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(11)

EP 1 271 238 A2

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
02.01.2003 Bulletin 2003/01

(51) Int Cl.7: **G03C 5/17**

(21) Application number: **02077368.5**

(22) Date of filing: **17.06.2002**

(84) Designated Contracting States:
**AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU
MC NL PT SE TR**
Designated Extension States:
AL LT LV MK RO SI

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(30) Priority: **28.06.2001 US 893955**
28.06.2001 US 894553
28.06.2001 US 894656

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(54) Portal imaging assembly with neutral density filter and method of use

(57) A radiographic imaging assembly has first and second radiographic silver halide films in association with two fluorescent intensifying screens. Disposed be-

tween one set of screen and film is a neutral density filter having a density of at least 0.3 to provide improved exposure latitude for use in various exposure conditions and equipment.

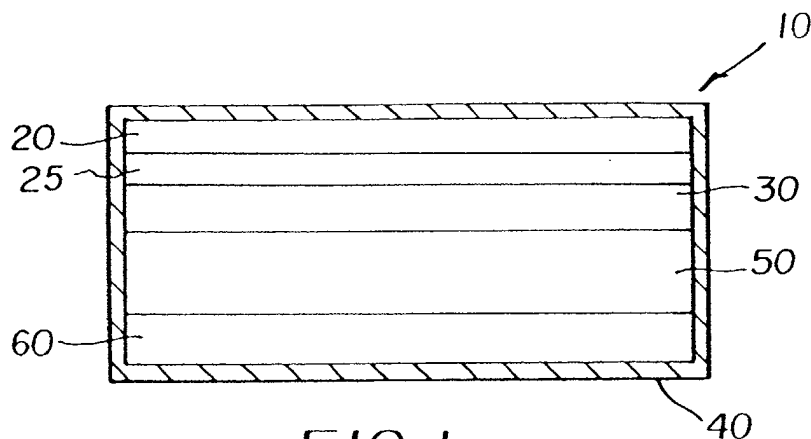


FIG. 1

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Description

[0001] This invention is directed to radiography in which radiation is aimed at certain regions of a subject to provide therapy treatment. In particular, it is directed to a radiographic portal imaging assembly containing two radiographic silver halide films, two fluorescent intensifying screen, and a neutral density or magenta filter between one film and one screen, and to methods of use. This invention is useful in portal radiography.

[0002] In conventional medical diagnostic imaging the object is to obtain an image of a patient's internal anatomy with as little X-radiation exposure as possible. The fastest imaging speeds are realized by mounting a dual-coated radiographic element between a pair of fluorescent intensifying screens for imagewise exposure. 5% or less of the exposing X-radiation passing through the patient is adsorbed directly by the latent image forming silver halide emulsion layers within the dual-coated radiographic element. Most of the X-radiation that participates in image formation is absorbed by phosphor particles within the fluorescent screens. This stimulates light emission that is more readily absorbed by the silver halide emulsion layers of the radiographic element.

[0003] Examples of radiographic element constructions for medical diagnostic purposes are provided by U. S. Patent 4,425,425 (Abbott et al.) and U.S. Patent 4,425,426 (Abbott et al.), U.S. Patent 4,414,310 (Dickerson), U.S. Patent 4,803,150 (Kelly et al.), U.S. Patent 4,900,652 (Kelly et al.), U.S. Patent 5,252,442 (Tsaur et al.), and *Research Disclosure*, Vol. 184, August 1979, Item 18431.

[0004] Radiation oncology is a field of radiology relating to the treatment of cancers using high energy X-radiation. This treatment is also known as teletherapy, using powerful, high-energy X-radiation machines (often linear accelerators) to exposure the cancerous tissues (tumor). The goal of such treatment is to cure the patient by selectively killing the cancer while minimizing damage to surrounding healthy tissues.

[0005] Such treatment is commonly carried out using high energy X-radiation, 4 to 25 MVp. The X-radiation beams are very carefully mapped for intensity and energy. The patient is carefully imaged using a conventional diagnostic X-radiation unit, a CT scanner, and/or an MRI scanner to accurately locate the various tissues (healthy and cancerous) in the patient. With full knowledge of the treatment beam and the patient's anatomy, a dosimetrist determines where and for how long the treatment X-radiation will be directed, and predicts the radiation dose to the patient.

[0006] Usually, this treatment causes some healthy tissues to be overexposed. To reduce this effect, the dosimetrist provides one or more custom-designed "blocks" or shields of lead around the patient's body to absorb X-radiation that would impact healthy tissues.

[0007] To determine and document that a treatment radiation beam is accurately aimed and is effectively killing the cancerous tissues, two types of imaging are carried out during the course of the treatment. "Portal radiography" is generally the term used to describe such imaging. The first type of portal imaging is known as "localization" imaging in which the portal radiographic film is briefly exposed to the X-radiation passing through the patient with the lead shields removed and then with the lead shields in place. Exposure without the lead shields provides a faint image of anatomical features that can be used as orientation references near the targeted feature while the exposure with the lead shields superimposes a second image of the port area. This process insures that the lead shields are in the correct location relative to the patient's healthy tissues. Both exposures are made using a fraction of the total treatment dose, usually 1 to 4 monitor units out of a total dose of 45-150 monitor units. Thus, the patient receives less than 20 RAD's of radiation.

[0008] If the patient and lead shields are accurately positioned relative to each other, the therapy treatment is carried out using a killing dose of X-radiation administered through the port. The patient typically receives from 50 to 300 RAD's during this treatment. Since any movement of the patient during exposure can reduce treatment effectiveness, it is important to minimize the time required to process the imaged films.

[0009] A second, less common form of portal radiography is known as "verification" imaging to verify the location of the cell-killing exposure. The purpose of this imaging is to record enough anatomical information to confirm that the cell-killing exposure was properly aligned with the targeted tissue. The imaging film/cassette assembly is kept in place behind the patient for the full duration of the treatment. Verification films have only a single field (the lead shields are in place) and are generally imaged at intervals during the treatment regime that may last for weeks. Thus, it is important to insure that proper targeted tissue and only that tissue is exposed to the high level radiation because the levels of radiation are borderline lethal.

[0010] Portal radiographic imaging film, assembly and methods are described, for example, in U.S. Patent 5,871,892 (Dickerson et al.) in which the same type of radiographic element can be used for both localization and portal imaging.

[0011] Portal imaging assemblies can be grouped into two categories. The first type of assemblies includes one or two metal plates and a radiographic silver halide film that is designed for direct exposure to X-radiation. Two such films that are commercially available are KODAK X-ray Therapy Localization (XTL) Film and KODAK X-ray Therapy Verification (XV) Film. Each of these films is generally used with a single copper or lead plate. They have the advantage of having low contrast so that a wide range of exposure conditions can be used to produce useful images. However, because high energy X-radiation is used to produce therapy portal images, the contrast of the imaged tissues (target

tissues) is also very low. Coupled with the low contrast of the imaging system, the final image contrast is very low and difficult to read accurately.

[0012] The second type of portal imaging assemblies includes a fluorescent intensifying screen and a silver halide radiographic film. These assemblies include one or two metal plates, one or two fluorescent intensifying screens, and a fine grain emulsion film. Because a significant amount of the film's exposure comes from the light emitted by the fluorescent screen(s), it is possible to use films that provide high contrast images. Thus, these imaging assemblies typically provide images having contrast 3.5 times higher than those direct imaging assemblies noted above do. However, the photospeed obtained with both types of assemblies is about the same.

[0013] However, the imaging assemblies of the prior art present some problems. Due to their high contrast images and the variations in patient treatment dosages, patient tissue conditions (thickness), and exposing equipment, it is more difficult to obtain correct exposures. The images are either too light or too dark. Exposure can be controlled by adjusting the so-called "air gap" distance and monitor setting between the patient and the imaging system. Unfortunately, many therapy machines used in therapy imaging (especially therapy verification imaging) do not allow for an adjustable "air gap". This is especially true for therapy verification imaging.

[0014] Thus, there is a continuing need in the health imaging industry to provide a highly effective means for portal imaging under a wide variety of exposure conditions. More particularly, there is a need for portal imaging assemblies that provide greater "exposure latitude" without loss of photospeed or contrast. The present invention is directed to solving these problems.

[0015] This invention provides a solution to the noted problems with a radiographic imaging assembly comprising the following components arranged in association, in order:

- (a) a first fluorescent intensifying screen,
- (b) a first radiographic silver halide film,
- (c) a second radiographic silver halide film, and
- (d) a second fluorescent intensifying screen,

the first radiographic silver halide film comprising a support having first and second major surfaces and is capable of transmitting X-radiation,

the first radiographic silver halide film having disposed on the first major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer, and on the second major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer,

each of said silver halide emulsion layers comprising silver halide cubic grains that have the same or different composition in each silver halide emulsion layer, and all hydrophilic layers of the first radiographic silver halide film being fully forehardened and wet processing solution permeable for image formation within 45 seconds,

the second radiographic silver halide film comprising a support having first and second major surfaces and is capable of transmitting X-radiation,

the second radiographic silver halide film having disposed on the first major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer, and on the second major support surface, one or more hydrophilic colloid layers including at least one silver halide layer, and

each of the silver halide emulsion layers comprising silver halide cubic grains that have the same or different composition in each silver halide emulsion layer, and all hydrophilic layers of the second radiographic silver halide film being fully forehardened and wet processing solution permeable for image formation within 45 seconds, and

the radiographic imaging assembly characterized as having disposed between the first fluorescent intensifying screen and the first radiographic silver halide film, or between the second fluorescent intensifying screen and the second radiographic silver halide film, a transparent neutral density filter having a density or magenta of at least 0.3.

[0016] Further, this invention provides a method of providing a black-and-white image comprising exposing the radiographic imaging assembly described above, and processing the first and second radiographic silver halide films, sequentially, with a black-and-white developing composition and a fixing composition, the processing being carried out within 90 seconds, dry-to-dry.

[0017] The present invention provides a means for providing high contrast images in portal imaging using a wide variety of therapy imaging machines under a wide variety of conditions. Thus, the present invention provides improved "exposure latitude" and "dynamic range" in this important field of radiology. In addition, the radiographic imaging assembly of this invention may provide improved image tone in the films and greater processing uniformity (less processing defects). In addition, all other desirable sensitometric properties are maintained and the first and second films can be rapidly processed in the same conventional processing equipment and compositions.

[0018] These advantages are achieved by including between either the first radiographic silver halide film and first fluorescent intensifying screen, or the second radiographic silver halide film and the second fluorescent intensifying screen, a neutral density filter that has a density of at least 0.3 and no more than 0.9. These components are arranged

"in association" meaning they are in physical contact with no significant gap between them in the imaging assembly.

[0019] In one embodiment, the neutral density filter is laminated to either the first or second fluorescent intensifying screen, a neutral density filter having a density of at least 0.3 and that comprises a transparent support having disposed thereon a hydrophilic neutral density filter layer, the neutral density filter being arranged so that its hydrophilic neutral density filter layer is in contact with the first or second fluorescent intensifying screen and its transparent support is adjacent the first or second radiographic silver halide film, respectively.

[0020] These components are arranged "in association" meaning they are in physical contact with no significant gap between them in the imaging assembly. The filter is actually laminated to one of the screens so that its transparent support is arranged next to the radiographic silver halide film and its hydrophilic neutral density filter layer is arranged in contact with the fluorescent intensifying screen. Thus, the neutral density filter and its associated screen can be removed and cleaned without damaging either component.

[0021] In still another embodiment, the magenta filter is laminated to either the first or second fluorescent intensifying screen, and comprises a transparent support having disposed thereon a hydrophilic layer comprising at least one spectral absorbing material that absorbs radiation in the range of from 500 to 600 nm and is dispersed in a hydrophilic binder, the magenta filter being arranged so that its hydrophilic layer is in contact with the first or second fluorescent intensifying screen and its transparent support is adjacent the first or second radiographic silver halide film, respectively.

BRIEF DESCRIPTION OF THE DRAWINGS

[0022]

FIG. 1 is a schematic cross-sectional illustration of an embodiment of this invention comprising first and second radiographic silver halide films, first and second fluorescent intensifying screens, and a neutral density or magenta filter in a cassette holder.

FIG. 2 is a schematic cross-sectional illustration of a preferred embodiment of this invention comprising first and second radiographic silver halide films, first and second fluorescent intensifying screens, a neutral density or magenta filter, and a metal screen in a cassette holder.

Definition of Terms:

[0023] The term "contrast" as herein employed indicates the average contrast derived from a characteristic curve of a radiographic film using as a first reference point (1) a density (D_1) of 0.25 above minimum density and as a second reference point (2) a density (D_2) of 2.0 above minimum density, where contrast is ΔD (i.e. 1.75) $\div \Delta \log_{10} E$ ($\log_{10} E_2 - \log_{10} E_1$), E_1 and E_2 being the exposure levels at the reference points (1) and (2).

[0024] "Gamma" is described as the instantaneous rate of change of a D logE sensitometric curve or the instantaneous contrast at any logE value.

[0025] "Peak gamma" is the point of the sensitometric curve where the maximum gamma is achieved.

[0026] Photographic "speed" refers to the exposure necessary to obtain a density of at least 1.0 plus D_{min} .

[0027] The term "fully forehardened" is employed to indicate the forehardening of hydrophilic colloid layers to a level that limits the weight gain of a radiographic film to less than 120% of its original (dry) weight in the course of wet processing. The weight gain is almost entirely attributable to the ingestion of water during such processing.

[0028] The term "rapid access processing" is employed to indicate dry-to-dry processing of a radiographic film in 45 seconds or less. That is, 45 seconds or less elapse from the time a dry imagewise exposed radiographic film enters a wet processor until it emerges as a dry fully processed film.

[0029] In referring to grains and silver halide emulsions containing two or more halides, the halides are named in order of ascending concentrations.

[0030] The term "equivalent circular diameter" (ECD) is used to define the diameter of a circle having the same projected area as a silver halide grain.

[0031] The term "aspect ratio" is used to define the ratio of grain ECD to grain thickness.

[0032] The term "coefficient of variation" (COV) is defined as 100 times the standard deviation (σ) of grain ECD divided by the mean grain ECD.

[0033] The term "covering power" is used to indicate 100 times the ratio of maximum density to developed silver measured in mg/dm^2 .

[0034] The term "dual-coated" is used to define a radiographic film having silver halide emulsion layers disposed on both the front- and backsides of the support. The radiographic silver halide films used in the present invention are "dual-coated."

[0035] The term "RAD" is used to indicate a unit dose of absorbed radiation, that is energy absorption of 100 ergs per gram of tissue.

[0036] The term "portal" is used to indicate radiographic imaging, films and intensifying screens applied to megavoltage radiotherapy conducted through an opening or port in a radiation shield.

[0037] The term "localization" refers to portal imaging that is used to locate the port in relation to the surrounding anatomy of the irradiated subject. Typically exposure times range from 1 to 10 seconds.

[0038] The term "verification" refers to portal imaging that is used to record patient exposure through the port during radiotherapy. Typically exposure times range from 30 to 300 seconds.

[0039] The term "exposure latitude" refers to the width of the gamma/logE curves for which contrast values were greater than 1.5.

[0040] The term "dynamic range" refers to the range of exposures over which useful images can be obtained (usually having a gamma greater than 2).

[0041] The term "crossover" as herein employed refers to the percentage of light emitted by a fluorescent intensifying screen that strikes a dual-coated radiographic film and passes through its support to reach the image forming layer unit disposed on the opposite side of the support. Crossover can be measured as described in U.S. Patent 4,425,425 (Abbott et al.).

[0042] The terms "kVp" and "MVp" stand for peak voltage applied to an X-ray tube times 10^3 and 10^6 , respectively.

[0043] The term "fluorescent intensifying screen" refers to a screen that absorbs X-radiation and emits light. A "prompt" emitting fluorescent intensifying screen will emit light immediately upon exposure to radiation while "storage" fluorescent screen can "store" the exposing X-radiation for emission at a later time when the screen is irradiated with other radiation (usually visible light).

[0044] The term "metal intensifying screen" refers to a metal screen that absorbs MVp level X-radiation to release electrons and absorbs electrons that have been generated by X-radiation prior to reaching the screen.

[0045] The terms "front" and "back" refer to layers, films, or intensifying screens nearer to and farther from, respectively, the X-radiation source.

[0046] The term "rare earth" is used to indicate chemical elements having an atomic number of 39 or 57 through 71.

[0047] The present invention uses two radiographic silver halide films to achieve the desired advantages. The films can be the same or different in speed and/or provide images with the same or different contrast. In a preferred embodiment, the "first" film can be considered a "high contrast" radiographic silver halide film while the "second" film can be considered a "lower contrast" radiographic silver halide film because the contrast of images it provides is lower than that of images provided by the "first" film.

[0048] In another embodiment, the two films can have different photographic speeds, for example, differing in photographic speed by at least 0.15 logE, and preferably by at least 0.3 logE.

[0049] The following discussion will be directed to features useful in both first and second radiographic silver halide films unless otherwise noted.

[0050] The radiographic silver halide films useful in this invention include a flexible support having disposed on both sides thereof, one or more photographic silver halide emulsion layers and optionally one or more non-radiation sensitive hydrophilic layer(s). The silver halide emulsions in the various layers can be the same or different in the same first or second film, and can comprise mixtures of various silver halide emulsions in one or more of the layers.

[0051] In preferred embodiments, each photographic silver halide film has the same silver halide emulsions on both sides of the support. It is also preferred that each film have a protective overcoat (described below) over the silver halide emulsions on each side of the support.

[0052] The support can take the form of any conventional radiographic film support that is X-radiation and light transmissive. Useful supports for the films of this invention can be chosen from among those described in *Research Disclosure*, September 1996, Item 38957 XV. Supports and *Research Disclosure*, Vol. 184, August 1979, Item 18431, XII. Film Supports.

[0053] The support is preferably a transparent film support. In its simplest possible form the transparent film support consists of a transparent film chosen to allow direct adhesion of the hydrophilic silver halide emulsion layers or other hydrophilic layers. More commonly, the transparent film is itself hydrophobic and subbing layers are coated on the film to facilitate adhesion of the hydrophilic silver halide emulsion layers. Typically the film support is either colorless or blue tinted (tinting dye being present in one or both of the support film and the subbing layers). Referring to *Research Disclosure*, Item 38957, Section XV Supports, cited above, attention is directed particularly to paragraph (2) that describes subbing layers, and paragraph (7) that describes preferred polyester film supports.

[0054] In the more preferred embodiments, at least one non-light sensitive hydrophilic layer is included with the one or more silver halide emulsion layers on each side of the film support. This layer may be called an interlayer or overcoat, or both.

[0055] The silver halide emulsion layers comprise one or more types of silver halide grains responsive to X-radiation. Silver halide grain compositions particularly contemplated include those having at least 50 mol % chloride (preferably at least 70 and more preferably at least 80 mol % chloride), and up to 50 mol % bromide, based on total silver in a given emulsion layer. Such emulsions include silver halide grains composed of, for example, silver chloride, silver

iodochloride, silver bromochloride, silver iodobromochloride, and silver bromoiodochloride. Iodide is generally limited to no more than 2 mol % (based on total silver in the emulsion layer) to facilitate more rapid processing. Preferably iodide is from 0.5 to 1.5 mol % (based on total silver in the emulsion layer) or eliminated entirely from the grains. The silver halide grains in each silver halide emulsion unit (or silver halide emulsion layers) can be the same or different, or mixtures of different types of grains.

[0056] The silver halide grains useful in this invention can have any desirable morphology including, but not limited to, cubic, octahedral, tetradecahedral, rounded, spherical or other non-tabular morphologies, or be comprised of a mixture of two or more of such morphologies. Preferably, the grains in each silver halide emulsion have cubic morphology.

[0057] It may also be desirable to employ silver halide grains that exhibit a coefficient of variation (COV) of grain ECD of less than 20% and, preferably, less than 10%. In some embodiments, it may be desirable to employ a grain population that is as highly monodisperse as can be conveniently realized.

[0058] The average silver halide grain size can vary within each radiographic silver halide film, and within each emulsion layer within that film. For example, the average grain size in each radiographic silver halide film is independently and generally from 0.1 to 0.3 μm (preferably from 0.1 to 0.2 μm), but the average grain size can be different in the various emulsion layers.

[0059] A variety of silver halide dopants can be used, individually and in combination, to improve contrast as well as other common properties, such as speed and reciprocity characteristics. A summary of conventional dopants to improve speed, reciprocity and other imaging characteristics is provided by *Research Disclosure*, Item 38957, cited above, Section I. Emulsion grains and their preparation, sub-section D. Grain modifying conditions and adjustments, paragraphs (3), (4), and (5).

[0060] The emulsions used in the radiographic silver halide films can be doped with any of conventional rhodium dopants to increase the contrast. These dopants can be present in an amount of from 1×10^{-5} to 5×10^{-5} mole per mole of silver in each emulsion layer, and preferably at from 2×10^{-5} to 4×10^{-5} mol/mol Ag in each emulsion layer.

The amount of rhodium dopant can be the same or different in the various emulsion layers.

[0061] Useful rhodium dopants are well known in the art and are described for example in U.S. Patent 3,737,313 (Rosecrants et al.), U.S. Patent 4,681,836 (Inoue et al.), and U.S. Patent 2,448,060 (Smith et al.). Representative rhodium dopants include, but are not limited to, rhodium halides (such as rhodium monochloride, rhodium trichloride, diammonium aquapentachlororhodate, and rhodium ammonium chloride), rhodium cyanates {such as salts of $[\text{Rh}(\text{CN})_6]^{-3}$, $[\text{RhF}(\text{CN})_5]^{-3}$, $[\text{RhI}_2(\text{CN})_4]^{-3}$ and $[\text{Rh}(\text{CN})_5(\text{SeCN})]^{-3}$ }, rhodium thiocyanates, rhodium selenocyanates, rhodium tellurocyanates, rhodium azides, and others known in the art, for example as described in *Research Disclosure*, Item 437013, page 1526, September 2000 and publications listed therein. The preferred rhodium dopant is diammonium aquapentachloro-rhodate. Mixtures of dopants can be used also.

[0062] A general summary of silver halide emulsions and their preparation is provided by *Research Disclosure*, Item 38957, cited above, Section I. Emulsion grains and their preparation. After precipitation and before chemical sensitization the emulsions can be washed by any convenient conventional technique using techniques disclosed by *Research Disclosure*, Item 38957, cited above, Section III. Emulsion washing.

[0063] The emulsions can be chemically sensitized by any convenient conventional technique as illustrated by *Research Disclosure*, Item 38957, Section IV. Chemical Sensitization: Sulfur, selenium or gold sensitization (or any combination thereof) are specifically contemplated. Sulfur sensitization is preferred, and can be carried out using for example, thiosulfates, thiosulfonates, thiocyanates, isothiocyanates, thioethers, thioureas, cysteine or rhodanine. A combination of gold and sulfur sensitization is most preferred.

[0064] In addition, if desired, the silver halide emulsions can include one or more suitable spectral sensitizing dyes, for example cyanine and merocyanine spectral sensitizing dyes, including the benzimidazolocarbo-cyanine dyes described in U.S. Patent 5,210,014 (Anderson et al.). The useful amounts of such dyes are well known in the art but are generally within the range of from 200 to 1000 mg/mole of silver in the emulsion layer.

[0065] Instability that increases minimum density in negative-type emulsion coatings (that is fog) can be protected against by incorporation of stabilizers, antifoggants, antikinking agents, latent-image stabilizers and similar addenda in the emulsion and contiguous layers prior to coating. Such addenda are illustrated by *Research Disclosure*, Item 38957, Section VII. Antifoggants and stabilizers, and Item 18431, Section II: Emulsion Stabilizers, Antifoggants and Antikinking Agents.

[0066] It may also be desirable that one or more silver halide emulsion layers include one or more covering power enhancing compounds adsorbed to surfaces of the silver halide grains. A number of such materials are known in the art, but preferred covering power enhancing compounds contain at least one divalent sulfur atom that can take the form of a -S- or =S moiety. Such compounds include, but are not limited to, 5-mercapotetrazoles, dithioxotriazoles, mercapto-substituted tetraazaindenes, and others described in U.S. Patent 5,800,976 (Dickerson et al.) for the teaching of the sulfur-containing covering power enhancing compounds.

[0067] The silver halide emulsion layers and other hydrophilic layers on both sides of the support of the first and

second radiographic films generally contain conventional polymer vehicles (peptizers and binders) that include both synthetically prepared and naturally occurring colloids or polymers. The most preferred polymer vehicles include gelatin or gelatin derivatives alone or in combination with other vehicles. Conventional gelatino-vehicles and related layer features are disclosed in *Research Disclosure*, Item 38957, Section II. Vehicles, vehicle extenders, vehicle-like addenda and vehicle related addenda. The emulsions themselves can contain peptizers of the type set out in Section II, paragraph A. Gelatin and hydrophilic colloid peptizers. The hydrophilic colloid peptizers are also useful as binders and hence are commonly present in much higher concentrations than required to perform the peptizing function alone. The preferred gelatin vehicles include alkali-treated gelatin, acid-treated gelatin or gelatin derivatives (such as acetylated gelatin, deionized gelatin, oxidized gelatin and phthalated gelatin). Cationic starch used as a peptizer for tabular grains is described in U.S. Patent 5,620,840 (Maskasky) and U.S. Patent 5,667,955 (Maskasky). Both hydrophobic and hydrophilic synthetic polymeric vehicles can be used also. Such materials include, but are not limited to, polyacrylates (including polymethacrylates), polystyrenes and polyacrylamides (including polymethacrylamides). Dextrans can also be used. Examples of such materials are described for example in U.S. Patent 5,876,913 (Dickerson et al.).

[0068] The silver halide emulsion layers (and other hydrophilic layers) in the radiographic films are generally fully hardened using one or more conventional hardeners. Thus, the amount of hardener in each silver halide emulsion and other hydrophilic layer is generally at least 2% and preferably at least 2.5%, based on the total dry weight of the polymer vehicle in each layer.

[0069] Conventional hardeners can be used for this purpose, including but not limited to formaldehyde and free dialdehydes such as succinaldehyde and glutaraldehyde, blocked dialdehydes, α -diketones, active esters, sulfonate esters, active halogen compounds, s-triazines and diazines, epoxides, aziridines, active olefins having two or more active bonds, blocked active olefins, carbodiimides, isoxazolium salts unsubstituted in the 3-position, esters of 2-alkoxy-N-carboxy-dihydroquinoline, N-carbamoyl pyridinium salts, carbamoyl oxypyridinium salts, bis(amidino) ether salts, particularly bis(amidino) ether salts, surface-applied carboxyl-activating hardeners in combination with complex-forming salts, carbamoylonium, carbamoyl pyridinium and carbamoyl oxypyridinium salts in combination with certain aldehyde scavengers, dication ethers, hydroxylamine esters of imidic acid salts and chloroformamidinium salts, hardeners of mixed function such as halogen-substituted aldehyde acids (for example, mucochloric and mucobromic acids), onium-substituted acroleins, vinyl sulfones containing other hardening functional groups, polymeric hardeners such as dialdehyde starches, and poly(acrolein-co-methacrylic acid).

[0070] The levels of silver and polymer vehicle in each radiographic silver halide film used in the present invention are not critical except that the levels can be adjusted to provide the desired difference in image contrast and/or photographic speed between the first and second radiographic silver halide films. In general, the level of silver on each side of each film is at least 9 and no more than 15 mg/dm². In addition, the total coverage of polymer vehicle on each side of each film is generally at least 30 and no more than 36 mg/dm². The amounts of silver and polymer vehicle on the two sides of the support in each radiographic silver halide film can be the same or different. These amounts refer to dry weights.

[0071] As noted above, the ratio of contrast of images provided by the first radiographic silver halide film to the contrast of images provided by the second radiographic silver halide film can be different. In this embodiment, the contrast difference is at least 1.25 and preferably at least 1.75. As is well known, image contrast can be provided by making adjustments in radiographic silver halide films in various ways, for example by using different levels of dopants (or none at all in one film), by adjusting silver coverage, or by blending emulsions of different sensitivity. One skilled in the art would have the skill and knowledge to prepare first and second radiographic silver halide films with the desired difference in image contrast.

[0072] Also as noted above, the ratio of photographic speed of the first radiographic silver halide film to the photographic speed of the second radiographic silver halide can be different, for example at least 0.15 logE. Preferably, the speed ratio is at least 0.3 logE. As is well known, photographic speed can be adjusted in various radiographic silver halide films in various ways, for example by using various amounts of spectral sensitizing dyes, varying the silver halide grain size, or the use of specific dopants. In view of the teaching provided herein, one skilled in the art would have the skill and knowledge to prepare first and second radiographic silver halide films with the desired difference in photographic speed.

[0073] The radiographic silver halide films useful in this invention generally include a surface protective overcoat on each side of the support that is typically provided for physical protection of the emulsion layers. Each protective overcoat can be sub-divided into two or more individual layers. For example, protective overcoats can be sub-divided into surface overcoats and interlayers (between the overcoat and silver halide emulsion layers). In addition to vehicle features discussed above the protective overcoats can contain various addenda to modify the physical properties of the overcoats. Such addenda are illustrated by *Research Disclosure*, Item 38957, Section IX. Coating physical property modifying addenda, A. Coating aids, B. Plasticizers and lubricants, C. Antistats, and D. Matting agents. Interlayers that are typically thin hydrophilic colloid layers can be used to provide a separation between the emulsion layers and the surface overcoats. It is quite common to locate some emulsion compatible types of protective overcoat addenda, such as anti-

matte particles, in the interlayers. The overcoat on at least one side of the support can also include a blue toning dye or a tetraazaindene (such as 4-hydroxy-6-methyl-1,3,3a,7-tetraazaindene) if desired.

[0074] The protective overcoat is generally comprised of one or more hydrophilic colloid vehicles, chosen from among the same types disclosed above in connection with the emulsion layers. Protective overcoats are provided to perform two basic functions. They provide a layer between the emulsion layers and the surface of the film for physical protection of the emulsion layer during handling and processing. Secondly, they provide a convenient location for the placement of addenda, particularly those that are intended to modify the physical properties of the radiographic film. The protective overcoats of the films of this invention can perform both these basic functions.

[0075] The various coated layers of radiographic silver halide films used in this invention can also contain tinting dyes to modify the image tone to transmitted or reflected light. These dyes are not decolorized during processing and may be homogeneously or heterogeneously dispersed in the various layers. Preferably, such non-bleachable tinting dyes are in a silver halide emulsion layer.

[0076] The radiographic imaging assemblies of the present invention are composed of two radiographic silver halide films as described herein and two fluorescent intensifying screens. Fluorescent intensifying screens are typically designed to absorb X-rays and to emit electromagnetic radiation having a wavelength greater than 300 nm. These screens can take any convenient form providing they meet all of the usual requirements for use in radiographic imaging. Examples of conventional, useful fluorescent intensifying screens are provided by *Research Disclosure*, Item 18431, cited above, Section IX. X-Ray Screens/Phosphors, and U.S. Patent 5,021,327 (Bunch et al.), U.S. Patent 4,994,355 (Dickerson et al.), U.S. Patent 4,997,750 (Dickerson et al.), and U.S. Patent 5,108,881 (Dickerson et al.). The fluorescent layer contains phosphor particles and a binder, optimally additionally containing a light scattering material, such as titania.

[0077] Any conventional or useful phosphor can be used, singly or in mixtures, in the intensifying screens used in the practice of this invention. For example, useful phosphors are described in numerous references relating to fluorescent intensifying screens, including but not limited to, *Research Disclosure*, Vol. 184, August 1979, Item 18431, Section IX, X-ray Screens/Phosphors, and U.S. Patent 2,303,942 (Wynd et al.), U.S. Patent 3,778,615 (Luckey), U.S. Patent 4,032,471 (Luckey), U.S. Patent 4,225,653 (Brixner et al.), U.S. Patent 3,418,246 (Royce), U.S. Patent 3,428,247 (Yocon), U.S. Patent 3,725,704 (Buchanan et al.), U.S. Patent 2,725,704 (Swindells), U.S. Patent 3,617,743 (Rabatin), U.S. Patent 3,974,389 (Ferri et al.), U.S. Patent 3,591,516 (Rabatin), U.S. Patent 3,607,770 (Rabatin), U.S. Patent 3,666,676 (Rabatin), U.S. Patent 3,795,814 (Rabatin), U.S. Patent 4,405,691 (Yale), U.S. Patent 4,311,487 (Luckey et al.), U.S. Patent 4,387,141 (Patten), U.S. Patent 5,021,327 (Bunch et al.), U.S. Patent 4,865,944 (Roberts et al.), U.S. Patent 4,994,355 (Dickerson et al.), U.S. Patent 4,997,750 (Dickerson et al.), U.S. Patent 5,064,729 (Zegarski), U.S. Patent 5,108,881 (Dickerson et al.), U.S. Patent 5,250,366 (Nakajima et al.), U.S. Patent 5,871,892 (Dickerson et al.), EP-A-0 491,116 (Benzo et al.), with respect to the phosphors.

[0078] Useful classes of phosphors include, but are not limited to, calcium tungstate (CaWO_4), activated or unactivated lithium stannates, niobium and/or rare earth activated or unactivated yttrium, lutetium, or gadolinium tantalates, rare earth (such as terbium, lanthanum, gadolinium, cerium, and lutetium)-activated or unactivated middle chalcogen phosphors such as rare earth oxychalcogenides and oxyhalides, and terbium-activated or unactivated lanthanum and lutetium middle chalcogen phosphors.

[0079] Still other useful phosphors are those containing hafnium as described for example in U.S. Patent 4,988,880 (Bryan et al.), U.S. Patent 4,988,881 (Bryan et al.), U.S. Patent 4,994,205 (Bryan et al.), U.S. Patent 5,095,218 (Bryan et al.), U.S. Patent 5,112,700 (Lambert et al.), U.S. Patent 5,124,072 (Dole et al.), and U.S. Patent 5,336,893 (Smith et al.).

[0080] Some preferred rare earth oxychalcogenide and oxyhalide phosphors are represented by the following formula (1):



wherein M' is at least one of the metals yttrium (Y), lanthanum (La), gadolinium (Gd), or lutetium (Lu), M'' is at least one of the rare earth metals, preferably dysprosium (Dy), erbium (Er), europium (Eu), holmium (Ho), neodymium (Nd), praseodymium (Pr), samarium (Sm), tantalum (Ta), terbium (Tb), thulium (Tm), or ytterbium (Yb), X' is a middle chalcogen (S, Se, or Te) or halogen, n is 0.002 to 0.2, and w is 1 when X' is halogen or 2 when X' is a middle chalcogen. These include rare earth-activated lanthanum oxybromides, and terbium-activated or thulium-activated gadolinium oxides such as $\text{Gd}_2\text{O}_2\text{S:Tb}$.

[0081] Other suitable phosphors are described in U.S. Patent 4,835,397 (Arakawa et al.) and U.S. Patent 5,381,015 (Dooms), and including for example divalent europium and other rare earth activated alkaline earth metal halide phosphors and rare earth element activated rare earth oxyhalide phosphors. Of these types of phosphors, the more preferred

phosphors include alkaline earth metal fluorohalide prompt emitting and/or storage phosphors [particularly those containing iodide such as alkaline earth metal fluorobromiodide storage phosphors as described in U.S. Patent 5,464,568 (Bringley et al.)].

[0082] Another class of useful phosphors includes rare earth hosts such as rare earth activated mixed alkaline earth metal sulfates such as europium-activated barium strontium sulfate.

[0083] Particularly useful phosphors are those containing doped or undoped tantalum such as YTaO_4 , $\text{YTaO}_4\text{:Nb}$, Y(Sr)TaO_4 , and $\text{Y(Sr)TaO}_4\text{:Nb}$. These phosphors are described in U.S. Patent 4,226,653 (Brixner), U.S. Patent 5,064,729 (Zegarski), U.S. Patent 5,250,366 (Nakajima et al.), and U.S. Patent 5,626,957 (Benso et al.).

[0084] Other useful phosphors are alkaline earth metal phosphors that can be the products of firing starting materials comprising optional oxide and a combination of species characterized by the following formula (2):



wherein "M" is magnesium (Mg), calcium (Ca), strontium (Sr), or barium (Ba), "F" is fluoride, "X" is chloride (Cl) or bromide (Br), "I" is iodide, M^a is sodium (Na), potassium (K), rubidium (Rb), or cesium (Cs), X^a is fluoride (F), chloride (Cl), bromide (Br), or iodide (I), "A" is europium (Eu), cerium (Ce), samarium (Sm), or terbium (Tb), "Q" is BeO, MgO, CaO, SrO, BaO, ZnO, Al_2O_3 , La_2O_3 , In_2O_3 , SiO_2 , TiO_2 , ZrO_2 , GeO_2 , SnO_2 , Nb_2O_5 , Ta_2O_5 , or ThO_2 , "D" is vanadium (V), chromium (Cr), manganese (Mn), iron (Fe), cobalt (Co), or nickel (Ni). The numbers in the noted formula are the following: "z" is 0 to 1, "u" is from 0 to 1, "y" is from 1×10^{-4} to 0.1, "e" is from 0 to 1, and "t" is from 0 to 0.01. These definitions apply wherever they are found in this application unless specifically stated to the contrary. It is also contemplated that "M", "X", "A", and "D" represent multiple elements in the groups identified above.

[0085] Storage phosphors can also be used in the practice of this invention. Various storage phosphors are described for example, in U.S. Patent 5,464,568 (noted above). Such phosphors include divalent alkaline earth metal fluorohalide phosphors that may contain iodide are the product of firing an intermediate, comprising oxide and a combination of species characterized by the following formula (3):



wherein X, M^a , X^a , A, z, and y have the same meanings as for formula (2) and the sum of a, b, and c is from 0 to 4, and r is from 10^{-6} to 0.1. Some embodiments of these phosphors are described in more detail in U.S. Patent 5,464,568 (noted above).

[0086] Still other storage phosphors are described in U.S. Patent 4,368,390 (Takahashi et al.), and include divalent europium and other rare earth activated alkaline earth metal halides and rare earth element activated rare earth oxyhalides, as described in more detail above.

[0087] Examples of useful phosphors include: SrS:Ce,Sm , SrS:Eu,Sm , $\text{ThO}_2\text{:Er}$, $\text{La}_2\text{O}_2\text{S:Eu,Sm}$, ZnS:Cu,Pb , and others described in U.S. Patent 5,227,253 (Takasu et al.).

[0088] A variety of such screens are commercially available from several sources including by not limited to, LAN-EX™, X-SIGHT™ and InSight™ Skeletal screens available from Eastman Kodak Company.

[0089] The neutral density filters (or "optical spacers") used in the imaging assemblies of this invention are transparent elements that have one or more hydrophilic neutral density filter layers that provide a total density of at least 0.3 (preferably at least 0.45) and up to 0.9. In some embodiments, these layers are disposed on a transparent support. The density can be measured using a standard densitometer (using "visual status").

[0090] In one embodiment, such neutral density filters can be comprised of a single polymeric film that has carbon or one or more neutral density pigments uniformly dispersed therein. The necessary amount of carbon or pigments for a desired density would be readily apparent to one skilled in the art.

[0091] Alternatively, the neutral density filters can have one or more hydrophilic filter layers comprising a dispersion of silver metal or colloidal carbon in one or more hydrophilic binders (such as hardened or unhardened gelatin or other binders described above for radiographic silver halide films) disposed on transparent films (such as those described above for supports). The amount of silver metal or colloidal carbon would vary depending upon the density desired for the filter and a skilled worker would be able to readily determine the appropriate amount of either or both silver metal and colloidal carbon and hydrophilic binder. Techniques for dispersing the silver metal or colloidal carbon in the hydrophilic binder(s) would be readily apparent to one skilled in the art.

[0092] Still again, the neutral density filters can be prepared by coating one or more dispersions (or emulsions) of a silver halide (such as silver bromide or silver iodobromide) in a hydrophilic binder (such as gelatin) on one or both sides of a transparent support. This filter element is then appropriately photographically exposed, for example, to a

conventional step tablet having the desired density and photochemically processed in conventional photochemical processing solutions to provide a neutral density image. Any of a variety of commercial radiographic or black-and-white photographic films can be used for this purpose.

[0093] As noted above, the neutral density filters are arranged between one set of fluorescent intensifying screen and radiographic silver halide film, that is, in either the "front" or "back" of the imaging assembly. The neutral density filter can be disposed in the imaging assembly in any desirable manner so that it is in contact with both the fluorescent intensifying screen and the adjacent radiographic film. For example, the neutral density filter is laminated to the screen so that its hydrophilic layer(s) are in contact with the screen and the transparent support is oriented towards the radiographic silver halide film. The neutral density filter can be laminated to the screen using any suitable technique, such as vacuum pressing.

[0094] The magenta filters (or "magenta spacers") used in the imaging assemblies of this invention are transparent elements that have one or more layers hydrophilic layers that provide a total density of at least 0.3 (preferably at least 0.45) and up to 0.9 at a preferred wavelength of 545 nm and that are disposed on a transparent support. The density can be measured using a standard densitometer (using "visual status").

[0095] Such filters have one or more hydrophilic layers comprising a dispersion of one or more spectral absorbing materials (such as dyes or pigments) in one or more hydrophilic binders (such as hardened or unhardened gelatin or other hydrophilic binders described above for radiographic silver halide films) on transparent films (such as those described above for supports). The spectral absorbing materials absorb electromagnetic radiation in the range of from 500 to 600 nm (preferably from 530 to 570 nm). Thus, they are considered "magenta" filters.

[0096] Pigments and dyes that can be used in this manner include various water-soluble, liquid crystalline, or particulate magenta filter dyes or pigments including those described for example in U.S. Patent 4,803,150 (Dickerson et al.), U.S. Patent 5,213,956 (Diehl et al.), U.S. Patent 5,399,690 (Diehl et al.), U.S. Patent 5,922,523 (Helber et al.), U.S. Patent 6,214,499 (Helber et al.), and Japanese Kokai 2-123349. One useful class of magenta filter dyes are oxonol dyes as described in JP Kokai 2-123349 and U.S. Patent 4,803,150 (noted above).

[0097] The magenta filters can also be provided as commercially available KODAK Wratten Filters No. 32 and 33.

[0098] The amount of the various spectral absorbing materials would vary depending upon the density and spectral absorption desired for the filter and a skilled worker would be able to readily determine their appropriate amount as well as that of the hydrophilic binder(s). The dyes and pigments can be dispersed within the hydrophilic binder(s) using techniques readily known to a worker skilled in the art.

[0099] As noted above, the magenta filters are arranged between one set of fluorescent intensifying screen and radiographic silver halide film, that is, in either the "front" or "back" of the imaging assembly. The magenta filter is laminated to the screen so that its hydrophilic layer(s) are in contact with the screen and the transparent support is oriented towards the radiographic silver halide film. The magenta filter can be laminated to the screen using any suitable technique, such as vacuum pressing.

[0100] Two embodiments of the present invention are illustrated in FIGS. 1 and 2. In reference to the imaging assembly **10** shown in FIG. 1, first fluorescent intensifying screen **20** is arranged in association with first radiographic silver halide film **30** in cassette holder **40**. Neutral density or magenta filter **25** is arranged in association between first fluorescent intensifying screen **20** and first radiographic silver halide film **30**. Imaging assembly **10** also includes second radiographic silver halide film **50** and second fluorescent intensifying screen **60**.

[0101] FIG. 2 shows imaging assembly **10** that is similar to that shown in FIG. 1 except that it also includes metal intensifying screen **70** in the front of first fluorescent intensifying screen **20**.

[0102] Front and back screens can be appropriately chosen depending upon the type of emissions desired, the photicity desired, whether the films are symmetrical or asymmetrical, film emulsion speeds, and % crossover.

[0103] Metal intensifying screens can also be used in the practice of this invention, or included within the radiographic imaging assemblies of the invention. The metal intensifying screens can also take any convenient conventional form. While the metal intensifying screens can be formed of many different types of materials, the use of metals is most common, since metals are most easily fabricated as thin foils, often mounted on radiation transparent backings to facilitate handling. Convenient metals for screen fabrication are in the atomic number range of from 22 (titanium) to 82 (lead). Metals such as copper, lead, tungsten, iron and tantalum have been most commonly used for screen fabrication with lead and copper in that order being the most commonly employed metals. Generally the higher the atomic number, the higher the density of the metal and the greater its ability to absorb MVp X-radiation.

[0104] Exposure and processing of the radiographic silver halide films can be undertaken in any convenient conventional manner. The exposure and processing techniques of U.S. Patent 5,021,327 and U.S. Patent 5,576,156 (both noted above) are typical for processing radiographic films. Other processing compositions (both developing and fixing compositions) are described in U.S. Patent 5,738,979 (Fitterman et al.), U.S. Patent 5,866,309 (Fitterman et al.), U.S. Patent 5,871,890 (Fitterman et al.), U.S. Patent 5,935,770 (Fitterman et al.), U.S. Patent 5,942,378 (Fitterman et al.). The processing compositions can be supplied as single- or multi-part formulations, and in concentrated form or as more diluted working strength solutions. Thus, both first and second radiographic silver halide films can be similarly

processed, and preferably processed using the same processing compositions and conditions.

[0105] Exposing X-radiation is generally directed through a fluorescent intensifying screen before it passes through the neutral density or magenta filter and radiographic silver halide film, in either orientation of the imaging assembly.

[0106] It is particularly desirable that the radiographic silver halide films be processed within 90 seconds ("dry-to-dry") and preferably within 45 seconds and at least 20 seconds, for the developing, fixing and any washing (or rinsing) steps. Such processing can be carried out in any suitable processing equipment including but not limited to, a Kodak X-OMAT™ RA 480 processor that can utilize Kodak Rapid Access processing chemistry. Other "rapid access processors" are described for example in U.S. Patent 3,545,971 (Barnes et al) and EP-A-0 248,390 (Akio et al). Preferably, the black-and-white developing compositions used during processing are free of any gelatin hardeners, such as glutaraldehyde.

[0107] Since rapid access processors employed in the industry vary in their specific processing cycles and selections of processing compositions, the preferred radiographic films satisfying the requirements of the present invention are specifically identified as those that are capable of dry-to-dye processing according to the following reference conditions:

Development	11.1 seconds at 35°C,
Fixing	9.4 seconds at 35°C,
Washing	7.6 seconds at 35°C,
Drying	12.2 seconds at 55-65°C.

Any additional time is taken up in transport between processing steps. Typical black-and-white developing and fixing compositions are described in the Example below.

[0108] Radiographic kits of the present invention can include a radiographic imaging assembly of this invention, one or more additional fluorescent intensifying screens and/or metal screens, and/or one or more suitable processing compositions (for example black-and-white developing and fixing compositions). Preferably, the kit includes all of these components. Alternatively, the radiographic kit can include a radiographic imaging assembly as described herein and one or more of the noted processing compositions.

[0109] In practicing the therapy imaging method of this invention, X-radiation, typically of from 4 to 25 MVp, is directed at a region of the subject (that is, patient) containing features to be identified by different levels of X-radiation absorption. This exposed region is generally somewhat larger than the radiotherapy target area for the purpose of obtaining a discernible image of anatomy reference features outside the targeted area. Thus, a first image is created in the one of the radiographic films (for example, the first radiographic film) as the X-radiation penetrates the subject.

[0110] A shield containing a port is generally placed between the subject and the source of X-radiation, and X-radiation is again directed at the subject, this time through the portal, thereby creating a second image through the port that is superimposed on the first image in the first exposed radiographic film. The total exposure during these steps A and B for localization imaging is generally limited to 10 seconds or less.

[0111] The following example is presented for illustration and the invention is not to be interpreted as limited thereby.

Example 1:

Radiographic Film A:

[0112] Radiographic Film A is a dual coated film having the same silver halide emulsion on both sides of a blue-tinted 178 µm transparent poly(ethylene terephthalate) film support. The emulsions were chemically sensitized with sodium thiosulfate, potassium tetrachloroaurate, sodium thiocyanate, and potassium selenocyanate.

[0113] Radiographic Film A had the following layer arrangement on each side of the film support:

Overcoat
Interlayer
Emulsion Layer

[0114] The noted layers were prepared from the following formulations.

Overcoat Formulation	Coverage (mg/dm ²)
Gelatin vehicle	3.4
Methyl methacrylate matte beads	0.14
Carboxymethyl casein	0.57

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(continued)

Overcoat Formulation	Coverage (mg/dm ²)
Colloidal silica (LUDOX AM)	0.57
Polyacrylamide	0.57
Chrome alum	0.025
Resorcinol	0.058
Whale oil lubricant	0.15

Interlayer Formulation	Coverage (mg/dm ²)
Gelatin vehicle	3.4
Carboxymethyl casein	0.57
Colloidal silica (LUDOX AM)	0.57
Polyacrylamide	0.57
Chrome alum	0.025
Resorcinol	0.058
Nitron	0.044

Emulsion Layer Formulation	Coverage (mg/dm ²)
Cubic grain emulsion [AgClBr (70:30 halide ratio) 0.25 µm average size]	11.5
Gelatin vehicle	26
Spectral sensitizing dye S-1 (shown below)	350 mg/Ag mole
Diammonium aquapentachlororhodate	3.89 x 10 ⁻⁵ mol/Ag mole
2-Carboxy-4-hydroxy-6-methyl-1,3,3a,7-tetraazaindene	2.1 g/Ag mole
1-(3-acetamidophenyl)-5-mercaptotetrazole	0.012
Ethylenediamine tetraacetic acid, disodium salt	0.22
Bisvinylsulfonylmethylether	2.4% based on total gelatin in all layers on that side

Radiographic Film B:

[0115] Radiographic Film B was commercially available KODAK X-ray Therapy Localization (XTL) Film used in radiation therapy imaging.

Radiographic Film C:

[0116] Radiographic Film C had the following layer arrangement and formulations on both sides of the film support:

Overcoat
Interlayer
Emulsion Layer

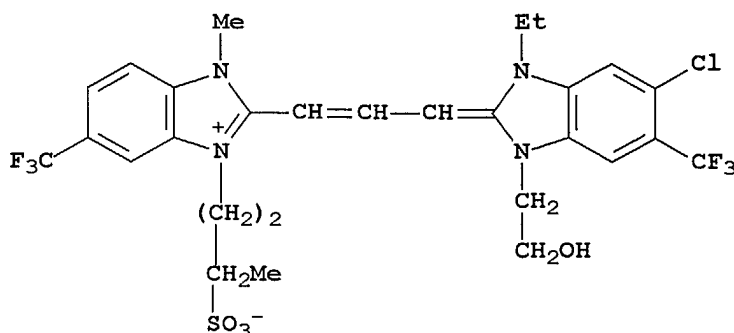
Overcoat Formulation	Coverage (mg/dm ²)
Gelatin vehicle	3.4
Methyl methacrylate matte beads	0.14
Carboxymethyl casein	0.57
Colloidal silica (LUDOX AM)	0.57
Polyacrylamide	0.57

(continued)

Overcoat Formulation	Coverage (mg/dm ²)
Chrome alum	0.025
Resorcinol	0.058
Whale oil lubricant	0.15

Interlayer Formulation	Coverage (mg/dm ²)
Gelatin vehicle	3.4
Carboxymethyl casein	0.57
Colloidal silica (LUDOX AM)	0.57
Polyacrylamide	0.57
Chrome alum	0.025
Resorcinol	0.058
Nitron	0.044

Emulsion Layer Formulation	Coverage (mg/dm ²)
Cubic grain emulsion [AgClBrI (90:9:1 halide ratio) 0.15 μ m average size]	11.5
Gelatin vehicle	26
Spectral sensitizing dye S-1 (see below)	250 mg/Ag mole
2-Carboxy 4-hydroxy-6-methyl-1,3,3a,7-tetraazaindene	2.1 g/Ag mole
1-(3 -Acetamidophenyl)-5-mercaptotetrazole	0.012
Ethylenediaminetetraacetic acid, disodium salt	0.22
Bisvinylsulfonylmethylether	2.4 % based on total gelatin in all layers on that side



S-1

[0117] The cassettes used in the practice of this invention were those commonly used in localization imaging. It comprised a 1 mm thick copper front metal screen and two terbium activated gadolinium oxysulfite general purpose phosphor intensifying screens similar to commercially available KODAK EC-L screens. The phosphor medium particle size was 7 μ m and was dispersed in a PERMUTHANE™ polyurethane binder (phosphor at 7 g/dm², 15:1 phosphor to binder ratio) on a white pigmented polyester support. One screen was placed in back of the film (combination of films) and the other screen was laminated to the front copper metal screen to form a radiographic imaging assembly.

[0118] A neutral density filter was prepared from a conventional KODAK HeNe laser printer silver halide film comprising a transparent poly(ethylene terephthalate) support having silver bromide cubic grain emulsions coated thereon. Samples of this film were exposed to a 780 nm laser in a conventional KODAK 2180 laser printer and processed using

the conventional KODAK 3000RA processor containing conventional KODAK RP Developer and Fixer solutions using conventional conditions. The resulting exposed and processed film was then used as a neutral density filter having a density of 0.6. It was disposed between and in contact with the first fluorescent intensifying screen and the first radiographic film in the imaging assembly.

[0119] Samples of Radiographic Films A, B, and C (or combinations of two films) were exposed in the cassettes (imaging assemblies) using an inverse square X-ray sensitometer. This is a device that makes exceedingly reproducible exposures. A lead screw moves the detector between exposures. By use of the inverse square law, distances are selected that produce exposures that differ by 0.100 logE. The length of the exposures is a constant. With this instrument, we can obtain sensitometry that gives the response of the detector to an imagewise exposure. The image is exposed for the same length of time but the intensity changes due to the anatomy transmitting more or less of the X-radiation flux.

[0120] The inverse square X-ray sensitometer was set to make exposures at 100 kVp with 0.5 mm of copper and 1 mm aluminum added filtration. While this is not the same energy created by a radiation therapy treatment machine, it is suitable for demonstrating that one can control exposure latitude while maintaining excellent image contrast.

[0121] A worker skilled in the art would understand that at the energies used in radiation therapy, X-radiation uniformly stimulates the fluorescent intensifying screens throughout their thickness. They will also recognize that at the conditions used in this example, not all fluorescent intensifying screens will be uniformly illuminated throughout their thickness. This difference is not of a fundamental importance as the teaching herein is directly applicable to any X-radiation energy, including those lower than 100 kVp as well as those commonly used in radiation therapy.

[0122] Processing of the exposed film samples for sensitometric evaluation was carried out using a processor commercially available under the trademark KODAK RP X-OMAT film Processor M6A-N, M6B, or M35A. Development was carried out using the following black-and-white developing composition:

Hydroquinone	30 g
Phenidone	1.5 g
Potassium hydroxide	21 g
NaHCO ₃	7.5 g
K ₂ SO ₃	44.2 g
Na ₂ S ₂ O ₅	12.6 g
Sodium bromide	35 g
5-Methylbenzotriazole	0.06 g
Glutaraldehyde	4.9 g
Water to 1 liter, pH 10	

[0123] The film samples were in contact with the developer in each instance for less than 90 seconds. Fixing was carried out using KODAK RP X-OMAT LO Fixer and Replenisher fixing composition (Eastman Kodak Company).

[0124] Rapid processing has evolved over the last several years as a way to increase productivity in busy hospitals without compromising image quality or sensitometric response. Where 90-second processing times were once the standard, below 40-second processing is becoming the standard in medical radiography. One such example of a rapid processing system is the commercially available KODAK Rapid Access (RA) processing system that includes a line of X-radiation sensitive films available as T-MAT-RA radiographic films that feature fully forehardened emulsions in order to maximize film diffusion rates and minimize film drying. Processing chemistry for this process is also available. As a result of the film being fully forehardened, glutaraldehyde (a common hardening agent) can be removed from the developer solution, resulting in ecological and safety advantages (see KODAK KWIK Developer below). The developer and fixer designed for this system are Kodak X-OMAT RA/30 chemicals. A commercially available processor that allows for the rapid access capability is the Kodak X-OMAT RA 480 processor. This processor is capable of running in 4 different processing cycles. "Extended" cycle is for 160 seconds, and is used for mammography where longer than normal processing results in higher speed and contrast. "Standard" cycle is 82 seconds, "Rapid Cycle" is 55 seconds and "KWIK/RA" cycle is 40 seconds (see KODAK KWIK Developer below). The KWIK cycle uses the RA/30 processing compositions while the longer time cycles use standard commercially available RP X-OMAT compositions. The following Table I shows typical processing times (seconds) for these various processing cycles.

TABLE I

Cycle	Extended	Standard	Rapid	KWIK
Black-and-white Development	44.9	27.6	15.1	11.1
Fixing	37.5	18.3	12.9	9.4
Washing	30.1	15.5	10.4	7.6
Drying	47.5	21.0	16.6	12.2
Total	160.0	82.4	55	40.3

[0125] The black-and-white developing composition useful for the KODAK KWIK cycle contains the following components:

Hydroquinone	32 g
4-Hydroxymethyl-4-methyl-1-phenyl-3-pyrazolidone	6 g
Potassium bromide	2.25 g
5-Methylbenzotriazole	0.125 g
Sodium sulfite	160 g
Water to 1 liter, pH 10.35	

[0126] Optical densities are expressed below in terms of diffuse density as measured by a conventional X-rite Model 310TM densitometer that was calibrated to ANSI standard PH 2.19 and was traceable to a National Bureau of Standards calibration step tablet. The characteristic D vs. logE curve was plotted for each radiographic film that was imaged and processed. Speed was measured at a density of $1.4 + D_{\min}$. Gamma (contrast) is the slope of the noted curves. The results are shown in TABLE II below.

[0127] The "% Drying" was determined by feeding an exposed film flashed to result in a density of 1.0 into an X-ray processing machine in the KODAK KWIK cycle. As the film just exits the drier section, the processing machine was stopped and the film was removed. Roller marks from the processing machine can be seen on the film where the film has not yet dried. Marks from 100% of the rollers in the drier indicate the film has just barely dried. Values less than 100% indicate the film was dried partway into the drier. The lower the value the better the film is for drying.

TABLE II

Film	Relative Speed	Contrast	Image Quality	Drying KWIK Cycle
A	100	5.6	Excellent	50%
B**	100	1.6	Good	100%
C	100	2.6	Good	50%

** Film B was a direct exposure radiographic film (no screen needed). It is well known in the art that the contrast of such a film is 2.3 times (net density) up to about $0.25 D_{\max}$.

[0128] As can be seen from the data in TABLE II, Film A provided excellent image quality as a result of very high contrast. Film A also dried very quickly in the ultra-rapid KODAK KWIK cycle processing. However, due to the high contrast, it does not have much exposure latitude and is difficult to use when therapy machines of fixed film/focal length are used or when exposure settings are not sufficiently fine enough to get the proper exposure.

[0129] Film B provided reasonable image quality and exposure but cannot be processed in the KODAK KWIK cycle process. Film C provided good image quality and acceptable exposure latitude and was processable in the KODAK KWIK cycle processing.

[0130] The lower limit of exposure latitude corresponds to a contrast of 1.5, which occurs here at $\log E = 0.85$. The upper limit on latitude is reached when the density is 3.0. Above 3.0, the image is too dark to be read effectively. This density is reached at $\log E = 1.25$. Thus, the change in $\log E$ is about 0.4, producing an exposure latitude of 2.5:1. The results of exposure latitude (gamma > 2.0 in units of $\log E$) and dynamic range (relative to direct Film B) with individual films and the combination of first and second radiographic films according to the present invention are shown in TABLE III below.

TABLE III

Film	Filter?	Intensifying Screen?	Exposure Latitude	Dynamic Range
A	No	Yes	0.7	2X
B	No	No	0.4	1X
C	No	Yes	0.9	3.2X
A + A	No	Yes	0.7	2X
A + A	Yes	Yes	1.2	6.3X
C + C	No	Yes	0.8	2.5X
C + C	Yes	Yes	1.6	15.8X

[0131] The results in TABLE III indicate that considerable increase in exposure latitude and dynamic range were provided according to the present invention when two films were used in combination in an imaging assembly with the neutral density filter between the first fluorescent intensifying screen and the first radiographic silver halide film compared to the imaging assemblies lacking the filter. The greatest improvements were seen when two samples of the "lower contrast" Film C were used in the imaging assembly.

Example 2:

[0132] Radiographic imaging assemblies were prepared, imaged, and processed as described in Example 1 except a neutral density filter was prepared by coating a dispersion of silver metal (65 mg/m²) in hardened gelatin (3.24 g/m²) onto a blue-tinted poly(ethylene terephthalate) film support. This neutral density filter had a density of 0.6. It was laminated to the first fluorescent intensifying screen with the hardened gelatin layer in contact with the screen by vacuum pressing.

[0133] Optical densities are expressed below in terms of diffuse density as measured by a conventional X-rite Model 310TM densitometer that was calibrated to ANSI standard PH 2.19 and was traceable to a National Bureau of Standards calibration step tablet. The characteristic D vs. logE curve was plotted for each radiographic film that was imaged and processed. Speed was measured at a density of $1.4 + D_{\min}$. Gamma (contrast) is the slope of the noted curves. The results are shown in TABLE IV below.

[0134] The "% Drying" was determined by feeding an exposed film flashed to result in a density of 1.0 into an X-ray processing machine in the KODAK KWIK cycle. As the film just exits the drier section, the processing machine was stopped and the film was removed. Roller marks from the processing machine can be seen on the film where the film has not yet dried. Marks from 100% of the rollers in the drier indicate the film has just barely dried. Values less than 100% indicate the film was dried partway into the drier. The lower the value the better the film is for drying.

TABLE IV

Film	Relative Speed	Contrast	Image Quality	Drying KWIK Cycle
A	100	5.6	Excellent	50%
B**	100	1.6	Good	100%
C	100	2.6	Good	50%

** Film B was a direct exposure radiographic film (no screen needed). It is well known in the art that the contrast of such a film is 2.3 times (net density) up to about $0.25 D_{\max}$.

[0135] As can be seen from the data in TABLE IV, Film A provided excellent image quality as a result of very high contrast. Film A also dried very quickly in the ultra-rapid KODAK KWIK cycle processing. However, due to the high contrast, it does not have much exposure latitude and is difficult to use when therapy machines of fixed film/focal length are used or when exposure settings are not sufficiently fine enough to get the proper exposure.

[0136] Film B provided reasonable image quality and exposure but cannot be processed in the KODAK KWIK cycle process. Film C provided good image quality and acceptable exposure latitude and was processable in the KODAK KWIK cycle processing.

[0137] The lower limit of exposure latitude corresponds to a contrast of 1.5, which occurs here at $\log E = 0.85$. The

upper limit on latitude is reached when the density is 3.0. Above 3.0, the image is too dark to be read effectively. This density is reached at $\log E = 1.25$. Thus, the change in $\log E$ is about 0.4, producing an exposure latitude of 2.5:1. The results of exposure latitude ($\gamma > 2.0$ in units of $\log E$) and dynamic range (relative to direct Film B) with individual films and the combination of first and second radiographic films according to the present invention are shown in TABLE V below.

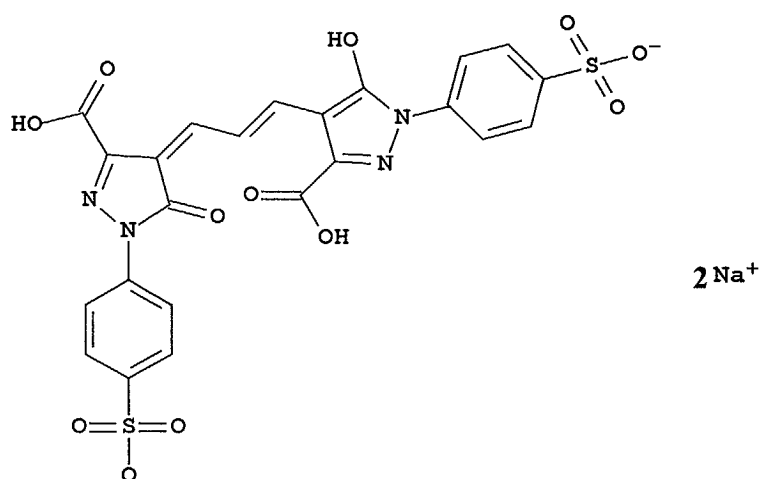
TABLE V

Film	Filter?	Intensifying Screen?	Exposure Latitude	Dynamic Range
A	No	Yes	0.7	2X
B	No	No	0.4	1X
C	No	Yes	0.9	3.2X
A + A	No	Yes	0.7	2X
A + A	Yes	Yes	1.0	4X
C + C	No	Yes	0.8	2.5X
C + C	Yes	Yes	1.5	12.6X

[0138] The results in TABLE V indicate that considerable increase in exposure latitude and dynamic range were provided according to the present invention when two films were used in combination in an imaging assembly with the filter between the first fluorescent intensifying screen and the first radiographic silver halide film compared to the imaging assemblies lacking the filter. The greatest improvements were seen when two samples of the "lower contrast" Film C were used in the imaging assembly.

Example 3:

[0139] Radiographic imaging assemblies were prepared, imaged, and processed as described in Example 1 except a magenta filter was prepared by coating a magenta filter dye as shown below (for example, as used in KODAK Wratten Filter No. 32) in hardened gelatin (3.24 g/m²) onto a blue-tinted poly(ethylene terephthalate) film support. This filter had a density of 0.6 at 545 nm. It was laminated to the first fluorescent intensifying screen with the hardened gelatin layer in contact with the screen by vacuum pressing.



[0140] Optical densities are expressed below in terms of diffuse density as measured by a conventional X-rite Model 310TM densitometer that was calibrated to ANSI standard PH 2.19 and was traceable to a National Bureau of Standards calibration step tablet. The characteristic D vs. $\log E$ curve was plotted for each radiographic film that was imaged and processed. Speed was measured at a density of $1.4 + D_{\min}$. Gamma (contrast) is the slope of the noted curves. The results are shown in TABLE VI below.

[0141] The "% Drying" was determined by feeding an exposed film flashed to result in a density of 1.0 into an X-ray

processing machine in the KODAK KWIK cycle. As the film just exits the drier section, the processing machine was stopped and the film was removed. Roller marks from the processing machine can be seen on the film where the film has not yet dried. Marks from 100% of the rollers in the drier indicate the film has just barely dried. Values less than 100% indicate the film was dried partway into the drier. The lower the value the better the film is for drying.

TABLE VI

Film	Relative Speed	Contrast	Image Quality	Drying KWIK Cycle
A	100	5.6	Excellent	50%
B**	100	1.6	Good	100%
C	100	2.6	Good	50%

** Film B was a direct exposure radiographic film (no screen needed). It is well known in the art that the contrast of such a film is 2.3 times (net density) up to about $0.25 D_{max}$.

[0142] As can be seen from the data in TABLE VI, Film A provided excellent image quality as a result of very high contrast. Film A also dried very quickly in the ultra-rapid KODAK KWIK cycle processing. However, due to the high contrast, it does not have much exposure latitude and is difficult to use when therapy machines of fixed film/focal length are used or when exposure settings are not sufficiently fine enough to get the proper exposure.

[0143] Film B provided reasonable image quality and exposure but cannot be processed in the KODAK KWIK cycle process. Film C provided good image quality and acceptable exposure latitude and was processable in the KODAK KWIK cycle processing.

[0144] The lower limit of exposure latitude corresponds to a contrast of 1.5, which occurs here at $\log E = 0.85$. The upper limit on latitude is reached when the density is 3.0. Above 3.0, the image is too dark to be read effectively. This density is reached at $\log E = 1.25$. Thus, the change in $\log E$ is about 0.4, producing an exposure latitude of 2.5:1. The results of exposure latitude (gamma > 2.0 in units of $\log E$) and dynamic range (relative to direct Film B) with individual films and the combination of first and second radiographic films according to the present invention are shown in TABLE VII below.

TABLE VII

Film	Filter?	Intensifying Screen?	Exposure Latitude	Dynamic Range
A	No	Yes	0.7	2X
B	No	No	0.4	1X
C	No	Yes	0.9	3.2X
A + A	No	Yes	0.7	2X
A + A	Yes	Yes	1.0	4X
C + C	No	Yes	0.8	2.5X
C + C	Yes	Yes	1.5	12.6X

[0145] The results in TABLE VII indicate that considerable increase in exposure latitude and dynamic range were provided according to the present invention when two films were used in combination in an imaging assembly with the magenta filter between the first fluorescent intensifying screen and the first radiographic silver halide film compared to the imaging assemblies lacking the filter. The greatest improvements were seen when two samples of the "lower contrast" Film C were used in the imaging assembly.

Claims

1. A radiographic imaging assembly comprising the following components arranged in association, in order:

- (a) a first fluorescent intensifying screen,
- (b) a first radiographic silver halide film,

- (c) a second radiographic silver halide film, and
- (d) a second fluorescent intensifying screen,

the first radiographic silver halide film comprising a support having first and second major surfaces and is capable of transmitting X-radiation,

the first radiographic silver halide film having disposed on the first major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer, and on the second major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer,

each of the silver halide emulsion layers comprising silver halide cubic grains that have the same or different composition in each silver halide emulsion layer, and all hydrophilic layers of the first radiographic silver halide film being fully forehardened and wet processing solution permeable for image formation within 45 seconds,

the second radiographic silver halide film comprising a support having first and second major surfaces and is capable of transmitting X-radiation,

the second radiographic silver halide film having disposed on the first major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer, and on the second major support surface, one or more hydrophilic colloid layers including at least one silver halide emulsion layer, and

each of the silver halide emulsion layers comprising silver halide cubic grains that have the same or different composition in each silver halide emulsion layer, and all hydrophilic layers of the second radiographic silver halide film being fully forehardened and wet processing solution permeable for image formation within 45 seconds,

the radiographic imaging assembly characterized as having disposed between either the first fluorescent intensifying screen and the first radiographic silver halide film, or between the second fluorescent intensifying screen and the second radiographic silver halide film, a transparent neutral density filter having a density or magenta of at least 0.3.

2. The radiographic imaging assembly of claim 1 wherein the cubic silver halide grains of the silver halide emulsions in the first and second radiographic silver halide films are independently composed of at least 50 mol % chloride based on total silver in the emulsion.
3. The radiographic imaging assembly of claim 1 or 2 wherein the cubic silver halide grains of the silver halide emulsions in the first and second radiographic silver halide films are independently composed of at least 80 mol % chloride based on total silver in the emulsion, and from 0.5 to 1.5 mol % iodide, based on total silver in the emulsion.
4. The radiographic imaging assembly of any of claims 1 to 3 wherein the cubic silver halide grains of each silver halide emulsion in each of the first and second radiographic silver halide films have the same composition.
5. The radiographic imaging assembly of any of claims 1 to 4 wherein the first radiographic silver halide film provides a high contrast image and the second radiographic silver halide film provides a lower contrast image, wherein the ratio of the contrast of an image provided by the first radiographic silver halide film to the contrast of an image provided by the second radiographic silver halide film is at least 1.25.
6. The radiographic imaging assembly of any of claims 1 to 5 wherein at least one silver halide emulsion in the first radiographic silver halide film is doped with a rhodium dopant.
7. The radiographic imaging assembly of any of claims 1 to 6 wherein each of the first and second radiographic silver halide films independently comprise a polymer vehicle on each side of its support in a total amount of from 30 to 36 mg/dm² and a level of silver on each side of from 9 to 15 mg/dm².
8. The radiographic imaging assembly of any of claims 1 to 7 wherein the neutral density filter has a density of from 0.45 to 0.9.
9. The radiographic imaging assembly of any of claims 1 to 8 wherein the neutral density filter comprises a hydrophilic neutral density layer comprising silver metal or colloidal carbon dispersed in hardened gelatin.
10. The radiographic imaging assembly of any of claims 1 to 8 wherein the neutral density filter comprises a hydrophilic neutral density layer comprising imagewise exposed and photochemically processed silver halide dispersed in a hydrophilic binder.
11. The radiographic imaging assembly of any of claims 1 to 8 wherein the neutral density filter is a single transparent

polymeric film having carbon or a pigment dispersed therein.

- 5 12. The radiographic imaging assembly of any of claims 1 to 11 wherein the neutral density is laminated to either said first or second fluorescent intensifying screen, said neutral density filter being arranged so that said hydrophilic layer is in contact with said first or second fluorescent intensifying screen and said transparent support is adjacent said first or second radiographic silver halide film, respectively.
- 10 13. The radiographic imaging assembly of any of claims 1 to 8 wherein said magenta filter is laminated to either said first or second fluorescent intensifying screen, and comprises a transparent support having disposed thereon a hydrophilic layer comprising at least one spectral absorbing material that absorbs radiation in the range of from about 500 to about 600 nm and is dispersed in a hydrophilic binder, said magenta filter being arranged so that its hydrophilic layer is in contact with said first or second fluorescent intensifying screen and its transparent support is adjacent said first or second radiographic silver halide film, respectively.
- 15 14. The radiographic imaging assembly of any of claims 1 to 8 and 13 wherein said magenta filter has a density of from about 0.45 to about 0.9 at 545 nm.
- 20 15. The radiographic imaging assembly of claim 13 or 14 wherein said spectral absorbing material is a pigment or dye having a spectral absorbance in the range of from about 530 to about 570 nm, dispersed in hardened gelatin.
- 25 16. The radiographic imaging assembly of claim 15 wherein spectral absorbing material is an oxonol dye.
- 30 17. A method of providing a black-and-white image comprising exposing the radiographic imaging assembly of any of claims 1 to 16, and processing the first and second radiographic silver halide films, sequentially, with a black-and-white developing composition and a fixing composition, the processing being carried out within 90 seconds, dry-to-dry.
- 35 18. The method of claim 17 wherein the black-and-white developing composition is free of any photographic film hardeners.
- 40 19. The method of claim 17 or 18 being carried out for 60 seconds or less.
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