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(54) **Process for casting pipe with transversal holes.**

(57) A process for casting a pipe (w) such as a delivery pipe with transversal holes, the pipe having an elongate longitudinal hole (h) and at least one pair of transversal holes (e1-e4) communicating with the longitudinal hole in a substantially normal direction thereto. The process comprises the steps of positioning a rod-like center pin (24) for forming the longitudinal hole in a predetermined positional relation to a cavity formation surface of a casting die

(12,14), positioning a pair of mandrel pins for forming the pair of transversal holes such that end faces thereof are in contact with side surfaces of the center pin, and charging molten metal into a die cavity (15) after the center pin and the pair of mandrel pins (12r,14r1-14r4) have been positioned. The molten metal is charged under the condition that the center pin (24) is prevented from deforming by the pair of mandrel pins.

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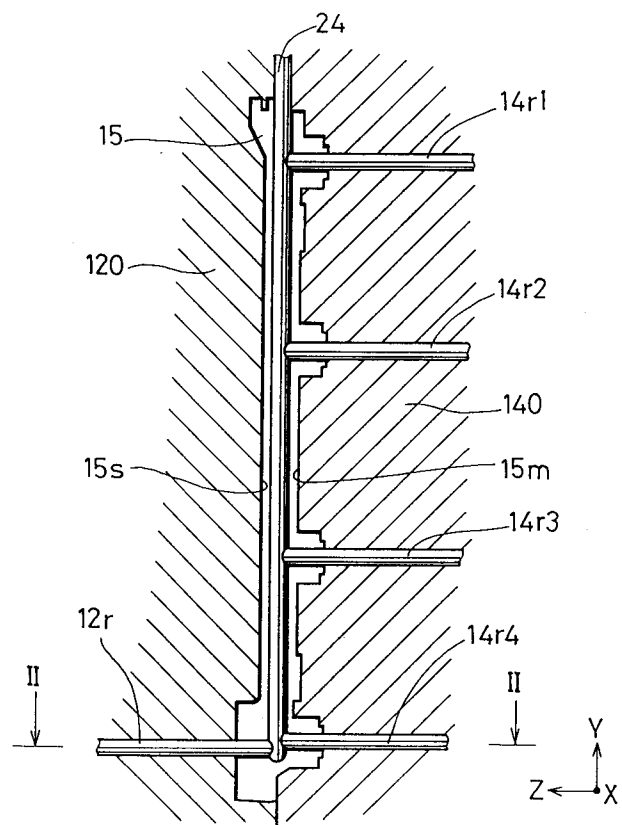


FIG.1

BACKGROUND OF THE INVENTION

1. Field of the Invention

FIG. 3 shows a delivery pipe for supplying fuel to an engine. The delivery pipe has an axially elongate longitudinal hole *h* and a plurality of transversal holes *e1* to *e4* communicating with the longitudinal hole *h* in a substantially normal direction thereto. Injectors are mounted in the transversal holes *e1* to *e4*.

This invention relates to a process of casting a pipe with a transversal hole, i.e., a pipe having an elongate longitudinal hole and at least one transversal hole communicating with the longitudinal hole in a substantially normal direction thereto like the delivery pipe noted above, and to a casting product produced by the same casting process and a casting die used for the same casting process.

2. Description of the Prior Art

A casting process for casting a pipe having an elongate longitudinal hole is well known in the art. In such a process, a center pin for forming the longitudinal hole is positioned in a cavity before charging molten metal thereinto. The longitudinal hole is formed in the casting product by withdrawing the center pin therefrom after the solidification of the molten metal.

In this technique, increasing the length of the center pin gives rise to a problem of the displacement and deformation of the center pin during the casting process. The problem is pronounced in case where the center pin is positioned like a cantilever in the cavity, that is, where a casting product having a longitudinal hole closed at one end is cast. Techniques for preventing the displacement and deformation of the center pin have been proposed, as disclosed in Japanese Laid-open Patent Publication No. 59-189062 and Japanese Laid-open Patent Publication No. 61-9959. In both these techniques, a core pipe is used and is left in the casting product, so that the shape accuracy of the longitudinal hole is maintained.

FIG. 11 shows the technique disclosed in the Japanese Laid-open Patent Publication 59-189062. Designated at 6 is a core pipe which is positioned in a cavity 4. A pair of center pins 8a and 8b are inserted downward and upward into the core pipe 6. In this state, molten metal is charged into the cavity 4. With the solidification of the molten metal, the core pipe 6 is cast in the eventual casting product, i.e., the core pipe 6 is left in the casting product. Afterwards, the pair center pins 8a and 8b are withdrawn from the core pipe 6.

In the technique disclosed in the Japanese Laid-open Patent Publication No. 61-9959, only the

core pipe is used, that is, no center pin is used. To position the core pipe in the cavity, the core pipe is provided with a projections projecting from its outer periphery. The projections are held in contact with a cavity formation surface. Afterwards, molten metal is charged into the cavity. With the solidification of the molten metal, the core pipe is cast in the casting product.

As shown above, by the use of a core pipe, it is possible to obtain a casting product having an elongate longitudinal hole. Particularly, according to the technique disclosed in the Japanese Laid-open Patent Publication 61-9959, it is possible to ensure a sufficiently long longitudinal hole closed at one end. When the core pipe is cast in the casting product, however, it is necessary to produce core pipes in number corresponding to the number of casting products, and this increases the cost of manufacture. Further, when it is desired to obtain a continuous integral casting product as overall produce, it is impossible to use any core pipe. When a process of forming a longitudinal hole without use of any core pipe but by using a center pin is adopted, on the other hand, there is the problem of center pin displacement and deformation, thus imposing restriction on the length of the obtainable longitudinal hole.

SUMMARY OF THE INVENTION

The present invention seeks to solve the above problems by permitting the casting of a pipe having an elongate longitudinal hole without use of any core pipe.

With a pipe having an elongate longitudinal hole, it is often required to form one or more transversal holes communicating with the longitudinal hole. According to the invention, the displacement and deformation of the center pin is prevented by utilizing a mandrel pin for the formation of the transversal hole.

In one aspect of the invention, there is provided a process for casting a pipe with transversal holes, the pipe having an elongate longitudinal hole and at least one pair of transversal holes communicating with the longitudinal hole in a substantially normal direction thereto, which comprises the steps of positioning a rod-like center pin for forming the longitudinal hole in a predetermined positional relation to a cavity formation surface of a casting die, positioning a pair of mandrel pins for forming the pair of transversal holes such that end faces thereof are in contact with side surfaces of the center pin, and charging molten metal into a die cavity after the center pin and the pair of mandrel pins have been positioned.

According to the invention, a casting die for carrying out the above casting process is also

provided. The casting die comprises a center pin disposed in a die cavity for forming the elongate longitudinal hole, and a pair of mandrel pins projecting into the die cavity in a substantially normal direction to the center pin for forming the pair of transversal holes, the position of the center pin being restricted in the radial direction thereof between end faces of the pair of mandrel pins when the casting die is closed.

With the above casting process and casting die, molten metal is charged and solidified with the center pin side surfaces positioned between the end faces of the pair of mandrel pins. It is thus possible to prevent the displacement and deformation of the center pin and ensure high shape accuracy of the longitudinal hole. In the above process, when the center pin is held in a cantilever support in the die cavity, the end of the center pin is suitably supported by the pair of mandrel pins. When the center pin is held in the cavity in its state of support at its opposite ends, its central portion is suitably supported by the pair of mandrel pins.

The above means, although very effective when casting a pipe having a pair of transversal holes, is difficult to carry out when the number of transversal holes is less than one pair. In such a case, the following means is used. That is, the end face of one mandrel pin is held in contact with a side surface of the center pin at least to prevent the center pin from being displaced toward that mandrel pin. This means alone, however, can not prevent the center pin from the displacement thereof away from the mandrel pin. Accordingly, in this process, molten metal is charged into the cavity toward the mandrel pin. When this is done so, the molten metal being charged pushes the center pin toward the mandrel pin and thus prevents the displacement thereof away from the mandrel pin. In this way, it is possible to cast a pipe having at least one transversal hole with satisfactory degree of shape accuracy.

According to the invention, this casting process is carried out with a casting die which comprises a center pin disposed in a die cavity for forming the elongate longitudinal hole, a mandrel pin projecting into the die cavity in a substantially normal direction to the center pin for forming the transversal hole, and a sprue for charging molten metal into the die cavity, an end face of the mandrel pin being brought into contact with a side surface of the center pin when the casting die is closed, the sprue and the mandrel pin being located on the opposite sides of the center pin.

According to the invention, it is possible to obtain a casting product which is integral and a one-piece casting as a whole and in which the surfaces of the longitudinal hole and the transversal hole are cast skin surfaces. This casting product

has satisfactory shape accuracy of the cast skin of the longitudinal hole, and it can be used as such. That is, there is no need of mechanically machining the cast skin to ensure accuracy, and thus, the product can be manufactured inexpensively.

The product can be suitably used as a delivery pipe. In this case, the longitudinal hole is used as a fuel path, and the transversal hole as an injector mounting hole. Such delivery pipes can be manufactured inexpensively in a large number by casting.

The present invention will be more fully understood from the following detailed description and appended claims when taken with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a fragmentary sectional view showing a casting die for carrying out a process of casting a pipe with transversal holes according to a first embodiment of the invention;

FIG. 2 is a fragmentary sectional view taken along arrow line II-II in FIG. 1;

FIG. 3 is a side view showing a delivery pipe as a product of casting;

FIG. 4 is an elevational view, partly in section, showing the casting die for carrying out the process of casting a pipe with transversal holes according to the first embodiment of the invention;

FIG. 5 is a view substantially taken along arrow line V-V in FIG. 4;

FIG. 6 is a fragmentary sectional view, partly broken away, showing a mandrel pin and push-out pins in detail;

FIG. 7 is a view similar to FIG. 1 but showing a second embodiment of the invention;

FIG. 8 is a view similar to FIG. 2 but showing the second embodiment;

FIG. 9 is a view similar to FIG. 8 but showing a third embodiment of the invention;

FIG. 10 is a view showing a different example of the relation between a mandrel pin and push-out pins from that shown in FIG. 6;

FIG. 11 is a fragmentary sectional view showing a casting die for carrying out a prior art pipe casting process; and

FIGS. 12(A) and 12(B) are fragmentary sectional views showing a relation between a return pin and a push-out pin in the prior art.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Now, a process for casting a pipe with transversal holes according to a first embodiment of the invention will be described with reference to FIGS.

1 to 6. In this embodiment, the pipe w with transversal holes to be cast is a delivery pipe with an injector mounted therein for supplying fuel to an engine. The pipe is shown in side view in FIG. 3.

The delivery pipe w has an axially elongate longitudinal hole h which extends in the axial direction and which is utilized as a fuel path, and has injector mounting transversal holes e1 to e4 communicating with the longitudinal hole h in a substantially normal direction thereto and formed at a uniform interval in the longitudinal direction. Further, the delivery pipe w has a pressure regulator mounting transversal hole p formed in its end portion and communicating with the longitudinal hole h in a substantially normal direction thereto and on the side opposite the injector mounting transversal hole e4.

FIG. 4 is an elevational view, partly in section, showing a casting die 10 for forming the delivery pipe w by the casting process according to this embodiment. FIG. 1 is a view showing a part of FIG. 4 in detail. FIG. 2 is a view taken along arrow line II-II in FIG. 1. FIG. 5 is a view taken substantially along arrow line V-V in FIG. 4. In the following description, the die width direction is referred to as X-axis direction, the die height direction as Y-axis direction, and the die closing direction (i.e., direction of movement of a movable die) as Z-axis direction.

The casting die 10 comprises a fixed die 12 provided with a fixed insert member 120, and a movable die 14 provided with a movable insert member 140. As shown in FIG. 4, in the closed state of the casting die, product formation spaces, i.e., cavities 15, are formed elongatedly in the longitudinal direction (i.e., Y-axis direction) between the fixed insert member 120 and the movable insert member 140. In this embodiment, as shown in FIG. 5, six cavities 15 are formed in juxtaposition in the width direction of the casting die 10 (i.e., X-axis direction).

In a lower portion of the fixed die 12, a sleeve 12s is provided such that it extends in the Z-axis direction, and molten metal injected by a plunger tip (not shown) from the sleeve 12s is led through molten metal paths 12t (see FIG. 5) to be charged into the cavities 15. The sectional area of the molten metal paths 12t is set such that it is reduced as one goes away from the sleeve 12s, that is, such that sectional area A1 > sectional area A2 > sectional area A3. With this arrangement, the charging rate of the cavity 15 at the end on the side of the vehement charging with the momentum of molten metal is suppressed to a certain extent, thus substantially uniforming the charging time of the individual cavities 15.

In the fixed die 12, a mandrel pin 12r for forming the pressure regulator mounting transver-

sal hole p in the delivery pipe w is mounted for each cavity 15. The mandrel pin 12r is positioned such that its axis is parallel to the Z-axis. As shown in FIGS. 1 and 2, its end face projects by a prescribed dimension from a cavity formation surface 15s of the fixed insert member 120. Further, its end face is formed with an arcuate recess 12u such as to be substantially in close contact with a side surface of a center pin 24 to be described later.

The movable die 14 is coupled via a die base 18 to a drive unit (not shown), and with the driving thereof, it is moved in the Z-axis direction from a position to close the die to a position to open the die or vice versa. To the top of the movable die 14 is secured a center pin insertion cylinder 20 for moving a movable unit 21 in the Y-axis direction (i.e., vertical direction). On the movable unit 21 of the center pin insertion cylinder 20 is mounted a support block 22 supporting center pins 24. Each center pin 24 is a mandrel pin for forming the longitudinal hole h in the delivery pipe w, and is mounted in the support block 22 for movement in the vertical direction along the center line of each cavity 15. The support block 22 has a raised portion 22t which is engaged in a recessed portion 12h of the fixed die 12 when the casting die is closed, thus preventing the support block 22 from being pushed back upward by high pressure applied to the interior of the cavities 15.

The movable die 14 is provided with two sets of center pin insertion cylinder 20 and support block 22. Three center pins 24 are raised and lowered simultaneously by one set of center pin insertion cylinder 20 and so forth.

As shown in FIGS. 1 and 4, in the movable die 14, four movable mandrel pins 14r1 to 14r4 for forming the injector mounting transversal holes e1 to e4 in the delivery pipe w, are provided for each cavity 15. The movable mandrel pins 14r1 to 14r4 are movable at right angles to the center pin 24 (i.e., Z-axis direction) and are moved axially by drive cylinders (not shown). Their end faces are each formed with an arcuate recess 14u to be substantially in close contact with a side surface of the center pin 24.

The movable mandrel pins 14r1 to 14r4, the fixed mandrel pins 12r and the center pins 24 all have their surfaces provided with TD treatment, P-CVT treatment, etc. for the seizure prevention purpose.

FIG. 6 shows the detailed structure of the mandrel pin 12r on the side of the fixed insert member 120. The fixed insert member 120 has a space 42s in which is accommodated a push-out member 44 having a pair of push-out pins 44p and 44q and a mandrel pin 12r.

The mandrel pin 12r is mounted on the center of the push-out member 44 such that it extends at right angles thereto, and the pair push-out pins 44p and 44q are provided in right angles around the mandrel pin 12r. The mandrel pin 12r and the push-out pins 44p and 44q are inserted in through holes 120k, 120h and 120i for axial movement through the same in a horizontal state. The space 42s is closed by a retainer member 42, and a spring member 44b biasing the push-out member 44 away from the retainer member 42 is mounted between the retainer member 42 and the push-out member 44. Thus, in the open state of the casting die, the push-out member 44 pushed by the spring force of the spring member 44b is held at a right set position in FIG. 6. In this state, the projection of the mandrel pin 12r and the push-out pins 44p and 44q from the fixed insert member 120 is maximum. The lengths of the push-out pins 44p and 44q and the mandrel pin 12r are set such that when the die closing is completed, the ends of the push-out pins 44p and 44q are substantially in accord with the position of the surface of each cavity 15 with the recessed end 12u of the mandrel pin 12r in contact with a side surface of the center pin 24.

Now, the process of casting a pipe (or delivery pipe w) with transversal holes according to this embodiment will be described.

First, in the open state of the casting die, the movable unit 21 is lowered with the operation of the center pin insertion cylinder 20 of the movable die 14. As a result, the center pin 24 is lowered along a center line of each cavity 15 to be positioned at a predetermined position. Then, each of the movable mandrel pins 14r1 to 14r4 is moved by a drive cylinder to be projected by a prescribed dimension from each cavity formation surface 15m of the movable insert member 140. With the movable mandrel pins 14r1 to 14r4 projected from each cavity formation surface 15m of the movable insert member 140, a clearance of about 0.3 mm is provided between the end recess 14u of each of the movable mandrel pins 14r1 to 14r4 and a side surface of each center pin 24. The end face 14u of each of the mandrel pins 14r1 to 14r4 and the side surface of each center pin 24 need not be in perfectly close contact with each other, but they may face each other with a slight clearance therebetween.

Then, the casting die is closed with the movable die 14 and the die base 18 moved by the drive unit, as shown in FIGS. 1 and 4. Thus, the cavities 15 are formed between the fixed insert member 120 and the movable insert member 140. Further, the side surface of each center pin 24 is brought into contact with the recessed end 12u of the mandrel pin 12r to contract the spring member 44b and cause retreat of the mandrel pin 12r. At

this time, the push-out pins 44p and 44q are also retreated to be flush with the cavity formation surface. When the closing of the casting die is completed in this way, molten metal injected from the sleeve 12s through the plunger tip is charged into each cavity 15 through each molten metal path 12t. When the molten metal is solidified after the lapse of a predetermined period of time, the casting die is opened again with the movable die 14 and the die base 18 moved by the drive unit. Further, each center pin 24 is taken out with the driving of each center pin insertion cylinder 20, and each of the movable mandrel pins 14r1 to 14r4 is taken out by the drive cylinder.

Since the sectional areas A1 to A3 of the molten metal paths 12t are set such as above to provide for a substantially uniform molten metal charging time for each cavity 15, the molten metal solidification time does not fluctuate for each cavity 15, and it is possible to set die opening timings satisfactorily.

With the movable die 14 separated from the fixed die 12 when the casting die is opened after the casting, the pushing force from the center pin 24 is no longer applied to the end of the mandrel pin 12r, and the push-out member 44 is moved away from the retainer member 42 by the spring force of the spring member 44b. As a result, the push-out pins 44p and 44q project from the cavity formation surface of the fixed die 12. Thus, the product of casting is kicked out from the surface of the cavity 15.

As shown above, according to the process for casting the delivery pipe w of this embodiment, in the closed state of the casting die 10, the end of the center pin 24 which is readily subject to displacement, is restricted radially by the recessed end 14u of the movable mandrel pin 14r4 and the recessed end 12u of the fixed mandrel pin 12r. Thus, with application of a high pressure to the center pin 24 as a result of forced charging of molten metal into the cavity 15, the end of the center pin 24 is not displaced radially, thus substantially eliminating the bending of the center pin 24 during the casting. It is thus possible to eliminate such inconvenience as failure of withdrawal of the center pin 24 after the solidification of molten metal. This means that, unlike the prior art, there is no need of providing any particular core pipe or the like for the reinforcement of the center pin 24. Further, since a clearance of about 0.3 mm is provided between the side surface of the center pin 24 and the recessed end 14u of the movable mandrel pin 14r4, it is possible to absorb thermal expansion of the center pin 24 and the movable mandrel pin 14r4 that is caused during the casting.

In the casting die of this embodiment, the mandrel pin 12r also serves the role of a return pin

for causing the retreat of the push-out pins 44p and 44q to the cavity formation surface.

FIGS. 12(A) and 12(B) show a prior art relationship between a push-out pin and a return pin as disclosed in Japanese Laid-open Patent Publication No. 1-3141127.

This casting die 401 comprises a fixed die 412 mounted on a fixed die mounting member 402 and a movable die 413 mounted on a movable die mounting member 403. As shown in FIG. 12(B), in the closed state of the casting die 401, a cavity 410 is formed therein. Further, the movable die 413 has a space 413s in which a push-out member 414 is accommodated for movement in the vertical direction in FIG. 12(B). The push-out member 414 has a push-out pin 413p for kicking out a casting product from the surface of the cavity 410 at the time of the die opening and a return pin 413r for returning the end of the push-out pin 413p to the position of the surface of the cavity 410 at the time of the die closing. A spring member (not shown) is provided between the push-out member 414 and the movable die mounting member 403, and the push-out member 414 is biased upward by the spring force. Thus, when the casting die 401 is open, the push-out pin 413p is projecting from the surface of the cavity 410 (movable die 413), while the return pin 413r is projecting from the engagement surface 413m of the movable die 413.

With the above construction, when the end of the return pin 413r is brought into contact with the engagement surface 412m of the fixed die 412 during the process of approach of the fixed die 412 by the movable die 413 at the time of the die closing, the return pin 413r is pushed into the movable die 413 to an extent corresponding to the distance of approach of the fixed die 412 by the movable die 413. Thus, the push-out member 414 is moved downward in FIG. 12(B) against the spring force. At this time, in the perfectly closed state of the casting die 401, the push-out pin 413p is returned to a position such that its end is substantially in accord with the surface of the cavity 410.

With the movable die 413 separated from the fixed die 412 when the casting die is opened after the casting, the push-out force from the fixed die 412 is no longer applied to the return pin 413r. As a result, the push-out member 414 is moved upward in FIG. 12(A) by the spring force, and the push-out pin 413p projects from the surface of the cavity 410 of the movable die 413. Thus, the product of casting is kicked out from the surface of the cavity 410, that is, prevented from remaining on the cavity surface.

With the above prior art casting die 401, however, the return pin 413r for returning the push-out pin 413p to a predetermined position is provided at

the position of the engagement surface 413m of the movable die 413. This means that in the casting die 401, it is necessary to set the width of the engagement surface 413m constituting the periphery of the cavity 410 by taking the space for mounting the return pin 413r into consideration. In addition, it is necessary to set the area of the push-out member 414 supporting the push-out pin 413p and the return pin 413r to be greater than the area of projection of the cavity 410. Therefore, a large space is necessary in the casting die 410, thus increasing the size of the casting die 401 and also dictating restrictions in the die design.

In contrast, with the construction shown in FIG. 6, the mandrel pin 12r also serves the role of the prior art return pin 413r, and thus the outer shape dimensions of the die are extremely reduced. In addition, while in the prior art, a clearance has to be provided between the center pin 24 and the mandrel pin 12r by taking the thermal expansion of the two pins into consideration, in this embodiment, no such clearance has to be provided because the mandrel pin 12r is capable of being retreated.

A second embodiment of the invention will be described with reference to FIGS. 7 and 8.

FIG. 7 is a view similar to FIG. 1, and FIG. 8 is a sectional view taken along line VIII-VIII in FIG. 7. Parts like those in the first embodiment are designated by like reference numerals with addition of 100, and their detailed description will be omitted.

What is produced in this embodiment is the delivery pipe w described before in connection with FIG. 3 with omission of the pressure regulator mounting transversal hole p. Without the pressure regulator mounting transversal hole p, the center pin 24 can not be restricted from the opposite sides with a mandrel pin. In the case of this embodiment, a center pin 124 is supported from a single side by a single mandrel pin 114r4, as is obvious from FIGS. 7 and 8.

In this case, the center pin 24 may be displaced away from the mandrel pin 114r4. Accordingly, in this embodiment, a sprue R2 through which to charge molten metal into the cavity 115 is provided at an angle with respect to a position to charge molten metal toward the mandrel pin 114r4. With this arrangement, the charging pressure acts in a direction of pushing the center pin 124 against the mandrel pin 114r4, and thus, there is no possibility of displacement of the center pin 124 away from the mandrel pin 114r4. Molten metal is further charged from a sprue R3 through a sprue R1 into the cavity 115, and this charging pressure again acts on the side of pushing the center pin 124 against the mandrel pin 114r4.

FIG. 9 shows a third embodiment. Again in this case, a sprue R5 and a mandrel pin 214r4 may not always face each other. In any case, molten metal

being charged flows toward the side of pushing a center pin 224 against the mandrel pin 214r4. Thus, the center pin 224 is not displaced or deformed.

FIG. 10 shows a different example of the relation between a mandrel pin and push-out pins.

In this embodiment, a casting die 320 comprises a fixed die 322 with a fixed insert member 322j mounted therein and a movable die 323 with a movable insert member 323j mounted therein. As shown in FIG. 10, a cavity 330 is formed in the die 320 when the die is closed. Then, molten metal forced out from a sleeve 326 provided in the fixed die 322 is charged through a molten metal path (not shown) into the cavity 330.

The fixed die 322 has a space 322s which is formed in the neighborhood of the back side of the fixed insert member 322j, and in the space 322s is accommodated a push-out member 324 with a push-out pin 324p and a mandrel pin 324n. The push-out pin 324p serves to push out a casting product from the fixed insert member 322j after the casting, and the mandrel pin 324n is used to form a through hole in the product.

The push-out member 324 has a mandrel pin 324n extending from and at right angles to its center and also has a plurality of push-out pins 324p which are likewise mounted by right angle mounting around the mandrel pin 324n. The mandrel pin 324n and the push-out pin 324p are inserted in through holes 322h and 322k of the fixed die 322 and the fixed insert member 322j, so that the mandrel pin 324n and the push-out pin 324p can be moved axially in their horizontal position. The space 322s is closed by a retainer member 322x. A spring member 324b biasing the push-out member 324 away from the retainer member 322x is provided between the retainer member 322x and the push-out member 324. Thus, in the closed state of the casting die, the push-out member 324 is held at a left set position in FIG. 10 by the spring force of the spring member 324b. Thus, the mandrel pin 324n and the push-out pin 324p are in maximum projection from the fixed insert member 322j. The length of the mandrel pin 324n is set to be greater than the length of the push-out pin 324p by an amount corresponding to the thickness of the cavity 330.

Further, a push-out pin 327 for kicking out a casting product from the movable insert member 323j after the casting, is mounted horizontally in the movable die 323 and movable insert member 323j. Further, in the movable die 323 is accommodated a push-out cylinder (not shown) for axially moving the push-out pin 327.

Now, the operation of the casting die 320 will be described.

First, during the approach of the movable die 323 toward the fixed die 322 when the casting die is closed, the mandrel pin 324n is brought into contact with the cavity surface of the movable insert member 323j. As this occurs, the movable insert member 323j pushes the mandrel pin 324n in the axial direction. As a result, the mandrel pin 324n is forced into the fixed insert member 322j and the fixed die 322 by the distance corresponding to the approach of the movable die 323 toward the fixed die 322, so that the push-out member 324 is moved toward the retainer member 322x against the spring force of the spring member 324b. Then, as the push-out member 324 is moved, the push-out pin 324p is received in the fixed insert member 322j. Since the length of the mandrel pin 324n is set to be greater than the length of the push-out pin 324p by an amount corresponding to the thickness of the cavity 330 as noted above, when the die 320 is completely closed, the push-out pin 324p is retreated into the fixed insert member 322j until its end is substantially in accord with the cavity surface of the fixed insert member 322j.

Subsequently, molten metal is forced through the sleeve 326 and molten metal path (not shown) into the cavity 330 for casting. With the movable die 323 separated from the fixed die 322 when the casting die is opened after the casting, the pushing force from the movable insert member 323j is no longer applied to the end of the mandrel pin 324n, and the push-out member 324 is thus moved away from the retainer member 322x by the spring force of the spring member 324b. As a result, the push-out pin 324p is projected from the surface of the cavity wall of the fixed insert member 322j to kick out the casting product from the surface of the cavity 330, that is, prevent the product from remaining on the cavity wall. Further, in the movable die 323 the push-out pin 327 is operated by a push-out cylinder (not shown) for separating the casting product from the surface of the cavity 330.

As shown above, with the casting die 320 of this embodiment, the mandrel pin 324n mounted on the push-out member 324 with the push-out pin 324p secured thereto, also serves as a return pin. Thus, unlike the prior art, there is no need of disposing any return pin at the position of the engagement surface of the cavity 330, thus permitting the reduction of the width of the engagement surface. Further, since the mandrel pin 324n is disposed at a position to penetrate the cavity 330, the area of the push-out member 324 supporting the mandrel pin 324n and the push-out pin 324p may be made smaller than the area of projection of the cavity 30. Thus, the die may have a reduced space for accommodation of the push-out member 324, thus permitting the die 320 to be made compact.

According to the invention, molten metal is charged in a state such that the center pin for forming a longitudinal hole in a pipe is restricted by the end face of the mandrel pin for forming a transversal hole in the pipe. Thus, application of a high molten metal pressure to the center pin during the casting does not cause displacement or deformation of the center pin in the radial direction, and it is possible to substantially eliminate the bending of the center pin. This eliminates the possibility of such inconvenience as failure of withdrawal of the center pin. Further, since unlike the prior art, no core pipe or the like is required, the cost of manufacture can be reduced.

Further, according to the invention, since the mandrel pin also has a role of a return pin for returning the push-out pin, there is no need of disposing any return pin at the position of the engagement surface of the cavity. Further, the area of the push-out member supporting the mandrel pin and the push-out pin may be made smaller than the area of projection of the cavity, thus permitting the reduction of the push-out member accommodation space in the die. The casting die thus may be made compact.

While the invention has been described with reference to preferred embodiments thereof, it is to be understood that modifications or variations may be easily made without departing from the scope of the present invention which is defined by the appended claims.

A process for casting a pipe such as a delivery pipe with transversal holes, the pipe having an elongate longitudinal hole and at least one pair of transversal holes communicating with the longitudinal hole in a substantially normal direction thereto. The process comprises the steps of positioning a rod-like center pin for forming the longitudinal hole in a predetermined positional relation to a cavity formation surface of a casting die, positioning a pair of mandrel pins for forming the pair of transversal holes such that end faces thereof are in contact with side surfaces of the center pin, and charging molten metal into a die cavity after the center pin and the pair of mandrel pins have been positioned. The molten metal is charged under the condition that the center pin is prevented from deforming by the pair of mandrel pins.

Claims

1. A process for casting a pipe with transversal holes, the pipe having an elongate longitudinal hole and at least one pair of transversal holes communicating with the longitudinal hole in a substantially normal direction thereto, comprising the steps of:
positioning a rod-like center pin for forming

the longitudinal hole in a predetermined positional relation to a cavity formation surface of a casting die;

positioning a pair of mandrel pins for forming the pair of transversal holes such that end faces thereof are in contact with side surfaces of the center pin; and

charging molten metal into a die cavity after the center pin and the pair of mandrel pins have been positioned.

2. A process for casting a pipe with a transversal hole, the pipe having an elongate longitudinal hole and at least one transversal hole communicating with the longitudinal hole in a substantially normal direction thereto, comprising the steps of:

positioning a rod-like center pin for forming the longitudinal hole in a predetermined positional relation to a cavity formation surface of a casting die;

positioning a mandrel pin for forming the transversal hole such that an end face thereof is in contact with a side surface of the center pin; and

charging molten metal into a die cavity toward the mandrel pin after the center pin and the mandrel pin have been positioned.

3. A casting die for casting a pipe with transversal holes, the pipe having an elongate longitudinal hole and at least one pair of transversal holes communicating with the longitudinal hole in a substantially normal direction thereto, comprising:

a center pin disposed in a die cavity for forming the elongate longitudinal hole; and

a pair of mandrel pins projecting into the die cavity in a direction substantially normal to the center pin for forming the pair of transversal holes;

the position of the center pin being restricted in the radial direction thereof between end faces of the pair of mandrel pins when the casting die is closed.

4. The casting die according to claim 3, further comprising a push-out pin for separating a casting product produced therein from a cavity formation surface, the push-out pin being rigidly coupled to one of the pair of mandrel pins.

5. A casting die for casting a pipe with a transversal hole, the pipe having an elongate longitudinal hole and at least one transversal hole communicating with the longitudinal hole in a substantially normal direction thereto, comprising:
a center pin disposed in a die cavity for

forming the elongate longitudinal hole;

a mandrel pin projecting into the die cavity in a direction substantially normal to the center pin for forming the transversal hole; and

a sprue for charging molten metal into the die cavity; 5

an end face of the mandrel pin being brought into contact with a side surface of the center pin when the casting die is closed, the sprue and the mandrel pin being located on the opposite sides of the center pin. 10

6. A casting product having an elongate longitudinal hole and at least one transversal hole communicating with the longitudinal hole in a substantially normal direction thereto, wherein the surfaces of the longitudinal hole and the transversal hole are cast skin surfaces. 15

7. The casting product according to claim 6, wherein the casting product is a delivery pipe with the longitudinal hole constituting a fuel path closed at one end and the transversal hole constituting an injector mounting hole. 20

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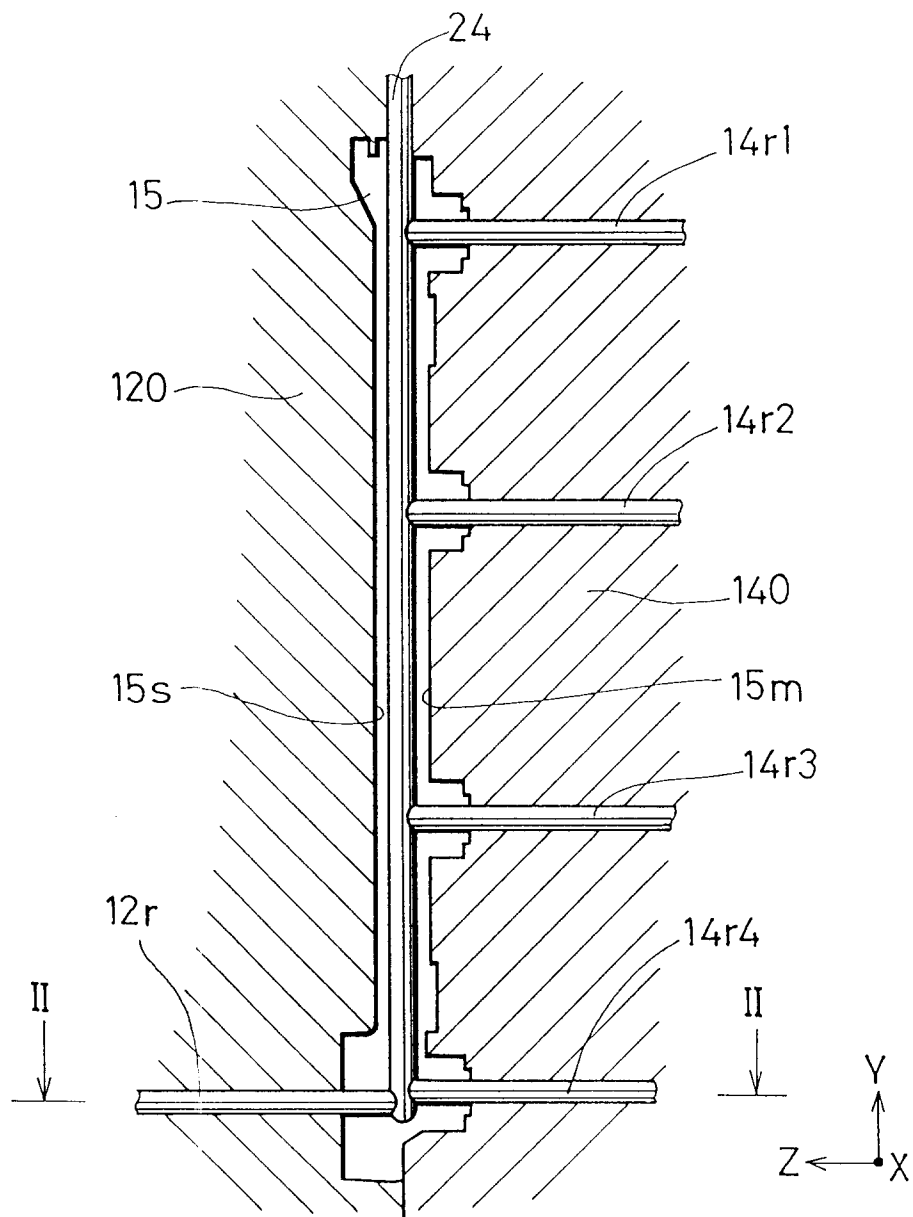


FIG.1

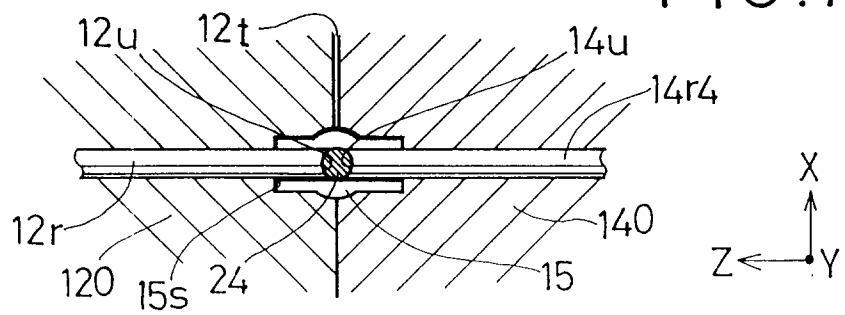


FIG.2

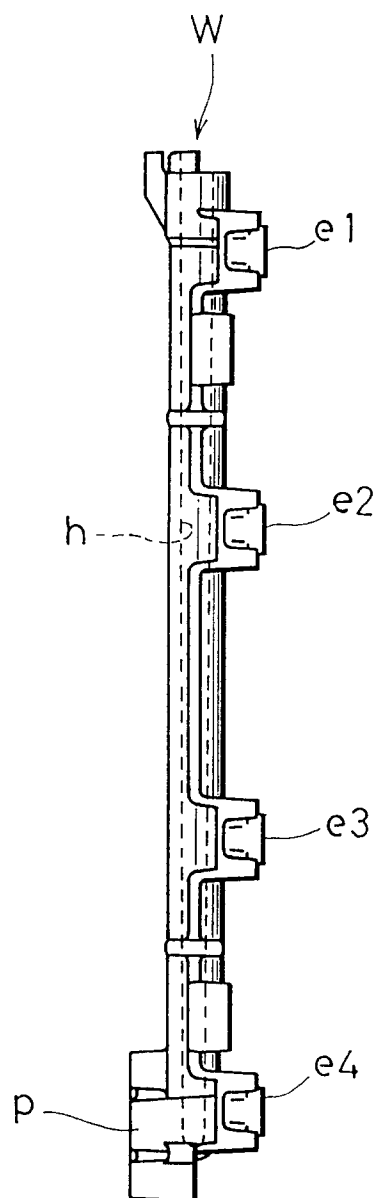


FIG.3

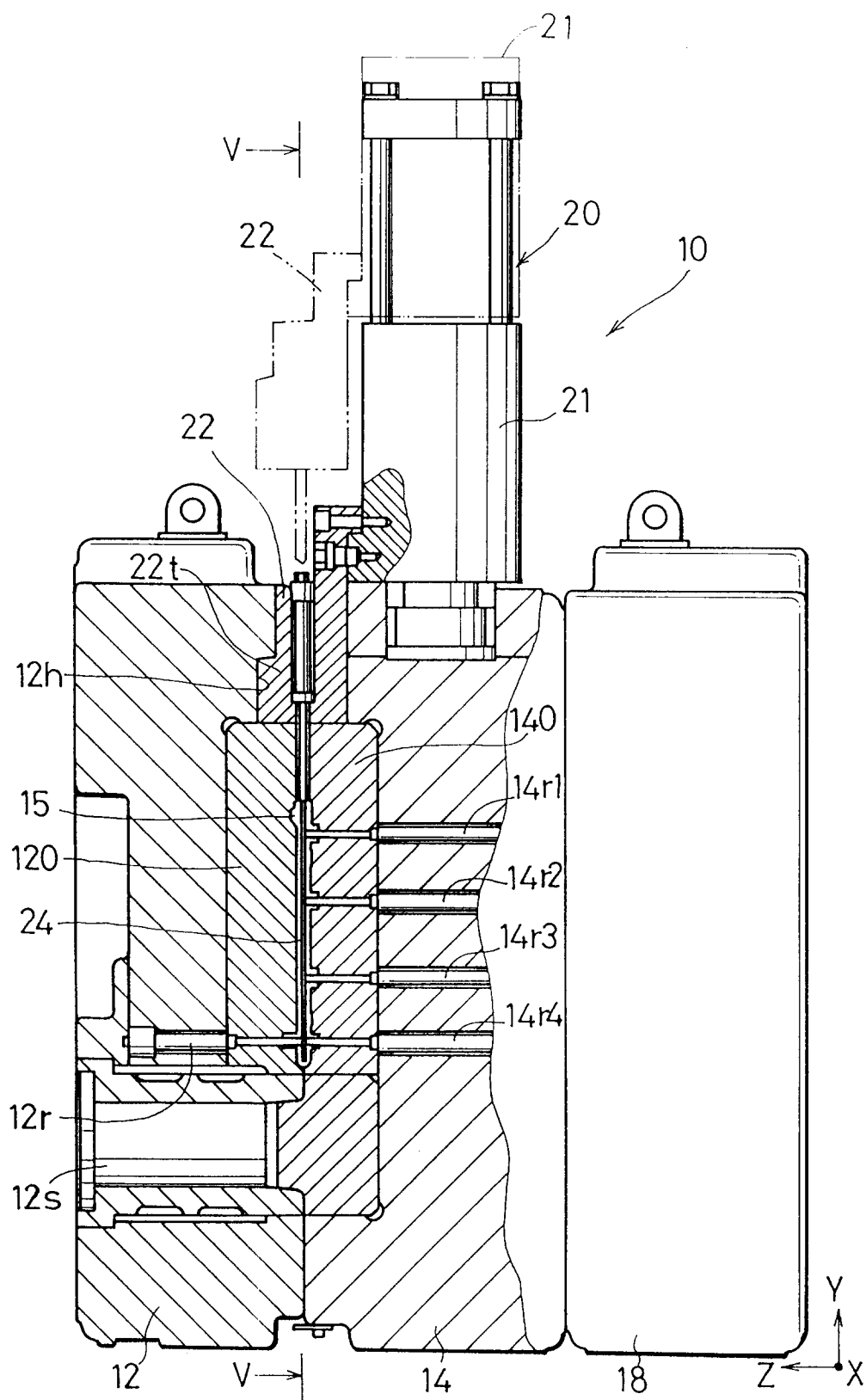


FIG.4

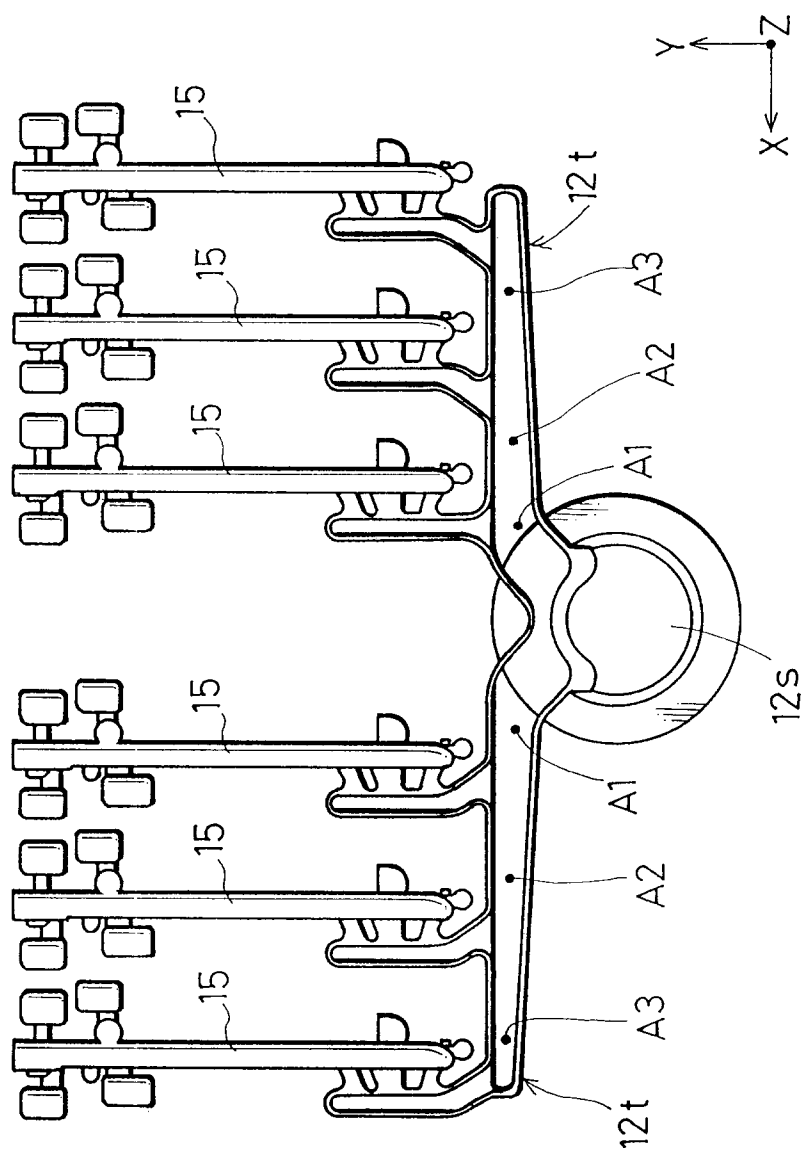


FIG. 5

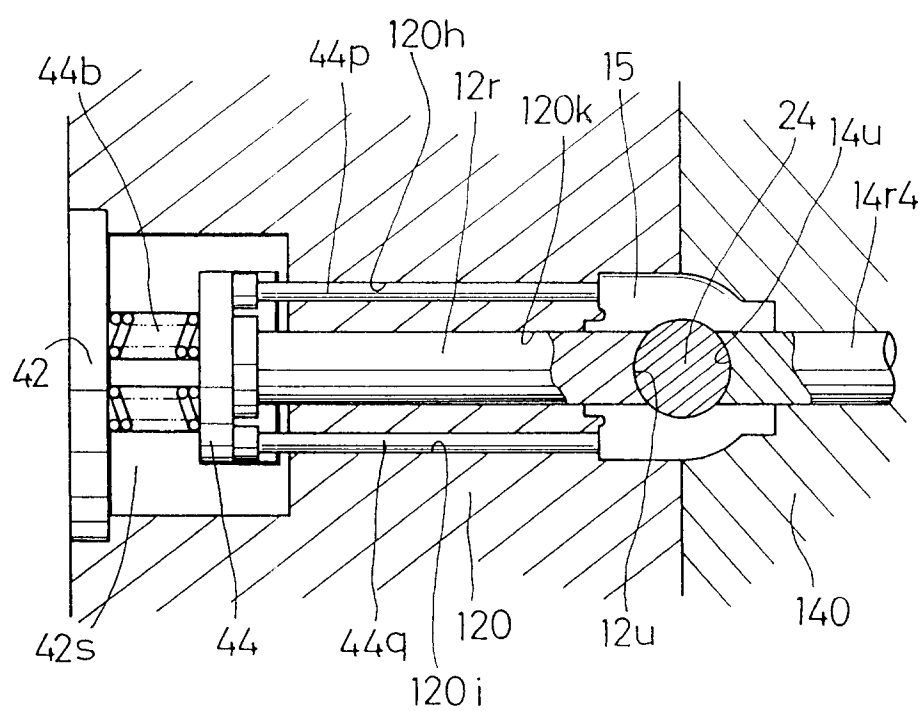


FIG.6

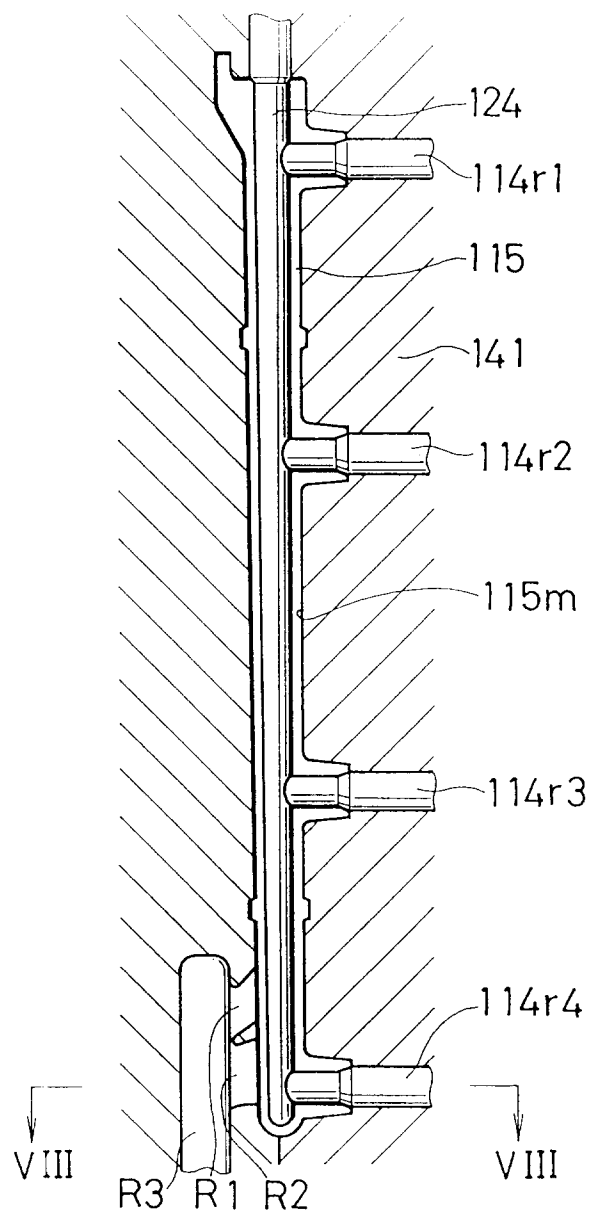


FIG. 7

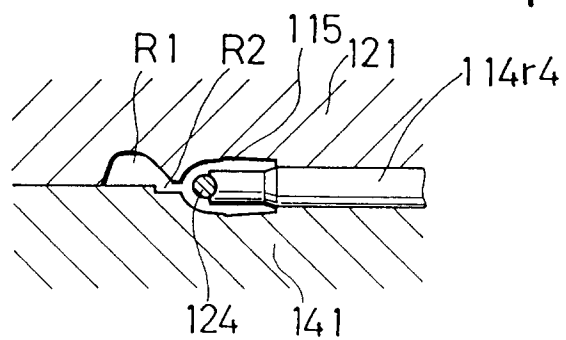


FIG. 8

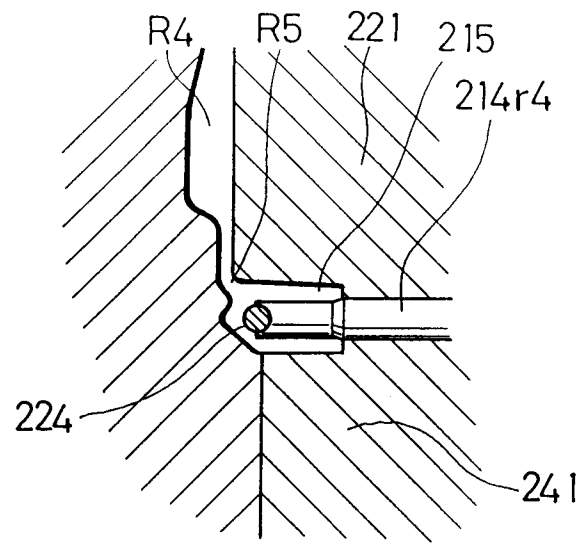


FIG. 9

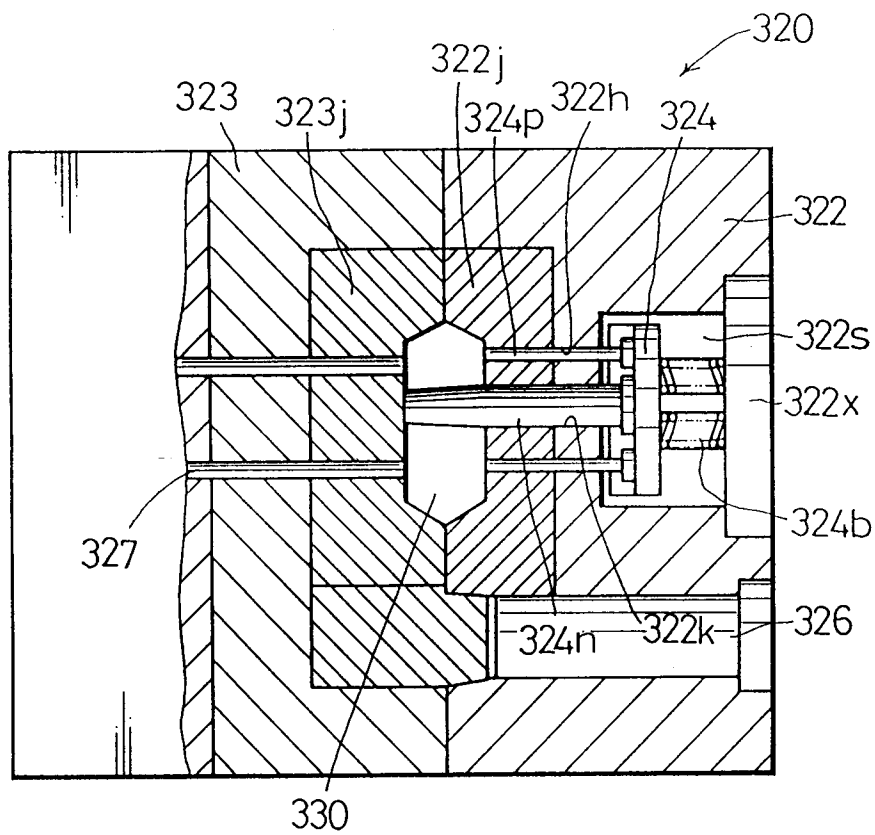


FIG. 10

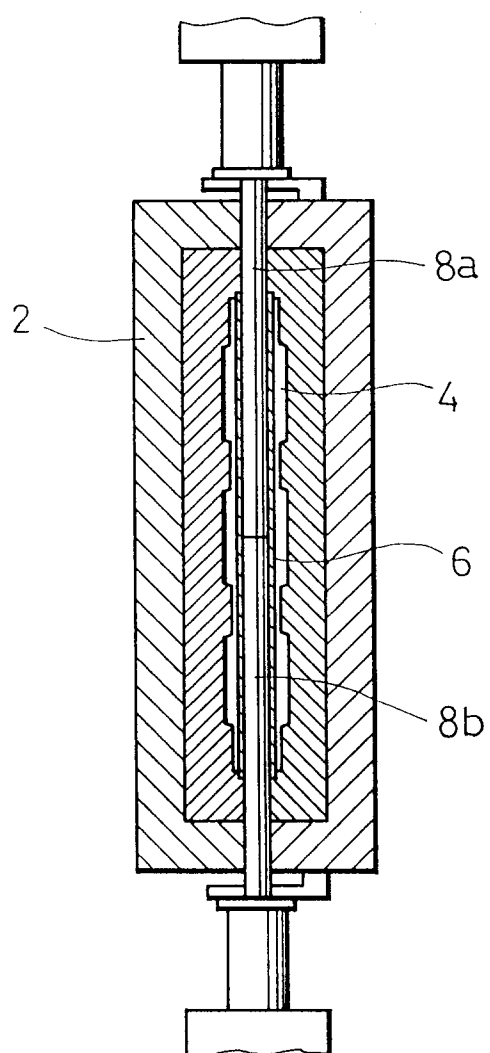


FIG.11
PRIOR ART

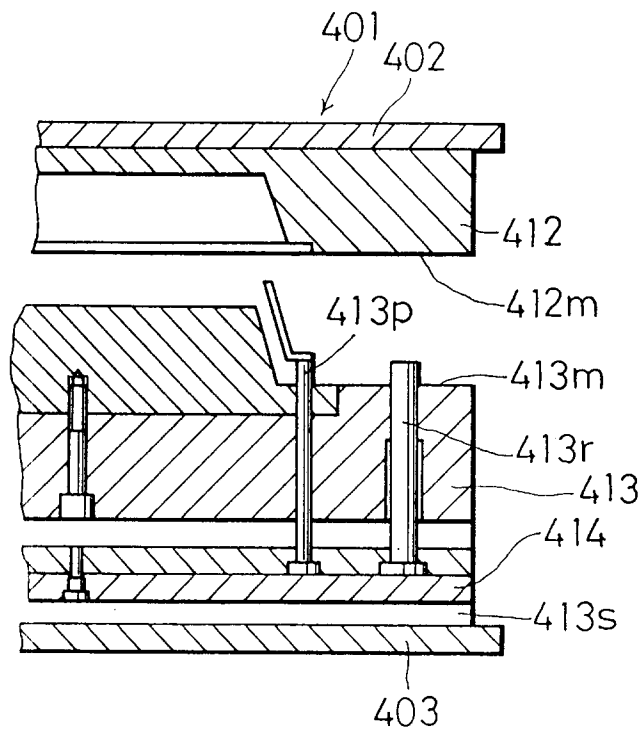


FIG.12(A)

PRIOR ART

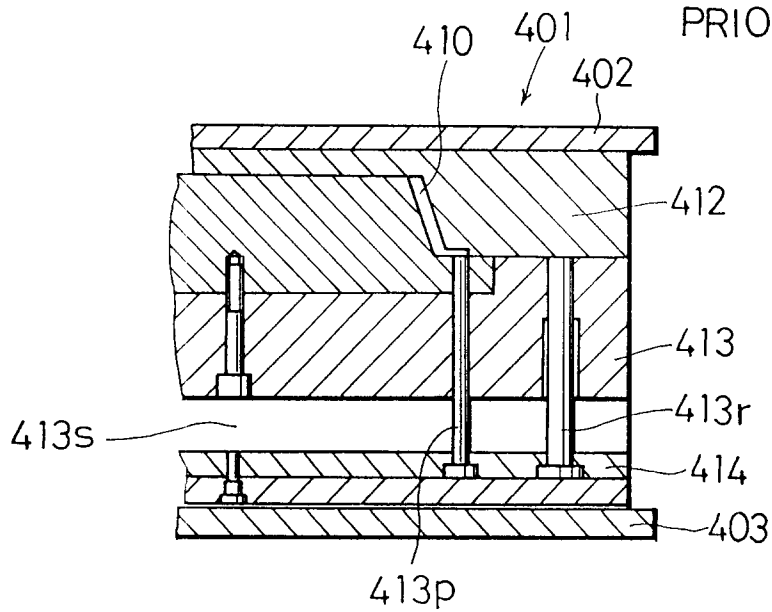


FIG.12(B)

PRIOR ART



European Patent
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EUROPEAN SEARCH REPORT

Application Number
EP 94 11 9750

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
A	FR-A-2 637 322 (WEBER S.R.L.) * abstract *	1-3, 5, 6	B22D17/24
D,A	--- PATENT ABSTRACTS OF JAPAN vol. 10, no. 155 (M-485) 4 June 1986 & JP-A-61 009 959 (HONDA GIKEN KOGYO KK) 17 January 1986 * abstract *		
D,A	--- PATENT ABSTRACTS OF JAPAN vol. 9, no. 55 (M-362) 9 March 1985 & JP-A-59 189 062 (TOUYOU DENSAN KK) 26 October 1984 * abstract *		
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			B22D F02M
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 12 April 1995	Examiner Hodiamont, S
CATEGORY OF CITED DOCUMENTS			
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