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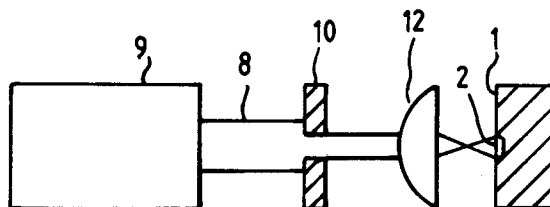
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(54) **A defect compensation method for smoothing a surface of a transparent plate.**

(57) A defect compensation method for smoothing a surface of a transparent plate by radiating an ArF excimer laser beam to a defect at the surface. The ArF excimer laser beam is radiated by use of a mask having an opening which is shaped in accordance with the shape of the defect, through a lens, or while the size of the beam at the defect is changed to a plurality of values. As the mask, an iris mask having an opening which is larger than the defect is usable. The size of the beam is changed by exchanging a plurality of masks each having an opening of a different size from one another, or by use of a mask having a plurality of openings of different sizes. Alternatively, the ArF excimer laser beam is radiated so as to have an energy which is high at a center and low at a periphery of the defect. Or, the ArF excimer laser beam has a smaller size than the size of the defect, and the transparent plate having the defect is moved so as to allow different portions of the defect to be irradiated sequentially by the ArF excimer laser beam and simultaneously the

number of shots of the ArF excimer laser beam is changed.

**FIG. 6**

BACKGROUND OF THE INVENTION

1. Field of the Invention:

The present invention relates to a defect compensation method for compensating for a defect generated at a surface of a plate formed of a transparent material such as glass without spoiling the light transmitting property thereof. In particular, the present invention relates to a defect compensation method for compensating for a microscopic concave defect at a display plane of a display apparatus such as a liquid crystal display apparatus.

2. Description of the Related Art:

When a linear or point concave defect such as a flaw, a scratch, a crack or the like is generated at a display plane of a display apparatus or the like, light radiated to the display plane is scattered or reflected by the defect, thereby adversely effecting the resultant display. In order to avoid such an inconvenience, defect compensation is performed for avoiding such a concave defect from effecting the display.

Conventionally, the defect compensation is performed in the following manner. By rotating a buff or the like coated with fine rubbing powders or by rotating a grinder coated with a rubbing liquid including rubbing powders, a portion including the concave defect is mechanically rubbed and thus removed by friction. Since such methods involve the following problems, a surface obtained by this type of defect compensation is not satisfactory. Hereinafter, the surface obtained by the defect compensation will be referred to as a "processed surface".

(1) Powders chipped away from the display plane formed of glass or the like and the rubbing powders splashed by rubbing causes problems in terms of cleanliness of the operational environment.

(2) In the case where the display plane is combined with a substrate including an LSI or the like, the LSI may be destroyed by vibration caused by rubbing. Further, static electricity generated by rubbing friction may destroy a thin film transistor or a driving circuit provided in the substrate.

(3) Powders of glass which have been rubbed off or rubbing powders enter the display apparatus to cause a display malfunction.

(4) The rubbing process requires a long period of time, which increases the compensation cost.

(5) Since the display plane treated with rubbing becomes rough with microscopic ruggedness, the light transmitting property of the display

plane is spoiled. This fact provides another display defect.

Recently, the use of excimer laser for smoothing a portion including the defect has been developed. For example, examples of utilization of excimer laser for precise processing of a polymer film or a ceramic material or for marking at a plastic or ceramic material are described in "Excimer Laser niyoru Bisai Kako eno Ohyo (Utilization of Excimer Laser for Precise Processing)" in Ohyo Kikai Kogaku (September, 1990). The processing described in this article is used for forming a hole, cutting, marking or the like, but not for smoothing the processed surface in order to reliably maintain the light transmitting property, which is indispensable for the defect compensation of a transparent plate of a display apparatus.

The use of a laser beam for the defect compensation in a liquid crystal display apparatus has also been developed. For example, Japanese Laid-Open Patent Publication No. 3-126913 discloses a method for separating a pair of substrates of a liquid crystal display apparatus by radiation of a laser beam. This method, according to which the laser beam is transmitted through the substrates, cannot be used for the defect compensation of the substrate itself. Japanese Laid-Open Patent Publication No. 3-265820 discloses a method for compensating for a defect by radiating a laser beam to a surface of a substrate of the liquid crystal display apparatus. According to this method, the surface is roughened to make a portion including the defect non-transparent, but not smoothed. The rough surface obtained by this method does not have a satisfactory light transmitting property, which may provide another defect.

SUMMARY OF THE INVENTION

A defect compensation method for smoothing a surface of a transparent plate according to the present invention is performed by radiating an ArF excimer laser beam to a defect at the surface.

An ArF excimer laser has a wavelength in the range of ultraviolet. By the use of ultraviolet, bonds between atoms of a transparent plate are disbonded. Accordingly, a portion irradiated by the ultraviolet is removed so as to form a substantially smooth surface, and thus the transparent surface maintains a satisfactory light transmitting property.

In the case where the ArF excimer laser beam is radiated while the size of the beam at the defect is changed, or the ArF excimer laser beam is radiated so as to have an energy which is high at a center and low at a periphery of the defect, a processed surface which is deep at a center and gets gradually shallow toward a periphery thereof is obtained.

In the case where the ArF excimer laser beam is radiated through a mask having an opening of the shape corresponding to the shape of the defect, a processed surface which is smooth with no microscopic ruggedness is obtained. Accordingly, the transparent plate maintains a satisfactory light transmitting property. Further, in the case where the degree of focus of the ArF excimer laser beam is changed and also the transparent plate having the defect is moved so as to allow different portions thereof to be irradiated sequentially by the ArF excimer laser beam, a profile or a peripheral edge of a processed surface is unclear. Such a processed surface is satisfactory since the profile is hardly visually recognized as a shadow. The profile of a processed surface can also be made unclear by changing the diameter of an iris mask during the radiation of the ArF excimer laser beam.

Thus, the invention described herein makes possible the advantages of providing a defect compensation method for smoothing a surface of a transparent plate, according to which a defect at a surface of a transparent plate is compensated for without spoiling the light transmitting property of the surface or generating residual powders and in a short period of time.

These and other advantages of the present invention will become apparent to those skilled in the art upon reading and understanding the following detailed description with reference to the accompanying figures.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a cross sectional view of a portion obtained by ArF excimer laser radiation.

Figure 2 is a cross sectional view of a portion obtained by KrF excimer laser radiation.

Figure 3 is a view schematically illustrating ArF excimer laser radiation to a surface of a transparent plate.

Figure 4 is a cross sectional view of a portion obtained by a defect compensation method according to the present invention.

Figure 5 is a cross sectional view of a portion obtained by ArF excimer laser radiation.

Figure 6 is a schematic view of an apparatus for radiating an ArF excimer laser beam used for a defect compensation method according to a second example of the present invention.

Figure 7 is a cross sectional view of a portion obtained by a conventional defect compensation method.

Figure 8 is a schematic view of a profile of a portion obtained by a defect compensation method which is visually recognized as a shadow.

Figure 9 is a schematic view of another profile of a portion obtained by a defect compensation

method which is visually recognized as a shadow.

Figure 10 is a cross sectional view of a portion obtained by the defect compensation method according to the second example of the present invention.

Figure 11 is a view illustrating energy distribution of an ArF excimer laser beam used in a defect compensation method according to a third example of the present invention.

Figure 12 is a cross sectional view of a portion obtained by the defect compensation method according to the third example of the present invention.

Figure 13 is a top view of a portion, to which an ArF excimer laser beam is radiated by a defect compensation method according to a fourth example of the present invention.

Figure 14 is a cross sectional view of a portion along line J-J' of Figure 13 obtained by the defect compensation method according to the fourth example of the present invention.

Figure 15 is a top view of a portion, to which an ArF excimer laser beam is radiated by a defect compensation method according to a fifth example of the present invention.

Figure 16 is a cross sectional view along line K-K' of Figure 15 of a portion obtained by the defect compensation method according to the fifth example of the present invention.

Figure 17 is a schematic view of an apparatus for radiating an ArF excimer laser beam used in a defect compensation method according to a sixth example of the present invention.

Figure 18 is a cross sectional view of a portion obtained by the defect compensation method according to the sixth example of the present invention.

Figure 19 is a timing chart for the defect compensation method according to the sixth example of the present invention.

Figure 20 is a timing chart for a defect compensation method according to a seventh example of the present invention.

Figure 21 is a schematic view of an apparatus for radiating an ArF excimer laser beam used in a defect compensation method according to an eighth example of the present invention.

Figure 22 is a top view of an iris mask used in the defect compensation method according to the eighth example of the present invention.

Figure 23 is a cross sectional view of a mechanism for changing the diameter of the iris mask shown in Figure 22.

Figure 24 is a timing chart for a defect compensation method according to the eighth example of the present invention.

Figure 25 is a cross sectional view of a portion obtained by the defect compensation method ac-

cording to the eighth example of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, the present invention will be described by way of illustrating examples with reference to the accompanying drawings.

When a defect is generated in the form of a point or a line and in various sizes and shapes at a surface of a transparent plate formed of a glass or the like, such a defect has an adverse effect on the quality of a display plane. Figure 3 shows an example of a cross section of such a defect 5 at a transparent plate 1 formed of glass. The defect 5 is compensated for so as to be visually unrecognizable by defect compensation. The defect compensation is performed by radiating an ArF excimer laser beam 8 to the defect 5 or a portion including the defect (hereinafter, referred to as a "defect portion").

An excimer laser emitter is a type of gas laser emitter for emitting a laser beam by use of a rare gas halogen, which forms a compound in an excited state. The excimer laser emitter can emit a laser beam having a wavelength in the range of ultraviolet. The laser beam having a wavelength in the range of ultraviolet has a high energy, and thus realizes processing having the following features.

(1) Since bonds between molecules and atoms are photochemically disbonded, thereby decomposing and thus removing a portion of a surface layer treated with radiation, the surface is exposed to no thermal effect.

(2) Since such a laser beam has the shortest wavelength among various types of laser beams used for processing, processing is possible in the order of microns.

According to the present invention, the ArF excimer laser beam is used for processing for the following reasons.

In processing a transparent material such as glass, a laser beam having a certain range of wavelength is transmitted through the material and cannot disbond the bonds between atoms. In order to avoid such an inconvenience, the excimer laser beam is required to have such a wavelength that allows the laser beam to be absorbed into the surface of the transparent material. Different types of excimer laser beams have different oscillating wavelengths in accordance with the type of gas used. For processing a transparent material such as glass, a KrF excimer laser beam having a wavelength of 248 nm or an ArF excimer laser beam having a wavelength of 193 nm can be used.

Figure 1 is a cross sectional view of a portion processed by use of an ArF excimer laser beam,

and Figure 2 is a cross sectional view of a portion processed by use of a KrF excimer laser beam. Reference numeral 2 denotes a portion receiving the ArF excimer laser beam (hereinafter, referred to as a "radiation portion"), and reference numeral 4 denotes a processed surface.

As is understood by Figures 1 and 2, in the case where the KrF excimer laser beam is used, a processed surface 3 in Figure 2 is rough with microscopic ruggedness. Accordingly, the light transmitting property of the display plane is poor. In contrast, the ArF excimer laser beam has a shorter wavelength than that of the KrF excimer laser beam. Accordingly, processing in a more microscopic order is possible, and thus the material is less effected by heat. As a result, a processed surface 4 in Figure 1 is smooth with no microscopic ruggedness. In this state, the light transmitting property of the display plane is not spoiled.

Example 1

When a defect 5 is generated at a surface of a transparent plate 1 formed of glass or the like as is shown in Figure 3, an ArF excimer laser beam 8 is radiated to the defect 5 from above. Figure 5 shows a cross sectional view of a portion obtained by such defect compensation. As is shown in Figure 5, a processed surface 4 is smooth with no microscopic ruggedness.

Further, by radiating the ArF excimer laser beam 8 to a defect portion including the defect 5 - (accordingly, larger than the defect 5), the defect portion is not wholly removed at one time, but is gradually shaved from an upper portion 7 to a bottom portion 6. Finally, a processed surface 4 which is slightly deep at a center and gets gradually shallower toward a periphery thereof to be continuous to the surface of the transparent plate 1 surrounding the processed surface 4 is obtained as is shown in Figure 4. The resultant processed surface 4 does not have any edge 20, which is obtained in the case shown in Figure 5. Due to the smoothness of the processed surface 4, the light transmitting property of the display plane is not spoiled.

Moreover, since the defect compensation process according to this example requires only a short period of time of several tens of seconds, the compensation cost can be reduced.

Excision of the transparent plate 1 splashes a small amount of powders of glass or the like, but this amount is significantly smaller than the case in which the transparent plate is rubbed by use of rubbing powders. In order to avoid the splashed powders from adhering to the processed surface 4, an area which is not to be irradiated by the ArF

excimer laser beam may be masked by a masking tape or the like.

Still further, a pattern mask may be provided on a path of the laser beam to obtain a desirable beam size and shape. The laser beam may be radiated through a lens to obtain a desirable beam size and intensity.

Example 2

An ArF excimer laser beam **8** is radiated to a defect portion at a surface of a transparent plate **1** formed of glass or the like, by use of a mask imaging method using an apparatus shown in Figure 6.

A pattern mask **10** having an opening formed of a metal plate or the like is provided on a path of the ArF excimer laser beam **8** emitted by an excimer laser emitter **9**. The ArF excimer laser beam **8** is transmitted through the pattern mask **10** and is reduced by a convex lens **12** to be projected and radiated to a radiation portion **2** in a pattern corresponding to the opening of the pattern mask **10**. As the pattern mask **10**, for example, a metal plate having a specified pattern of opening obtained by etching can be used.

In the case where a defect having a width of 0.3 mm or less and a depth of 0.04 mm or less is compensated for, using the apparatus shown in Figure 6, a processed surface **4** shown in Figure 7 is obtained. As is shown in Figure 7, there is an undesirable possibility that an edge **20** of the processed surface **4** is visually recognized as a shadow when observed from above. Especially when the transparent plate **1** is formed of glass, 1,000 or more shots of the ArF excimer laser beam **8** having a radiation energy of 5 J/cm² or higher is required in order to completely compensate for the defect. Accordingly, the undesirable possibility that the edge **20** is recognized as a shadow is high. When the ArF excimer laser beam **8** is projected in a rectangular pattern, a rectangular edge **20** is clearly projected and recognized as a shadow as is shown in Figure 8. When the ArF excimer laser beam **8** is projected in a circular pattern, a circular edge **20** is clearly projected and recognized as a shadow as is shown in Figure 9. Although the light transmitting property of the display plane is maintained due to a smooth processed surface **4** with no microscopic ruggedness, this shadow may provide another display defect.

In this example, the ArF excimer laser beam **8** is radiated in the following manner to make the edge **20** unclear.

One thousand shots or less of the ArF excimer laser beam **8** are radiated to the radiation portion **2** while the size of the beam is changed step by step. As is shown in Figure 10, for example, sev-

eral hundred shots of the ArF excimer laser beam **8** having a size **A** are radiated, then several hundred shots of the ArF excimer laser beam **8** having a size **B** are radiated, and finally several hundred shots of the ArF excimer laser beam **8** having a size **C** are radiated. The beam size can be changed, for example, by using a plurality of the pattern masks **10** having different sizes of openings one after another. Alternatively, a pattern mask having a plurality of openings having different sizes from one another may be provided. In this case, the beam size is changed by allowing the ArF excimer laser beam **8** to be transmitted through the different openings.

In this example, the radiation energy of the ArF excimer laser beam **8** is 40 mJ/cm² for all of the sizes **A**, **B**, and **C**. The sizes **A**, **B**, and **C** are 0.5 mm, 0.4 mm, and 0.3 mm, respectively.

As is shown in Figure 10, the processed surface **4** obtained according to this example is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized as a shadow when observed from above. Moreover, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled. As a result, a satisfactory display plane is obtained.

Further, the defect compensation according to this example takes only 1 minute for each defect on average, in contrast with 10 to 20 minutes in the case of a conventional method. Accordingly, the compensation cost can be reduced.

Still further, substantially no residual powders are generated in contrast with a conventional rubbing method by which rubbing powders are splashed to cause various problems.

Example 3

In this example, an ArF excimer laser beam **8** is radiated to a radiation portion **2** so as to have an energy which is high at a center and low at a periphery of the radiation portion **2**. In this way, a processed surface **4** having no clear edge to be visually recognized as a shadow when observed from above is obtained.

In a usual laser radiation, a part of the laser beam which has a uniform energy level distribution both in an X axis and a Y axis as is indicated by hatching in Figure 11 is used. In this example, a peripheral part of the laser beam where the energy level distribution shows a curve (indicated by mesh) is also used. By radiating such a part of the laser beam **8** to the radiation portion **2**, a processed surface **4** which is slightly deep at a center and gets gradually shallower toward a periphery

thereof is obtained.

In this example, 500 shots of the ArF excimer laser beam **8** having a radiation energy of 40 J/cm² at a center of the radiation portion **2** is radiated. This radiation energy is gradually lowered toward a periphery thereof. As is shown in Figure **12**, the processed surface **4** is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized as a shadow when observed from above. Further, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled. As a result, a satisfactory display plane is obtained. The defect compensation takes only 1 minute for each defect on average, and further no residual powders are generated.

Example 4

A linear defect **5** at a transparent plate **1** formed of glass or the like as is shown in Figure **13** is compensated for by radiating an ArF excimer laser beam **8** while the number of shots of the beam is changed. Figure **14** shows a cross sectional view along line **J-J'** of a portion obtained by the defect compensation.

In more detail, the defect compensation is performed in the following manner.

First, the defect **5** at a surface of the transparent plate **1** is recognized by an image processing apparatus. As is shown in Figure **13**, coordinates of a plurality of points **31**, **32** and **33** are measured with respect to an arbitrary point as an origin. After it is confirmed that the defect **5** is substantially linear, a distance required for the defect compensation is calculated based on the coordinates of the points **31** and **33**, in order to find out by which beam size **A**, **B** or **C** the defect compensation is possible.

Next, a display apparatus having the transparent plate **1** is mounted on a movable stage (not shown), and the ArF excimer laser beam is radiated to the radiation portion **2** while the stage is moved based on the coordinates obtained by the image recognition.

In this example, the ArF excimer laser beam having a size of **A** is radiated with a radiation energy of 40 J/cm².

The number of shots may be adjusted in accordance with the depth and length of the defect **5**.

In Figure **14**, a processed surface **4** is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized as a shadow when observed from above. Further, due to the smoothness of the pro-

cessed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled. As a result, a satisfactory display plane is obtained. The defect compensation takes only 1 minute for each defect **5** on average, and further no residual powders are generated.

Example 5

According to this example, a linear defect **5** at a transparent plate **1** formed of glass or the like as is shown in Figure **15** is compensated for, by radiating an ArF excimer laser beam **8**. The ArF excimer laser has a radiation energy which is distributed to be high at a center and low at a periphery thereof at a radiation portion **2** as in the third example. Figure **16** shows a cross sectional view along line **K-K'** of Figure **15** of a portion obtained by the defect compensation.

In more detail, the defect compensation is performed in the following manner.

First, the defect **5** at a surface of the transparent plate **1** is recognized by an image processing apparatus in the same manner as in the fourth example.

Next, a display apparatus having the transparent plate **1** is mounted on a movable stage, and the ArF excimer laser beam is radiated to a radiation portion **2** while the stage is moved based on the coordinates obtained by the image recognition. By moving the stage in the vicinity of a starting point and a stopping point of the movement faster than at other points, a processed surface **4** having no clear edge to be visually recognized as a shadow when observed from above is obtained.

In this example, the ArF excimer laser beam is radiated with a radiation energy of 40 J/cm². The moving speed of the stage is 2 in the vicinity of the starting point and the stopping point while 1 at the other points.

The number of shots may relatively be adjusted in accordance with the depth and length of the defect **5**.

As is shown in Figure **16**, the resultant processed surface **4** is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized as a shadow when observed from above. Further, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled. As a result, a satisfactory display plane is obtained.

The defect compensation takes only 1 minute for each defect **5** on average, and further no residual powders are generated.

Further, by pasting a masking tape such as a cellophane tape on an area of the transparent plate

1 except for the radiation portion, fine powders splashed during the compensation process can be collected, and also formation of an edge at the border between the radiation portion and the other area can be prevented.

In the second to the fifth examples, the size of the ArF excimer laser beam **8** and the number of shots may be varied.

Example 6

A defect **5** at a surface of a transparent plate **1** formed of glass or the like is compensated for by radiating an ArF excimer laser beam **8** by a mask imaging method using an apparatus shown in Figure **17**.

In the apparatus shown in Figure **17**, a pattern mask **10** formed of a metal plate or the like is provided on a path of the ArF excimer laser beam **8** emitted by an excimer laser emitter **9**. The ArF excimer laser beam **8** is transmitted through the pattern mask **10** and is reduced by a convex lens **12** to be projected and radiated to a radiation portion **2** of the transparent plate **1**. As the pattern mask **10**, for example, a metal plate having a specified pattern of opening obtained by etching can be used.

The reduction ratio and the radiation energy of the ArF excimer laser beam **8** are obtained in the following manner.

Where the distance between the pattern mask **10** and the convex lens **12** is G, the distance between the convex lens **12** and the surface of the transparent plate **1** is H, and the distance of the convex lens **12** is f, the relationship among G, H, and f is:

$$1/G + 1/H = 1/f$$

from a formula concerning lenses (Gauss' theorem).

The reduction ratio M of the ArF excimer laser beam **8** is:

$$M = G/H$$

Where the energy density at an emitting point of the excimer laser emitter **9** is E_1 , the energy density E_2 at a surface of the transparent plate **1** is:

$$E_2 = M^2 \cdot E_1$$

By adjusting and controlling the relationship among G, H and f in terms of distance, the reduction and projection can accurately be performed at the radiation portion **2**.

Further, by setting the above-mentioned relationship among G, H and f very precisely, fluctuation of the energy density E_2 at the radiation portion **2** is reduced, thereby stabilizing the processing precision in a depth direction of the defect **5**.

In the state where the pattern mask **10**, the convex lens **12**, and the surface of the transparent plate **1** are fixed with respect to one another in terms of distance, there is an undesirable possibility that an edge of a processed surface **4** is visually recognized as a shadow when observed from above. When the ArF excimer laser beam **8** is projected in a rectangular pattern, a rectangular edge **20** is clearly projected and recognized as a shadow as is shown in Figure **8**. When the ArF excimer laser beam **8** is projected in a circular pattern, a circular edge **20** is clearly projected and recognized as a shadow as is shown in Figure **9**. Although the light transmitting property of the display plane is maintained by the smooth processed surface **4** with no microscopic ruggedness, this shadow may provide another display defect.

In this example, the ArF excimer laser beam **8** is radiated in the following manner to make the edge **20** unclear.

The apparatus shown in Figure **17** includes a stage **13** movable in a direction of line **X-X'** and a stage **14** movable in a direction of line **Y-Y'**. In such an apparatus, a distance between the convex lens **12** and the surface of the transparent plate **1** is sequentially changed as follows.

The stage **13** is moved in the direction of line **X-X'**, thereby moving the radiation portion **2** in a direction of being distanced from the convex lens **12** or in a direction of approaching the convex lens **12**. Namely, the radiation portion **2** is moved from a position where the profile of the projected pattern is focused and thus clearly displayed thereon to a position where the profile of the projected pattern is not focused and thus unclearly expanded. Simultaneously, the stage **14** is moved in the direction of line **Y-Y'**. By this movement, the ArF excimer laser beam **8** is radiated to different parts of the radiation portion **2** sequentially.

Figure **18** is a cross sectional view of a portion obtained according to this example. As is shown in Figure **18**, a processed surface **4** is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized when observed from above. Further, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled.

Figure **19** is a timing chart showing the relationship between the degree of focus and the movement of the part exposed to the ArF excimer

laser beam **8** during the radiation thereof (from time T_1 to time T_2).

At time T_1 , the radiation portion **2** is relatively far from convex lens **12** (position P_0), and thus the profile of the projected pattern is not focused thereon. When the radiation portion **2** approaches the convex lens **12** (position P), the profile of the projected pattern is focused thereon. Then, the radiation portion **2** is again distanced from the convex lens **12** (toward position P_0).

The radiation portion **2** is simultaneously moved in the direction of line $Y-Y'$ from Q_1 to Q_2 through Q_0 , so as to allow the ArF excimer laser beam **8** to be radiated to different parts of the radiation portion **2**. The distance of the movement in the direction of line $Y-Y'$ can be adjusted in accordance with the size of the defect **5**.

As a result of the above process, a processed surface **4** which is slightly deep at a center and gets gradually shallow toward a periphery thereof is obtained.

The defect compensation takes only 1 minute for each defect on average, which reduces the compensation cost compared with a conventional rubbing method which requires 10 to 20 minutes to compensate for one defect.

Further, no residual powders are generated, which solves the problem that the powders splashed during the process causes other inconveniences.

Example 7

Figure **20** is another timing chart showing the relationship between the degree of focus and the movement of the portion exposed to the ArF laser beam **8** during the radiation thereof (from time T_1 to time T_4), which is performed by use of the apparatus shown in Figure **17**.

The timing chart shown in Figure **20** concerns the radiation performed for compensating for a defect **5** which is relatively deep. The ArF excimer laser beam radiation is performed twice, namely, from time T_1 to time T_2 (during which time the stage **14** is moved from Q_1 to Q_0) and from time T_3 to time T_4 (during which time the stage **14** is moved from Q_2 to Q_0). The degree of focus is changed twice accordingly.

According to this example, a processed surface **4** which is slightly deep at a center and gets gradually shallower toward a periphery thereof is obtained. In this state, the processed surface **4** has no clear edge to be visually recognized when observed from above. Further, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is not spoiled. As a result, a satisfactory display plane is obtained.

The defect compensation takes only 1 minute for each defect **5** on average, and further no residual powders are generated.

The timing relationship of the degree of focus and the movement of the part exposed to the ArF excimer laser beam **8** is not limited to the above-mentioned ones in the sixth and the seventh examples. As the pattern mask **10**, various other types may be used.

Example 8

An ArF excimer laser beam **8** is radiated to a radiation portion **2** using an apparatus shown in Figure **21**. Identical members as those in Figure **17** bear identical reference numerals, respectively.

The apparatus shown in Figure **21** includes an iris mask **11** used as a pattern mask shown in Figure **22**. Blade-like members **23** forming a circular opening at a center of the iris mask **11** are opened or closed by a pin **21** provided at a side of a housing **22**. The pin **21** is movable at an angle of substantially 90° between a position corresponding to a minimum diameter D_{min} of the opening to a maximum diameter D_{max} of the opening, thereby changing the diameter D of the opening.

The pin **21** is driven, for example, in the following manner. As is shown in Figure **23**, a bottom surface of the housing **22** is fixed on a base plate **24** by an adhesive or the like, and a rotating pulley **25** is engaged around an outer peripheral surface of the housing **22**. The pulley **25** is driven by a motor or the like (not shown) through a belt **26**. When the pulley **25** is rotated, the pin **21** is moved, thereby sequentially changing the diameter D of the opening. By using a motor of a reversible type, the pin **21** can be moved both in forward and reverse directions.

In such an apparatus also, in the state where the iris mask **11**, the convex lens **12**, and the surface of the transparent plate **1** are fixed with respect to one another in terms of distance, there is an undesirable possibility that an edge **20** of a processed surface **4** is visually recognized as a shadow when observed from above as is shown in Figure **9**. In this example, such an inconvenience is avoided by radiating the ArF excimer laser beam **8** in the following manner.

The iris mask **11** is provided on a path of the ArF excimer laser beam **8** so that the opening of the iris mask **11** can be larger than a defect **5**. As is shown in Figure **24**, and the diameter D of the opening of the iris mask **11** is sequentially increased from D_1 to D_2 during the radiation (from time T_1 to time T_2).

According to this method, the ArF excimer laser beam **8** is radiated to a periphery of the processed surface **4** for a shortest period of time.

The resultant processed surface **4** is slightly deep at a center and gets gradually shallower toward a periphery thereof. In this state, the processed surface **4** has no clear edge to be visually recognized when observed from above. Further, due to the smoothness of the processed surface **4** with no microscopic ruggedness, the light transmitting property thereof is maintained. As a result, a satisfactory display plane is obtained.

The defect compensation takes only 1 minute for each defect **5** on average, and further no residual powders are generated.

The change in the diameter of the opening of the iris mask **11** is not limited to the one described in this example. Further, the change in the degree of focus and the movement of the part exposed to the ArF excimer laser beam **8** may be utilized in combination with the change in the diameter of the iris mask **11**.

In the first to the eighth examples, the transparent plate **1** is formed of glass. Instead of glass, any other material which absorbs an ArF excimer laser beam at a surface thereof may be used as the transparent plate **1**. For example, a resin such as plastic or an acrylic resin may be used.

As is apparent from the above description, according to the present invention, a processed surface with no microscopic ruggedness is obtained by use of an ArF excimer laser beam. Thus, defect compensation can be performed without spoiling the light transmitting property of the display plane. Since the time required for the defect compensation is shortened, the compensation cost is reduced. Since the amount of the residual powders generated by the compensation process is significantly smaller when compared with the case of a conventional method using rubbing powders or the like, the operational environment can be clean and problems caused by the residual powders or rubbing powders can be avoided. As a result, satisfactory display planes can be obtained with a high yield. Even in the case where an LSI or the like is mounted on the transparent substrate subjected to the defect compensation, there is no undesirable possibility that the LSI is destroyed by static electricity generated by vibration or friction.

By radiating an ArF excimer laser beam while the size of the beam is changed or by radiating an ArF excimer laser beam to have an energy which is high at a center and low at a periphery of a radiation portion, a satisfactory processed surface having no clear edge to be visually recognized as a shadow can be obtained.

Alternatively, such a satisfactory processed surface can be obtained by changing the degree of focus and exposing different parts of the radiation portion to the ArF excimer laser beam during the radiation thereof.

In the case where an iris mask is used as a pattern mask, a satisfactory processed surface having no clear edge to be visually recognized as a shadow can be obtained by sequentially changing the diameter of a circular opening of the iris mask.

Various other modifications will be apparent to and can be readily made by those skilled in the art without departing from the scope and spirit of this invention. Accordingly, it is not intended that the scope of the claims appended hereto be limited to the description as set forth herein, but rather that the claims be broadly construed.

Claims

1. A defect compensation method for smoothing a surface of a transparent plate by radiating an ArF excimer laser beam to a defect at the surface.
2. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated by use of a mask having an opening which is shaped in accordance with the shape of the defect.
3. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated through a lens.
4. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated while the size of the beam at the defect is changed to a plurality of values.
5. A defect compensation method for smoothing a surface of a transparent plate according to claim 4, wherein the size of the beam is changed by exchanging a plurality of masks each having an opening of a different size from one another.
6. A defect compensation method for smoothing a surface of a transparent plate according to claim 4, wherein the size of the beam is changed by use of a mask having a plurality of openings of different sizes.
7. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated so as to have an energy which is high at a center and low at a periphery of the defect.

8. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam has a smaller size than the size of the defect, and wherein the transparent plate having the defect is moved so as to allow different portions of the defect to be irradiated sequentially by the ArF excimer laser beam and simultaneously the number of shots of the ArF excimer laser beam is changed. 5 10
9. A defect compensation method for smoothing a surface of a transparent plate according to claim 8, wherein the number of the shots of the beam is changed in accordance with at least one of a depth and a length of the defect. 15
10. A defect compensation method for smoothing a surface of a transparent plate according to claim 8, wherein the transparent plate having the defect is moved slowly when a center of the defect is exposed to the ArF excimer laser beam and fast when a periphery of the defect is exposed to the ArF excimer laser beam. 20 25
11. A defect compensation method for smoothing a surface of a transparent plate according to claim 3, wherein the degree of focus of the ArF excimer laser beam is changed and also the transparent plate having the defect is moved so as to allow different portions of the defect to be irradiated sequentially by the ArF excimer laser beam. 30
12. A defect compensation method for smoothing a surface of a transparent plate according to claim 11, wherein the change in the degree of focus and the movement of the transparent plate having the defect are performed by moving a stage having the transparent plate thereon in a direction substantially parallel to the radiation of the ArF excimer laser beam and a direction crossing the radiation. 35 40
13. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated by use of an iris mask having an opening which is larger than the defect. 45 50
14. A defect compensation method for smoothing a surface of a transparent plate according to claim 13, wherein a diameter of the opening of the iris mask is sequentially changed during the radiation of the ArF excimer laser beam. 55
15. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the ArF excimer laser beam is radiated in the state where the surface of the transparent plate is masked except for the defect.
16. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the transparent plate is formed of glass.
17. A defect compensation method for smoothing a surface of a transparent plate according to claim 1, wherein the transparent plate is a display plane of a display apparatus.

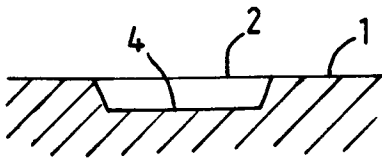


FIG. 1

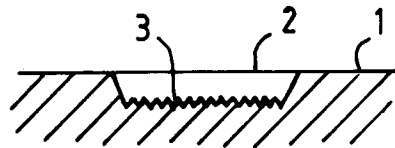


FIG. 2

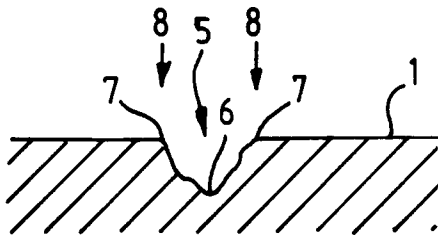


FIG. 3

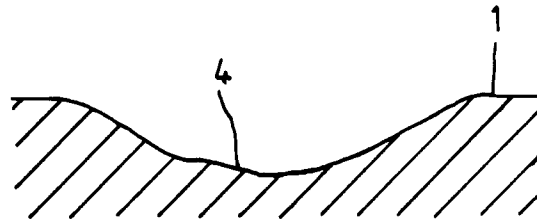


FIG. 4

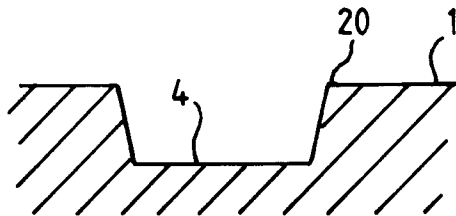


FIG. 5

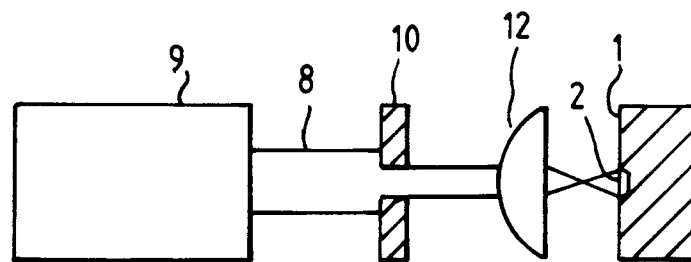


FIG. 6

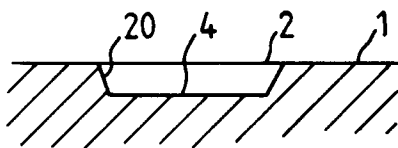


FIG. 7

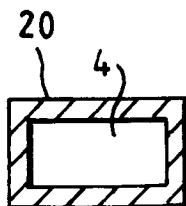


FIG. 8

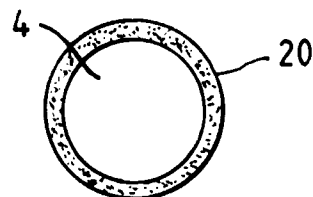


FIG. 9

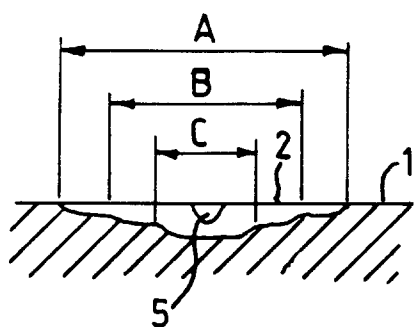


FIG. 10

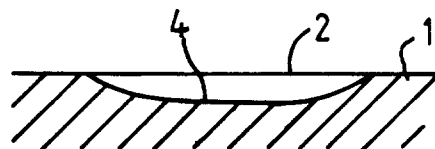


FIG. 12

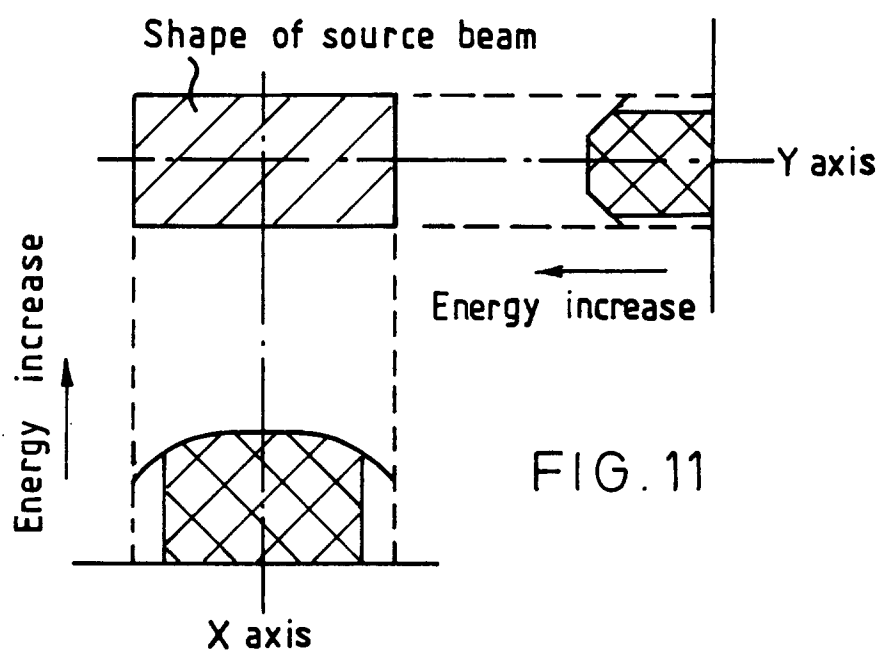


FIG. 11

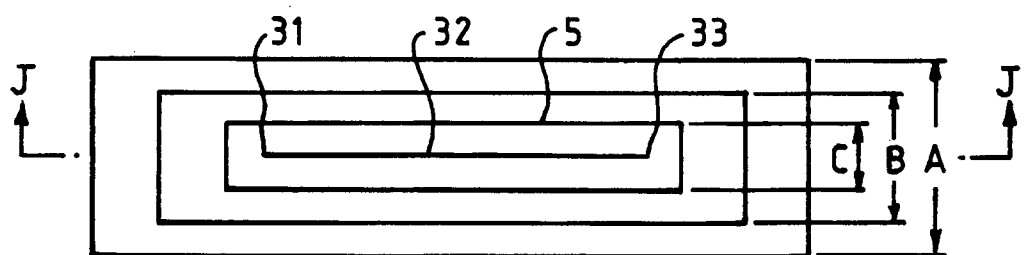


FIG. 13

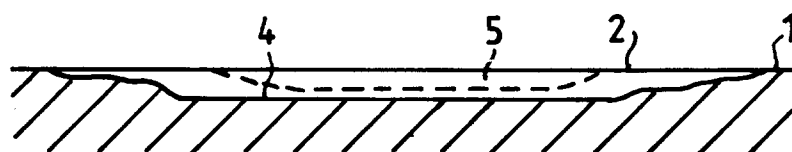


FIG. 14

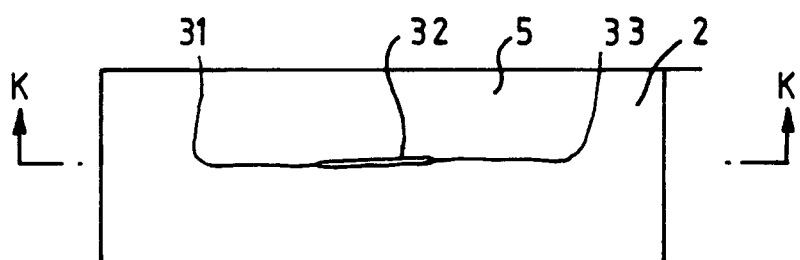


FIG. 15



FIG. 16

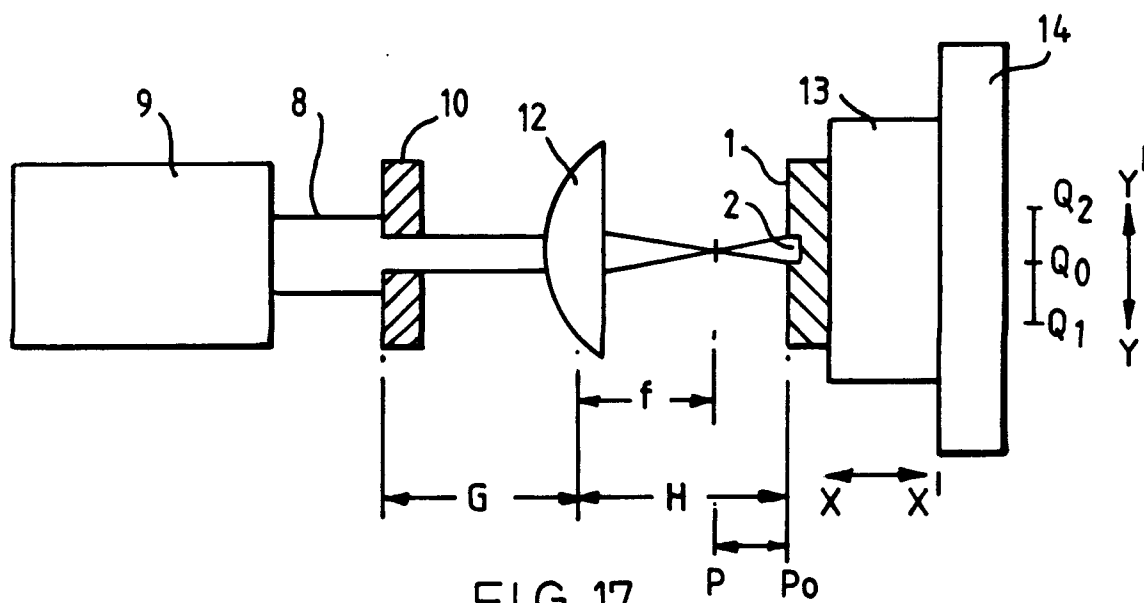


FIG. 17

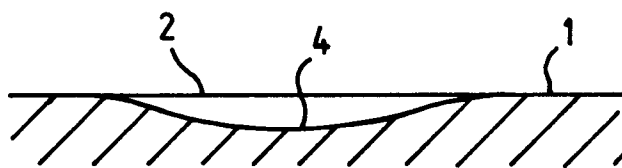


FIG. 18

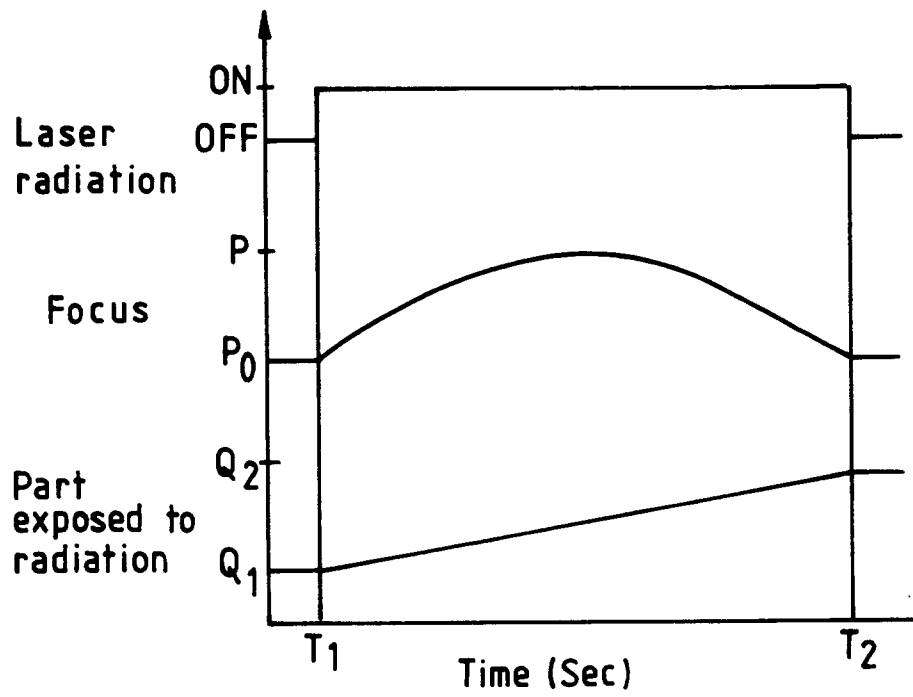


FIG. 19

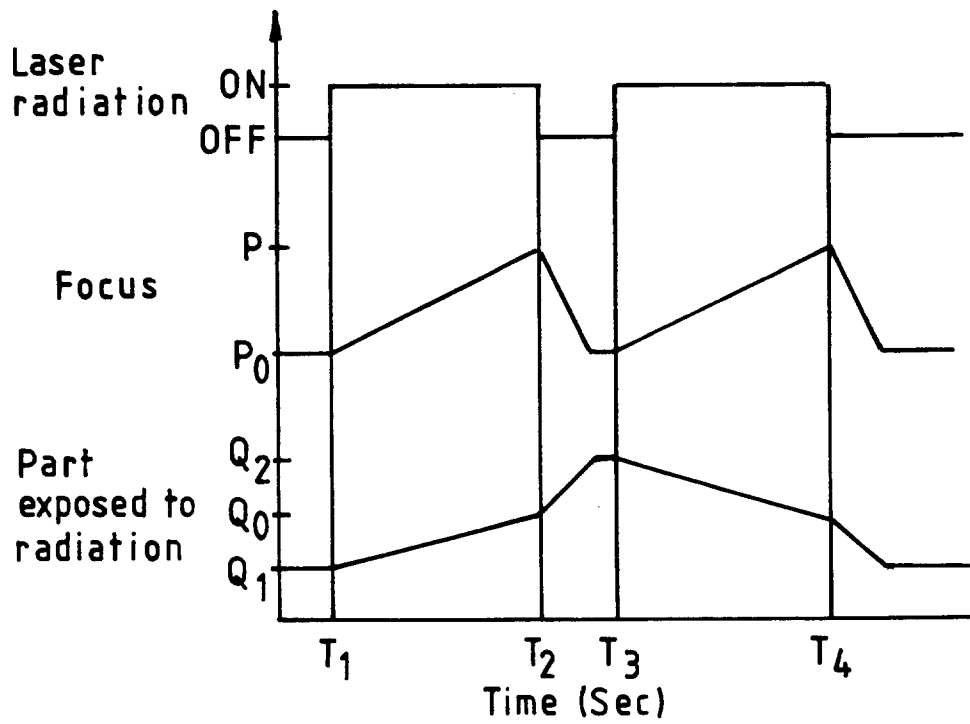


FIG. 20

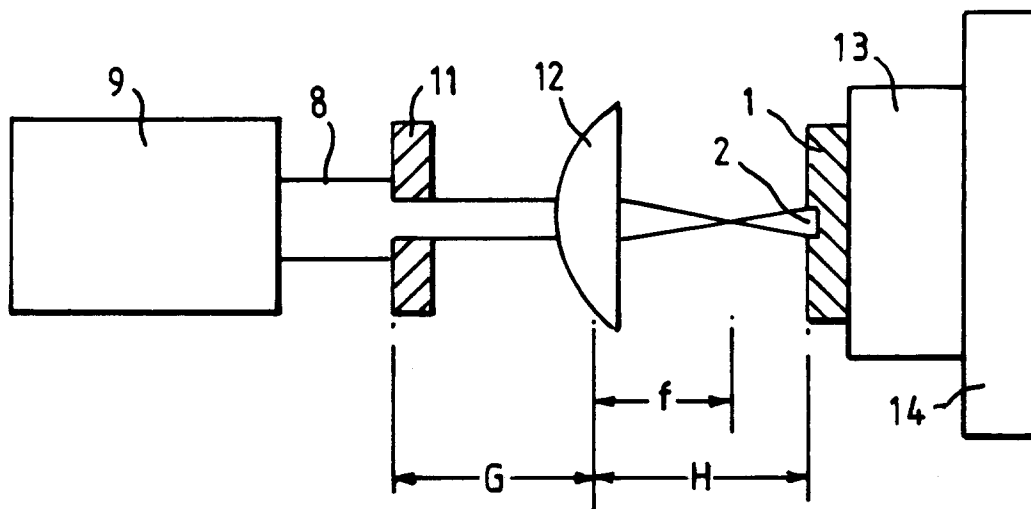


FIG. 21

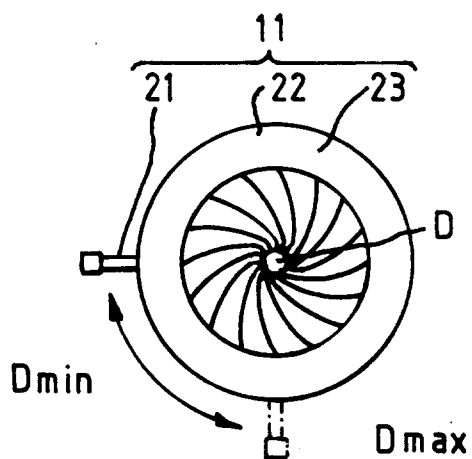


FIG. 22

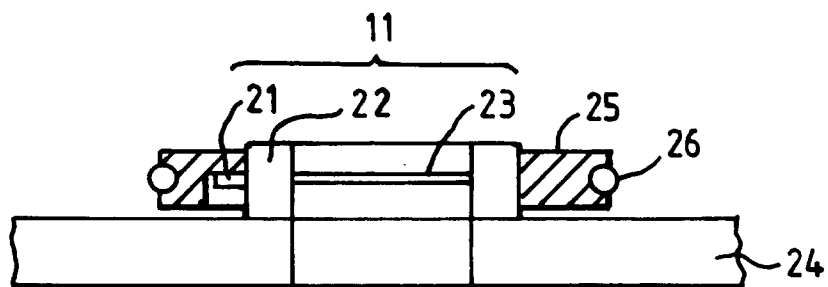


FIG. 23

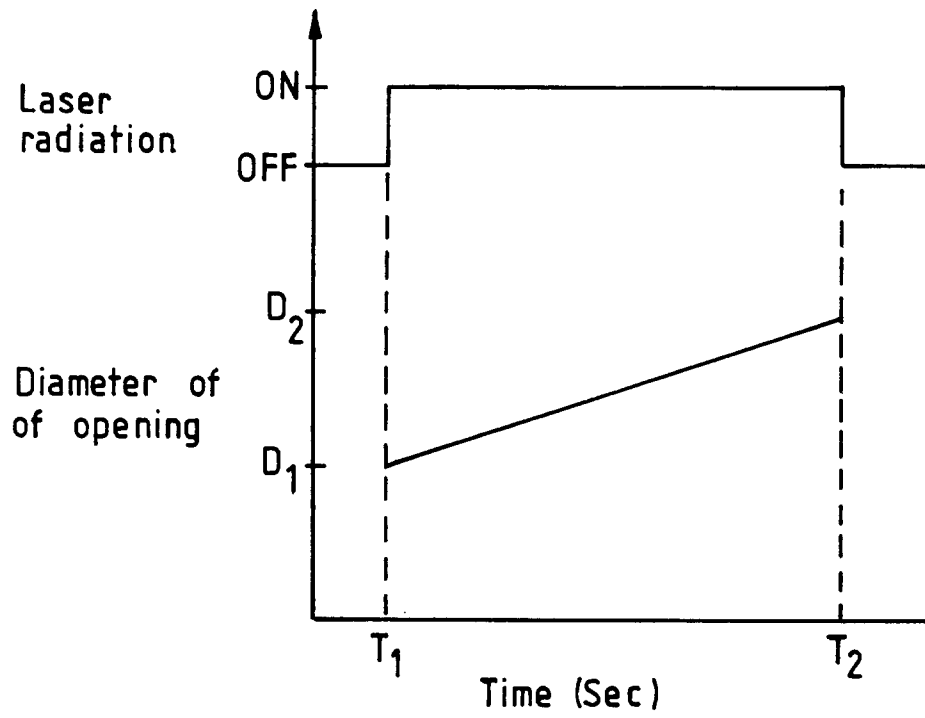


FIG. 24

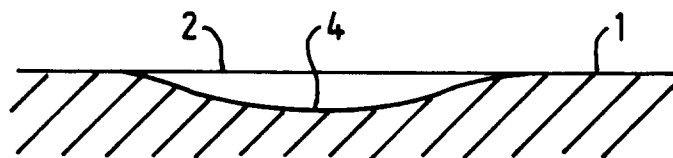


FIG. 25