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DE FR GB IT(71) Applicant: Hashimoto, Koji
2-25-5, Shogen Izumi-ku
Sendai-shi Miyagi(JP)
Applicant: YOSHIDA KOGYO K.K.
No. 1 Kanda Izumi-cho Chiyoda-ku
Tokyo(JP)(72) Inventor: Hashimoto, Koji
2-25-5, Shogen, Izumi-ku
Sendai-shi, Miyagi(JP)
Inventor: Kim, Jinhan
4-25-14-203, Moniwadai, Taihaku-ku
Sendai-shi, Miyagi(JP)
Inventor: Yoshioka, Hideaki
4016, Mikkaichi
Kurobe-shi, Toyama(JP)
Inventor: Habazaki, Hiroki
101 Midoriso, 2-13-26, Kunimi, Aoba-ku
Sendai-shi, Miyagi(JP)
Inventor: Kawashima, Asahi
37-17, Hiyoridai, Taihaku-ku
Sendai-shi, Miyagi(JP)
Inventor: Asami, Katsuhiko
2-5-3, Taihaku, Taihaku-ku
Sendai-shi, Miyagi(JP)(74) Representative: Patentanwälte Leinweber &
Zimmermann
Rosental 7/II Aufg.
D-80331 München (DE)

(54) Highly corrosion-resistant amorphous aluminum alloy.

(57) A highly corrosion resistant amorphous aluminum alloy which consists of more than 7 to not more than 55 atomic %, in total, of Cr, at least one element selected from the group consisting of Mo and W, at least one element selected from the group consisting of Ta, Nb and Ti and at least one element selected from the group consisting of Mg, Fe, Co, Ni and Cu, the total of Cr and at least one element selected from the group consisting of Mo and W being 7 atomic % or more, the balance being substantially Al. The amorphous aluminum alloy has excellent characteristics such as ultrahigh corrosion resistance and high corrosion resistance at high temperatures and is self-passivated by the formation of a stable protective film even in a Cl⁻ ion-containing solution which is a severe corrosive environment for Al.

BACKGROUND OF THE INVENTION1. Field of the Invention

5 The present invention relates to novel amorphous aluminum alloys which have excellent characteristics such as ultrahigh corrosion resistance and high corrosion resistance at high temperatures and which are useful in a variety of fields including domestic uses as well as industrial uses such as a chemical process plant.

10 2. Description of the Prior Art

The present inventors have found various amorphous alloys having high corrosion resistance that could never have been embodied with any of crystalline alloys. These amorphous alloys are broadly classified into metal-semimetal alloys and metal-metal alloys. The metal-semimetal alloy comprises an iron group element such as Fe, Co or Ni and a semimetal element such as P, C, B or Si in an amount of 10 to 25 atomic % which is necessary for amorphization. The high corrosion resistance of the metal-semimetal alloy is embodied by the addition of Cr thereto. On the other hand, the metal-metal alloy comprises an element such as Fe, Co, Ni, Cu or Al and a valve metal belonging to the group IVa or Va metals, such as Ta, Nb, Zr or Ti. The corrosion resistance of the metal-metal alloy is due to the valve metal which constitutes the amorphous alloy. Among the alloys, those containing Ta or Nb of the group Va are extremely corrosion resistant.

As mentioned hereinbefore, the amorphous alloy containing an effective amount of Cr for high corrosion resistance entails a semimetal element for amorphization, while the amorphous metal-metal alloy has been embodied only by those comprising the elements belonging to the different groups each lying relatively apart from each other in the Periodic Table. On the other hand, Al is attacked by both acid and alkali and easily subjected to pitting corrosion in the presence of chlorine ions even in a neutral environment. It is expected that a highly corrosion resistant aluminum alloy may be obtained if a single phase alloy is materialized by the addition of Cr, which plays a role in attaining corrosion resistance, or a corrosion resistant element other than Cr to relatively less corrosion resistant Al.

30 An alloy is usually crystalline in a solid state, but is brought into an amorphous state that is similar to liquid structure without having any crystallinity by, for example, ultrarapid cooling solidification of an alloy having a specific composition from the molten state or sputtering deposition by the use of a given target, that is, by a method wherein any long period regularity in the atomic arrangement is not formed in the course of solid formation. The alloy thus obtained is termed "amorphous alloy". An amorphous alloy is a 35 homogeneous single-phase alloy consisting of a supersaturated solid solution, possesses a markedly high strength as compared with conventional practical metals and exerts a variety of characteristics such as extraordinarily high corrosion resistance depending upon the composition thereof.

The present inventors have created new amorphous alloys and made an extensive research on the properties. As a result, they have found that an amorphous alloy composed of a low melting metal and a 40 high melting metal can be produced by the sputtering method which can dispense with melting in the course of alloy formation, and succeeded in the production of amorphous alloys each comprising a group IVa, Va or VIa metal, such as Ti, Nb, Ta, Mo or W, and a group Ib or IIIb metal, such as Cu or Al. Some of them were filed as Japanese Patent application Nos. 51568/1988 (filed on the basis of Application No. 103296/1987), 51567/1988 and 260020/1988 which have been laid open to public inspection under Laid-45 Open Nos. 25934/1989, 225737/1989 and 107750/1990, respectively.

They have continued the research and made an attempt to produce a highly corrosion resistant metal-metal amorphous alloy comprising metals belonging to the close groups of the Periodic Table. As a result, they have succeeded in the production of amorphous alloys, one comprising Ti or Zr of the group IVa and Cr of the group VIa, and the other comprising Ta or Nb of the group Va and Cr of the group VIa, and have 50 applied for patents as Japanese Patent Application Nos. 138575/1991 (Laid-Open No. 337053/1992) and 3-267542.

The present inventors have further continued the research and investigated the production conditions for amorphous alloys. As a result, they have succeeded in the production of a highly corrosion resistant amorphous aluminum alloy comprising Al, that is, a low melting-point and light-weight metal and Cr, and 55 other amorphous aluminum alloys containing, in addition to Al and Cr, various elements which further improve corrosion resistance, thus accomplishing the present invention.

SUMMARY OF THE INVENTION

The present invention provides an amorphous aluminum alloy which is obtained by adding to Al, Cr that is indispensable for imparting a high corrosion resistance to an amorphous alloy comprising an iron group element as a principal component, Mo and W that can take the place of Cr, and Ta, Nb, Ti, Mg, Fe, Co, Ni and Cu that are effective in materializing a corrosion resistant metal-metal amorphous alloy.

The present invention relates to a highly corrosion resistant amorphous aluminum alloy which consists of more than 7 to not more than 55 atomic %, in total, of Cr, at least one element selected from the group consisting of Mo and W, at least one element selected from the group consisting of Ta, Nb and Ti and at least one element selected from the group consisting of Mg, Fe, Co, Ni and Cu, the total of Cr and at least one element selected from the group consisting of Mo and W being 7 atomic % or more, the balance being substantially Al.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic illustration of one example of the sputtering device to be used for preparing the amorphous alloy of the present invention.

FIG. 2 is a schematic illustration of another example of the sputtering device to be used for preparing the amorphous alloy of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The sputtering method is one of the methods for producing an amorphous alloy. An amorphous alloy is produced by the sputtering method in which a target comprising a plurality of crystalline phases instead of a single phase which have the same average composition as that of the amorphous alloy to be produced is prepared by sintering, melting or the like and brought into use, or alternatively a metallic plate comprising the principal components of the amorphous alloy to be produced and having the element to be alloyed placed thereon or embedded therein is employed.

In the present invention, the above-mentioned method is utilized and improved as will be described hereunder.

Although it is not so easy to produce a Cr-Al alloy target by the melting method or the like, a highly corrosion resistant amorphous Al-Cr alloy is obtained by the sputtering method using a target comprising an Al plate and a Cr lump placed thereon or embedded therein. In this method, for the purpose of preventing nonuniformity from occurring in the amorphous alloy to be formed depending on the position, it is desirable that, for example, as shown in FIG. 1, a plurality of substrates 2 in a sputtering device chamber 6 be allowed to revolve about the central axis 1 of the chamber and, at the same time, the substrates themselves be allowed to rotate on their axes 7. Moreover, in order to vary the compositions of the amorphous alloys to be formed in a wide range, as shown in FIG. 2 for example, one target 4 made of Cr and the other target 5 made of Al are obliquely placed and allowed to simultaneously act by means of two power sources while regulating each output, and the substrate 2 is located near the intersection of normals of the centers of the targets 4 and 5. By the above-mentioned method, the concentration of each element in the amorphous alloy to be formed can be arbitrarily varied. Further, as a variation of this method, by the combination of various targets with this method, for example, by the use of an Al-plate target having Ta, Nb, Ti, Fe, Co, Ni, Cu, Mo, W or the like embedded therein, it is possible to obtain highly corrosion resistant amorphous alloys such as Al-Cr-Mo-Nb-Co-Ni, Al-Cr-W-Ti-Fe-Ni, Al-Cr-Mo-Nb-Cu, Al-Cr-W-Ta-Mg, Al-Cr-W-Ta-Cu, Al-Cr-Mo-Ta-Co, Al-Cr-Mo-Ta-Fe, Al-Cr-W-Nb-Ni, Al-Cr-Mo-Ti-Co-Cu, Al-Cr-W-Nb-Mg-Ni, Al-Cr-Mo-Ta-Ni-Cu, Al-Cr-W-Ti-Mg-Fe and Al-Cr-Mo-W-Ta-Nb-Ti-Fe-Co-Ni-Cu. In the method wherein two targets are simultaneously employed, both revolution and rotation of the substrate are particularly necessary in order to form a homogeneous amorphous alloy.

The amorphous alloy having the composition of the present invention which is prepared by the sputtering method is a single-phase amorphous alloy in which the above-mentioned elements form a uniform solid solution. A protective film assuring an extreme uniformity and high corrosion resistance can be formed onto the homogeneous solid solution amorphous alloy. Since a metallic material is easily dissolved in a solution which is extremely corrosive and poor in oxidative power, such as hydrochloric acid, it is necessary that the metallic material have a capability of forming a secure protective film in order that it may be used in such an environment. This situation can be materialized by the formation of an alloy containing required amounts of effective elements. In the case of a crystalline metal, however, the addition of large amounts of various alloying elements thereto sometimes gives rise to a polyphase structure having different

chemical properties without forming a uniform protective film securing high corrosion resistance, thereby failing to achieve a prescribed corrosion resistance. In addition, the occurrence of chemical nonuniformity is rather detrimental to corrosion resistance.

On the other hand, since the amorphous alloy of the present invention is a uniform solid solution and

5 uniformly contains effective elements in amounts required for the formation of a secure protective film, the alloy exhibits a sufficiently high corrosion resistance by virtue of the uniformly formed protective film. The condition to be given to a metallic material capable of withstanding a severely corrosive environment is a capability of uniformly forming a high protective stable film on the material even in a nonoxidative environment. The aforementioned requirement is materialized by the alloy compositions according to the
10 present invention. Moreover, amorphous alloys having intricate compositions can be formed in a single-phase solid solution and the formation of a uniform protective film can be assured.

Now, the reasons for restricting the compositions of the alloys of the present invention will be described.

Cr is an element which constitutes an amorphous structure when it coexists with Al. Mo and W belong

15 to the group VIa elements as is the case with Cr and, therefore, can substitute Cr and are effective in improving the corrosion resistance of the alloy in an acid. In order to constitute the amorphous structure, the total amount of Cr and at least one of Mo and W is required to be 7 atomic % or more.

When Cr or Cr and some of the group VIa elements other than Cr, i.e., at least one of Mo and W, are replaced with at least one element selected from among Ta, Nb and Ti and further with at least one

20 selected from among of Mg, Fe, Co, Ni and Cu, the corrosion resistance of the alloy is further enhanced. When, however, Cr is not contained, failure to add a large amount of at least one of Ta, Nb and Ti, and at least one of Mg, Fe, Co, Ni and Cu does not constitute an amorphous structure. Accordingly, even when at least one of Ta, Nb and Ti and at least one of Mg, Fe, Co, Ni and Cu are contained in the alloy, the sum of Cr and the other group VIa elements, i.e., at least one of Mo and W, need be contained in an amount of 7
25 atomic % or more to obtain an amorphous structure. In the case where the sum of Cr and the other group VIa elements other than Cr is contained in an amount of 7 atomic % or more, the total amount of at least one element selected from among Ta, Nb and Ti, and at least one selected from among of Mg, Fe, Co, Ni and Cu and the group VIa elements shall be 55 atomic % or less.

Now the present invention will be described with reference to Examples.

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Example 1

A target was prepared by placing discs made of Cr, Mo, Nb, Co, Ni and alloys thereof, each having a diameter of 20 mm and a thickness of 1 mm, on an Al disc with a diameter of 100 mm and a thickness of 6
35 mm in such a manner that the centers of the Cr or other discs were arranged on the circumference of a circle having a radius of 29 mm and the same center as that of the Al disc. Using the thus prepared target, each of substrates made of aluminum or glass was subjected to sputtering deposition while being revolved and rotated by the use of the apparatus as shown in FIG. 1 maintained at a vacuum of 2×10^{-4} Torr with argon allowed to flow at a flow rate of 5 ml/min. As a result of X-ray diffractometry, the alloy thus formed
40 was confirmed to be amorphous, and analysis with an X-ray microanalyzer revealed that the alloy composition was Al-15Cr-3Mo-18Nb-6Co-3Ni alloy. The alloy was self-passivated in a neutral solution containing Cl⁻ ions at 30 °C and the weight loss thereof due to corrosion was undetectable even after one-month immersion therein and even by the use of a microbalance.

45 Example 2

A target was prepared by placing discs made of Cr, W, Ti, Fe, Ni and alloys thereof, each having 20 mm diameter and 1 mm thickness, on an Al disc with 100 mm diameter and 6 mm thickness in such a manner that the centers of the Cr and other discs were arranged on the circumference of a circle having 29
50 mm radius and the same center as that of the Al disc. The thus prepared target was used in the following sputtering deposition. Each of substrates made of aluminum or glass was subjected to sputtering deposition while being revolved and rotated by the use of the apparatus as shown in FIG. 1 maintained at a vacuum of 2×10^{-4} Torr with argon allowed to flow at a flow rate of 5 ml/min. As a result of X-ray diffractometry, the alloy thus formed was confirmed to be amorphous, and analysis with an X-ray microanalyzer revealed that
55 the alloy composition was Al-21Cr-2W-20Ti-5Fe-4Ni alloy. The alloy was self-passivated in a neutral solution containing Cl⁻ ions at 30 °C and the weight loss thereof due to corrosion was undetectable even after one-month immersion therein and even by the use of a microbalance.

Example 3

Targets were prepared by placing discs made of Cr and other various metals and alloys, each having 20 mm diameter and 1 mm thickness, on an Al disc with 100 mm diameter and 6 mm thickness in such a 5 manner that the Cr or other discs were arranged on the circumference of a circle having 29 mm radius and the same center as that of the Al disc. The thus prepared targets were used in the following sputtering deposition. Each of substrates made of aluminum or glass was subjected to sputtering deposition while being revolved and rotated by the use of the apparatus as shown in FIG. 1 maintained at a vacuum of 5×10^{-3} to 1×10^{-4} Torr with argon allowed to flow at a flow rate of 5 ml/min. As a result of X-ray 10 diffractometry, the alloys thus formed were confirmed to be amorphous, and the results of analysis with an X-ray microanalyzer were as given in Table 1. These alloys were subjected to corrosion test in a buffer solution containing 0.5 N NaCl at 30°C and pH 8.4 to reveal that they were self-passivated in a neutral solution containing Cl⁻ ions at 30°C and highly corrosion resistant alloys.

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Table 1

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Alloy (atomic %)	Corrosion state
Al-15Cr-3Mo-18Nb-6Co-3Ni	unchanged
Al-21Cr-2W-20Ti-5Fe-4Ni	unchanged
Al-22Cr-18W-10Ta-5Cu	unchanged
Al-3Cr-4Mo-30Ta-12Co	unchanged
Al-12Cr-18Mo-10Ta-15Fe	unchanged
Al-10Cr-10W-15Nb-10Ni	unchanged
Al-4Cr-3Mo-5Ta-11Ni-2Cu	unchanged
Al-7Cr-3Mo-30Ti-3Co-11Cu	unchanged
Al-5Cr-2W-5Nb-12Mg-25Ni	unchanged
Al-8Cr-10W-10Ti-3Mg-12Fe	unchanged

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As detailed hereinbefore, the amorphous alloy according to the present invention is one containing Al and Cr as the essential components and easily producible by the sputtering method. It is also corrosion resistant alloy which is self-passivated by the formation of a stable protective film even in a Cl⁻ ion-containing solution which is a severe corrosive environment for Al.

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Claims

1. A highly corrosion resistant amorphous aluminum alloy which consists of more than 7 to not more than 55 atomic %, in total, of Cr, at least one element selected from the group consisting of Mo and W, at least one element selected from the group consisting of Ta, Nb and Ti and at least one element selected from the group consisting of Mg, Fe, Co, Ni and Cu, the total of Cr and at least one element selected from the group consisting of Mo and W being 7 atomic % or more, the balance being substantially Al.

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FIG.1

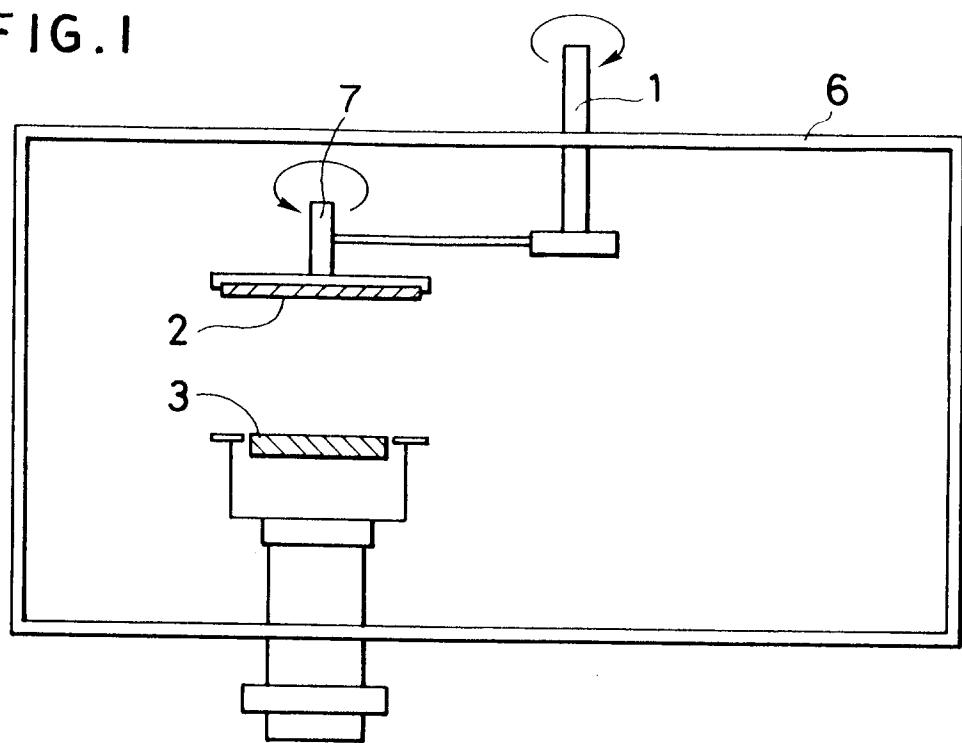
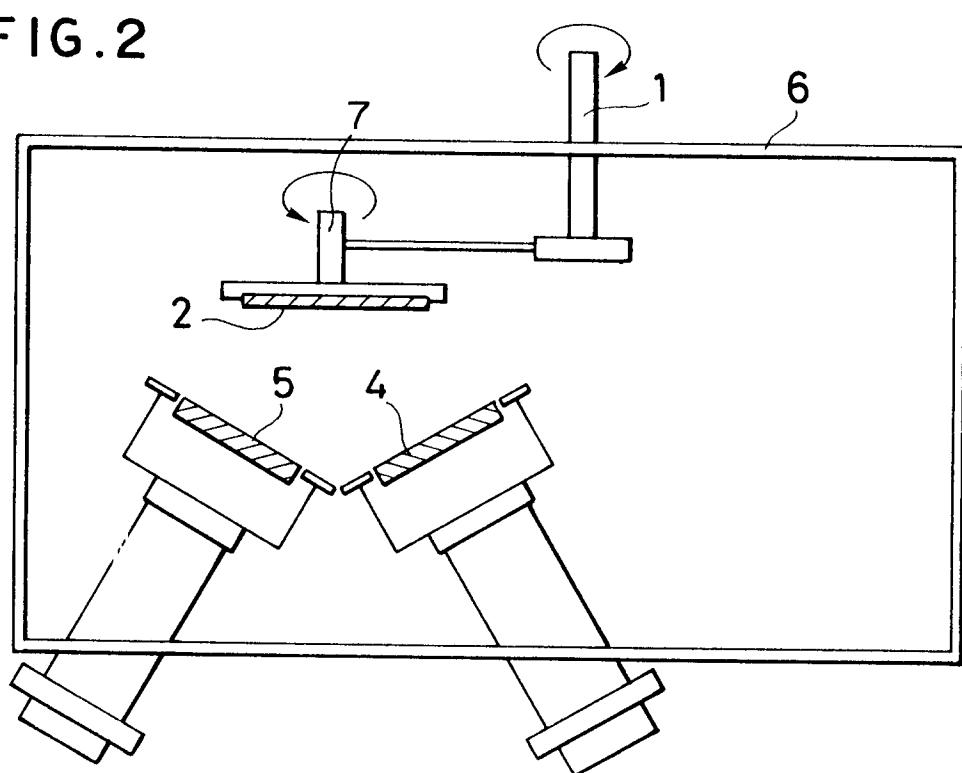


FIG.2





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 93 10 2487

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	US-A-4 347 076 (R. RAY ET AL) * example 42 * ---	1	C22C45/08
X	PATENT ABSTRACTS OF JAPAN vol. 11, no. 232 (C-437) 29 July 1987 & JP-A-62 047 448 (TOYO ALUM K.K.) 2 March 1987 * abstract * ---	1	
A	GB-A-2 196 647 (H. JONES ET AL) * claim 1; table 1 * ---	1	
A	EP-A-0 303 100 (YOSHIDA KOGYO K.K.) * claims 1,2; table 1 * ---	1	
A	WO-A-9 114 013 (SUMITOMO ELECTRIC INDUSTRIES LTD) * table 1 * ---	1	
A	EP-A-0 458 029 (YOSHIDA KOGYO K.K.) * claim 1; table 1 * ---	1	
A	CHEMICAL ABSTRACTS, vol. 107 Columbus, Ohio, US; SCHARF, G. ET AL. 'Preparation of wrought aluminum alloys from rapidly solidified powders' * abstract * & METALL (BERLIN), 41(6), 608, 611-16 1987, -----	1	TECHNICAL FIELDS SEARCHED (Int. Cl.5) C22C
<p>The present search report has been drawn up for all claims</p>			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	13 APRIL 1993	GREGG N.R.	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			