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(11) **EP 0 734 084 B9**

(12) **CORRECTED EUROPEAN PATENT SPECIFICATION**

Note: Bibliography reflects the latest situation

(15) Correction information: (51) Int Cl.7: **H01M 2/28**

Corrected version no 1 (W1 B1)
Corrections, see page(s) 3

(48) Corrigendum issued on:
02.01.2002 Bulletin 2002/01

(45) Date of publication and mention
of the grant of the patent:
17.05.2000 Bulletin 2000/20

(21) Application number: **95111870.2**

(22) Date of filing: **27.07.1995**

(54) **Lead acid storage battery and method for making same**

Bleiakkumotor und Verfahren zu ihrer Herstellung

Accumulateur au plomb et procédé de fabrication

(84) Designated Contracting States:
DE FR GB

(30) Priority: **20.03.1995 JP 6076895**

(43) Date of publication of application:
25.09.1996 Bulletin 1996/39

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- **PATENT ABSTRACTS OF JAPAN vol. 94, no. 010 & JP-A-06 290770 (JAPAN STORAGE BATTERY CO LTD), 18 October 1994,**
- **JOURNAL OF POWER SOURCES, vol. 46, no. 2/03, 1 October 1993, pages 311-326, XP000483137 CHEN Z W ET AL: "JOINING OF LEAD-ANTIMONY AND LEAD-CALCIUM ALLOY LUGS BY A LABORATORY CAST-ON-STRAP PROCESS"**
- **PATENT ABSTRACTS OF JAPAN vol. 017, no. 653 (E-1469), 3 December 1993 & JP-A-05 217572 (JAPAN STORAGE BATTERY CO LTD), 27 August 1993,**
- **PATENT ABSTRACTS OF JAPAN vol. 017, no. 668 (E-1473), 9 December 1993 & JP-A-05 225967 (JAPAN STORAGE BATTERY CO LTD), 3 September 1993,**
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Description

BACKGROUND OF THE INVENTION

[0001] The present invention relates to a method for producing a lead acid storage battery as well as to a battery being produced by said method.

Prior Art

[0002] As for lead acid storage batteries, there have been various proposals on the process of parallel connection of plates of the same polarity in the same cell compartment by inserting a plate group in the cell compartments of a monoblock container in which a plurality of cell compartments are integrally provided and a method of series connection of plate groups different in polarity in adjacent cell compartments through partition walls in the container.

[0003] For example, there is a cast-on-strap process as one of processes for formation of straps for parallel connection of plates of the same polarity in lead acid storage batteries. Typical examples of formation of straps by such process will be explained below.

[0004] A plate group comprising positive plates, negative plates and separators is put in each cell compartment of a container in such a state that the plate lugs project from the container and the container is turned upside down so that the lug of each plate faces downward. A mold for forming a strap is placed under the container held upside down and a given amount of molten lead is fed in this mold. The tips of the plate lugs are dipped in this molten lead and are molten together with the molten lead. Then, the molten lugs and the molten lead are solidified together, thereby to form a strap and simultaneously bond the plate lugs to each other. The mold for forming the strap is heated to and kept at a temperature by a heater provided in the mold and by a cooling water so that the molten lead fed to the mold can be kept at good molten state, and after the molten lead and the plate lugs are molten together, the mold can be cooled.

[0005] When a strap is formed by the above process, the mold is previously heated, and lead which is kept in molten state by heating to a temperature higher than the mold temperature is fed in the mold. The temperature of the fed molten lead begins to lower immediately after being poured into the mold due to the diffusion of heat to the atmosphere and the mold. Furthermore, when the tips of the lugs of the plate group are dipped in the molten lead, the temperature of the lugs rises while the temperature of the molten lead in the mold further rapidly lowers due to the conduction of heat from the molten lead to the lugs. After they are left in this state for a given period, when the temperature of the molten lead lowers to the solidification temperature, solidification starts and the strap is formed.

[0006] In addition to the cast-on-strap process men-

tioned above, there is a process described in JP 60-138848A which comprises allowing the plate lugs and a solder to contact with each other in a connecting tool and melting the solder by high-frequency heating or induction heating to solder the tips the plate lugs, whereby parallel connection of plates of the same polarity in the same cell compartment and series connection of the plate groups of different polarity in the adjacent two cell compartments are simultaneously carried out. According to this process, a solder which is lower in melting point than the lead alloy used in the above cast-on-strap process is used to weld the plate lugs. Therefore, cost for strap increases due to the use of solder.

[0007] However, the cast-on-strap process has the following various problems.

(1) The control of welding conditions for welding of the plate lugs with the strap in formation of the strap is carried out only by the temperature of molten lead fed in the mold. Furthermore, since the strap is formed utilizing only the heat energy of the molten lead fed in the mold, when the number of the plates increases, much heat energy is needed in order to obtain a sufficient bond strength between the plate lugs and the strap, which causes increase in the amount of molten lead used as a source for the heat energy. As a result, it becomes difficult to form a strap of small and thin type.

(2) At the time of dipping the plate lugs in the molten lead fed in the mold, the surface of the molten lead fluctuates, and since the molten lead is cooled and solidified before a sufficient time is given for the surface returning to the smooth state, the surface of the strap waves, and thickness of the strap becomes uneven.

(3) If the plate lugs are not positioned at equal intervals, the heat balance between the plates is lost, resulting in variation in welding state of the plates and the strap.

(4) Defects such as cavity and shrinkage are apt to occur inside the strap.

(5) Flux coated on the surface of the plate lugs decomposes with heat and gasifies. The solidification completes in a short time before the generated gas is released to the outside, and, hence, the gas remains as voids in the strap.

[0008] As stated above, the formation of a strap by the conventional cast-on-strap process has many problems. The main reason therefor is that the heat source for welding of plates and strap is only the molten lead fed from the outside.

[0009] In order to solve the problems, it is necessary to instantaneously and accurately supply the energy required for welding from the outside. For example, in the case of the mold having a heater therein, the mold per se becomes a great heat block and it is very difficult to perform the control of rapid rising of temperature and

the accurate control of temperature of the melt.

[0010] The cooling and solidification of the molten lead for formation of strap start from the portion which contacts with the plate lugs and the mold. Therefore, the central portion finally solidifies, and defects such as cavity and shrinkage occur in the central portion owing to the difference in solidification rate.

[0011] Furthermore, preheating of the plate lugs is carried out for improving weldability at the time of formation of strap and for removing flux with drying. For this purpose, equipments such as hot-air heating devices are needed. **[deletion(s)]**

[0012] JP-A-6290770 discloses a method for forming a strap for a lead acid battery, according to which method the tips of lugs are inserted in a mold. Subsequently, molten lead is fed to the mold and then the mold and its contents are heated. Afterwards, the mold is cooled by water.

[0013] According to the present invention, the above-mentioned problems are solved by a method as laid down in claim 1 and by a lead acid storage battery produced by said method and constructed as laid down in claim 8, respectively. Preferred embodiments are claimed in the subclaims.

[0014] According to the present invention, a strap is formed with carrying out accurate control of temperature of molten lead or lead alloy and using an induction heating device as a heating source. Therefore, even when the number of the plates of the same polarity is great, for example, more than ten, control of the temperature can be accurately carried out and it becomes possible to form the strap of thin thickness of about 2/3 of the strap formed by the conventional cast-on-strap process, and, furthermore, the strap formed is satisfactory in strength and corrosion resistance. Accordingly, amount of lead or lead alloy used can be reduced as compared with the conventional method.

[0015] Moreover, by carrying out the cooling by spraying water as a coolant against the mold from the underside, solidification of molten lead alloy for formation of strap rapidly proceeds from the lower part of the mold and occurrence of poor weld can be prevented.

BRIEF DESCRIPTION OF THE DRAWINGS

[0016] Fig. 1(a) is a cross sectional view of a tool for forming a strap of lead acid storage battery according to the present invention.

[0017] Fig. 1(b) is a longitudinal sectional view of the tool shown in Fig. 1(a).

[0018] Fig. 2 is an oblique view of a tool for the formation of strap used in the present invention.

[0019] Fig. 3 is a flow chart of the steps in the Example of the present invention.

[0020] Fig. 4 is a graph which shows change of temperature in the system in the Example of the present invention.

[0021] Fig. 5 is an external view of the strap of the

present invention.

DESCRIPTION OF THE INVENTION

5 **[0022]** An example of the present invention will be explained below.

[0023] In the following example explained referring to the accompanying drawings, formation of a strap of a plate group consisting of nine positive plates and ten negative plates having a lug of 10 mm in length, 1.5 mm in thickness and 10 mm in width and series connection of current collector of plate groups of different polarity are simultaneously carried out using an induction heating device of 5 kW in output power and a grid comprising a lead-calcium-tin alloy.

10 **[0024]** As shown in Fig. 1(a) and Fig. 1(b), a plate group consisting of positive plates 5, negative plates 6 and separators is inserted in each of the cell compartment of monoblock container 1 comprising a synthetic resin in such a state as the upper part of the plate group being exposed outside the container, and this container is turned upside down by 180° and held so that the plate lugs face downward as shown in Fig. 1(a) and Fig. 1(b). Under the plate lugs, a stainless steel mold 3 for formation of strap provided with induction heating coil 2 is placed opposing the plate lugs. The induction heating coil 2 is provided spacing about 2 mm from the tool and surrounding the mold 3 so that heat is uniformly generated from the mold 3. The mold 3 for formation of the strap is preferably made of a heat-resistant material high in permeability and excellent in heat conduction. Moreover, a shower spraying means 4 for water cooling is provided under the mold 3.

15 **[0025]** By passing an electric current through the induction coil 2 with an initial applied power of 5 kW (200 V, 25 A) and a frequency of 120 kHz, the mold 3 per se surrounded by the coil can generate heat of up to about 300°C in about 5 seconds (Fig. 4). Control of the heating state is carried out by detecting the heating state in accordance with signals from a temperature detector, with which the mold 3 is equipped, and by changing the output to be applied to the coil from the electric source. A flux is coated on the lugs of the plate group and the tips of the lugs are positioned at about 3 mm above the mold 3 and are kept at that position. As a result, the lugs of the plate group also generate heat with line of magnetic force of the induction coil 2 and the temperature of the tips of the lugs rise to near 200°C. When a molten lead obtained by heating pure lead to 400°C is fed into the mold 3 for formation of strap, the temperature of the molten lead lowers to near 310°C. However, even after the molten lead is fed, the molten lead is again heated to the preset temperature of 350°C in about 3 seconds by passing an electric current through induction coil 2 to cause the mold 3 per se to generate heat. When the temperature of the molten lead reaches the preset temperature, the plate lugs kept above the mold 3 are dipped in the molten lead in the mold 3.

[0026] Simultaneously with the tips of the lugs being inserted, the temperature of the molten lead lowers about 10°C, but rises again to 350°C of the preset temperature in about 1.5 seconds due to heat generation of the mold 3 caused by line of magnetic force from the coil 2. After the temperature of the molten lead has reached the preset temperature and after lapse of further 3 seconds, passing of electric current through the induction coil 2 is stopped. At the same time, water is sprayed against the underpart of mold 3 from cooling shower spraying means 4 for 3 seconds to forcedly cool the mold 3 and the strap from the underside. By carrying out a series of these steps, the formation of strap for plate group of the same polarity in the same cell compartment and the series connection between the collector parts of the plates of different polarity adjacent through partition walls of the container are completed.

[0027] Fig. 3 shows the series connection step of the lugs of the plate group of the same polarity in the same cell compartment and Fig. 4 shows the change of temperature with time during the step. According to the present invention, not only the heating of the molten lead to the preset temperature can be carried out instantaneously in 3-5 seconds, but also the heating time after dipping of the tips of the lugs of the plate group can be optionally controlled. Therefore, rapid decrease of temperature of the molten lead when the tips of the lugs of the plate group are dipped in the molten lead in the strap forming tool can be inhibited and, thus, welding of the strap and the tips of the lugs can be performed under the conditions of small fluctuation in the temperature. Furthermore, even when the lugs of the plates are not arranged at equal intervals, balance of heat applied to each plate can be made uniform by controlling the molten state by heating and, as a result, weld strength with no fluctuation can be obtained. Moreover, after the lugs are dipped in the tool, good molten state of lead or lead alloy can be maintained by induction heating, and, therefore, it becomes possible to ensure the time necessary for the waving of the surface of the molten lead caused by dipping of the lugs to return to a smooth surface, and, as a result, the thickness of the strap can be made uniform. Furthermore, even if the flux coated on the surface of the lugs decomposes with heat to generate a gas, since the molten lead does not immediately solidify, the gas is not trapped in the strap and is smoothly released. Therefore, the gas does not remain in the strap as voids after formation of the strap. Moreover, rapid decrease of the temperature of the molten lead can be prevented by preheating the lugs by keeping them facing downward above the strap forming tool. In addition, by spraying water just under the strap forming tool to forcedly cool the tool, the texture inside the strap becomes fine and, thus, formation of defects such as cavity and shrinkage in the central portion of the strap caused by ununiform cooling and solidification can be prevented. In this example, formation of the strap was carried out in normal atmosphere, and when this is car-

ried out in an inert gas atmosphere, oxidation of the surface portion of strap forming alloy in molten state can be prevented and the strap can be kept in more preferred state.

[0028] The strap 9 shown in Fig. 5 which was produced by the present invention has a length of 60 mm, a width of 13 mm and a thickness of 5 mm, and is thin and has a uniform thickness. Observation of the section of the welded portion of the strap and the plate lugs showed that when the plate lugs were dipped in the molten lead at a depth of 3 mm, the portion of about 1 mm from the tip of the lug was in melt-bonded state, and the remainder portion of 2 mm was sore, but retained the shape of lug. Furthermore, a fillet (thick-wall) was sufficiently formed at the intersection of the plate lug and the strap, and no voids were seen.

[0029] In this example, explanation is made of using pure lead as a material for forming the strap. However, a strap can be similarly formed by using a lead alloy. Furthermore, the similar effects can also be obtained when a lead alloy other than the lead-calcium-tin alloy is used as a grid alloy. Furthermore, in this example, a strap forming mold made of a stainless steel was used, but a mold made of brass or ceramic coated with a metal thin film may also be used. The preset temperature of the strap forming mold, the time of passing of electric current through coil and the cooling condition of the tool vary depending on the composition of the strap alloy used, construction of the plate group, and shape of the strap and the tip of the lug, and optimum values thereof can be easily found.

[0030] As explained above, according to the present invention, it becomes possible to easily carry out the formation of the strap and the connection of the strap to the lugs of a plurality of plates of the same polarity contained in the cell compartment of the container.

[0031] Moreover, the molten state of the strap forming material is accurately controlled by using an induction coil and, further, the thickness of the strap is made thin, whereby the amount of lead used can be reduced and the weight of batteries can be greatly decreased. Further advantages are improvement in productivity and reduction of cost for production of lead acid storage batteries.

Claims

1. A method for producing a lead acid storage battery by integrally connecting lugs of a plurality of plates (5, 6) of the same polarity placed in a cell compartment of a container (1) to a strap (9) by cast-on-strap process, said method comprising the following steps:

pre-heating a strap forming mold (3) equipped with an induction heating (2);

feeding pure lead or a lead alloy in a molten state into said mold (3);

partially inserting the lugs of the plates (5, 6) in the pure lead or lead alloy to melt at least the tips of the lugs, and

forcibly cooling the whole melt.

2. The method according to claim 1, wherein the induction heating (2) comprises a coil provided surrounding the strap forming mold (3), an electric current with a frequency of 20-150 kHz being applied to said coil, and control of the heating state is carried out by an electric source adjusted by a signal from a temperature detector with which the strap forming mold (3) is equipped. 10
3. The method according to claim 1 or 2, wherein the forced cooling of the strap forming mold (3) and the strap (9) is carried out by a coolant spraying means (4) provided under the strap forming mold (3). 20
4. The method according to any preceding claim, wherein the formation of the strap (9) is carried out in an inert gas atmosphere. 25
5. The method according to any preceding claim, wherein the strap forming mold (3) is made of a stainless steel. 30
6. The method according to any preceding claim, wherein the tips of the plate lugs are preheated by induction heating and then inserted into the molten lead or lead alloy in the strap forming mold (3). 35
7. The method according to claim 6, wherein after the step of inserting a part of the lugs of the plates (5, 6) preheated by said induction heating (2) in the pure lead or lead alloy and prior to the step of cooling, the whole mold (3) is heated again by the induction heating (2) for a given period to melt at least the tips of the lugs together with the molten pure lead or lead alloy. 40
8. A lead acid storage battery having a construction in which lugs of a plurality of plates (5, 6) of the same polarity placed in a cell compartment of a container (1) are connected to a plate-like strap (9) molded from pure lead or a lead alloy, said battery being produced by the method according to any preceding claim, so that said strap (9) has a uniform and thin thickness and no voids therein. 50
9. The battery according to claim 8, wherein the pure lead or lead alloy which forms the strap (9) is solidified in such a state as molten with a part of the tips of the plate lugs. 55

10. The battery according to claim 8 or 9, wherein the thickness of said strap (9) is 5 mm or less.

5 Patentansprüche

1. Verfahren zur Herstellung einer Blei-Säure-Speicherbatterie durch integrales Verbinden von Nasen einer Mehrzahl von in einem Zellabteil eines Behälters (1) angeordneten Platten (5, 6) gleicher Polarität mit einem Bügel (9) durch einen Bügel-Angußprozeß, wobei das Verfahren folgende Schritte umfaßt:

Vorheizen einer mit einer Induktionsheizung (2) ausgerüsteten Bügelerzeugungs-Gußform (3);

Zuführen von Reinblei oder einer Bleilegierung in geschmolzenem Zustand in die Gußform (3);

teilweises Einführen der Nasen der Platten (5, 6) in das reine Blei oder die Bleilegierung, um zumindest die Spitzen der Nasen zu schmelzen, und

Zwangskühlen der gesamten Schmelze.

2. Verfahren nach Anspruch 1, bei welchem die Induktionsheizung (2) eine Spule aufweist, welche die Bügelerzeugungs-Gußform (3) umgibt, wobei ein elektrischer Strom mit einer Frequenz von 20-150 kHz an die Spule angelegt ist und die Steuerung des Heizzustands durch eine Stromquelle ausgeführt wird, die durch ein Signal von einem Temperaturdetektor geregelt wird, mit dem die Bügelerzeugungs-Gußform (3) ausgerüstet ist. 35

3. Verfahren nach Anspruch 1 oder 2, bei welchem die Zwangskühlung der Bügelerzeugungs-Gußform (3) und des Bügels (9) durch eine Kühlmittelsprüheinrichtung (4) ausgeführt wird, die unter der Bügelerzeugungs-Gußform (3) vorgesehen ist. 40

4. Verfahren nach einem der vorstehenden Ansprüche, bei welchem die Erzeugung des Bügels (9) in einer Inertgasatmosphäre ausgeführt wird. 45

5. Verfahren nach einem der vorstehenden Ansprüche, bei welchem die Bügelerzeugungs-Gußform (3) aus rostfreiem Stahl besteht. 50

6. Verfahren nach einem der vorstehenden Ansprüche, bei welchem die Spitzen der Plattennasen durch eine Induktionsheizung vorgeheizt werden und dann in das geschmolzene Blei oder die geschmolzene Bleilegierung, welche(s) sich in der Bügelerzeugungs-Gußform (3) befindet, eingeführt werden. 55

7. Verfahren nach Anspruch 6, bei welchem nach dem Schritt des Einführens der durch die Induktionsheizung (2) vorgeheizten Nasen der Platten (5, 6) in das Reinblei oder die Bleilegierung und vor dem Schritt des Kühlens, die gesamte Gußform (3) für eine gegebene Zeitdauer durch die Induktionsheizung (2) wieder aufgeheizt wird, um zumindest die Spitzen der Nasen zusammen mit dem geschmolzenen Reinblei oder der Bleilegierung zu schmelzen. 5
8. Blei-Säure-Speicherbatterie, welche einen Aufbau besitzt, bei dem Nasen einer Mehrzahl von in einem Zellabteil eines Behälters (1) angeordneten Platten (5, 6) gleicher Polarität mit einem plattenartigen Bügel (9) verbunden sind, der aus Reinblei oder einer Bleilegierung formgegossen ist, wobei die Batterie durch das Verfahren nach einem der vorstehenden Ansprüche erzeugt ist, so daß der Bügel (9) eine einheitliche und geringe Dicke besitzt und sich in ihm keine Lunker befinden. 10
9. Batterie nach Anspruch 8, bei welcher das Reinblei oder die Bleilegierung, welche(s) den Bügel (9) bildet, in einem Zustand, bei dem er mit einem Teil der Spitzen der Plattennasen verschmolzen ist, verfestigt ist. 15
10. Batterie nach Anspruch 8 oder 9, bei welcher die Dicke des Bügels (9) 5 mm oder weniger beträgt. 20
3. Procédé selon la revendication 1 ou 2, dans lequel le refroidissement forcé du moule de formation de barrette (3) et de la barrette (9) est exécuté un moyen de pulvérisation de réfrigérant (4) disposé sous le moule de formation de barrette (3). 25
4. Procédé selon l'une quelconque des revendications précédentes, dans lequel la formation de la barrette (9) est exécutée sous une atmosphère de gaz inerte. 30
5. Procédé selon l'une quelconque des revendications précédentes, dans lequel le moule de formation de barrette (3) est fait d'un acier inoxydable. 35
6. Procédé selon l'une quelconque des revendications précédentes, dans lequel les extrémités des queues de plaques sont préchauffées par un chauffage par induction et insérées ensuite dans le plomb ou l'alliage de plomb fondu dans le moule de formation de barrette (3). 40
7. Procédé selon la revendication 6, dans lequel, après l'étape d'insertion d'une partie des queues des plaques (5, 6) préchauffées par ledit chauffage par induction (2) dans le plomb pur ou l'alliage de plomb et avant l'étape de refroidissement, la totalité du moule (3) est chauffée à nouveau par le chauffage par induction (2) pendant un intervalle de temps donné afin de fondre au moins les extrémités des queues en même temps que le plomb pur ou l'alliage de plomb fondu. 45
8. Batterie d'accumulateurs au plomb présentant une conception dans laquelle des queues d'une pluralité de plaques (5, 6) de même polarité placées dans un compartiment d'éléments d'un récipient (1) sont raccordées à une barrette semblable à une plaque (9) moulée à partir de plomb pur ou d'un alliage de plomb, ladite batterie étant fabriquée par le procédé selon l'une quelconque des revendications précédentes, de sorte que ladite barrette (9) présente une épaisseur uniforme et mince et aucun vide dans celle-ci. 50
9. Batterie selon la revendication 8, dans laquelle le plomb pur ou l'alliage de plomb qui forme la barrette (9) est solidifié dans un état tel qu'il a été fondu avec une partie des extrémités des queues de plaques. 55
10. Batterie selon la revendication 8 ou 9, dans laquelle l'épaisseur de ladite barrette (9) est de 5 mm ou moins.

Revendications

1. Procédé de fabrication d'une batterie d'accumulateurs au plomb en raccordant de façon intégrée des queues d'une pluralité de plaques (5, 6) de même polarité placées dans un compartiment d'élément d'un récipient (1) à une barrette (9) grâce à un procédé de barrettes montées par moulage, ledit procédé comprenant les étapes suivantes :
- préchauffage d'un moule de formation de barrette (3) équipé d'un chauffage par induction (2), 45
- introduction de plomb pur ou d'alliage de plomb à l'état fondu dans ledit moule (3),
- insertion partielle des queues des plaques (5, 6) dans le plomb pur ou l'alliage de plomb afin de fondre au moins les extrémités des queues, et 50
- refroidissement de façon forcée de l'ensemble de masse fondue.
2. Procédé selon la revendication 1, dans lequel le chauffage par induction (2) comprend une bobine disposée autour du moule de formation de barrette (3), un courant électrique présentant une fréquence

FIG. 1A

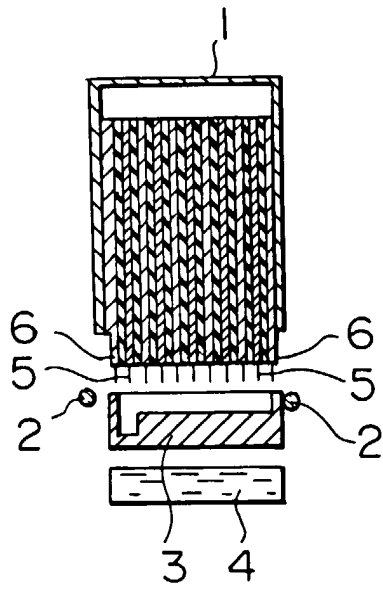


FIG. 1B

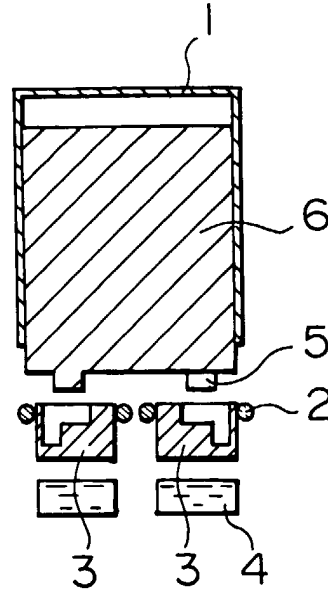


FIG. 2

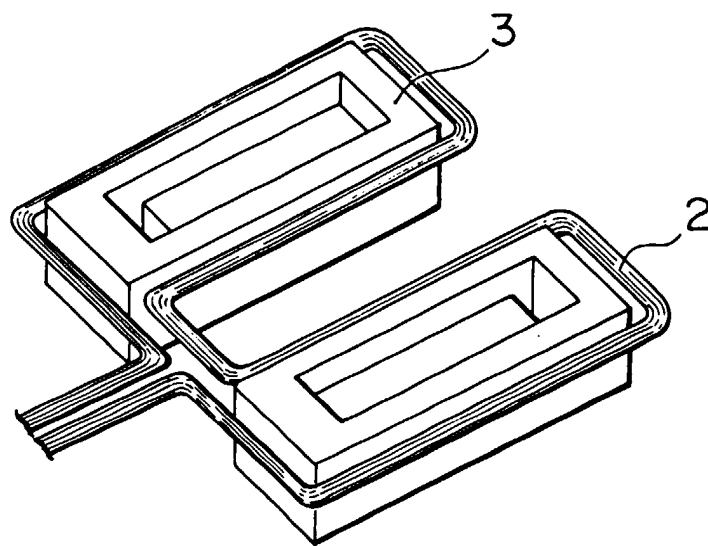


FIG. 3

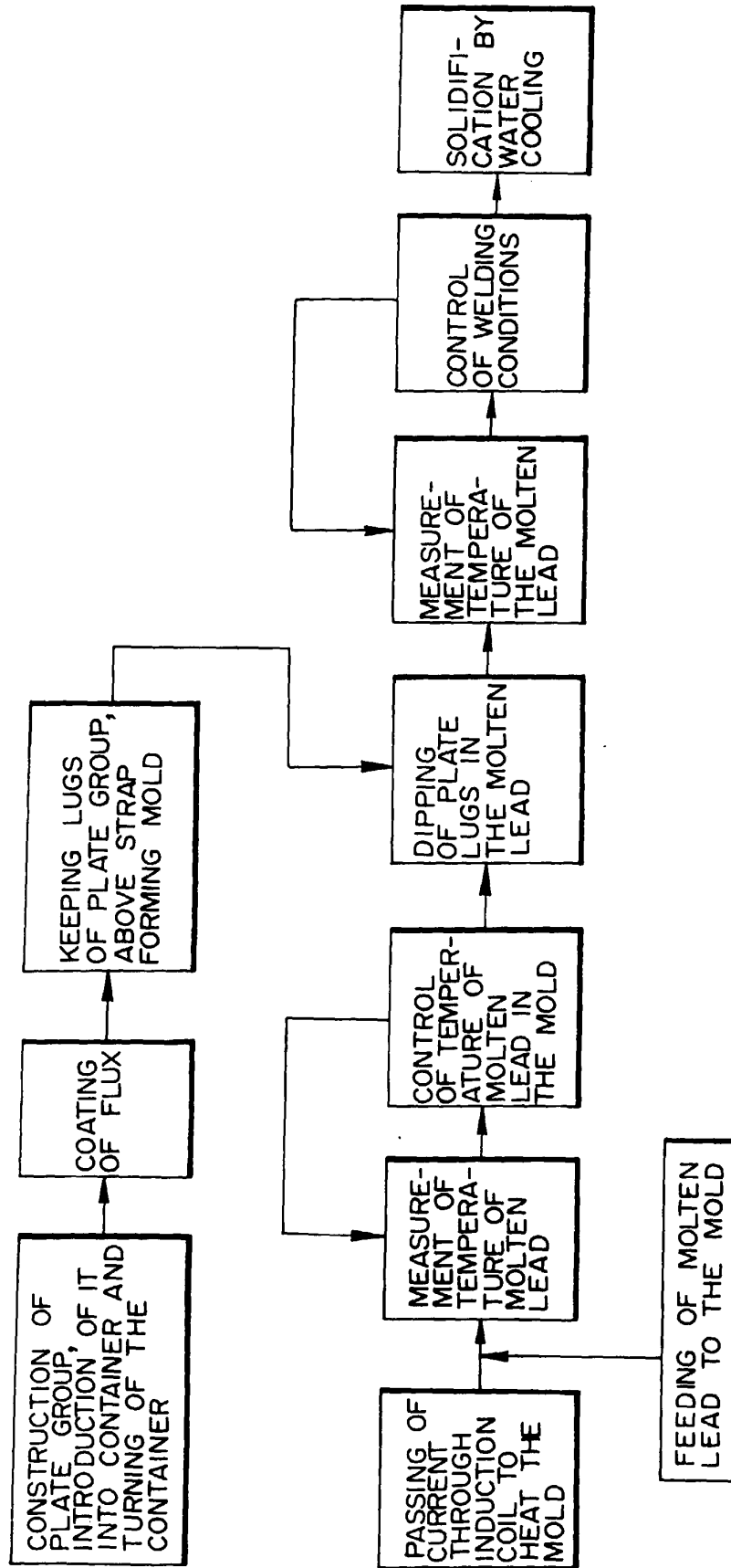


FIG. 4

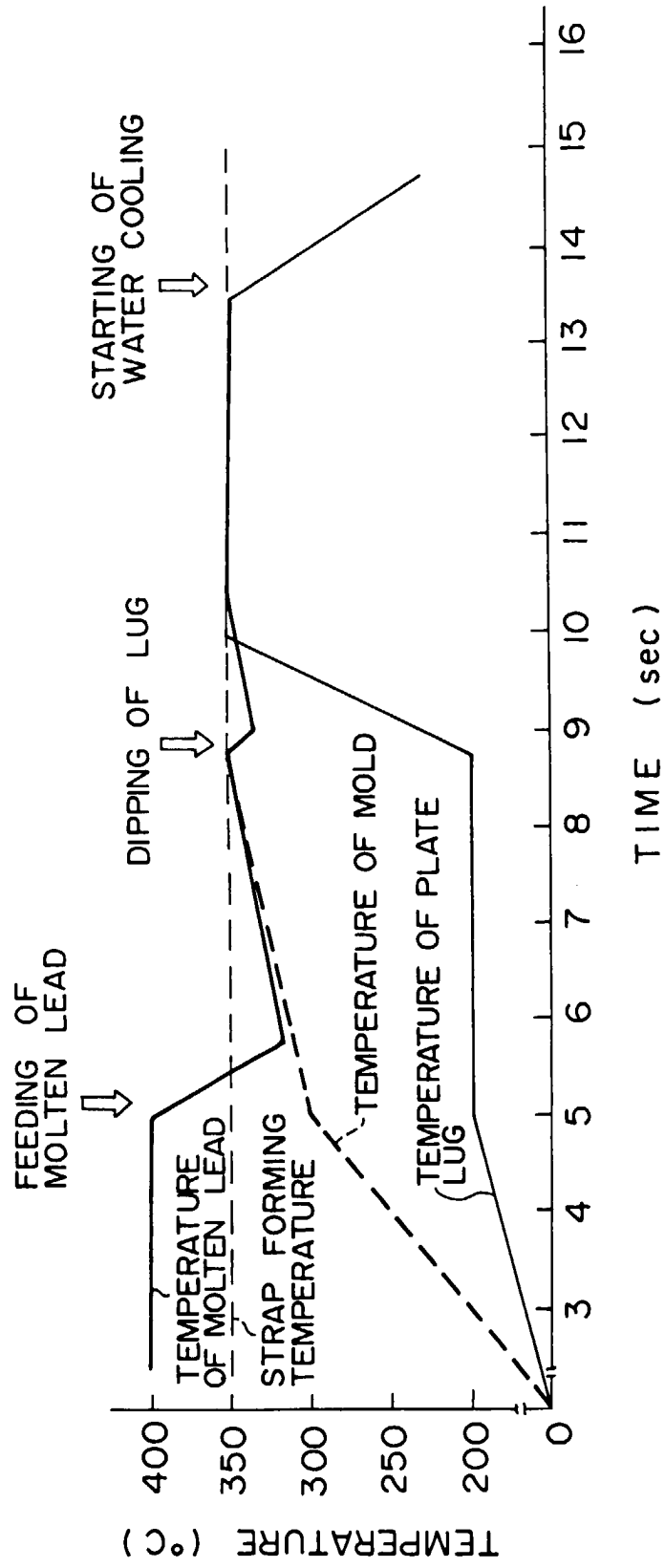


FIG. 5

