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(54) FLUID-CONDUCTING SWIVEL AND METHOD

STRÖMUNGSLEITENDE DREHKUPPLUNG UND VERFAHREN

DISPOSITIF PIVOTANT GUIDANT UN FLUIDE ET PROCEDE

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Description

This invention relates to a fluid-conducting swivel and method for making the same.

Fluid-conducting swivels are known and commercially available. Typical applications include fluid-driven rotating machinery and tools and fluid-spraying rotating cleaning equipment. Shortcomings of prior fluid-conducting swivels include the use of O-rings, packing, or other friction-generating seals which make surface contact to seal and prevent fluid passage between the relatively rotating members of the swivels. The physical contact between such seals and the rotating member(s) generates the friction which retards the ability of the members to rotate and which causes the seal to deteriorate relatively rapidly.

U.S. Patent No. 4,923,120 discloses a nozzle device having a labyrinth-like sealing gap which uses a vacuum created at the outlet of a pressurized orifice to draw fluid through the sealing gap and improve its sealing action. This ingestion or inspiration through the gap increases the pressure loss in the nozzle device.

U.S. Patent No. 5060862 discloses a fluid-conducting swivel comprising an upstream conduit having a first end connectable to a fluid source, a second end, and a first fluid passageway extending between the first and second ends, said first fluid passageway having an upstream nozzle of reducing diameter upstream of the second end and an upstream throat extending between the nozzle and the second end; a downstream conduit having a first end connectable to a fluid user, a second end, and a second fluid passageway extending between the first and second ends said second fluid passageway having a downstream nozzle and a downstream throat extending between the downstream nozzle and the second end; and support means which hold the upstream and downstream conduits with the first and second passageways aligned, while allowing rotation of one of the upstream and downstream conduits, and maintaining a space between the upstream and downstream conduits.

Starting from this document the present invention is characterised in that said upstream nozzle and the upstream throat are sized substantially to prevent expansion, in use, of the fluid discharged from the upstream conduit; and

the sizing of the nozzles, the throats and the space between the upstream and the downstream conduits substantially preventing, in use, expansion of the accelerated fluid in the space, thereby substantially preventing fluid leakage and pressure loss between the upstream and downstream conduit.

The present invention provides also a method of making a fluid-conducting swivel according to claim 9. US Patent No. 5060862 represents the prior art such as referred to in the preamble of claim 9.

The present invention provides a fluid-conducting swivel which does not require the use of friction-gener-

ating seals or relatively expensive labyrinth-type seals, which requires little if any pressure loss across the swivel, and which is relatively inexpensive to manufacture and maintain.

Furthermore, as compared with US Patent No. 5060862, the nozzles and throats of the present invention have been deliberately sized, in view of the operating conditions, to prevent expansion of the fluid, thereby substantially preventing fluid leakage and pressure loss between the upstream and downstream conduit.

The upstream acceleration nozzle is sized to reduce the size of the fluid passageway and accelerate the velocity of the fluid flow to such a velocity that the fluid creates a substantially self-contained fluid jet which exerts substantially no pressure on the walls of the upstream and downstream throats. The upstream and downstream throats are sized to maintain the fluid flow at a substantially constant velocity between the upstream throat and the downstream nozzle.

The present invention provides a fluid-velocity-coupled swivel which eliminates the need for friction-generating surface-contacting seals and has the advantages of a sealed coupling (low pressure drop and low leakage); but does not require the maintenance or have the friction-generating seal contact of the sealed couplings.

The present invention provides a swivel which is adaptable for use with fluid-driven rotating surface-cleaning devices and which will facilitate higher rotational velocities than prior swivels having friction-generating contact sealing and which will therefore clean much faster and require less maintenance.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be better understood by reference to the examples of the following drawings:

Fig. 1 is a schematic diagram of an embodiment of a swivel of the present invention;

Fig. 2 is a sectional side view of an embodiment of a swivel of the present invention; and

Fig. 3 is a view along line 3-3 of Fig. 2.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Preferred embodiments of the invention will now be described with reference to the drawings. Like characters refer to like or corresponding parts throughout the drawings and description.

Figures 1-3 present embodiments of the apparatus and method of the fluid-conducting swivel, generally designated 20, of the present invention. Although a preferred embodiment of the swivel 20, described herein to facilitate an enabling understanding of the invention, is a high pressure surface cleaning device, as is used with pressure washing equipment for cleaning surfaces such as concrete and asphalt parking areas, sidewalks,

driveways, swimming pool decks, garage floors, restaurant floors, and traffic areas; it is intended to be understood that the invention may be adapted to many applications, including snowmaking equipment, humidifying equipment for food storage and nursery hot-houses, fire sprinkler heads for enclosed rooms, fire fighting diffusion nozzles for close flame suppression, showerhead spinners, fruit orchard fogging equipment, insect spray fogging equipment, private automobile and home cleaning nozzles, pollution-reducing oil and gas aerating combustion nozzles, pollution-reducing refinery flare fuel mixing and aeration nozzles, pollution-reducing incineration liquid or gas mixing nozzles, municipal sewage aeration nozzles which speed up the oxidation process, and as a fluid-conducting coupling for fluid-driven rotating equipment. It is also contemplated that the swivel of the present invention may be used as a low-friction, high-efficiency jet engine thrust-coupling which provides direct propulsion through the rotors on helicopters and eliminates the need for a rotor drive section and its mechanical losses; as a low-friction, high-efficiency thrust-coupling for the operation of turbo-prop engines which allows the jet exhaust to pass directly through the inside of each propeller blade and discharges the exhaust at right angles to the blade rotation; and as a coupling device for a high RPM turbine drive attached to an external stoichiometric, high-efficiency, pressurized combustion system capable of generating pollution-free electrical and mechanical power for municipal use and private transportation use.

Referring to the example of Fig. 1, the fluid-conducting swivel 20 may be generally described as including an upstream conduit 22, a downstream conduit 24, and support means 26 (Fig. 2) for allowing rotation of one of the upstream and downstream conduit 22, 24 and for maintaining a space or gap 28 between the upstream and downstream conduit 22, 24. The support means 26 may be designed to allow rotation of both the upstream and downstream conduit 22, 24, as would be known to one skilled in the art in view of the disclosure contained herein. The support means 26 may also be used to hold the upstream and downstream conduit 22, 24 in proper alignment, as is discussed below. The preferred support means 26 includes a bearing assembly 30 (Fig. 2) which may be connected to allow rotation of one or both of the upstream and downstream conduit 22, 24.

The upstream conduit 22 has a first end 36 connectable to a fluid source 38 (Fig. 2), a second end 40, and a fluid passageway 42 extending through the first and second ends 36, 40. The upstream conduit 22 also includes an acceleration nozzle 44 disposed in the fluid passageway 42 for accelerating the velocity of fluid flow through the fluid passageway 42 and an upstream throat 46 which extends between the acceleration nozzle 44 and the second end 40 of the upstream conduit 22 for maintaining the accelerated velocity of the fluid flow from the acceleration nozzle 44.

The acceleration nozzle 44 reduces the size of the fluid passageway 42 and thereby provides a means for accelerating the velocity of the fluid flow to such a velocity that the fluid exerts substantially no pressure on the walls 48 of the upstream throat 46. The acceleration nozzle 44 may also be described as providing a means for reducing the size of the fluid passageway 42 and thereby accelerating the velocity of the fluid flow to such a velocity that the fluid creates a substantially self-contained fluid jet which exerts little or no radially outward pressure and has little dissociation, particularly at points on the fluid jet in close proximity to its discharge from the second end 40 of the upstream conduit 22, as does a nozzle on a garden hose or high pressure air hose.

The upstream throat 46 has a substantially constant cross-sectional area (in radial cross-section with respect to the axis 50) in order to maintain the accelerated velocity of the fluid flow and to maintain a self-contained fluid jet created by the acceleration nozzle 44. Preferably, the acceleration nozzle 44 is frusto-conically shaped (in axial cross-section), converges in the direction of fluid flow, and the converging walls 44 form an angle of 60° or less with the axis 50 of the fluid passageway 42 and upstream throat 46. The preferred upstream throat 46 maintains the reduced size of the fluid passageway 42 created by the acceleration nozzle 44 and extends the reduced size to the upstream conduit second end 40.

The downstream conduit 24 has a first end 56 connectable to a fluid user 58 (Figs. 2 and 3), a second end 60, and a fluid passageway 62 extending through the first and second ends 56, 60. The downstream conduit 24 also includes a deceleration nozzle 64 disposed in the fluid passageway 62 for decelerating the velocity of the fluid flow through the fluid passageway 62 and a downstream throat 66 which extends between the deceleration nozzle 64 and the second end 60 of the downstream conduit 24. The downstream throat 66 provides a means for receiving the accelerated fluid from the upstream throat 46 and for substantially preventing expansion of the accelerated fluid, thereby substantially preventing fluid leakage and pressure loss between the upstream and downstream conduit 22, 24. The downstream throat 66 receives the substantially self-contained fluid jet from the upstream throat 46 before the discharged fluid jet has time to expand or dissociate and is sized (in radial cross-section) to prevent expansion of the stream inside the throat 66.

The preferred downstream throat 66 has substantially the same radially cross-sectional area and shape (with respect to the axis 50 of the downstream throat) as the upstream throat 46 in order to substantially prevent dissociation and expansion of the fluid between the upstream and downstream throats 46, 66. If the downstream throat is substantially larger than the upstream throat, the fluid received by the downstream throat 66 will expand and ingest or inspire air or other fluid through the gap 28 which will cause an undesirable irre-

coverable pressure loss between the upstream and downstream conduit 22, 24. By being designed and sized to have substantially the same radially cross-sectional area and shape as the upstream throat 46 and to have a substantially constant radially cross-sectional area along its axis 50, the downstream throat 66 also maintains the fluid flow at a substantially constant velocity between the upstream throat 46 and the deceleration nozzle 64.

The downstream throat 66 receives the accelerated fluid from the upstream throat 46 and creates a fluid seal between the second end 60 of the downstream conduit 24 and the deceleration nozzle 64 which substantially prevents expansion of the accelerated fluid upstream of the deceleration nozzle 64. In other words, by having substantially the same cross-sectional shape and area as the upstream throat, the downstream throat 66 receives the fluid discharged from the upstream throat 46 and the fluid contacts the walls 68 of the downstream throat 66 which creates a fluid seal which prevents the ingestion or inspiration of air or other fluid through the gap 28 into the downstream throat 66 and thereby prevents an undesirable, irrecoverable loss of fluid pressure between the upstream and downstream conduit 22, 24. The fluid passageway 62 and fluid user 58 should be sized to allow fluid flow through the swivel 20 without sufficient restriction to cause back pressure in the downstream throat 66 and space or gap 28.

The deceleration nozzle 64 provides a means for enlarging the size of the fluid passageway 62 and thereby decelerates the velocity of the fluid flow through the passageway 62. The preferred deceleration nozzle 64 is frusto-conically shaped (in axial cross-section), diverges in the direction of flow, and has walls 64 which form an angle of 60° or less with the flow axis 50 of the downstream throat 66. Preferably, the acceleration and deceleration nozzles 44, 64 are substantially identical and equidistantly spaced from the second ends 40, 60 of the upstream and downstream conduit 22, 24. More preferably, the nozzles 44, 64; upstream and downstream conduit 22, 24; and upstream and downstream throats 46, 66 are substantially symmetrical in axial cross-section, as exemplified in Figs. 1 and 2.

In a preferred embodiment, referring to the example of Figs. 2 and 3, the fluid user 58 includes at least one discharge nozzle 72 in fluid communication with the first end 56 of the downstream conduit 24. The discharge nozzle 72 is displaced radially with respect to the axis 50 of the downstream throat 66 and is directed downstream along an axis that is skewed with respect to the axis 50 and lies in a plane parallel to the axis 50 in order to cause rotation of the downstream conduit 24 about the axis 50.

Figs. 2 and 3 exemplify a prototype of the inventive swivel 20 which is adapted for use as a high-pressure rotating cleaning device such as may be used in cleaning concrete surfaces, cleaning rusted surfaces, cleaning painted surfaces, in rotating car wash nozzles, etc.

Since the swivel 20 does not have friction-generating, surface-contacting seals but instead uses the accelerated velocity of the fluid stream to effectively seal the gap 28 between the upstream and downstream conduit 22, 24 and recovers on the order of 97% of the pressure drop used to accelerate the fluid, the fluid pressure may be efficiently used to both rotate the discharge nozzles 72 and clean the desired surface.

In the swivel 20, the fluid user 58 includes two diametrically opposed discharge nozzles 72. Each nozzle 72 is displaced radially with respect to the axis 50. The nozzles 72 are directed so that they discharge downstream (in the same general direction as the flow through the swivel 20 and downstream conduit 24) along an axis that is skewed or at an angle with respect to the axis 50 and which lies in a plane parallel to the axis 50 in order to cause rotation of the discharge nozzle 72 and downstream conduit 24 about the axis 50. Preferably, the discharge nozzles 72 are equidistantly spaced from the axis 50. The distance between the axis 50 and the discharge axis of the discharge nozzle 72 may be selected to control the speed of rotation of the discharge nozzle 72. Also, the angle at which the discharge nozzles 72 discharge may be selected to control the speed of rotation of the discharge nozzles for a given fluid and discharge pressure, as would be known to one skilled in the art in view of the disclosure contained herein. The speed of rotation will be proportional to the thrust generated at the discharge nozzles and the skew or angle of the discharge nozzles, i.e., since the swivel 20 has no friction-creating sealing surfaces to retard the speed of rotation, the swivel's ability to operate within a broad range of rotational speeds is dependent only on the selection of the bearing assembly 30, the distance the discharge nozzles 72 are displaced from the flow axis 50, and the skew or angle at which the discharge nozzles 72 discharge with respect to the axis 50. Preferably, the discharge nozzles 72 are located at the end of conduital arms 76 which transmit the fluid to the nozzles 72 along a flow path about perpendicular to the axis 50 of the downstream conduit 24. In the prototype swivel, as viewed in Fig. 3, the nozzles 72 are skewed an angle of about twenty degrees (20°) counter-clockwise with respect to the longitudinal axis of arms 76) so that the thrust generated at the nozzles rotates the arms 76 in a clockwise direction (as viewed in Fig. 3).

The fluid user 58 is connected to the downstream conduit 24. The downstream conduit 24 and deceleration nozzle 64 may be integrally formed with the fluid user 58 or may be separate components, depending upon the materials of construction. The fluid user 58 is also connected to the bearing retainer 78 so that the fluid user 58 and downstream conduit 24 rotate with the inner bearing race 80. Orifices 82 are provided in bearing retainer housing 84 to allow for discharge of any leakage or fluid accumulation (such as will occur if the gap 28 is adjusted so that there is a positive pressure

outside the conduit 22, 24 at the gap 28). Preferably, three evenly spaced orifices 82 are provided. In the prototype swivel 20, the bearing retainer housing 84 is a component of the support means 26 and as such is used to align and position the upstream and downstream conduit 22, 24. The upstream and downstream conduit are positioned so that the upstream and downstream throats 46, 66 are axially and concentrically aligned along axis 50. The fluid user 58 is threadably engaged with the bearing retainer housing 84 to allow adjustment of the size of the space or gap 28, i.e., to adjust the distance between the second ends 40, 60 of the upstream and downstream conduit 22, 24, as will be further discussed below.

The upstream conduit 22 extends inside the bearing retainer 78 so that the second ends 40, 60 of the upstream and downstream conduit 22, 24 are adjacent. The upstream conduit 22 does not contact the bearing retainer 78. The first end 36 of the upstream conduit is connected to a fluid source 38, which is illustrated as a high pressure fluid connection or fitting which can be connected to a pump, compressor, or other fluid supply. The maximum pressure rating of the swivel 20 is limited only by the strength of the materials of which the swivel 20 and fluid user 58 are manufactured. The first end 36 of the upstream conduit 22 is also connected to the support means 26 which forms the bearing housing, also designated 26. The bearing housing 26 and upstream conduit 22 are fixed so that the downstream conduit 24 and fluid user 58 rotate with respect to the bearing housing 26.

The fluid user 58 and downstream conduit 24 are screwed into the bearing retainer housing 84 until contact is made between the second ends 40, 60 of the upstream and downstream conduit 22, 24. The fluid user 58 is then unscrewed just enough to allow rotation of the fluid user 58 and downstream conduit 24 without contact between the second ends 40, 60. This creates a space or gap 28 between the second ends 40, 60 on the order of one or two thousandths of an inch. The space or gap 28 should be adjusted so that there is zero or slightly positive pressure on the outside of the conduit 22, 24 adjacent the gap 28 during operation of the swivel 20, in order to prevent inspiration of air or fluid through the gap and undesirable irrecoverable pressure loss in the fluid flowing through the swivel 20. Normally, the gap 28 will be as small as mechanically possible without the second ends 40, 60 of the conduit 22, 24 making contact. The gap 28 should be sufficiently spaced to accommodate expansion characteristics of the materials of which the swivel 20 is constructed and to allow for thermal expansion of the materials at the operating temperatures of the swivel 20.

As previously mentioned, the fluid user 58 and fluid passageways downstream of the deceleration nozzle 64 should be sized, in view of the anticipated fluid properties and operating pressures within the swivel, to pass the fluid without creating undesirable back pressure in

the downstream throat 66 and gap 28. In the prototype swivel 20, the upstream conduit 22 has an internal diameter of 0.272 inches, the upstream throat 46 has an internal diameter of 0.073 inches, and the acceleration nozzle 44 converges at an angle of about 60°. The downstream conduit 24 has an internal diameter of 0.272 inches, the downstream throat 66 has an internal diameter of 0.076 inches, and the deceleration cone diverges at an angle of approximately 60°. The internal diameter of each of the upstream and downstream throats 46, 66 is constant along the length or flow axis of the throat in order to stabilize the rate of change of the fluid velocity at the gap 28 and minimize the possibility of fluid expansion and fluid inspiration at the gap 28.

In an operational test of the swivel 20, the fluid source 38 was connected to a pump having a discharge pressure of 1000 psig at 3 gallons per minute. In the test, the pressure in the upstream conduit 22 was measured at 1000 psig and the recovered pressure in the downstream conduit 24 downstream of the deceleration nozzle 64 was measured at 975 psig. Subsequent tests with pumps having capacities of 4 gallons per minute and 4.5 gallons per minute and discharge pressures of up to 3000 psi have also resulted in pressure recoveries downstream of the deceleration nozzle 64 on the order of about 97% of the pressure upstream of the acceleration nozzle 44.

Although the swivel will work with liquid or gas, gas will require a higher velocity to prevent dissociation at the gap 28. In the operational test, water was used as the test fluid. It was observed that the swivel worked best at fluid velocities in the upstream and downstream throats 46, 66 of between 200 and 320 feet per second. It is intended to be understood that subsequent swivel designs using this invention may, because of different cross-sectional areas and shapes or many other factors, operate best at substantially higher or lower velocity rates. In any given application, good design criteria dictate that the conduit 22, 24, throats 46, 66, and nozzles 44, 64 should be sized, taking into account the fluid properties and operating pressures, as well as other relevant factors, so that the fluid velocities in the throats 46, 66 are high enough to prevent dissociation of the fluid stream at the gap 28 and are low enough to prevent developing a vacuum at the gap 28.

In the prototype swivel 20, the internal diameter of the downstream throat 66 was three thousandths of an inch larger than the upstream throat 46 to allow for a slight misalignment between the upstream and downstream conduit 22, 24 and greater than 97% pressure recovery was obtained, as previously discussed. Only a small, insignificant loss of fluid occurred at the gap 28 and it is contemplated that this was due to the concentricity mismatch of the upstream and downstream throats 46, 66. Ideally, the upstream and downstream throats 46, 66 would be identically the same shape (normally circular or cylindrical) and internal diameter and the reason they are not in the prototype swivel 20 is to

compensate for alignment variations. The internal diameter of the downstream throat 66 is sufficiently matched to that of the upstream throat 46 that it is possible to create a slightly positive pressure outside the conduit 22, 24 at the gap 28 while maintaining a large enough gap to prevent contact between the first and second conduit 22, 24 during rotation. It is contemplated that pressure recoveries downstream of the deceleration nozzle 64 much closer to 100% of the applied pressure upstream of the acceleration nozzle 44 may be obtained as the dimensions and shapes of the fluid passageways 42, 62, nozzles 44, 64, and throats 46, 66 are optimized.

Another discovery made during testing was that when the static recovered pressure downstream of the deceleration nozzle 64 is added to the calculated pressure increase due to the centrifugal pump effect of the discharge nozzles 72 rotating at high speeds, the effective discharge pressure downstream of the discharge nozzles 72 may be higher than the pump discharge pressure at the fluid source 38. At the present time, the inventors have not actually measured this pressure, although it is contemplated that it may be calculated from the length of the conduit arm 76 and the rotational velocity of the nozzles 72.

Two or more of the swivels 20 may be serially connected or staged to achieve higher rotational speeds without multiplying any form of sealing friction, as would occur if conventionally sealed swivels were mounted serially. For example, the conduit arms 76 and discharge nozzles 72 of Fig. 2 may be replaced with a second bearing housing 26 having a second bearing assembly 30, second upstream conduit 22, and second acceleration nozzle 44 with the fluid user 58 connected to a second bearing retainer housing for the second bearing assembly 30. This sequential staging of two swivels would allow the discharge nozzles to rotate at twice the maximum speed of the individual bearing assemblies, e.g., if the bearing assemblies were individually rotated for 5,000 RPM, the discharge nozzles would rotate at a maximum speed of approximately 10,000 RPM with each individual bearing assembly rotating at its maximum of 5,000 RPM.

Referring to Figs. 1 and 2, the method of making a fluid-conducting swivel 20 includes accelerating the velocity of a fluid flowing in a fluid passageway 42 from a first end 36 through a second end 40 of an upstream conduit 22; receiving the fluid discharged from the second end 40 of the upstream conduit 22 in a fluid passageway 62 in the second end 60 of a downstream conduit 24 and substantially preventing expansion of the fluid discharge from the upstream conduit 22; substantially preventing expansion of the fluid in a downstream throat 66 of the fluid passageway 62 of the downstream conduit 24, the downstream throat 66 extending from the second end 60 of the downstream conduit 24 to a deceleration nozzle 64 in the fluid passageway 62 of the downstream conduit 24; rotatably mounting one of the upstream and downstream conduit

22, 24 for rotation about an axis 50 extending through the adjacent second ends 40, 60 of the upstream and downstream conduit 22, 24; and maintaining a space 28 between the adjacent second ends 40, 60 of the upstream and downstream conduit 22, 24. The method provides for reducing the size of the fluid passageway 42 with an acceleration nozzle 44 disposed in the upstream conduit 22 and thereby accelerating the fluid velocity to such a velocity that the fluid exerts substantially no pressure on the walls 48 of the fluid passageway. The method also provides for reducing the size of the fluid passageway 42 with the acceleration nozzle 44 and accelerating the velocity of the fluid flow to such a velocity that the fluid creates a substantially self-contained fluid jet. The upstream conduit 22 includes an upstream throat 46 having a substantially constant cross-sectional area in order to maintain the velocity of the self-contained fluid jet from the acceleration nozzle 44 to the upstream conduit second end 40.

The method provides the downstream throat 66 having substantially the same cross-sectional area and shape as the upstream throat 46 in order to substantially prevent dissociation and expansion of the fluid in the gap 28 between the upstream and downstream throats 44, 66. The downstream throat 66 maintains the fluid flow at a substantially constant velocity between the upstream throat 46 and the deceleration nozzle 64. The downstream throat 66 provides for receiving the accelerated fluid and creating a fluid seal between the second end 60 of the downstream conduit 24 and the deceleration nozzle 64 in order to substantially prevent expansion of the accelerated fluid upstream of the deceleration nozzle 64.

While presently preferred embodiments of the invention have been described herein for the purpose of disclosure, numerous changes in the construction and arrangement of parts and the performance of steps will suggest themselves to those skilled in the art in view of the disclosure contained herein, within the scope of the following claims.

Claims

1. A fluid-conducting swivel (20) comprising an upstream conduit (22) having a first end (36) connectable to a fluid source (38), a second end (40), and a first fluid passageway (42) extending between the first and second ends (36,40), said first fluid passageway having an upstream nozzle (44) of reducing diameter upstream of said second end and an upstream throat (46) extending between the nozzle (44) and the second end (40);

a downstream conduit (24) having a first end (56) connectable to a fluid user (58), a second end (60), and a second fluid passageway (62) extending between the first and second ends (56,60), said second fluid passageway having

- a downstream nozzle (64) of increasing diameter downstream of said second end (60) and a downstream throat (66) extending between the nozzle (64) and the second end (60); and support means (26) which hold the upstream and downstream conduits (22,24) with the first and second passageways (42,62) aligned, while allowing rotation of one of the upstream and downstream conduits (22,24), and maintaining a space (28) between the upstream and downstream conduits (22,24); characterised in that said upstream nozzle (44) and the upstream throat (46) are sized substantially to prevent expansion, in use, of the fluid discharged from the upstream conduit (22); and the sizing of the nozzles (44,64), throats (46,66), and the space (28) between the upstream and the downstream conduits substantially preventing, in use, expansion of the accelerated fluid in the space (28), thereby substantially preventing fluid leakage and pressure loss between the upstream and downstream conduits (22,24).
2. A swivel according to claim 1, characterised in that the support means (26) allows rotation of both the upstream and downstream conduits (22,24).
 3. A swivel according to claim 1 or 2, wherein the upstream nozzle (44) is characterised as reducing the size of the fluid passageway (42) and thereby accelerating the velocity of the fluid flow to such a velocity that the fluid exerts substantially no pressure on the walls (48) of the upstream throat (46).
 4. A swivel according to claim 1, wherein the upstream nozzle (44) is characterised as reducing the size of the fluid passageway (42) and thereby accelerating the velocity of the fluid flow to such a velocity that the fluid creates a substantially self-contained fluid jet, the upstream throat (46) being of substantially constant cross-sectional area in order to maintain the self-contained fluid jet.
 5. A swivel according to any preceding claim, wherein the downstream throat (66) is characterised as having substantially the same cross-sectional area and shape as the upstream throat (46) in order to substantially prevent dissociation and expansion of the fluid between the upstream and downstream throats (46,66).
 6. A swivel according to claim 5, wherein the downstream throat (66) is characterised as maintaining the fluid flow at a substantially constant velocity between the upstream throat (46) and the downstream nozzle (64).
 7. A swivel according to any preceding claim, wherein the downstream throat (66) is characterised as receiving the accelerated fluid and creating a fluid seal between the second end (60) of the downstream conduit (24) and the downstream nozzle (64) in order to substantially prevent expansion of the accelerated fluid upstream of the downstream nozzle (64).
 8. A swivel according to any preceding claim, characterised in that the fluid user (58) comprises at least one discharge nozzle (72) in fluid communication with the first end (56) of the downstream conduit (24) and displaced radially with respect to the flow axis of the downstream throat (66) and directed downstream along an axis that is skewed with respect to the flow axis and lies in a plane parallel to the flow axis in order to cause rotation of the downstream conduit (24) about the flow axis.
 9. A method of making a fluid-conducting swivel (20), comprising the steps of:-
 - (a) accelerating the velocity of a fluid flowing in a fluid passageway (42) from a first end (36) through a second end (40) of an upstream conduit (22); characterised by
 - (b) receiving the fluid discharged from the second end (40) of the upstream conduit (22) in a fluid passageway (62) in the second end (60) of a downstream conduit (24) and substantially preventing expansion of the fluid discharged from the upstream conduit (22);
 - (c) substantially preventing expansion of the fluid in a downstream throat (66) of the fluid passageway (62) of the downstream conduit (24), the downstream throat (66) extending from the second end (60) of the downstream conduit (24) to a deceleration nozzle (64) in the fluid passageway (62) of the downstream conduit (24);
 - (d) rotatably mounting one of the upstream and downstream conduits (22,24) for rotation about an axis extending through the adjacent second ends (40,60) of the upstream and downstream conduits (22,24); and
 - (e) maintaining a space (28) between the adjacent second ends (40,60) of the upstream and downstream conduit (22,24).
 10. A method according to claim 9 in which step (a) comprises:

rotatably mounting both the upstream and the downstream conduits (22,24).
 11. A method according to claim 9 or 10 in which step (a) comprises:

reducing the size of the fluid passageway (42) with an acceleration nozzle (44) disposed in the upstream conduit (22) and thereby accelerating the fluid velocity to such a velocity that the fluid exerts substantially no pressure on the walls (48) of the fluid passageway (42).

12. A method according to claim 9, 10 or 11 in which step (a) comprises:

reducing the size of the fluid passageway (42) with an acceleration nozzle (44) disposed in the upstream conduit (22) and thereby accelerating the velocity of the fluid flow to such a velocity that the fluid creates a substantially self-contained fluid jet, the upstream throat (46) having a substantially constant cross-sectional area in order to maintain the velocity of the self-contained fluid jet.

13. A method according to claim 12 wherein the downstream throat (66) is defined as having substantially the same cross-sectional area and shape as the upstream throat (46) in order to substantially prevent dissociation and expansion of the fluid between the upstream and downstream throats (46,66).

14. A method according to claim 13, wherein the downstream throat (66) is defined as maintaining the fluid flow at a substantially constant velocity between the upstream throat (46) and the deceleration nozzle (64).

15. A method according to any one of claims 10 to 14, wherein the downstream throat (66) is defined as receiving the accelerated fluid and creating a fluid seal between the second end (60) of the downstream conduit (24) and the deceleration nozzle (64) in order to substantially prevent expansion of the accelerated fluid upstream of the deceleration nozzle (64).

Patentansprüche

1. Eine fluidführende Drehbefestigung (20), aufweisend: eine Stromaufwärtsleitung (22) mit einem ersten Ende (36), das mit einer Fluidquelle (38) verbindbar ist, einem zweiten Ende (40) und einer ersten Fluidpassage (42), die sich zwischen dem ersten Ende (36) und dem zweiten Ende (40) erstreckt, wobei die erste Fluidpassage eine Stromaufwärtsdüse (44) mit einem reduzierten Durchmesser stromaufwärts von dem genannten zweiten Ende und einen Stromaufwärtsdurchlaß (46) aufweist, der sich zwischen der Düse (44) und dem zweiten Ende (40) erstreckt;

eine Stromabwärtsleitung (24) mit einem ersten Ende (56), das mit einem Fluidverbraucher (48) verbindbar ist, einem zweiten Ende (60) und einer zweiten Fluidpassage (62), die sich zwischen dem ersten Ende (56) und dem zweiten Ende (60) erstreckt, wobei die genannte zweite Fluidpassage eine Stromabwärtsdüse (64) von zunehmendem Durchmesser stromabwärts von dem genannten zweiten Ende (60) sowie einen Stromabwärtsdurchlaß (66) aufweist, der sich zwischen der Düse (64) und dem zweiten Ende (60) erstreckt; und

eine Trageinrichtung (26), welche die Stromaufwärtsleitung (22) und die Stromabwärtsleitung (24) hält, wobei die erste Passage (42) und die zweite Passage (62) ausgerichtet sind, während die Trageinrichtung (26) eine Drehung der einen von beiden Leitungen, nämlich der Stromaufwärtsleitung (22) und der Stromabwärtsleitung (24) erlaubt und einen Raum (28) zwischen der Stromaufwärtsleitung (22) und der Stromabwärtsleitung (24) aufrechterhält; **dadurch gekennzeichnet, daß**

die genannte Stromaufwärtsdüse (44) und der Stromaufwärtsdurchlaß (46) so bemessen sind, um bei Anwendung eine Expansion des von der Stromaufwärtsleitung (22) abgegebenen Fluids zu verhindern; und

die Bemessung der Düsen (44, 64), der Durchlässe (46, 66) und des Raums (28) zwischen der Stromaufwärtsleitung und der Stromabwärtsleitung bei der Anwendung eine Expansion des beschleunigten Fluids in dem Raum (28) im wesentlichen verhindert, wodurch eine Fluidleckage und ein Druckverlust zwischen der Stromaufwärtsleitung (22) und der Stromabwärtsleitung (24) im wesentlichen verhindert wird.

2. Eine Drehbefestigung nach Anspruch 1, **dadurch gekennzeichnet, daß** die Trageinrichtung (26) eine Drehung sowohl der Stromaufwärtsleitung (22) als auch der Stromabwärtsleitung (24) erlaubt.
3. Eine Drehbefestigung nach Anspruch 1 oder 2, bei welcher die Stromaufwärtsdüse (44) als die Größe der Fluidpassage (42) reduzierend gekennzeichnet ist und dadurch die Geschwindigkeit des Fluidstroms auf eine solche Geschwindigkeit beschleunigt, daß das Fluid im wesentlichen keinen Druck auf die Wände (48) des Stromaufwärtsdurchlasses (46) ausübt.
4. Eine Drehbefestigung nach Anspruch 1, bei welcher die Stromaufwärtsdüse (44) als die Größe der

Fluidpassage (42) reduzierend gekennzeichnet ist und dadurch die Geschwindigkeit des Fluidstroms auf eine solche Geschwindigkeit beschleunigt, daß das Fluid einen im wesentlichen in sich geschlossenen Fluidstrahl erzeugt, wobei der Stromaufwärtsdurchlaß (46) von einem im wesentlichen konstanten Querschnittsbereich ist, um den in sich geschlossenen Fluidstrahl aufrecht zu erhalten.

5. Eine Drehbefestigung nach einem der vorhergehenden Ansprüche, bei welcher der Stromabwärtsdurchlaß (66) als im wesentlichen denselben Querschnittsbereich und dieselbe Gestalt wie der Stromaufwärtsdurchlaß (46) aufweisend gekennzeichnet ist, um eine Dissoziation und eine Expansion des Fluids zwischen dem Stromaufwärtsdurchlaß (46) und dem Stromabwärtsdurchlaß (66) im wesentlichen zu verhindern. 10
6. Eine Drehbefestigung nach Anspruch 5, bei welcher der Stromabwärtsdurchlaß (66) als den Fluidstrom auf einer im wesentlichen konstanten Geschwindigkeit zwischen dem Stromaufwärtsdurchlaß (46) und der Stromabwärtsdüse (64) haltend gekennzeichnet ist. 20
7. Eine Drehbefestigung nach einem der vorhergehenden Ansprüche, bei welcher der Stromabwärtsdurchlaß (66) als das beschleunigte Fluid aufnehmend und eine Fluiddichtung zwischen dem zweiten Ende (60) der Stromabwärtsleitung (24) und der Stromabwärtsdüse (64) erzeugend gekennzeichnet ist, um eine Expansion des beschleunigten Fluids stromaufwärts von der Stromabwärtsdüse (64) im wesentlichen zu verhindern. 25
8. Eine Drehbefestigung nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet**, daß der Fluidverbraucher (58) wenigstens eine Abgabledüse (72) in Fluidverbindung mit dem ersten Ende (56) der Stromabwärtsleitung (24) aufweist, wobei diese Abgabledüse (72) in Bezug auf die Stromachse des Stromabwärtsdurchlasses (66) radial versetzt und stromabwärts entlang einer Achse gerichtet ist, welche in Bezug auf die Stromachse abgeschrägt ist und in einer Ebene parallel zu der Stromachse liegt, um eine Drehung der Stromabwärtsleitung (24) um die Stromachse zu verursachen. 30
9. Ein Verfahren zum Herstellen einer fluidführenden Drehbefestigung (20), wobei das Verfahren die folgenden Schritte aufweist: 35

(a) Beschleunigen der Geschwindigkeit eines Fluids, das in einer Fluidpassage (42) von einem ersten Ende (36) durch ein zweites

Ende (40) einer Stromaufwärtsleitung (22) strömt; **gekennzeichnet durch**

(b) Aufnehmen des Fluids, das von dem zweiten Ende (40) der Stromaufwärtsleitung (22) abgegeben wird, in einer Fluidpassage (62) in dem zweiten Ende (60) einer Stromabwärtsleitung (24) und im wesentlichen Verhindern einer Expansion des von der Stromaufwärtsleitung (22) abgegebenen Fluids;

(c) im wesentlichen Verhindern einer Expansion des Fluids in einem Stromabwärtsdurchlaß (66) der Fluidpassage (62) der Stromabwärtsleitung (24), wobei sich der Stromabwärtsdurchlaß (66) von dem zweiten Ende (60) der Stromabwärtsleitung (24) zu einer Verlangsamungsdüse (64) in der Fluidpassage (62) der Stromabwärtsleitung (24) erstreckt;

(d) drehbares Anbringen der einen der beiden Leitungen, nämlich der Stromaufwärtsleitung (22) und der Stromabwärtsleitung (24) zum Drehen um eine Achse, die sich durch die benachbarten zweiten Enden (40 bzw. 60) der Stromaufwärtsleitung (22) bzw. der Stromabwärtsleitung (24) erstreckt; und

(e) Aufrechterhalten eines Raumes (28) zwischen den benachbarten zweiten Enden (40 bzw. 60) der Stromaufwärtsleitung (22) bzw. der Stromabwärtsleitung (24).

10. Ein Verfahren nach Anspruch 9, bei welchem der Schritt (a) aufweist:

drehbares Anbringen sowohl der Stromaufwärtsleitung (22) als auch der Stromabwärtsleitung (24).

11. Ein Verfahren nach Anspruch 9 oder 10, bei welchem der Schritt (a) aufweist:

Reduzieren der Größe der Fluidpassage (42) mit einer Beschleunigungsdüse (44), die in der Stromaufwärtsleitung (22) angeordnet ist, und hierdurch Beschleunigen der Fluidgeschwindigkeit auf eine solche Geschwindigkeit, daß das Fluid im wesentlichen keinen Druck auf die Wände (48) der Fluidpassage (42) ausübt.

12. Ein Verfahren nach Anspruch 9, 10 oder 11, bei welchem der Schritt (a) aufweist:

Reduzieren der Größe der Fluidpassage (42) mit einer Beschleunigungsdüse (44), die in der Stromaufwärtsleitung (22) angeordnet ist, und

hierdurch Beschleunigen der Geschwindigkeit des Fluidstroms auf eine solche Geschwindigkeit, daß das Fluid einen im wesentlichen in sich geschlossenen Fluidstrahl erzeugt, wobei der Stromaufwärtsdurchlaß (46) einen im wesentlichen konstanten Querschnittsbereich aufweist, um die Geschwindigkeit des in sich geschlossenen Fluidstrahls aufrecht zu erhalten.

13. Ein Verfahren nach Anspruch 12, bei welchem der Stromabwärtsdurchlaß (66) als im wesentlichen denselben Querschnittsbereich und dieselbe Gestalt wie der Stromaufwärtsdurchlaß (46) aufweisend definiert ist, um eine Dissoziation und eine Expansion des Fluids zwischen dem Stromaufwärtsdurchlaß (46) und dem Stromabwärtsdurchlaß (66) im wesentlichen zu verhindern.

14. Ein Verfahren nach Anspruch 13, bei welchem der Stromabwärtsdurchlaß (66) als den Fluidstrom auf einer im wesentlichen konstanten Geschwindigkeit zwischen dem Stromaufwärtsdurchlaß (46) und der Verlangsamungsdüse (64) haltend definiert ist.

15. Ein Verfahren nach einem der Ansprüche 10 bis 14, bei welchem der Stromabwärtsdurchlaß (66) als das beschleunigte Fluid aufnehmend und eine Fluidichtung zwischen dem zweiten Ende (60) der Stromabwärtsleitung (24) und der Verlangsamungsdüse (64) erzeugend definiert ist, um eine Expansion des beschleunigten Fluids stromaufwärts von der Verlangsamungsdüse (64) im wesentlichen zu verhindern.

Revendications

1. Dispositif pivotant (20) de guidage de fluide, comprenant :

- un conduit amont (22) avec une première extrémité (36) pouvant être raccordée à une source de fluide (38), une deuxième extrémité (40) et une première voie (42) de passage de fluide qui s'étend entre les première et deuxième extrémités (36, 40), ladite première voie de passage de fluide comportant une buse amont (44) de diamètre décroissant en amont de ladite deuxième extrémité et un étranglement amont (46) qui s'étend entre la buse (44) et la deuxième extrémité (40),
- un conduit aval (24) avec une première extrémité (56) pouvant être raccordée à dispositif (58) d'utilisation de fluide, une deuxième extrémité (60) et une deuxième voie (62) de passage de fluide qui s'étend entre les première et deuxième extrémités (56, 60), ladite deuxième voie de passage de fluide comportant une buse

aval (64) de diamètre croissant en aval de ladite deuxième extrémité (60) et un étranglement aval (66) qui s'étend entre la buse (64) et la deuxième extrémité (60), et

- des moyens de support (26) qui maintiennent les conduits amont et aval (22, 24) avec les première et deuxième voies de passage (42, 62) alignées tout en permettant une rotation de l'un des conduits amont et aval (22, 24) et en maintenant un espace (28) entre les conduits amont et aval (22, 24), caractérisé en ce que :

ladite buse amont (44) et ledit étranglement amont (46) sont dimensionnés sensiblement pour empêcher une détente, en cours d'utilisation, du fluide déchargé du conduit amont (22), et la taille des buses (44, 64), des étranglements (46, 66) et de l'espace (28) entre les conduits amont et aval empêche sensiblement, en cours d'utilisation, la détente du fluide accéléré dans l'espace (28), empêchant ainsi sensiblement les fuites de fluide et les pertes de pression entre les conduits amont et aval (22, 24).

2. Dispositif pivotant selon la revendication 1, caractérisé en ce que le moyen de support (26) permet une rotation des deux conduits amont et aval (22, 24).

3. Dispositif pivotant selon la revendication 1 ou 2, dans lequel la buse amont (44) est caractérisée par le fait qu'elle réduit la taille de la voie (42) de passage de fluide et accélère ainsi la vitesse de l'écoulement de fluide jusqu'à une vitesse telle que le fluide n'exerce sensiblement aucune pression sur les parois (48) de l'étranglement amont (46).

4. Dispositif pivotant selon la revendication 1, dans lequel la buse amont (44) est caractérisée par le fait qu'elle réduit la taille de la voie (42) de passage de fluide et accélère ainsi la vitesse de l'écoulement de fluide jusqu'à une vitesse telle que le fluide crée un jet de fluide sensiblement auto-confiné, l'étranglement amont (46) ayant une section sensiblement constante pour maintenir le jet de fluide auto-confiné.

5. Dispositif pivotant selon l'une quelconque des précédentes revendications, dans lequel l'étranglement aval (66) est caractérisé par le fait qu'il a sensiblement la même section et la même forme que l'étranglement amont (46) afin d'empêcher sensiblement la dissociation et la détente du fluide entre les étranglements amont et aval (46, 66).

6. Dispositif pivotant selon la revendication 5, dans

lequel l'étranglement aval (66) est caractérisé par le fait qu'il maintient l'écoulement de fluide à une vitesse sensiblement constante entre l'étranglement amont (46) et la buse aval (64).

7. Dispositif pivotant selon l'une quelconque des précédentes revendications, dans lequel l'étranglement aval (66) est caractérisé par le fait qu'il reçoit le fluide accéléré et crée un joint étanche de fluide entre la deuxième extrémité (60) du conduit aval (24) et la buse aval (64) afin d'empêcher sensiblement la détente du fluide accéléré en amont de la buse aval (64).

8. Dispositif pivotant selon l'une quelconque des précédentes revendications, caractérisé en ce que le dispositif (58) d'utilisation de fluide comprend au moins une buse de décharge (72) en communication de passage des fluides avec la première extrémité (56) du conduit aval (24), décalée radialement par rapport à l'axe d'écoulement de l'étranglement aval (66) et dirigée en aval suivant un axe qui est incliné par rapport à l'axe d'écoulement et placé dans un plan parallèle à l'axe d'écoulement afin de provoquer une rotation du conduit aval (24) autour de l'axe d'écoulement.

9. Procédé de réalisation d'un dispositif pivotant (20) de guidage de fluide, comprenant les étapes consistant à :

a) accélérer la vitesse d'un fluide s'écoulant dans une voie (42) de passage de fluide d'une première extrémité (36) à une deuxième extrémité (40) d'un conduit amont (22), caractérisé par les étapes consistant à :

b) recevoir le fluide déchargé par la deuxième extrémité (40) du conduit amont (22) dans une voie (62) de passage de fluide formé dans la deuxième extrémité (60) d'un conduit aval (24) et empêcher sensiblement la détente du fluide déchargé du conduit amont (22),

c) empêcher sensiblement la détente du fluide dans un étranglement aval (66) de la voie (62) de passage de fluide du conduit aval (24), ledit étranglement aval (66) s'étendant de la deuxième extrémité (60) du conduit aval (24) à une buse de décélération (64) dans la voie (62) de passage de fluide du conduit aval (24),

d) monter de manière à ce qu'il puisse tourner l'un des conduits amont et aval (22, 24) en vue d'une rotation autour d'un axe qui passe par les deuxièmes extrémités adjacentes (40, 60) des conduits amont et aval (22, 24), et

e) maintenir un espace (28) entre les deuxièmes extrémités adjacentes (40, 60) des conduits amont et aval (22, 24).

10. Procédé selon la revendication 9, dans lequel l'étape (a) comprend le fait de monter les deux conduits amont et aval (22, 24) de manière à ce qu'ils puissent tourner.

11. Procédé selon la revendication 9 ou 10, dans lequel l'étape (a) comprend le fait de réduire la taille de la voie (42) de passage de fluide à l'aide d'une buse d'accélération (44) disposée dans le conduit amont (22) en accélérant ainsi la vitesse du fluide jusqu'à une vitesse telle que le fluide n'exerce sensiblement aucune pression sur les parois (48) de la voie (42) de passage de fluide.

12. Procédé selon la revendication 9, 10 ou 11, dans lequel l'étape (a) comprend le fait de réduire la taille de la voie (42) de passage de fluide à l'aide d'une buse d'accélération (44) disposée dans le conduit amont (22) en accélérant ainsi la vitesse de l'écoulement de fluide jusqu'à une vitesse telle que le fluide crée un jet de fluide sensiblement auto-confiné, l'étranglement amont (46) ayant une section sensiblement constante afin de maintenir la vitesse du jet de fluide auto-confiné.

13. Procédé selon la revendication 12, dans lequel l'étranglement aval (66) est défini comme ayant sensiblement la même section et la même forme que l'étranglement amont (46) afin d'empêcher sensiblement la dissociation et la détente du fluide entre les étranglements amont et aval (46, 66).

14. Procédé selon la revendication 13, dans lequel l'étranglement aval (66) est défini comme maintenant l'écoulement de fluide à une vitesse sensiblement constante entre l'étranglement amont (46) et la buse de décélération (64).

15. Procédé selon l'une quelconque des revendications 10 à 14, dans lequel l'étranglement aval (66) est défini comme recevant le fluide accéléré et créant un joint étanche de fluide entre la deuxième extrémité (60) du conduit aval (24) et la buse de décélération (64) afin d'empêcher sensiblement la détente du fluide accéléré en amont de la buse de décélération (64).

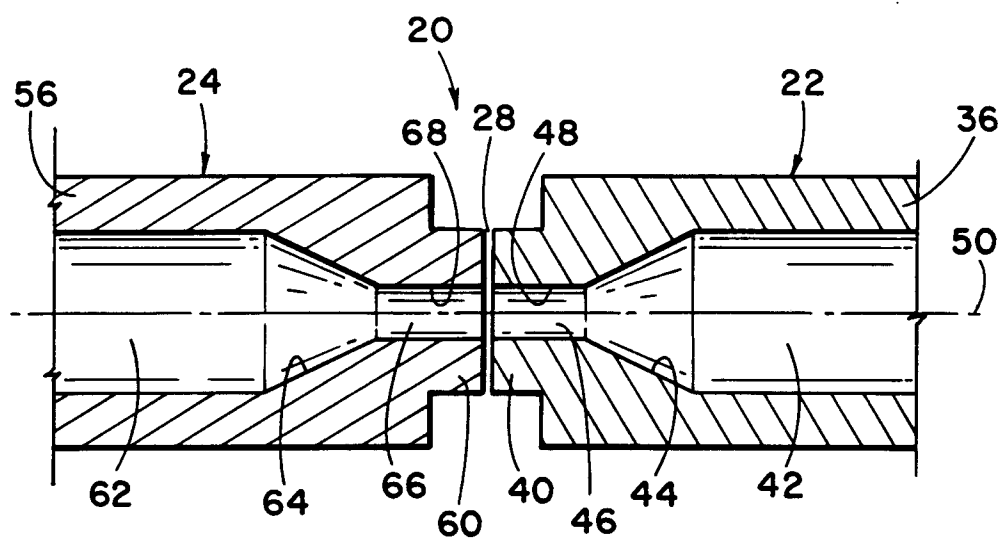
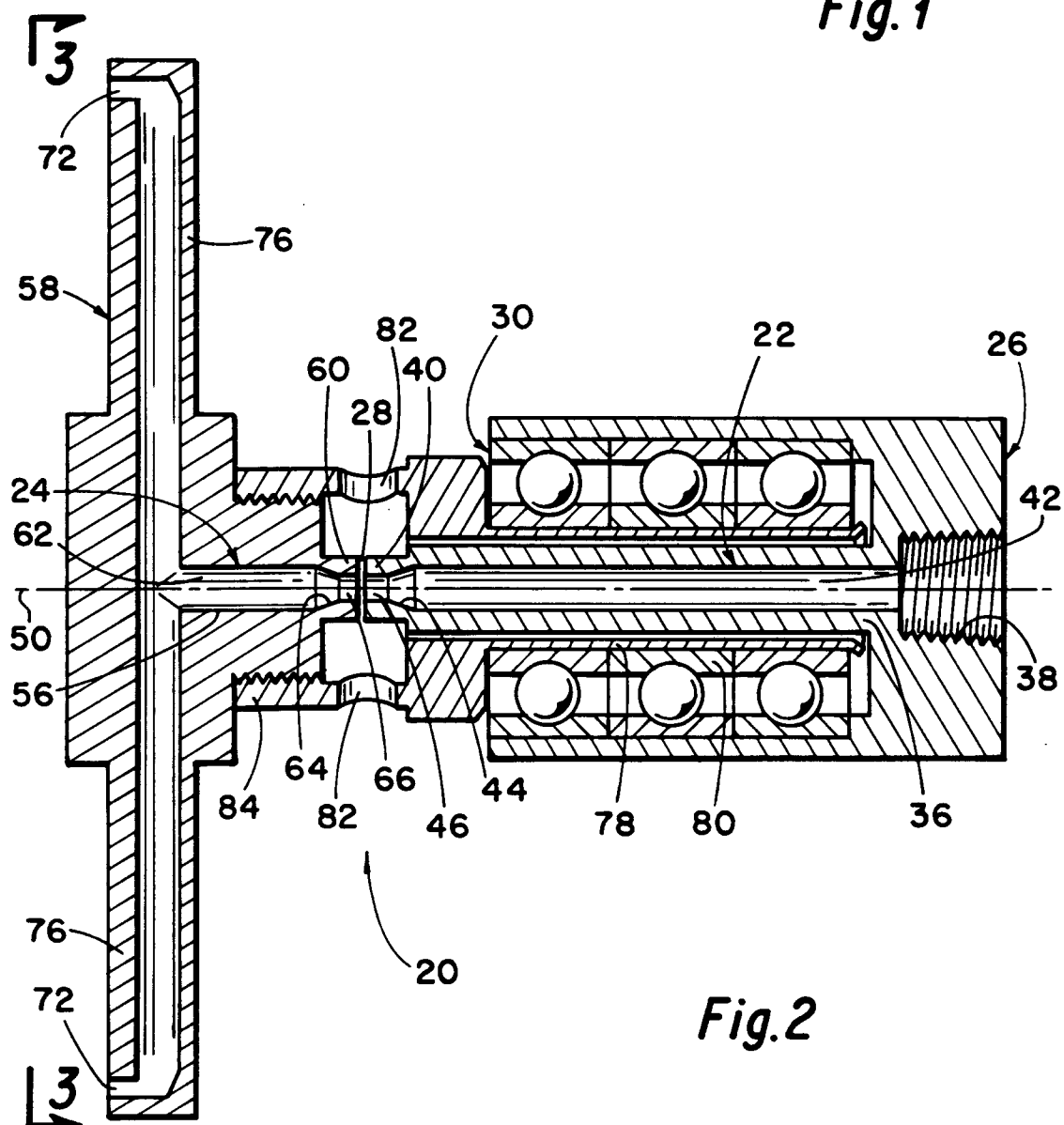


Fig. 1



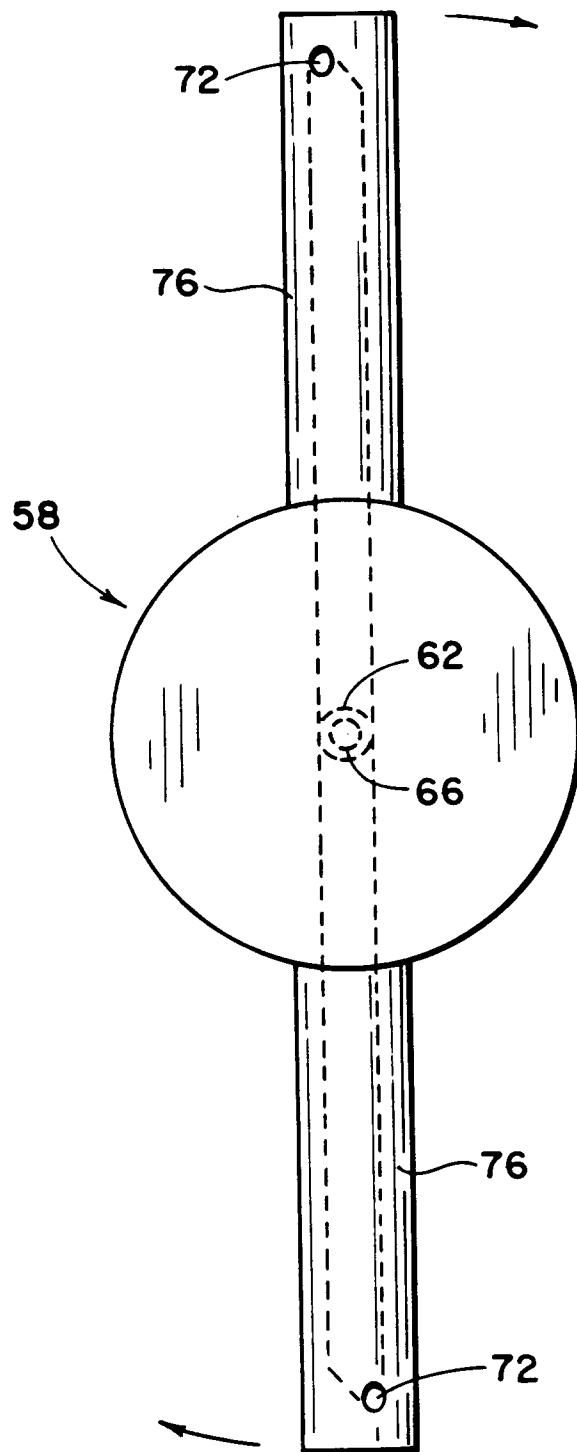


Fig. 3