifluoromethane) as a chlorofluorocarbon (CFC), R-22 (monochlorodifluoromethane) as a hydrochlorofluorocarbon (HCFC) and the like have been used as a refrigerant for freezers, air conditioners, refrigerators and the like. In connection with recent problem on breakage of ozone layer, new refrigerants containing no chlorine such as HFC-134a and so on are proposed as a possible replacement for R-12, causing no breakage of ozone layer.

As a refrigeration lubricant, there are known many mineral-series and synthetic oils. However, it has been confirmed that these oils are very poor in the compatibility with HFC-134a and can not be applied thereto. Therefore, it is important to take a countermeasure on this problem at the present. Furthermore, the lubricity, electric insulating property, energy saving property, anti-wear performance, sealability, thermal stability, prevention of sludge formation and the like are mentioned as performances required in the refrigeration lubricant, so that they are required to be considered in the development of the above countermeasure.

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Incidentally, there have hitherto been known polyether series synthetic lubricants as a synthetic oil, which are reported in Journal of the Oil Chemistry, vol. 29, No. 9, pp 336-343 (1980) and Journal of the Petroleum Technology, vol. 8, No. 6, pp 562-566 (1985). Furthermore, Japanese Patent laid open No. 61-281199 describes a mixture of polyglycol represented by a general formula of R<sub>1</sub>[O-(R<sub>2</sub>O)<sub>m</sub>-R<sub>3</sub>]<sub>n</sub>, an alkylbenzene and the like, and Japanese Patent laid open No. 57-63395 describes an oil obtained by mixing a polyether such as high molecular weight polyoxypropylene monobutyl ether with an epoxycycloalkyl compound, and Japanese Patent laid open No. 59-117590 describes a high viscosity mixed oil of a polyether compound and a paraffinic or naphthanic mineral oil.

However, the conventional synthetic lubricants as mentioned above can not be a refrigeration lubricant using HFC-134a as a refrigerant from a viewpoint of compatibility and the like.

In US Patent No. 4,755,316, polyoxyalkylene glycol (hereinafter abbreviated as PAG) having hydroxyl groups (-OH) at both terminals is reported as a refrigeration lubricant using HFC-134a. Further, it is described that PAG is dissolved in HFC-134a within a wide temperature range as compared with general PAG containing hydroxyl group and alkyl group at its terminals, whereby the recycle of the lubricant into a compressor is improved in the refrigeration system and the seizuring in the actuation of the compressor at high temperature is prevented. Moreover, the temperature range compatible with HFC-134a is described to be between -40 ° C and +50 ° C.

On the contrary, HFC-134a is a replacing refrigerant of R-12 and is mainly expected for use in a car air conditioner, a refrigerator and the like. In case of the refrigerator, it is required to have a good compatibility between lubricant and refrigerant, and further the lubricant itself is necessary to have an electric insulating property because the motor is substantially existent in the refrigeration system. However, the conventional compounds examined as a lubricant for HFC-134a refrigerant inclusive of PAG disclosed in US Patent No. 4,755,316 are remarkably poor in the electric insulating property as compared with the conventional refrigeration mineral oil and high in the hygroscopicity.

It is, therefore, an object of the invention to provide a refrigeration lubricant having an excellent compatibility with a new refrigerant such as HFC-134a or the like within a wide temperature range, a high electric insulating property and a low hygroscopicity.

At the present, a part of commercially available esters is used in systems using refrigerants R-12, R-22 and the like, but is incompatible with HFC-134a as a new refrigerant or is very narrow in the compatible range therewith. In this connection, the inventors have aimed at the fact that the ester has a high electric insulating property, a low hygroscopicity, a good lubricity and a high stability as compared with PAG and made various studies with respect to the molecule design of the ester showing a wide range of compatibility with HFC-134a, and found that only esters having a considerably restricted structure can be used in the HFC-134a refrigeration system, and as a result, the invention has been accomplished.

According to a first aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of neopentyl glycol and at least one straight or branched-chain monovalent fatty acid having a carbon number of 3-18.

According to a second aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of at least one of pentaerythritol, dipentaerythritol and tripentaerythritol represented by the following general formula (I):

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(in which n is 1, 2 or 3), and at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18.

According to a third aspect of the invention, there is the provision of a lubricant for hydrofluorocarbon refrigerant such as HFC-134a and the like comprising as a main component an ester comprised of a polyvalent alcohol represented by the following general formula (II):

(in which R is an alkyl group having a carbon number of not more than 3), at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18, and not more than 25 mol% per total fatty acid of at least one polybasic acid having a carbon number of 4-36.

In a preferred embodiment of the invention, the hydrofluorocarbon refrigerant is 1,1,1,2-tetrafluoroethane (HFC-134a).

The refrigeration lubricant for refrigerant HFC-134a and the like according to the first invention comprises an ester obtained by esterifying neopentyl glycol with at least one straight or branched-chain monovalent fatty acid having a carbon number of 3-18 as a main component.

In the first invention, the reason why the carbon number of the monovalent fatty acid is limited to 3-18 is due to the fact that when the carbon number is less than 3, the viscosity is too low, while when it exceeds 18, the resulting ester becomes cloudy or becomes very poor in the compatibility with the refrigerant HFC-134a and the like.

As the monovalent fatty acid, mention may be made of propionic acid, isopropionic acid, butanoic acid, isobutanoic acid, pentanoic acid, isopentanoic acid, hexanoic acid, heptanoic acid, isoheptanoic acid, octanoic acid, 2-ethyl hexanoic acid, nonanoic acid, 3,5,5-trimethyl hexanoic acid, decanoic acid, undecanoic acid, lauric acid, myristic acid, palmitic acid, palmitooleic acid, stearic acid, isostearic acid, oleic acid, and the like.

In the first invention, at least one of these monovalent fatty acids is properly mixed and esterified with neopentyl glycol to obtain an ester satisfying desirable physical properties required for various refrigerators.

In order to obtain a sufficiently satisfactory compatibility with the refrigerant HFC-134a and the like, it is preferable to use a mixture of straight chain fatty acid having a carbon number of 3-11, preferably 5-10 and a branched-chain fatty acid having a carbon number of 3-14, preferably 7-9 as the monovalent fatty acid. In this case, the amount of the straight or branched-chain fatty acid used is preferable to be not less than 50 mol% per the total monovalent fatty acid used.

According to the invention, in order to give a proper viscosity to the resulting ester, at least one polybasic acid having a carbon number of 4-36 may be esterified with neopentyl glycol in an amount of not more than 80 mol% per total fatty acid. Among the polybasic acids, considering the more compatibility with the refrigerant HFC-134a and the like and the physical properties of the resulting ester, a polybasic acid having a carbon number of 4-10 is preferable. Concretely, the polybasic acid includes succinic acid, glutaric acid, adipic acid, pimelic acid, suberic acid, azelaic acid, sebacic acid, phthalic acid, maleic acid, trimellitic acid and so on. Moreover, the polybasic acid having a carbon number of not more than 3 is a special product and is difficult to be cheaply available and is poor in the stability of the ester after the synthesis. While, when the carbon number exceeds 36, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. In the invention, the reason why the amount of the polybasic acid added is limited to not more than 80 mol% per the total fatty acid is due to the fact that when it exceeds 80 mol%, the gelation

may be caused and it is difficult to obtain desirable physical properties.

The ester compounds according to the first invention can be obtained by the esterification reaction through dehydration reaction between the specified polyvalent alcohol and the specified fatty acid as mentioned above, or the general esterification reaction through an acid anhydride, an acid chloride or the like as a derivative of the fatty acid.

Since the ester according to the invention can be obtained by the above method, the remaining acid value and hydroxyl value are not particularly critical. However, when the acid value exceeds 3, there may be caused an unfavorable phenomenon that the metal soap is formed and precipitated by the reaction with a metal used inside the refrigerator, so that the acid value is preferable to be not more than 3. Furthermore, when the hydroxyl value exceeds 50, there may be caused an unfavorable phenomenon that the resulting ester becomes cloudy, so that the hydroxyl value is preferable to be not more than 50.

The lubricant for refrigerant HFC-134a and the like according to the second invention comprises an ester obtained by esterifying at least one of pentaerythritol, dipentaerythritol and tripentaerythritol represented by the aforementioned general formula (I) with at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18 as a main component.

In the condensate of pentaerythritol, the polymerization degree may be determined in accordance with the viscosity required in the resulting synthesized ester.

In the second invention, the carbon number of the monovalent fatty acid is limited to 2-18 because when it exceeds 18, the resulting ester becomes cloudy or becomes very poor in the compatibility with the refrigerant HFC-134a and the like.

As the monovalent fatty acid, mention may be made of acetic acid, propionic acid, isopropionic acid, butanoic acid, isobutanoic acid, pentanoic acid, isopentanoic acid, hexanoic acid, heptanoic acid, isoheptanoic acid, octanoic acid, 2-ethyl hexanoic acid, nonanoic acid, 3,5,5-trimethyl hexanoic acid, decanoic acid, undecanoic acid, lauric acid, myristic acid, palmitic acid, palmitooleic acid, stearic acid, isostearic acid, oleic acid, linoleic acid, linolenic acid and the like.

In the second invention, at least one of these monovalent fatty acids is properly mixed and esterified with pentaerythritol or its condensate to obtain an ester satisfying desirable physical properties required for various refrigerators.

In order to obtain a sufficiently satisfactory compatibility with the refrigerant HFC-134a and the like, it is preferable to use a mixture of straight chain fatty acid having a carbon number of 3-11, preferably 5-10 and a branched-chain fatty acid having a carbon number of 3-14, preferably 7-9 as the monovalent fatty acid. In this case, the amount of the straight or branched-chain fatty acid used is preferable to be not less than 50 mol% per the total monovalent fatty acid used.

On the other hand, in order to give a proper viscosity to the resulting ester, at least one polybasic acid having a carbon number of 4-36 may be esterified with at least one of pentaerythritol, dipentaerythritol and tripentaerythritol in an amount of not more than 80 mol% per total fatty acid. In this case, the same polybasic acids as described in the first invention are used in the same manner as in the first invention.

The ester compounds according to the second invention can be obtained by the same method as in the first invention.

In the esters according to the second invention, the acid value is preferable to be not more than 3 and the hydroxyl value is preferable to be not more than 50 likewise the case of the first invention.

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The lubricant for refrigerant HFC-134a and the like according to the third invention comprises an ester obtained by esterifying a polyvalent alcohol represented by the aforementioned general formula (II) with at least one straight or branched-chain monovalent fatty acid having a carbon number of 2-18 and not more than 25 mol% per total fatty acid of at least one polybasic acid having a carbon number of 4-36 as a main component.

When the carbon number of R in the general formula (II) is not less than 4, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. As the polyvalent alcohol, mention may be made of trimethylol ethane, trimethylol propane, trimethylol butane and the like.

In the third invention, when the carbon number of the monovalent fatty acid is more than 18, it becomes very poor in the compatibility of the resulting synthesized ester with HFC-134a and the like. Particularly, the straight or branched-chain monovalent fatty acids having a carbon number of 3-10 are preferable. As the monovalent fatty acid, mention may be made of the same compounds as described in the second invention.

As to the polybasic acid, the polybasic acid having a carbon number of not more than 3 is a special product and is difficult to be cheaply available and is poor in the stability of the ester after the synthesis. While, when the carbon number exceeds 36, the compatibility of the resulting ester with HFC-134a and the like is largely lowered. Therefore, the carbon number of the polybasic acid is preferable to be 4-36, and particularly the carbon number of 4-10 is favorable for ensuring the compatibility with HFC-134a at a wide

range. As the polybasic acid, mention may be made of adipic acid, azelaic acid, sebacic acid and so on. Preferably, the monovalent fatty acid is 2-ethylhexanoic acid, and the polybasic acid is adipic acid.

Moreover, the reason why the amount of the polybasic acid added in the invention is limited to not more than 25 mol% per the total fatty acid is due to the fact that when it exceeds 25 mol%, the gelation may be caused and it is difficult to obtain desirable physical properties.

The ester compounds according to the third invention can be obtained by the same method as in the first and second inventions. In any case, it is desirable that the ester does not contain carboxyl group.

The esters according to the invention exhibit a good compatibility with the refrigerant HFC-134a and the like over a wide range of from low temperature to high temperature as a lubricant for use in a refrigerator using HFC-134a as a refrigerant, whereby the lubricity and thermal stability of the refrigeration lubricant can be considerably improved. Furthermore, they are high in the electric insulating property and small in the hygroscopicity as compared with PAG conventionally examined as a refrigeration lubricant for HFC-134a. Therefore, the refrigeration lubricants comprising the ester according to the invention as a main component can solve the problems on the compatibility with HFC-134a and the hygroscopicity, which have never been solved in the conventional technique, and can further enhance the electric insulating property, which comes into problem when HFC-134a is used in a compressor for a refrigerator.

Moreover, additives usually used in the lubricant such as antioxidant, anti-wear agent, epoxy compound and the like may properly be added to the refrigeration lubricant according to the invention.

The following examples are given in illustration of the invention and are not intended as limitations thereof.

## Examples 1-8, Comparative Examples 1-5

The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with respect to eight esters A-1 - A-8 shown in the following Table 1 (all of which esters were not commercially available but were prepared according to the first invention). For the comparison, the same evaluation as mentioned above was made with respect to commercially available PAG (B-1 - B-3, made by Asahi Denka Co., Ltd.) and esters (C-1 - C-2, made by Nippon Oil and Fats Co., Ltd.) as a refrigeration lubricant shown in the following Table 2.

The lubricity, compatibility, thermal stability, electric insulating property and hygroscopicity as performances of the refrigeration lubricant for the compressor shown in Tables 1 and 2 were evaluated under the following conditions.

### Lubricity

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Seizuring load (Falex load-carrying capacity) was measured according to ASTM D-3233-73 under a controlled atmosphere of HFC-134a blown.

## Compatibility

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After 0.6 g of the test lubricant and 2.4 g of the refrigerant (HFC-134a) were sealed in a glass tube, the cooling at 1°C/min and the heating were carried out, during which a temperature causing two-phase separation was measured.

## 5 Thermal stability

After 1 g of the test lubricant, 1 g of the refrigerant (HFC-134a or R-12) and a catalyst (wire of iron, copper or aluminum) were sealed in a glass tube, the mixture was heated to 175°C, and a color of the lubricant after 10 days was judged by ASTM color system according to ANSI/ASHRAE 97-1983.

## Electric insulating property

It was evaluated by a dielectric constant at 80°C according to JIS C-2101.

### 5 Hygroscopicity

Into a beaker of 100 ml was charged 60 g of the test lubricant, which was left to stand at a temperature of 25 °C and a humidity of 70% for 3 hours and then the water concentration was measured.

The evaluation results are shown in the following Table 3.

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בן קפוד	4

Color (ASTM)		L 0.5	L 0.5	L 0.5	L 0.5	L 0.5	L 0.5	L 0.5	L 0.5
Dynamic viscosity	(cSt)	4.6	7.0	14.4	6.5	11.9	20.9	7.4	22.1
	sebacic acid	ı	1	ŀ	ı	ı	25	ı	ı
Polybas	adipic acid	1	°I	1	1	10	ı	ı	40
lin	$C_{18}$	ı	ı	ı	5	ı	ı	ı	I
d-cha acid	ပ်	1	ı	40	í	ı	1	ı	10
nche	ီ၁	50	ı	1	ı	75	1	100	ı
Bra	c <sub>2</sub>	ı	50	40	75	l	65	ſ	40
in	C <sub>18</sub>		10	10	1	ı	1	ı	ŀ
t cha acid	C <sub>12</sub>	ı	10	ı	ı	10	ı	ı	1
raigh Eatty	ညီ	20	1	t	20	Z.	10	ı	10
Stı	င်	30	30	10	ı	ı	1	i	ı
Item	Ester	A-1	A-2	A-3	A-4	A-5	A-6	A-7	A-8
	Straight chain Branched-chain Polybasic acid Satty acid fatty acid	Item Straight chain Branched-chain Polybasic acid fatty acid fatty acid $C_5 \mid C_8 \mid C_{12} \mid C_{18} \mid C_7 \mid C_8 \mid C_9 \mid C_{18} \mid C_{18} \mid C_7 \mid C_8 \mid C_9 \mid C_{18} \mid C_{18} \mid C_9 \mid C_{18} $	Item Straight chain Branched-chain Polybasic acid $\frac{\text{Dynamic}}{\text{viscosity}}$ C <sub>5</sub> C <sub>8</sub> C <sub>12</sub> C <sub>18</sub> C <sub>7</sub> C <sub>8</sub> C <sub>9</sub> C <sub>18</sub> adipic acid sebacic acid $\frac{\text{Dynamic}}{\text{at } 40^{\circ}\text{C}}$	Item         Straight chain         Branched-chain         Polybasic acid         Dynamic viscosity at 40°C           C <sub>5</sub> C <sub>8</sub> C <sub>12</sub> C <sub>8</sub> C <sub>7</sub> C <sub>8</sub> C <sub>9</sub> C <sub>18</sub> C <sub>18</sub> C <sub>9</sub> C <sub>18</sub> <td>Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C         CA           1         C<sub>5</sub>         C<sub>8</sub>         C<sub>12</sub>         C<sub>7</sub>         C<sub>8</sub>         C<sub>9</sub>         C<sub>18</sub>         C<sub>18</sub>         C<sub>19</sub>         C<sub>19</sub>         C<sub>19</sub>         C<sub>10</sub>         C<sub>10</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>1</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>2</sub>         C<sub>3</sub>         C<sub>4</sub>         C<sub>4</sub></td> <td>Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C         Canal Anneholus         Carrendate Anneholus</td> <td>Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic viscosity at 40°C         Canadia at 40°C         Cat.         Cat.</td> <td>Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C (Ascosity) acid         Cs         Cs&lt;</td> <td>Item         Stratight scident         Prinched - Chain         Polybasic acid         Dynamic viscosity at 40°C (A at ty acid         Cs         Cs&lt;</td>	Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C         CA           1         C <sub>5</sub> C <sub>8</sub> C <sub>12</sub> C <sub>7</sub> C <sub>8</sub> C <sub>9</sub> C <sub>18</sub> C <sub>18</sub> C <sub>19</sub> C <sub>19</sub> C <sub>19</sub> C <sub>10</sub> C <sub>10</sub> C <sub>1</sub> C <sub>2</sub> C <sub>3</sub> C <sub>4</sub>	Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C         Canal Anneholus         Carrendate Anneholus	Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic viscosity at 40°C         Canadia at 40°C         Cat.         Cat.	Item         Straight chain         Branched-chain         Polybasic acid         Polybasic acid         Dynamic at 40°C (Ascosity) acid         Cs         Cs<	Item         Stratight scident         Prinched - Chain         Polybasic acid         Dynamic viscosity at 40°C (A at ty acid         Cs         Cs<

Note) Amount of starting material was represented by mol%.

# Table 2

	Type	Trade name	Color (ASTM)	Dynamic viscosity at 40 °C (cSt)
B-1	PAG 1	Adekapol M-30 1)	L 0.5	32.8
B-2	PAG 1	Adekapol M-110 2)	L 0.5	105.2
B-3	PAG 1	Adekapol MH-50 3)	L 0.5	54.6
C-1	ester	dioctyl sebacate	L 0.5	11.4
C-2	ester	Unistar MB-816 4)	L 0.5	8.1

1) polyoxypropylene glycol monoalkyl ether

- 2) polyoxypropylene glycol monoalkyl ether
- 3) polyoxyethylene propylene glycol monoalkyl ether4) monoester of 2-ethylhexanol and palmitic acid

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		Hygroscopicity (water content,	( wdd	320	335	309	317	364	371	315	330	1600	1200	2100	340	365	
	:y	erant 134a	sludge	none	none	none	none	none	none	none	none	none	none	none	none	none	
	stability	refrigerant HFC-134a	color (ASTM)	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	
	Thermal s	erant 12	sludge	none	none	none	none	none	none	none	none	тапу	many	many	none	none	
	The	refrigerant R-12	color (ASTM)	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	≥0.8	8.0≤	8.0≤	L 1.0	L 1.0	
		Seizuring load	(Kgf)	510	519	555	541	572	603	569	648	430	460	430	570	590	
Table 3	separation	ature 3)	high temperature	** ≥08	≥08	>08	>08	≥08	≥08	≥08	≥08	67	insoluble	53	insoluble	insoluble	
	Two-phase separation	temperature (°C)	low temperature	<-50 *	<>	<-50	50	-45	-41	<->0<->	-36	<-50	insoluble	<-50	insoluble	insoluble	higher than -50°C lower than 80°C
		Dielectric constant	(A·cm)	$7.5 \times 10^{12}$	$6.1\times10^{12}$	$4.9 \times 10^{13}$	$1.7\times10^{13}$	$\textbf{8.0}\times \textbf{10}^{12}$	$5.6 \times 10^{12}$	$2.6  imes 10^{13}$	$4.8 \times 10^{12}$	$2.1 \times 10^7$	2.8 × 10 <sup>7</sup>	<10 <sup>7</sup>	$5.1 \times 10^{12}$	$\textbf{4.3}\times \textbf{10}^{12}$	not higher not lower
		Test	1001	A-1	<b>A</b> -2	A-3	A-4	A-5	A-6	A-7	A-8	B-1	B-2	B-3	C-1	C-2	* *
							Acceptable	Example						Comparative Example			

As seen from Table 3, when the esters according to the invention are compared with the conventional PGA (B-1 - B-3), the electric insulating property represented by the dielectric constant is 100,000 times or more and the two-phase separation at a high temperature is not caused. Furthermore, the seizuring load is excellent and the hygroscopicity is low. The thermal stability is equal in case of the HFC-134a system, but is considerably excellent in case of the R-12 system. This is very advantageous in practical use because the mixing of HFC-134a and R-12 is not avoided at a stage of replacing the refrigerant from R-12 to HFC-

134a.

On the other hand, when the esters according to the invention are compared with the commercially available esters (C-1 - C-2), the two-phase separation temperature is extremely different and the conventional esters are insoluble in HFC-134a. In this point, the molecule designed esters according to the invention have a great merit.

As seen from the above, the esters according to the invention are fairly excellent in the performances as a lubricant as compared with Comparative Examples.

### Examples 9-17

The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with respect to nine esters A-9 - A-17 shown in the following Table 4 (all of which esters were not commercially available but were prepared according to the second invention). The same evaluation as in Example 1 was made to obtain results as shown in the following Table 5.

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Item	Polyvalent alcohol	straight chain fatty acid	branched-chain fatty acid (mol%)	polybasic acid (mol%)	viscosity at 40°C (cSt)	Color (ASTM)
A-9	pentaerythritol		isononanoic acid (100)		125.4	L 0.5
A-10	pentaerythritol。	pentanoic acid (100)	0	•	14.5	L 0.5
A-11	pentaerythritol	propionic acid (70) stearic acid (30)			33.4	L 0.5
A-12	pentaerythritol		2-ethylhexanoic acid (100)		42.3	L 0.5
A-13	pentaerythritol	heptanoic acid (15)	heptanoic acid (15) sobutanoic acid (75)	adipic acid (10)	110.9	L 0.5
A-14	dipentaerythritol	propionic acid (30)	propionic acid (30) 2-ethylhexanoic acid(70)		123.9	L 0.5
A-15	dipentaerythritol	isostearic acid (10)	isostearic acid (10) isobutanoic acid (90)		68.4	L 0.5
A-16	dipentaerythritol	butanoic acid (95)		sebacic acid (5)	89.4	L 0.5
A-17	tripentaerythritol	propionic acid (20)	tripentaerythritol propionic acid (20) 2-ethylhexanoic aid (80)		146.3	L 0.5

Note) Mol% is an amount per total acid.

				Table	2					
			Two-phase separation	separation		Th	Thermal s	stability	.у	
	Test	Dielectric constant	tempeı (°	temperature (°C)	Seizuring load	refrigerant R-12	erant 12	refrigerant HFC-134a	erant 134a	Hygroscopicity (water content,
	TONT TONT	-	low temperature	high temperature	(Kgf)	color (ASTM)	sludge	color (ASTM)	sludge	( wdd
	<b>A</b> -9	6.5×10 <sup>13</sup>	-38	≥08	641	L 1.0	none	L 1.0	none	292
	A-10	$1.2 \times 10^{13}$	<-50	≥08	524	L 1.0	none	L 1.0	none	319
	A-11	7.6 $\times$ 10 <sup>12</sup>	≥-50	≥08	541	L 1.0	none	L 1.0	none	344
Acceptable Example	<b>A</b> -12	$1.7 \times 10^{13}$	<b>≤−50</b>	<b>80</b> ≥	549	r 1.0	none	L 1.0	none	331
	<b>A</b> -13	$4.1\times10^{12}$	-43	<b>80</b> ≥	610	L 1.0	none	L 1.0	none	348
	A-14	$2.6 \times 10^{12}$	-40	>08	623	L 1.0	none	L 1.0	none	325
	A-15	$1.4 \times 10^{13}$	<-50	VI 08	581	L 1.0	none	L 1.0	none	339
	<b>A</b> -16	$5.1 \times 10^{12}$	<-50	80 ≥	602	L 1.0	none	L 1.0	none	358
	A-17	4.5 $ imes$ 10 $^{12}$	-31	≥08	654	L 1.0	none	L 1.0	none	324

As seen from Table 5, when the esters according to the invention are compared with the conventional PGA (B-1 - B-3) shown in Tables 2 and 3, the electric insulating property represented by the dielectric constant is 100,000 times or more and the two-phase separation at a high temperature is not caused. Furthermore, the seizuring load is excellent and the hygroscopicity is low. The thermal stability is equal in case of the HFC-134a system, but is considerably excellent in case of the R-12 system. This is very advantageous in practical use because the mixing of HFC-134a and R-12 is not avoided at a stage of

replacing the refrigerant from R-12 to HFC-134a.

On the other hand, when the esters according to the invention are compared with the commercially available esters (C-1 - C-2) shown in Tables 2 and 3, the two-phase separation temperature is extremely different and the conventional esters are insoluble in HFC-134a. In this point, the molecule designed esters according to the invention have a great merit.

As seen from the above, the esters according to the invention are fairly excellent in the performances as a lubricant as compared with Comparative Examples.

The HFC-134a has been mentioned as a possible replacement for R-12 and is used for car air conditioner, refrigerator and the like. Particularly, in case of the car air conditioner, the compressor is driven in summer season, so that the compatibility between oil and refrigerant at high temperature becomes important. When the two-phase separation between oil and refrigerant is caused in the compressor during the driving, the refrigerant having a larger specific gravity remains in the lower portion of the compressor, resulting in the occurrence of compressor seizuring.

In case of the refrigerator, the motor is included in the compressor, so that leakage of electricity comes into problem. In this connection, the esters according to the invention have a dielectric constant higher by 100,000 times or more than that of the conventional PAG and are excellent in the electric insulating property, so that they can be said to be a refrigeration lubricant for the refrigerator.

Concretely, lubricants having a dynamic viscosity of 10-50 cSt at 40 °C are used as a lubricant for the refrigerator requiring a two-phase separation temperature of not higher than -40 °C, so that the esters A-10, A-11 and A-12 are particularly suitable therefor. On the other hand, lubricants having a dynamic viscosity of 80-150 cSt at 40 °C are used as a lubricant for the car air conditioner requiring a two-phase separation temperature of not higher than -20 °C, so that the esters A-9, A-13, A-14, A-16 and A-17 are particularly suitable therefor.

## 25 Examples 18-25

The performances as a refrigeration lubricant using HFC-134a as a refrigerant were evaluated with respect to eight esters A-18 - A-25 shown in the following Table 6 (all of which esters were not commercially available but were prepared according to the third invention). The same evaluation as in Example 1 was made to obtain results as shown in the following Table 7.

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5	Dynamic viscosity at 40°C (cSt)	17.9	84.1	105.4	15.1	18.2	20.4	19.1	15.4
10	Color (ASTM)	L 0.5	L, 0.5	L 0.5	L 0.5	L 0.5	L 0.5	L 0.5	L 0.5
15	Polybasic acid		azelaic acid (5)	sebacic acid (10)		1	ļ		
20	ty acid	acid (100)	-		100)	0) (50)	(30)	acid (100)	(60) c acid (40)
30 September 25	Monovalent fatty acid	2-ethylhexanoic	2-ethylhexanoic acid (95,)	2-ethylhexanoic acid (90)	heptanoic acid (100)	octanoic acid (50) isononanoic acid (	nonanoic acid (70) isononanoic acid (30)	2-ethylhexanoic acid (100)	heptanoic acid (( 2-ethylhexanoic a
35	alcohol	ethane	ethane	ethane	ethane	ethane	ethane	propane	propane
40	Polyvalent	trimethylol	trimethylol	trimethylol	trimethylol	trimethylol	trimethylol	trimethylol	trimethylol
45	Item	A-18	A-19	A-20	A-21	A-22	A-23	A-24	A-25

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Note) numerical value in parenthesis is mol% per total fatty acid

5			Hygroscopicity (water content,	( mgg	324	368	359	317	326	333	319	321
10		Υ.	erant 134a	sludge	none	none	none	none	none	none	none	none
		stability	refrigerant HFC-134a	color (ASTM)	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0
15		Thermal s	erant 12	sludge	none	none	none	none	none	none	none	none
		Th	refrigerant R-12	color (ASTM)	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0	L 1.0
20			Seizuring load	(Kgf)	564	612	641	541	550	581	534	519
25	Table 7	separation	ature	low high temperature	≥08	80≤	≥08	≥08	80≤	≥08	≥08	80≤
30		Two-phase separation	temperature (°C)	low temperature	<->20	-30	-28	-41	<-50	-38	<>	<-50
35			Dielectric constant	(A.cm)	5.6 × 10 <sup>12</sup>	$1.9 \times 10^{12}$	$\textbf{2.8}\times\textbf{10}^{12}$	$7.6 \times 10^{12}$	$5.9 \times 10^{12}$	$3.1 \times 10^{13}$	$8.6  imes 10^{12}$	$4.3 \times 10^{12}$
40			Test	Tabricant	A-18	A-19	A-20	A-21	A-22	A-23	A-24	A-25
45								Acceptable Example				

As seen from Table 7, when the esters according to the invention are compared with the conventional PGA (B-1 - B-3) shown in Tables 2 and 3, the electric insulating property represented by the dielectric constant is 100,000 times or more and the two-phase separation at a high temperature is not caused. Furthermore, the seizuring load is excellent and the hygroscopicity is low. The thermal stability is equal in case of the HFC-134a system, but is considerably excellent in case of the R-12 system.

Recently, HFC-134a causing substantially no breakage of ozone layer is closed up instead of R-12 widely used as a refrigerant in order to cope with the breakage of ozone layer through chlorofluorocarbon

and hydrochlorofluorocarbon being a greatest problem in world-wide scale, but is poor in the compatibility with the conventional refrigeration lubricant, which is a bar for the development of replacement system. However, the refrigeration lubricants according to the invention have a sufficient compatibility with HFC-134a as a refrigerant and a high electric insulating property and also are excellent in the total performances, so that they have an effect that the conventional systems can be used as they are even when HFC-134a is used instead of the conventional R-12 and R-22 as a refrigerant.

### Claims

- **1.** Use of a lubricant for compressors using a hydrofluorocarbon refrigerant containing no chlorine, comprising as a main component an ester(s) obtained by reacting (a) neopentyl glycol with (b) at least one branched-chain monovalent saturated fatty acid having a carbon number of 3-18, wherein said ester has a total acid value of not more than 3 mg KOH/g and a hydroxyl value of not more than 50 mg KOH/g.
  - **2.** Use of a lubricant according to claim 1, wherein said branched-chain monovalent saturated fatty acid is one having a carbon number of 7-9.
- 3. Use of a lubricant according to claim 1, wherein said branched-chain monovalent saturated fatty acid is at least one selected from the group consisting of isoheptanoic acid, 2-ethylhexanoic acid and 3,5,5-trimethylhexanoic acid.
  - **4.** Use of a lubricant according to claim 1, wherein said hydrofluorocarbon refrigerant is 1,1,1,2-tretrafluoroethane.



## **EUROPEAN SEARCH REPORT**

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Category	of relevant ps	ndication, where appropriate, ssages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
T	WO-A-9 201 030 (HEN * page 1, line 1 - 1-5,13-18; table 2	page 8, line 32; claims	1-4	C10M105/38 C10M171/00 //C10N40:00
P,Y	US-A-4 851 144 (PH. *ABSTRACT; COLUMN 1, 2,LINE 46; COLUMN 4, 1; CLAIMS 7,8,10,13- & EP-A-0 378 176 (T COMPANY)	LINE 10 TO COLUMN LINES 10-18;TABLE 15*	1,2,4	
Y	EP-A-0 272 575 (HEN * the whole documen		1-3	
Y	Derwent Publication AN 80-68649C & JP-A-55 105 644 ( * abstract *	s Ltd., London, GB; NIPPON OILS & FATS KK)	1-4	
Y	US-A-4 826 633 (D.D. * column 2, line 9 claims 1,2,14,17-19	- column 3, line 45;	1-3	TECHNICAL FIELDS SEARCHED (Int. Cl.5)
A	US-A-4 234 497 (M. * column 2, line 36 claims 2,4; example	- column 3, line 60;	1-3	C10M
	The present search report has be	peen drawn up for all claims  Date of completion of the search		Examiner
7	THE HAGUE	19 FEBRUARY 1993		FISCHER W.H.F.
X : par Y : par doc	CATEGORY OF CITED DOCUME ticularly relevant if taken alone ticularly relevant if combined with an unment of the same category hnological background	E : earlier patent do after the filing d	cument, but pub ate in the applicatio or other reasons	lished on, or n

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