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(54) **A blow out preventer adapter for subsea well completion**

(57) The blow out (BOP) preventer adapter (152) of the invention has a main body having top and bottom ends, said bottom end arranged and designed for connection to a standard xmas tree (150) re-entry hub (151), said top end having a top profile (302) suitable for interfacing with 18 $\frac{3}{4}$ " (476 mm) nominal bore configuration drilling or completion equipment. This provides the capability to use a BOP stack (120,160) or marine riser and completion landing string (122) (based on standard tubing) in both a tubing hanger interface mode and an xmas tree interface mode. This capability removes the requirement to retrieve a slimbore BOP stack (120) or conventional 18 $\frac{3}{4}$ " (476 mm) BOP stack (160) to permit the installation of the xmas tree using a dedicated open sea completion/intervention riser or a conventional riser.

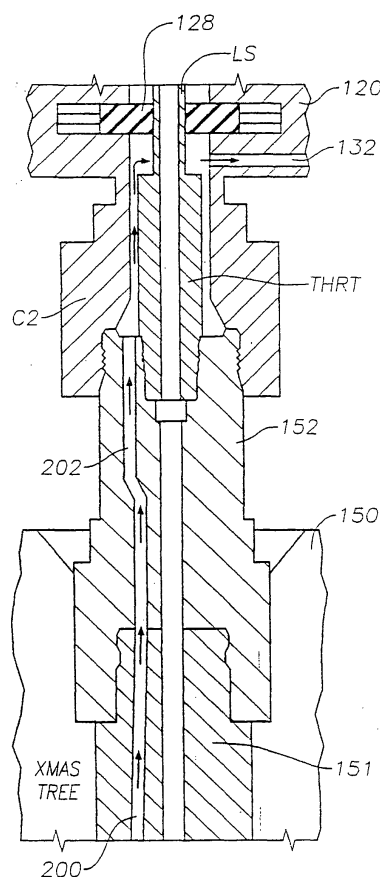


Fig. 14A

Description

Field of the Invention

[0001] This invention relates generally to subsea completion systems. In particular, the invention an arrangement whereby both "reduced bore" ("slimbore") and conventional BQP/marine riser systems may be interfaced both to the tubing spool and the xmas tree, such that the BOP stack need not be retrieved in order that the xmas tree may be installed, and so that the xmas tree need not be deployed with or interfaced at all by a conventional workover/intervention riser, if this is not desired.

Background and Objects of the Invention

[0002] The invention described below originates from an objective to provide a subsea completion system that is capable of being installed and serviced using a marine riser and BOP stack, especially those of substantially reduced size and weight as compared to conventional systems. One objective is to replace a conventional 19" (483 mm) nominal bore marine riser and associated 18-3/4" (476 mm) nominal bore BOP stack with a smaller bore diameter system, for example in the range between 14" (355 mm) and 11" (279 mm) for the marine riser and BOP stack. Preferably the internal diameter of the BOP stack is under 12" (304 mm). If the riser bore diameter is under 12" (304 mm), it will require only 40% of the volume of fluids to fill in comparison to 19" (483 mm) nominal conventional systems. The smaller riser/BOP stack and the resulting reduced fluids volume requirements result in a significant advantage for the operator in the form of weight and cost savings for the riser, fluids, fluid storage facilities, etc. These factors combine to increase available "deck loading" capacity and deck storage space for any rig using the arrangement of the invention and facilitates operations in deeper water as compared to arrangements currently available.

[0003] At the same time, it is desirable to accommodate a large number of electric (E) and hydraulic (H) conduits through the tubing hanger. A currently available tubing hanger typical of those provided throughout the subsea completion industry can accommodate a production bore, an annulus bore, and up to one electric (1E) plus five hydraulic (5H) conduits. An important objective of the invention is to provide a new system to accommodate production tubing and provide annulus communication, and to provide a tubing hanger that can accommodate (ideally) as many as 2E plus 7H independent conduits. The requirement for the large number of E and H conduits results from the desire to accommodate downhole "smart wells" hardware (smart wells have down-hole devices such as sliding sleeves, enhanced sensing and control systems, etc., which require conduits to the surface for their control).

[0004] It is also an object of the invention to provide

a subsea system that obviates the need for a conventional, and costly, "open sea" capable workover/intervention riser. The object is to provide a system which allows well access via a BOP stack/marine riser system on top of a subsea xmas tree. Such a system is advantageous, especially for deep water applications, where the xmas tree can be installed without first having to retrieve and subsequently re-run the BOP stack. Another important object of the invention is to provide a system which allows future intervention using a BOP stack/marine riser or a more conventional workover/intervention riser.

SUMMARY OF THE INVENTION

[0005] The present invention provides a subsea well completion apparatus comprising a blow out preventer (BOP) adapter in accordance with the claims which follow.

[0006] A BOP adapter is provided to connect the top of the conventional sized xmas tree to the bottom of the slimbore or conventional sized BOP stack and marine riser. The landing string, with tubing hanger running tool at its bottom end, is used along with other equipment to provide a high pressure conduit to the surface for production fluids, and to serve as a mandrel around which BOP rams and/or annular BOPs may be closed to create a fluid path for the borehole annulus which is accessed and controlled by the BOP choke and kill conduits.

[0007] After the BOP stack is removed by disconnecting the BOP adapter from the top of the xmas tree, the xmas tree may be capped. The tree cap can be removed later to allow well intervention operations, and the slimbore or a conventional sized BOP and marine riser along with the BOP adaptor, can be run onto the xmas tree. Alternatively, a conventional workover/intervention riser may be used to interface the top of the xmas tree.

BRIEF DESCRIPTION OF THE DRAWINGS

[0008] The objects, advantages, and features of the invention will become more apparent by reference to the drawings which are appended hereto and wherein like numerals indicate like parts and wherein an illustrative embodiment of the invention is shown, of which:

Figures 1A, 1B, 2,3 and 4 are diagrammatic sketches of various arrangements for providing an annulus conduit, a production conduit, and conduits for electric (E) and hydraulic (H) communication via conductors which extend from a surface location above a subsea well to the well below;

Figures 5A and 5B are diagrammatic sketches of an arrangement for providing an annulus conduit, a production conduit and electric (E) and hydraulic (H) conduits from above a subsea well to the well below in which the tubing hanger outer diameter is minimized while maximizing the number of E and H

lines and providing vertical coupling of same to a conventional monobore or dual bore xmas tree; Figures 6 through 8 illustrate prior art hydraulic and electric coupler arrangements possible for communication (via the tubing hanger) through the wellhead to the well below;

Figures 9 through 12 are schematic drawings which illustrate a preferred installation sequence for a tubing hanger/tubing spool arrangement for a slimbore marine riser and slimbore BOP stack and with Figure 12 A showing in an enlarged view the annulus path in the tubing spool which extends around the tubing hanger landing location to form a bypass and with Figure 12B showing a perspective view of the tubing spool with an external piping loop for the annulus path;

Figures 13 and 14 are schematic illustrations of xmas tree installation operations including removal of the slimbore BOP from the wellhead, installation of a xmas tree with an upwardly facing BOP adapter, in accordance with the present invention, and re-installation of the slimbore BOP on top of the XT; Figure 14A presents an enlarged view of the annulus path through the xmas tree, BOP adapter in accordance with the present invention, and BOP, and control of the path with the BOP choke and kill lines; Figure 14B shows the annulus path from the wellhead, through the tubing spool and into the xmas tree;

Figures 15 and 16 are schematic illustrations where the BOP stack and BOP adapter in accordance with the present invention, have been removed from the top of the xmas tree and a tree cap has subsequently been installed in the top profile of the xmas tree respectively;

Figure 17 shows a conventional (standard dimensions) BOP stack and marine riser system installed to the top profile of the xmas tree via the BOP adapter in accordance with the present invention; and

Figure 18 illustrates the provision of a conventional workover/intervention riser secured to the top profile of the xmas tree.

DESCRIPTION OF THE INVENTION

[0009] Figures 1A and 1B schematically illustrate a possible tubing hanger (TH) and xmas tree (XT) arrangement for meeting the objectives as described above. Figure 1A illustrates a tubing spool TS to which a conventional xmas tree XT is attached by means of a connector C. The tubing spool TS is secured to a wellhead housing WH. The outer profile of tubing spool TS shown is referred to as an 18-3/4" (476mm) mandrel style (the 18-3/4" designation referring to the nominal bore of the BOP stack normally associated with the subject profile) but with an internal diameter of under 11" (279mm) or 13-5/8" (346mm) depending on the BOP or marine riser internal diameter dimension. A tubing hang-

er TH is landed in the internal bore of tubing spool TS, and the tubing hanger TH has an annulus conduit A, a production conduit P, and several E and H ports or conduits through it. Couplers 10 are illustrated schematically at the top of hanger H. Figure 1 B is a cross section (taken along lines 1B-1B of Figure 1A) of the tubing hanger TH of Figure 1A and illustrates that for a tubing hanger TH with specified diameters for the production bore P and the annulus bore A, only a few electric and hydraulic bores of predetermined diameters can be provided.

[0010] Figure 2 schematically illustrates another arrangement.

[0011] A tubing spool TS2 is provided which includes an annulus bore bypass ABP2 with valves V2. A tubing hanger TH2 has a production bore P2 and electric and hydraulic conduits E2, H2. Such conduits are bores through the body of the hanger which communicate with vertical and horizontal couplers 12, 14. The tubing spool TS2 can accept either a conventional vertical xmas tree CXT or a horizontal christmas tree HXT. The advantage of the arrangement of Figure 2 over that of Figure 1A is that it includes a bypass annulus bore ABP2 in the tubing spool TS2 itself which provides room for the production bore P2 and an increased number of E and H conduits in the tubing hanger TH2 (as compared to the arrangement of Figures 1A, 1B). As mentioned above, it is assumed that the outer diameter of TH2 is the same as that of TH, i.e., under about 11" (279mm) or 13-5/8" (346mm) depending on the BOP and marine riser dimensions.

[0012] Figure 3 is another schematic illustration, which is similar to that of Figure 2. However, only horizontal couplers 16 for the E and H channels are provided. Such an arrangement is disadvantageous in that continuous vertical communication between the equipment installation vessel and downhole electric and hydraulic functions is not accommodated.

[0013] Figure 4 is another schematic illustration of a possible tubing hanger TH4/conventional vertical bore xmas tree combination where a xmas tree XT4 is secured to a tubing spool TS4. A concentric tubing hanger TH4 is provided in tubing spool TS4 and has annulus bore or bores A4 and production bore P4 through it. Valve or valves V, are provided in bore or bores A4. The arrangement of Figure 4 provides only vertical controls access.

[0014] Figures 5A and 5B schematically show the preferred embodiment of an arrangement to meet the objectives stated above. The arrangement of Figures 5A and 5B provide the best features of a CXT and an HXT in a hybrid arrangement, where a valved annulus bypass AS is provided in the tubing spool TS5, and with a production bore P5 and an increased number of E and H conduits 18 provided therein. In the preferred arrangement of Figure 5A, the tubing spool TS5 is arranged end designed to pass an 8½" (216mm) bit. Its top outer profile should be compatible with a standard 18-¾"

(476mm) system so as to accept a conventional sized CXT and standard sized BOP, as well as a slimbore BOP. Ideally it should have a bore protector and its upper internal profile (ID) diameter would be on the order of 11" (279mm) or 13-5/8" (346mm), depending on the bore size of the smallest BOP system to be interfaced. Ideally up to nine, but as many as 12-to-14 ports or conduits 18 of 1.50" (38mm) nominal diameter can be provided in tubing hanger THS. Of these ports, some may be required for alignment purposes, depending on the alignment method adopted.

[0015] The Figures I through 5 provide alternative tubing hanger (TH) and xmas tree (XT) combinations which are examined for their capability to meet the objectives as described above.

[0016] The arrangement of Figures 5A and 5B offer certain advantages regarding the desired specific objectives. The annulus communication path or passage AS is routed via the body of the tubing spool TS5 and passes "around" rather than "through" the tubing hanger, as is the case for Figures 1A, 1B and 4. In other words, a passage is provided around the sealed landing position between the tubing spool TS5 and the tubing hanger THS. This feature provides more space to accommodate a relatively large number of E and H conduits. As with horizontal tree (HXT) arrangements, the annulus passage A5, whether integrated with the body of the TS or attached externally by some means, is typically fitted with one or more valves VA5, VA6 in order to enable remote isolation/ sealing of the annulus flow path. Whereas a conventional "vertical dual bore" (VDB) xmas tree/completion system requires that a wireline plug be installed into the annulus bore of the conventional tubing hanger (or thereabouts) in order to seal it off, providing a valved annulus bypass port achieves savings in time and money associated with installing/ retrieving such a plug. Since the valves VA5, VA6 of Figure 5A are preferably (but not limited to) gate valves, the reliability of the annulus pressure barrier is also improved with the arrangement of Figure 5A as compared to a wireline plug. It is also notable that the annulus bypass conduit A5 is contained as part of a tubing spool assembly TS5 and not in the body of the tree as would be the case for HXTs.

[0017] Tubing spools ("TS"), also called tubing heads, offer advantages and disadvantages. Some of the more common characteristics associated with tubing spools include:

- (1) provides "clean" interfaces for a tubing hanger ("TH"),
- (2) reduces stack-up tolerances to "machine tolerances",
- (3) can be equipped with an orientation device, thereby minimizing TH "rotational" tolerance range and possibly removing the need to modify BOP stacks so that they can orient the TH (as is typically required for conventional vertical dual bore VDB

systems),

(4) can incorporate flowline/umbilical interface and parking facilities,

(5) represent an additional capital expenditure compared to both CXT systems (where the TH is landed directly in the wellhead) and HXT systems (TH landed in the body of the HXT),

(6) may require an extra trip (i.e., installation of TS) as compared to CXT and HXT systems, and

(7) requires that the BOP be removed from the wellhead so that the TS may be installed onto the wellhead, and the BOP subsequently landed on the TS, and the downhole completion/TH then subsequently installed.

[0018] While the above list is by no means complete, it shows advantages and disadvantages of a tubing spool/tubing hanger (TS/TH) arrangement as compared to CXT systems and HXT systems. The last three characteristics (5,6,7), represent drawbacks for a TS completion, especially because HXT systems provide most of the benefits of a TS without most of its disadvantages. Nevertheless, the advantages provided by the design of Figures 5A, 5B outweigh the disadvantages identified above, especially since the impact of the drawbacks are mediated in the design of the invention.

[0019] An important advantage of the arrangement of Figures 5A and 5B is its capability to pass a very large number of E and H lines 18 through the tubing hanger TH5 while requiring only a very small bore subsea BOP and marine riser. For example purposes only, a tubing hanger TH5 capable of suspending 4-1/2" (114mm) production tubing and providing on the order of 10 (combined total) E and H passages 18 of 1 1/2" (38mm) diameter can be passed through a roughly 11" (279mm) bore (drift) BOP stack and an associated "slimbore" marine riser (12" (304mm) ID).

[0020] A comparably capable HXT tubing hanger system would likely require a 13-5/8" (346mm) nominal bore BOP and a 14" (355mm) ID (approximate) bore marine riser. The cross sectional area of a 19" (483mm) bore marine riser (typically used with 18-3/4" (476mm) bore BOP stacks) is 283.5 in.² (1829 cm²). Cross sectional areas for 14" (355mm) and 12" (304mm) risers are 153.9 in.² (993 cm²) and 113.1 in.² (730 cm²) respectively. The volume of fluids required to fill these risers are 100%, 54.3% and 39.9% respectively, using the 19" (483mm) riser as the base case. Fluids savings translate into direct cost savings, and indirect savings associated with reduced storage requirements, pumping requirements, etc. Furthermore, "variable deck loading" is improved since smaller risers, less fluid, less fluid storage, etc., all weigh less. A 12" bore riser requires only 73.5% as much fluid volume as a 14" (355mm) riser (a significant advantage for the system of this invention when compared even to reduced bore HXT systems). As the water depth for subsea completions increases, the issue of variable deck loading be-

comes more important.

[0021] The arrangement of Figures 5A and 5B has characteristics of a conventional xmas tree completion system and an HXT (horizontal xmas tree) completion system. It is a hybrid of features of a CXT and an HXT connected to a well head, but it most closely resembles a CXT with a tubing spool.

[0022] Another significant advantage of the slimbore subsea completion system of Figures 5A and 5B is the manner in which E and H conduits 18 are handled. It is generally recognized in the subsea well completion/intervention industry that whenever (especially) electric lines are required to be installed into a wellbore, the most common failure mode is that the cables and/or end terminations become damaged during the installation process. It is, therefore, highly desirable that electric circuit continuity be monitored throughout the installation activity (i.e., from the time that the downhole electric component is made up into the completion string until the time that the TH is landed and tested). Whereas there have been many cases in which a downhole electric problem has been detected (i.e., communication with a downhole pressure and temperature gauge lost), and simply ignored (i.e., deemed not worth the cost to pull the completion to replace the damaged component). This will likely not be an acceptable practice where "smart well" hardware is integrated with the completion - there is too much money and potential well productivity impact involved. It is, therefore, important that electric circuit continuity can be monitored throughout the completion installation process.

[0023] The most efficient method traditionally employed to monitor downhole functions during the completion installation process has been to route lines from each downhole component through a series of interfaces all the way back to the surface. In the system of this invention, which is typical of CXT systems regarding electric conduit respects, lines are run from the downhole components alongside the production tubing (clamped thereto) and terminated into the bottom of the TH. The lines are routed through the TH and are equipped with "wet mateable" devices which have the capability to conduct power and data signals across the TH/TH Running Tool (THRT) interface during TH installation and related modes, and across the TH/xmas tree interface during production and intervention modes, etc. From the THRT bottom face, the electric conduits are typically routed through a variety of components (possibly ram and/or annular BOP seal spools, subsea test tree (SSTT)/ emergency disconnect (EDC) latch device, E/H control module, etc.) until they are ultimately combined into a bundle of lines (E and H) typically referred to as an umbilical. The umbilical conveniently can be reeled in or out for re-use in a variety of applications.

[0024] After the TH has been installed and tested, one completion scenario (one that is typically used throughout the industry) is for the landing string (LS, i.e., THAT on "up") to be retrieved, the BOP stack/marine riser dis-

connected and retrieved, and the xmas tree installed using typically a workover/intervention riser system. The xmas tree engages the same E and H control line (wet mateable) couplers at the top of the TH as previously interfaced by the THRT. It is a special attribute of the system of the invention that the THRT need only be unlatched from the TH and the LS lifted up into or just above the BOP stack, and the BOP stack need only be removed from the wellhead a sufficient lateral distance to facilitate installation of the xmas tree onto the TS. Specifically, the XT may be lowered by an independent hoisting unit and installed onto the wellhead using a cable or tubing string with ROV assistance, etc., or the xmas tree may previously have been "parked" at a laterally displaced seabed staging position for movement onto the wellhead using the LS and/or BOP stack/ marine riser, for example.

[0025] The procedure for installation of an HXT is different in that it is often preferred that no umbilical be used as part of the TH deployment process. During an HXT installation the SCSSV(s) are typically locked "open" prior to deployment of the TH, a purely mechanical or "external pressure" (possibly "staged") operated THRT/TH is employed, and no communication with downhole components is provided. Once the TH has been engaged (and typically locked) into the bore of the HXT, electric and hydraulic communication between the surface and downhole is established via the HXT using an umbilical run outside of the marine riser. A remotely operated vehicle (ROV) is typically used to engage the various couplers in a radial direction (not a vertical direction) into the TH from the HXT body (horizontal plane of motion). One supplier also employs "angled" interfacing devices for the hydraulic conduits (i.e., between a tapered lower surface of the TH and a shoulder in the HXT bore) which are engaged passively as part of the TH landing/locking operation.

[0026] It is the generally horizontal/radial orientation of couplers of especially the electric lines typical of an HXT system that tends to drive up the required diameter of the associated TH, and hence the required bore size for the related BOP stack and marine riser used to pass it. It is, of course, conceivable that a new design HXT and/or (wet-mateable electric) controls interface could be developed that would permit HXT TH size reduction (i.e., more compact coupler, or other than horizontal arrangement, or both, etc.), but HXTs for natural drive wells at least have used the "side-porting" of the controls interfaces between TH and HXT body to avoid complexity.

[0027] The VDB TH schematic of Figure 6 shows a conventional tubing hanger TH6 for a VDB completion system. It shows a production bore P and an annulus bore A and shows that the E and H conduits 18 are routed in a generally vertical manner from the top to the bottom of the tubing hanger TH6. A hydraulic coupler 20 and an electric coupler 22 are schematically illustrated. The HXT TH schematic of Figure 7 illustrates a tubing

hanger TH7 for an HXT with the vertical interface of electric and hydraulic conduits 18' at the bottom of the TH and the generally horizontal or radial couplers 20', 22' interface at the side of the TH. If it is desired to accommodate monitoring of the electric continuity to downhole equipment throughout the completion installation process as discussed above, it is necessary to have dual remotely engageable E and H controls interfaces for an HXT system: one "facing up" for engaging the THRT and one "facing sideways" or radially for engaging the HXT body conduit transfer devices. Figure 8 shows such an arrangement with vertical and radial couplers 20"V, 20"H for an electric lead coupler and vertical and radial hydraulic couplers 22"V, 22"H schematically illustrated. The arrangement of Figure 8 adds complexity to the system and greatly increases the risk of failure. Furthermore, one conduit access point (vertical or horizontal) must be positively de-activated whenever the alternative access point (horizontal or vertical) is active. There are obviously significant cost and packaging considerations also imposed on the HXT system when enhanced to provide all desired features. The HXT TH8 schematically illustrated in Figure 8 having both vertical and horizontal interfaces is typical of a system actually provided for a subsea application in the Mediterranean Sea.

[0028] The question arises as to why the E and H conduits need to exit sideways for a HXT system? Why can't the controls interface be presented only at the top of the TH, for interface both by the THRT and HXT tree cap? Such an arrangement has been used effectively for electrical submersible pump (ESP) applications for which the wells have insufficient energy to produce on their own. The limitations for "natural drive" well applications have to do with (1) the number of tested pressure barriers that must be in place before the BOP stack can be removed from the top of the HXT, and (2) the ability to provide adequate well control in the event pressure comes to be trapped under an HXT tree cap. To date, HXTs used on natural drive wells have typically required tree caps that can be installed and retrieved through the bore of a BOP stack. Electric submersible pump (ESP) equipped HXT wells that cannot produce without artificial lift have been accepted with an "external" tree cap (which also facilitates passage for E and H lines between the TH and HXT mounted control system). Great complexity (number of functions, orientation, leak paths, etc.) and risk would be added if an "internal" tree cap were required also to conduit E and H controls. In fact, two caps would likely be required, one through-BOP installable; a second to route the control functions over to the HXT. The conduits between the external tree cap and the HXT would also be limited regarding the depth of water in which they can be operated, assuming they were to be comprised of flexible hoses. Conduits exposed externally to sea water pressure have a limited "collapse" resistance capability.

[0029] The fact that HXTs used on natural drive wells currently require an internal (through-BOP deployed)

tree cap further increases the size penalty of HXT systems. This is because the tree cap needs a landing shoulder, seal bores, locking profiles, etc., all of which are generally larger than the diameter of the TH it will ultimately be positioned above.

[0030] The slimbore system of this invention, on the other hand, needs to pass nothing larger than the TH, THRT and landing string (LS) through the subsea BOP stack. A more or less conventional VDB or alternatively a "monobore" xmas tree (both of which are referred herein generically as conventional xmas trees, CXT) can be installed on top of the "slimbore" TS/TH like that of Figures 5A, SB, because the outer profile of the "slimbore" tubing spool is a conventional 18³/₄" (476mm) configuration. An associated tree cap for the CXT can be ROV deployed, which saves a trip between the surface and subsea tree, which would normally be required for CXT systems. Some advantages of using a subsea completion arrangement that does not include an HXT tree concern relative smaller size and lower weight. These advantages are important for deployment from some deepwater capable rigs. Furthermore, CXTs can be "intervened" using simpler tooling packages deployed from lower cost vessels.

[0031] Associated with the slimbore completion system permanently installed hardware (TS, TH, XT, etc.) of this invention as schematically illustrated in Figures 5A, 5B, are a suite of tools that make its installation and subsequent interface effective. The installation sequence of figures 9 to 18 illustrate completion/intervention systems and running tools and methods for these activities.

[0032] Figure 9 shows a conventional subsea wellhead system 100, comprising a high pressure wellhead housing 102 and associated conductor housing and well conductor 104, installed, at the subsea mudline 106. The internal components of the system 100 including casing hangers/ casing strings and seal assemblies, etc., (not illustrated) are conventional in the art of subsea wellhead systems.

[0033] Figure 10 shows a tubing spool TS10 (also known as a tubing "head"), secured on top of the high pressure wellhead housing 102 by means of a connector C1. The connector C1 is preferably a hydraulic wellhead connector which establishes a seal and locks the interface of the tubing spool TS10 to the wellhead housing 102. Other securing means can be used in place of the connector C1. The tubing spool TS10 provides an upward-facing profile which typically, but not necessarily, matches the profile of the wellhead housing 102. The tubing spool TS 10 is constructed according to the arrangement illustrated in Figures 5A and 5B. It contains internal profiles and flow paths that are discussed below.

[0034] Figure 11 shows a slimbore BOP stack 120 landed, locked and sealed (by means of hydraulic connector C2) on top of the tubing spool TS10 of Figure 10. Slimbore in this context means that the I.D. of the BOP is about 13-5/8" (346mm). Connector C2 is arranged

and designed to connect the 13-5/8" (346mm) nominal slimbore BOP stack to the (typically) 18³/₄" (476mm) nominal configuration outer profile of tubing spool TS10. The purpose of the BOP stack 120 is primarily to provide well control capability local to the wellhead system components. An integral but independently separable part of the slimbore BOP stack is the lower marine riser package (LMRP) 122. It provides for quick release of the marine riser 124 from the slimbore BOP stack 120 in an emergency, such as would be required if the surface vessel to which the marine riser is connected were to move off location unexpectedly. Within the LMRP 122 is a "flex-joint" 123 that eases riser bending loads and the transition angle associated with the interface of the marine riser 124 with the substantially stiffer LMRP 122 and BOP stack 120 components. The LMRP 122 also contains redundant control modules, choke and kill line terminations and, typically, a redundant annular blow-out preventer. By retrieving the LMRP 122, any of these items can be repaired or replaced, if the need were to arise, without requiring that the BOP stack 120 be disturbed. This feature is important, because the BOP stack could be required to maintain well control.

[0035] The marine riser 124 itself is the component of the system that enables the BOP stack 120 to be lowered to and retrieved from the high pressure wellhead housing 102 (drilling mode) and tubing spool TS10 at sea floor 106. It is also, however, the conduit through which drilling and completion fluids are circulated, and through which all wellbore tools are deployed. The internal diameter of the marine riser defines to a significant extent (especially in deep water) the volume of fluids that must be handled by the associated deployment vessel, and also defines the maximum size of any elements that can pass through the riser. The internal diameters of the riser 124, the lower marine riser package 122 and the BOP stack 120 must be sufficient to pass the equipment and tooling that will be run into the bore of the tubing spool TS10 which is designed like the tubing spool TS5 of Figures 5A and 5B. The small internal bore diameter of tubing spool TS 10, enabled by its arrangement with a tubing hanger having a production bore (but no annulus bore) and an increased number of E and H conduits, determines the minimum size acceptable for the inner diameter of BOP stack 120 and Lower Marine Riser Package 122 and marine riser 124. It is preferred that the tubing hanger TH12 (see Figure 12 and Figure 12A) have a maximum external diameter of slightly less than 11" (279mm) and that the internal bore of BOP stack 120 and LMRP 122 be slightly greater, e.g., 11" (279mm) drift so as to be able to pass tubing hanger TH12 through them. The internal diameter of marine completion riser 124 is preferably about 12" (304mm).

[0036] Alternatively, for a slightly larger system the tubing hanger TH12 may have a maximum external diameter of slightly less than 13-5/8" (346mm), with the internal bore of BOP stack 120 and LMRP of slightly

greater dimension, 13-5/8" (346mm) drift, and with the internal diameter of marine completion riser 124 about 14" (355mm).

[0037] Figure 12 shows a sectional view of Figure 11. Figure 12A shows an enlarged sectional view of Figure 12. In Figures 12A and 12B the tubing hanger, TH12 has been landed, locked and sealed to the bore of the tubing spool TS10. The arrangement of tubing hanger/tubing spool TH12/TS10 is like that of TH5/TS5 of the schematic illustrations of Figures 5A, 5B. The orientation of the tubing hanger TH12 within the tubing spool TS10 is achieved passively by engagement typically of a tubing hanger - integral key into a tubing spool - fixed cam/vertical slot device (not shown). Alternative passive alignment arrangements are also known to those skilled in the art of well completions. For the arrangement shown in Figure 12A, the key is preferably located below the tubing hanger TH12 landing shoulder, but another location for such a key may be provided. Figure 12 and enlarged portion Fig. 12A further show an annulus path or passage A12 that allows communication of fluids around the tubing hanger TH12 (i.e., from above to below the sealed landing location of TH12/TS10, and vice-versa). This "bypass" path A12 is equipped with a remotely operable valve V12 that permits remote control closure of the passage A12 whenever desired, without the need for an associated wireline operation. Figure 12A most clearly shows the completion landing string LS made up to the top of the tubing hanger TH12. The landing string LS is typically defined as everything above the tubing hanger TH12 as illustrated in Figure 12.

[0038] As illustrated in Figure 12, the subsea test tree SSTT and associated emergency disconnect latch ED-CL (if required) are positioned above the lowermost BOP stack 120 ram 128 and below the BOP blind/shear ram 130. Such an arrangement is conventional. By closing the lowermost ram 128 on the pipe section between the tubing hanger running tool THRT and the subsea test tree, SSTT, the well annulus can be accessed via port A12 using the BOP stack choke and kill system flow paths 132. The communication path is illustrated by arrows AP in Figure 12A. All of these system characteristics cooperate to enable use of a simple, tubing-based slimbore monobore landing string LS and a very small outside diameter (OD) tubing hanger TH12.

[0039] Figure 12B is a perspective view of tubing spool TS10 which shows that the annulus path A12 may include an external piping loop A12' as an alternative to the internal conduit illustrated in Figure 5A. The annulus bypass conduit may also reside fully within either a bolt-on or flange-on block attached to the side of the tubing spool TS10. Valve V12 is remotely controllable.

[0040] Figure 13 illustrates the state of the subsea system with the slimbore BOP stack 120/122 removed from the tubing spool TS10 (with the bottom of the landing string LS suspended therein) and offset laterally a relatively small distance from the top of the tubing spool

TS10. Figure 13 also shows that a subsea xmas tree 150 and BOP adaptor 152 have been installed in place of BOP 120 with connector C3 securing xmas tree 150 to tubing spool TS10. Connector C3 connects the xmas tree 150 to the typically 18³/₄" (476mm) configuration nominal profile of the tubing spool TS10. The xmas tree 150 may be deployed to the tubing spool TS10 by means of a cable in coordination with a ROV, or on drill pipe or tubing, or even using the BOP stack 120 and/or landing string LS themselves as the transport devices. Note that for the case where a conventional size BOP stack is used in place of the slimbore system, it is also conceivable that the BOP stack could be "parked" on top of an appropriate seabed facility (typically a preset pile or another wellhead arrangement) and the LMRP used as the transport tool.

[0041] Figure 13 further shows a BOP adaptor 152 removably secured to the top of the conventional xmas tree 150, preferably installed to the top of xmas tree 150 while it was on the vessel prior to deployment. Its purpose is to adapt the upper profile 300 of an otherwise conventional xmas tree (e.g., a 13-5/8" (346mm) clamp hub or similar profile as compared to a standard 18³/₄" (476mm) configuration top interface) for an interface 302 with the larger connector C2, typically 18³/₄" (476mm), on the bottom of the slimbore BOP stack 120, or the BOP stack LMRP 122 (with connector C2', for example) or a standard BOP stack 160 or its LMRP 170 (see Figure 17). In other words, BOP adaptor 152 has a bottom profile of typically 13- 5/8" (346mm) nominal configuration and a top profile 302 of 18³/₄" (476mm) nominal configuration. Figure 13 illustrates the slimbore BOP stack 120 prior to its connection to the conventional xmas tree 150 by means of the BOP adaptor 152. The BOP adaptor 152 has an internal profile that emulates the upper internal profile of the tubing hanger TH12 so that the tubing hanger running tool THRT of landing string LS may be used to "tieback" the production bore of the xmas tree 150. In other words, the inner profile of the BOP adaptor 152 includes a central production bore and at least "dummy" plural E and H receptacles which match those of the tubing hanger, and also includes an annulus passage. The BOP adaptor 152 is arranged and designed to provide all interface/guidance facilities required, such as a guidelineless (GLL) re-entry funnel, if required (not shown).

[0042] Figure 14 and the enlarged sectional views of Figures 14A, 14B show the slimbore BQP stack 120 and landing string LS after engagement of connector C2 to the top of the BOP adaptor 152 and thereby to the 13-5/8" (346mm) re-entry hub 151 of xmas tree 150. The physical relationship between the landing string LS components and BOP stack 120 are identical to such relationship in Figure 12 (orientation, elevation, etc.). Control of the annulus bore is by means of the choke and kill lines 132 of the BOP stack 120 via the annulus port A12 of Figure 12A and of Figures 14 and 14B. Note that for the scenario where a conventional size LMRP

170 is interfaced with the BOP adaptor 152, receptacles and appropriate conduits for the choke and kill lines would have to be provided. The BOP adaptor 152 enables such identical physical arrangements along with various other advantages. Such advantages are listed below.

(1) The BOP stack 120 and landing string LS need not be retrieved to the surface to permit deployment/installation of the tree 150 as illustrated in Figure 13. This advantage represents substantial cost savings because of the "trip time" saved (likely >\$1 million for deep water).

(2) Because the BOP adaptor 152 resides between the top of the xmas tree 150 and the bottom of a BOP connector C2 (or LMRP connector C2', the packaging of the xmas tree 150 upper profile need not be modified to accommodate the larger connector of an 18-3/4" BOP stack or LMRP to achieve the benefit of eliminating a trip of the BOP stack 120 to permit installation of the xmas tree 150.

(3) No special completion riser is required to install or intervene the xmas tree 150. Nevertheless, such a conventional approach could be used for the installation or any subsequent intervention or retrieval exercise simply by foregoing use of the BOP adaptor 152. In other words, the standard xmas tree top profile would not be changed.

(4) Standard (light weight) tubing/casing can be used to deploy the tubing hanger TH12, because the landing string LS is not required to be operated outside of the slimbore marine riser 124 (or even a conventional marine riser). This results in an advantage that tubing hanger TH12 can be installed with the benefit of "heave compensation" in deeper water, since the lighter weight landing string will not exceed the capacity of typical compensators (whereas most dedicated riser/landing string designs do).

(5) One and the same BOP adaptor 152 can be used to facilitate interface with a conventional (typically 18-3/4" (476mm)) BOP stack and/or LMRP, if a slimbore BOP stack 120 is not available. This assumes that a sufficiently strong bottom connector/XT top profile interface is provided.

[0043] Figure 15 shows the condition of the subsea well after the landing string LS, BOP stack 120, marine riser 124, and BQP adaptor 152 have been retrieved from the top of the xmas tree 150. The BOP adaptor 152 is retrieved during the same trip as retrieval of the BOP stack 120 in order to save a trip. Specifically, there are no dedicated trips (or tools) required for the BOP adaptor 152. It is installed already made up to the xmas tree

150, yet it can be retrieved at the same time as the BOP stack 120 or 160 (see Figure 17 and discussion below) leaving the xmas tree 150 connected to tubing spool TS10. Retrieval of the xmas tree 150 by one approach is simply the reverse of the installation process. The BOP adaptor 152 may be secured to the bottom of an appropriate BOP stack 120 or LMRP 122, and the BOP adaptor 152 subsequently connected to xmas tree 150. After appropriate pressure barriers have been established in the wellbore, the xmas tree 50 may be retrieved. A variety of other means may also be employed to achieve securing the well and retrieving the tree (including use of a conventional completion/intervention riser system).

[0044] Figure 16 shows a tree cap 158 installed to the top of the xmas tree 150 re-entry profile 300 as a conventional redundant barrier to the xmas tree swab valves and as a "critical surfaces" protector.

[0045] Figure 17 is essentially the same as Figure 14, with the significant difference that the BOP stack 160 shown is a conventional deepwater 18-3/4" (476mm) nominal size version. The BOP adaptor 152 is connected to the larger BOP stack 160 via the connector C4 attached to the 18³/₄" (476mm) configuration profile at the top of the adaptor. Specifically, the BOP adaptor 152 provides a common top profile for interface of both slimbore and conventional BOP stacks.

[0046] Figure 18 is an alternative arrangement for the xmas tree 150 secured to a slimbore tubing spool TS10/tubing hanger TH12 without the BOP adaptor being secured thereto for interface with a traditional approach open-sea completion/intervention riser. A tree running tool TRT secures a Lower Workover Riser Package (LWRP) and emergency disconnect package EDP to xmas tree 150. Because of the flexibility afforded by the BOP adaptor, there are few limitations as to the intervention configuration scenarios.

Summary of Advantageous Features For The Slimbore Completion System

[0047]

(1) The arrangement of a tubing spool TS5 - tubing hanger TH5 of Figures 5A and 5B enables use of a slimbore BOP 120 and slimbore marine riser 124 to minimize riser fluid requirements. As a result, less volume of fluids is required, which results in less storage required, less weight to be handled, more available vessel deck space and load capacity for other needs. Alternatively, it provides the capability to reduce required vessel size to carry out desired operations, etc. - all contributing to lower cost to the field operator.

(2) The tubing hanger TH5/tubing spool TS5 arrangement of the invention accommodates a relatively large number of electric (E) and hydraulic (H)

controls conduits through a very small diameter tubing hanger, which in turn matches the small diameter limitations of the slimbore riser system. The relatively large number of conduits satisfies both current and perceived future (expanded) requirements of "smart wells".

(3) Because of the vertical orientation of the control conduits 18 of tubing hanger TH5, downhole functions can be monitored for integrity throughout the installation process. This arrangement allows any damage related failures to be quickly and efficiently rectified as soon as they occur, a requirement for "smart well" applications. Because the xmas tree 150 is installed on top of the tubing hanger TH12 following its installation in tubing spool TS10, the same control interfaces used during the tubing hanger installation operation can be accessed for production mode (tree) requirements. As a result, there are fewer potential failure points as compared to traditional horizontal xmas tree HXT designs, providing comparable functionality.

(4) The BOP adaptor 152 arrangement of the invention facilitates interface of both slimbore (11" (279mm) or 13-5/8" (346mm) bore) BOP stacks 120 and LMRPs 122, and conventional (18-3/4" (476mm)) BOP stacks 160 and LWRPs 170 with the top of the xmas tree, while also eliminating the requirement to provide a large (typically 18-3/4" (476mm) nominal configuration) re-entry profile at the top of the xmas tree. The BOP adaptor 152 removes the interface problems normally associated with providing enough space to accept a "BOP stack of convenience", particularly for guidelineless (GLL) applications. An 18-3/4" (476mm) (typical) top interface on a xmas tree would result in a substantial increase in the footprint (and therefore weight, handling difficulties, etc.) of the tree (especially for GLL applications), if the traditional requirement were imposed that control modules and choke trim/actuator modules, etc., be vertically retrievable by GLL means.

(5) The tubing hanger TH5 is characterized by a concentric production bore (no annulus conduit therethrough) and by concentrically arranged conventional vertically-oriented electric (E) and hydraulic (H) couplers for interfacing control functions. Should circumstances dictate (such as the desire to provide multiple completion strings or special/non-conventional profile E/H conduit connectors), the tubing hanger characteristics described above could be altered. Because the annulus conduit is not routed through the tubing hanger TH5, several modifications of the routing of the E and H conduits and/or their couplers may be made. So long as the annulus conduit is not routed through the TH, such

modifications should be considered to be anticipated by the subject invention.

(6) The tubing hanger TH5/Tubing Spool TS5 arrangement of the invention represents a hybrid of the conventional (vertical bore) tree and horizontal tree completion systems.

(7) The subsea arrangement described above allows use of more or less conventional vertical dual bore or "monobore" xmas trees which have size and weight advantages compared with horizontal xmas trees, especially for guidelineless applications. The enhanced design features such as an ROV deployed tree cap (see tree cap 158 of Figure 16) and optimized installation procedures give these slimbore "conventional" trees further advantages in comparison to HXT designs. For example, a conventional xmas tree can be "intervened" using a simpler tooling package deployed from a lower cost vessel.

(8) The BOP adaptor depicted in Figures 13, 14 and 14A provides the capability to use the BOP stack/marine riser and completion landing string (based on standard tubing) in both the tubing hanger interface mode of Figure 12 and the xmas tree interface mode of Figures 14, 14A and 14B. This capability removes the requirement to retrieve the BOP stack 120 (or the larger BOP stack 160, if used) to permit installation of the xmas tree using a dedicated open-sea completion/intervention (C/I) riser. On the other hand, the system also retains the ability to interface a conventional C/I riser, should this be desired (see Figure 18). The flexibility of the latter feature (allowing lower cost interventions), combined with the cost savings of the first feature (trip time savings plus Capital Expense (CAPEX) savings are key advantages of the BOP adaptor 152 of the invention.

(9) The tubing hanger/tubing spool arrangement of Figures 5A and 5B incorporates a tubing spool to accept the tubing hanger and in which a conduit is provided for annulus communication "around", rather than "through" the tubing hanger. This feature enables a substantial size reduction for the tubing hanger. The annulus "bypass" conduit A5 is routed past one or more (but typically one) remotely operable (actuated or manual/ROV operated, etc.) valves VA5, VA6 incorporated either integral to the TS body or unitized thereto. This valve VA5 (for example) provides closure capability for the annulus conduit that does not require wireline trips for operation. This results in cost savings and reliability improvement from many perspectives - not least of which is that it permits use of a true monobore riser (that is, no "diverter" required, simple tubing possibly acceptable, etc.). In the tubing hanger interven-

tion modes, annulus communication is achieved in cooperation with the BOP stack choke and kill conduits, without the requirement for incorporating special rams in the BOP or relying on the annular blow out preventers for high pressure sealing. In the xmas tree intervention mode, annulus communication is achieved in the same manner (unless a dedicated traditional type open-sea completion/intervention riser is employed), although in this mode there will be a xmas tree 150 placed between the tubing spool TS10 and BOP stack 120, 160 (see Figures 14A, 14B and 17). The xmas tree 150 provides an annulus flow conduit from its bottom surface to its upper re-entry profile (via one or more valves), not shown, integral to the xmas tree block or unitized to the side thereof. See conduit 200 in xmas tree 150 and associated conduit 202 of BOP adaptor 152 in Figures 13, 14, 14A, 17 and 18. The annulus bypass conduit A12 around the tubing hanger is contained completely within the tubing spool TS10, as opposed to the xmas tree body as is the case horizontal xmas tree designs. All benefits normally associated with tubing spools are incorporated in the arrangement of the invention.

(10) Special handling operations as depicted in Figures 12, 12A, 13, 14, 14A and 14B can save BOP stack /marine riser, and completion riser trips between the sea floor and the surface, in comparison to conventional operations.

[0048] While preferred embodiments of the present invention have been illustrated and/or described in some detail, modifications and adaptations of the preferred embodiments will occur to those skilled in the art. Such modifications and adaptations are within the scope of the present invention.

Claims

1. A subsea well completion apparatus comprising,
 - a blow out preventer (BOP) adapter (152) having a main body having top and bottom ends, said bottom end arranged and designed for connection to a standard xmas tree (150) re-entry hub (151),
 - said top end having a top profile (302) suitable for interfacing with 18¾" (476 mm) nominal bore configuration drilling or completion equipment.
2. The subsea apparatus of claim 1, wherein,
 - said re-entry hub (151) is substantially smaller than an 18¾" (476 mm) nominal bore configuration profile.

3. The subsea apparatus of claim 1, wherein,
said re-entry hub (151) is a 13⁵/₈" (346 mm)
clamp hub.
4. The subsea apparatus of claim 1, further compris- 5
ing,
a slimbore BOP stack (120,160) fastened to
said top profile (302) at said top end, where slim-
bore is defined as a substantially smaller diameter
than a standard bore of an 18³/₄" (476 mm) BOP 10
stack.
5. The subsea apparatus of claim 1, further compris-
ing,
a standard 18³/₄" (476 mm) BOP stack fas- 15
tened to said top profile (302) at said top end.
6. The subsea apparatus of claim 1, further compris-
ing,
a slimbore lower marine riser package (122) 20
fastened to said top profile (302) at said top end,
where slimbore is defined as a substantially smaller
diameter than a standard bore of an 18³/₄" (476 mm)
BOP stack, 25
7. The subsea apparatus of claim 1, further compris-
ing,
a standard lower marine riser package (122)
fastened to said top profile (302) at said top end. 30
8. The subsea apparatus of any one of claims 1 to 7,
further comprising,
a standard xmas tree (CXT, 150) connected
to said bottom end of said BOP adapter (152). 35
9. The subsea apparatus of any one of claims 1 to 8,
wherein,
said top end of said main body includes an
internal profile arranged and designed to receive a
tubing hanger running tool (THRT). 40
10. The subsea apparatus of claim 8, further compris-
ing,
a tubing spool (TS) having a top end connected 45
to a bottom end of said xmas tree (CXT,150),
said tubing spool having a tubing spool internal
profile which is arranged and designed to re-
ceive a tubing hanger (TH) and running tool
(THRT) through a previously connected BOP 50
stack (120,160), said tubing spool profile defin-
ing a tubing hanger and running tool depth in
said spool with respect to said BOP stack when
said tubing hanger running tool lands a tubing
hanger in said spool, 55
said top end of said main body of said BOP
adapter (152) including a BOP adapter internal
profile which is arranged and designed to have

a same running tool depth with respect to said
BOP stack when connected to said top end of
said BOP adapter as said tubing hanger and
said running tool depth.

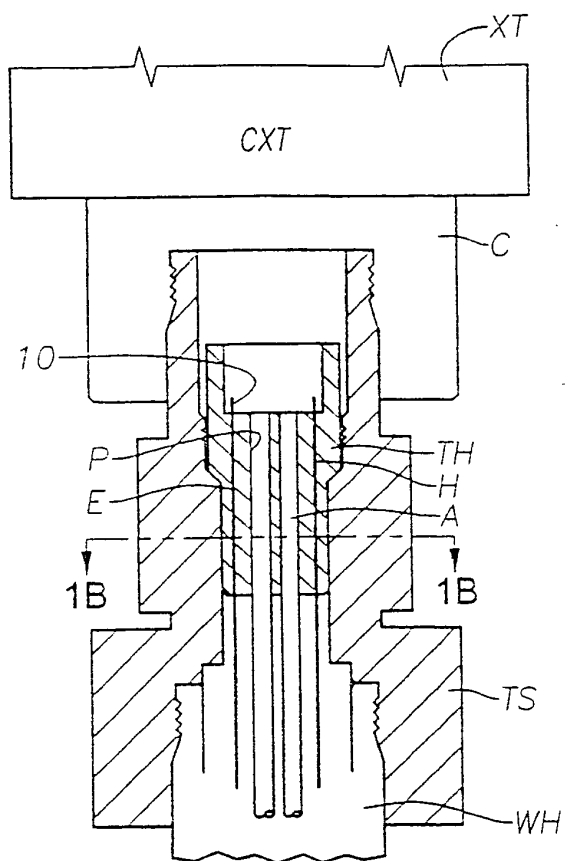


Fig. 1A

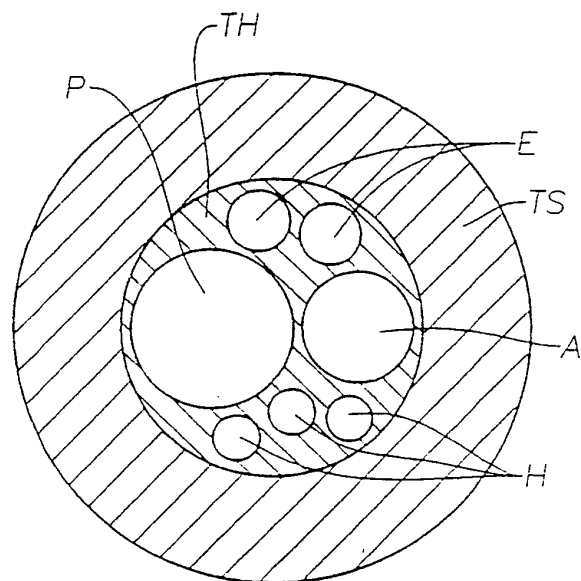


Fig. 1B

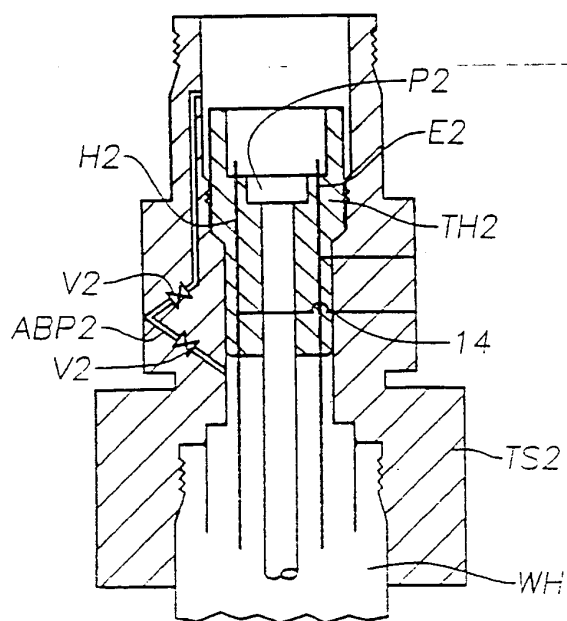


Fig. 2

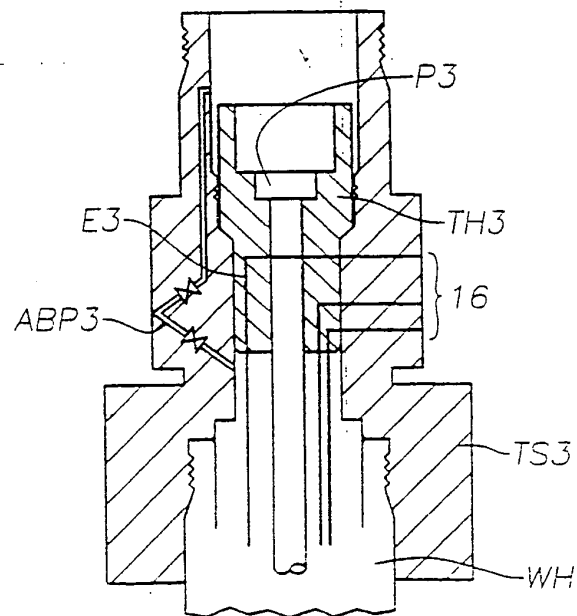


Fig. 3

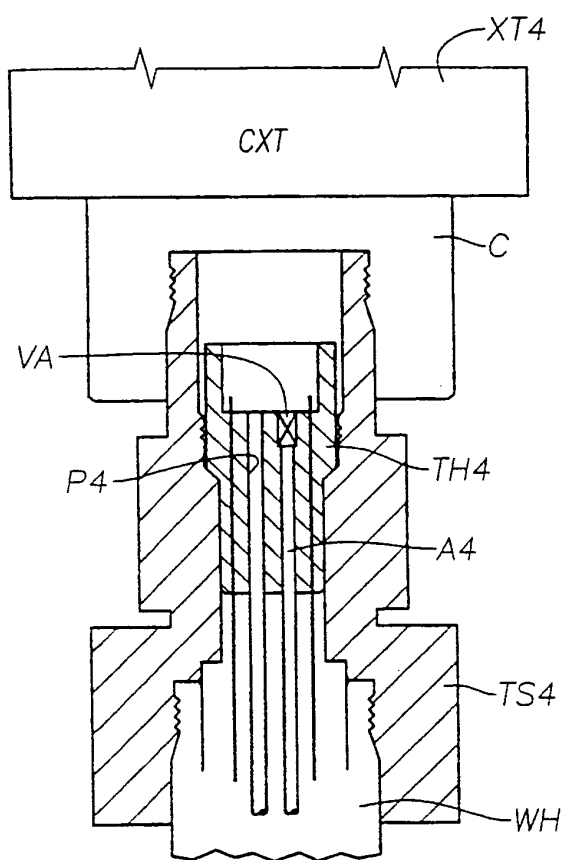


Fig. 4

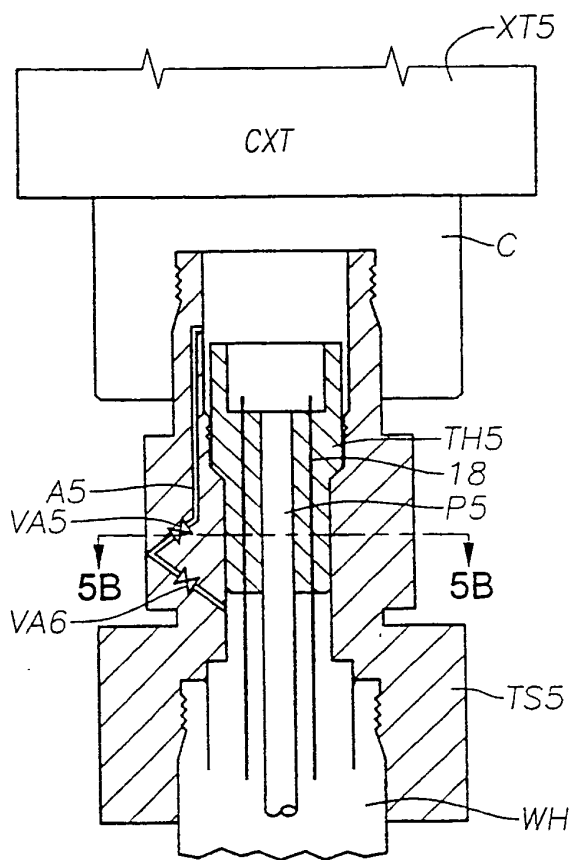


Fig. 5A

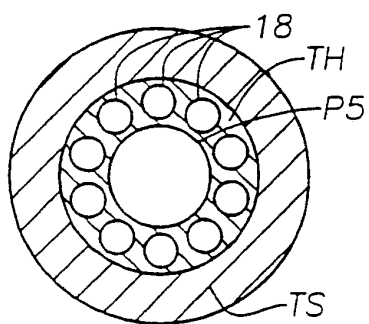


Fig. 5B

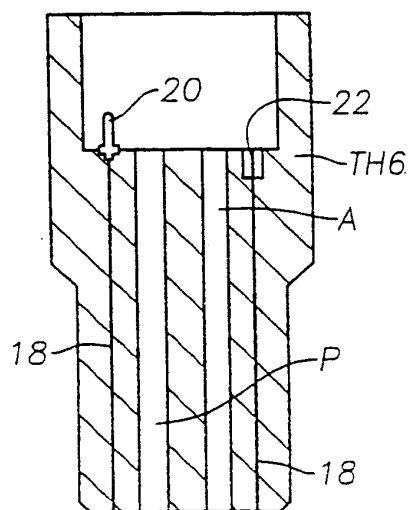


Fig. 6
(PRIOR ART)

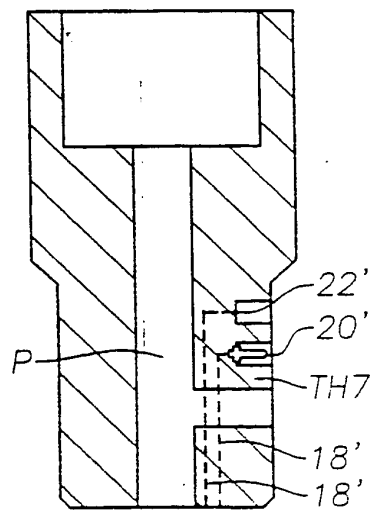


Fig. 7
(PRIOR ART)

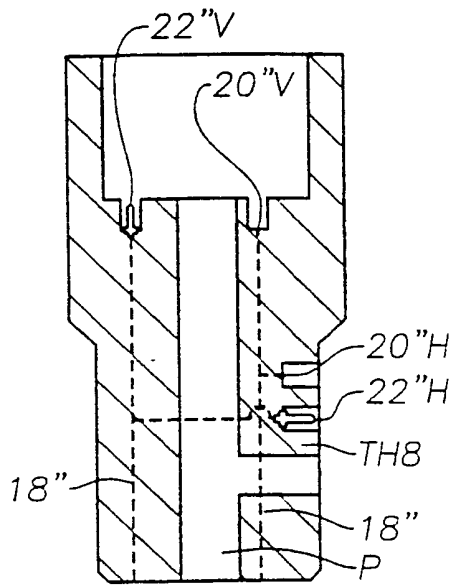


Fig. 8
(PRIOR ART)

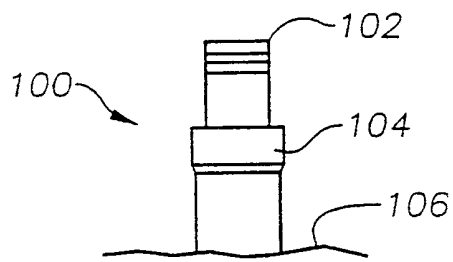


Fig. 9

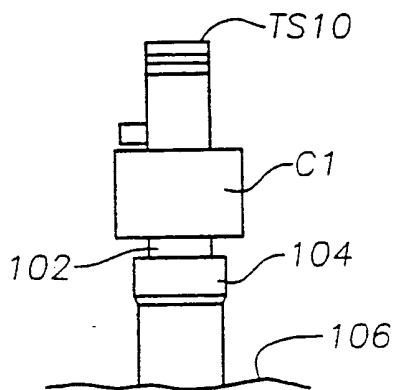


Fig. 10

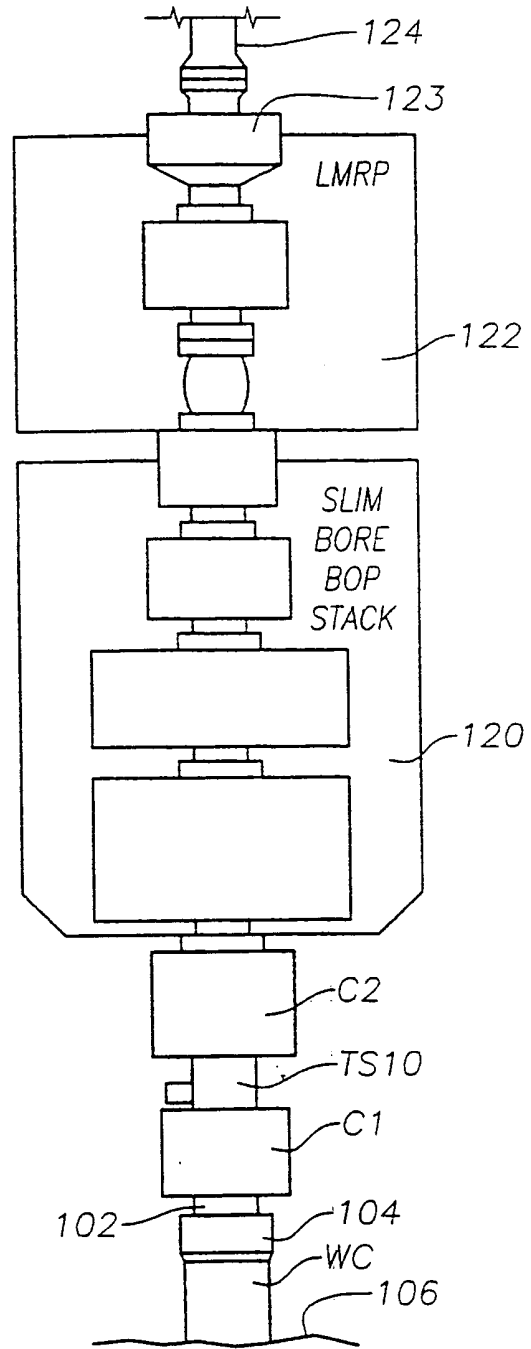


Fig. 11

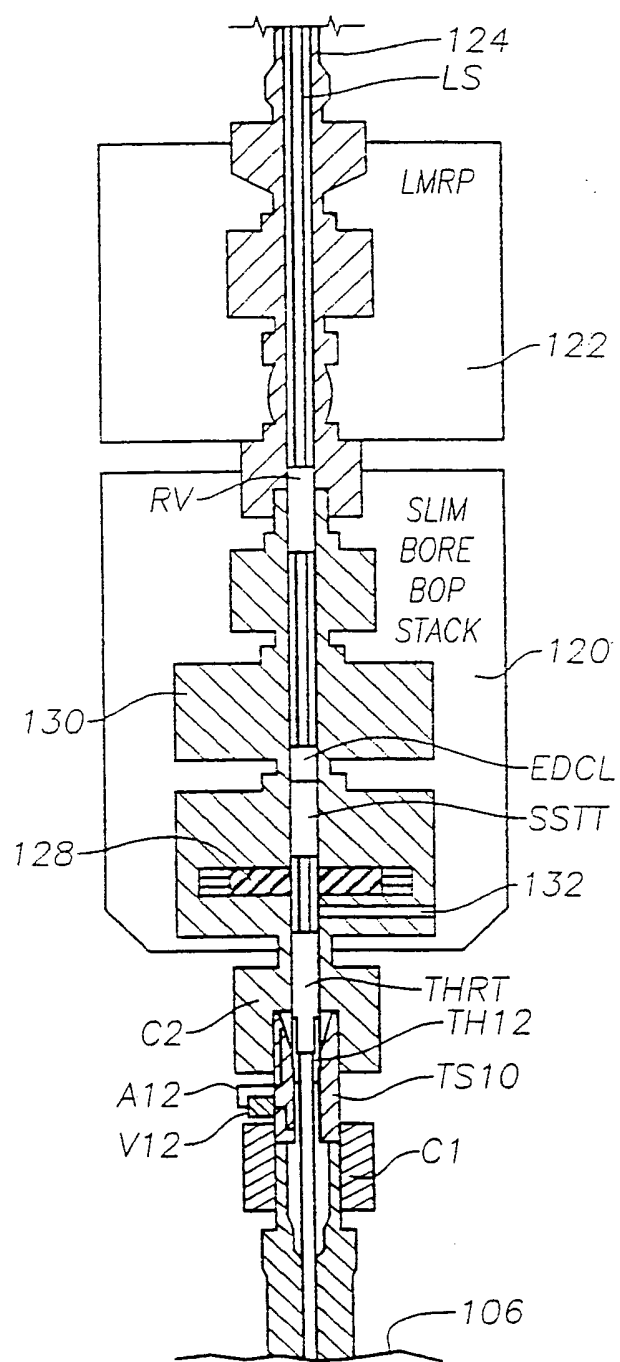


Fig. 12

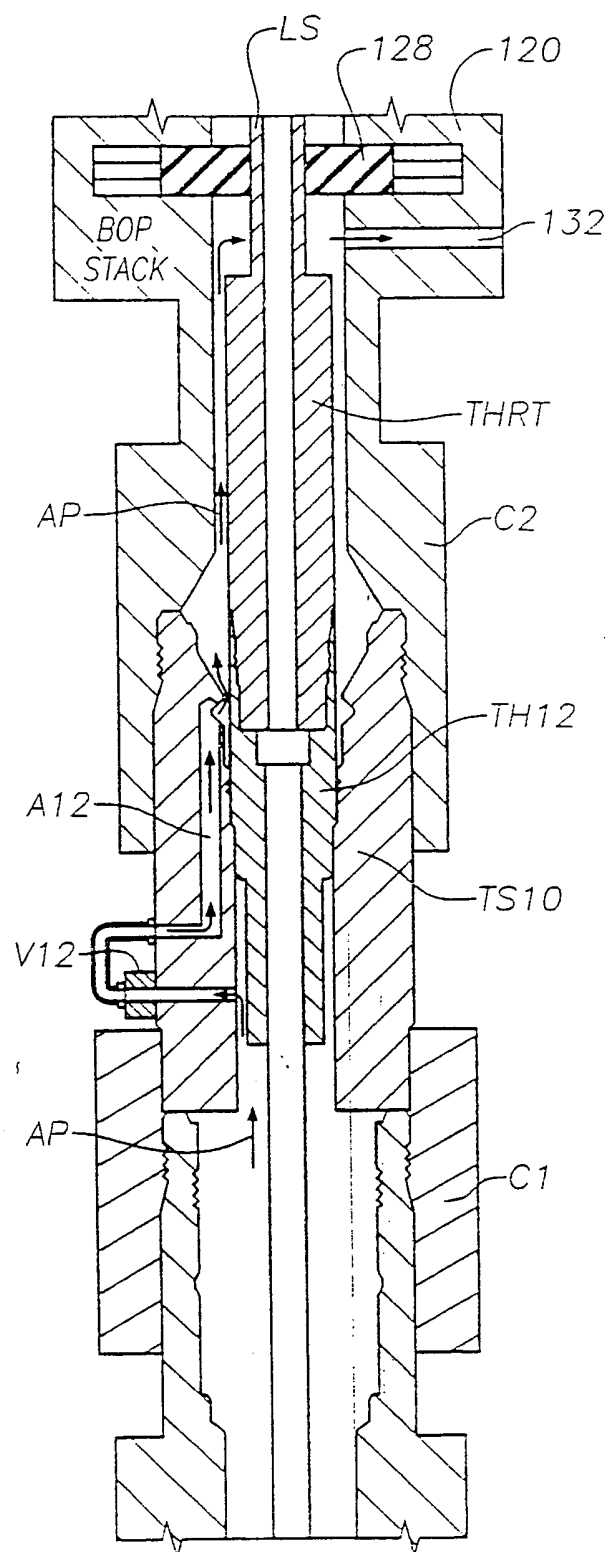


Fig. 12A

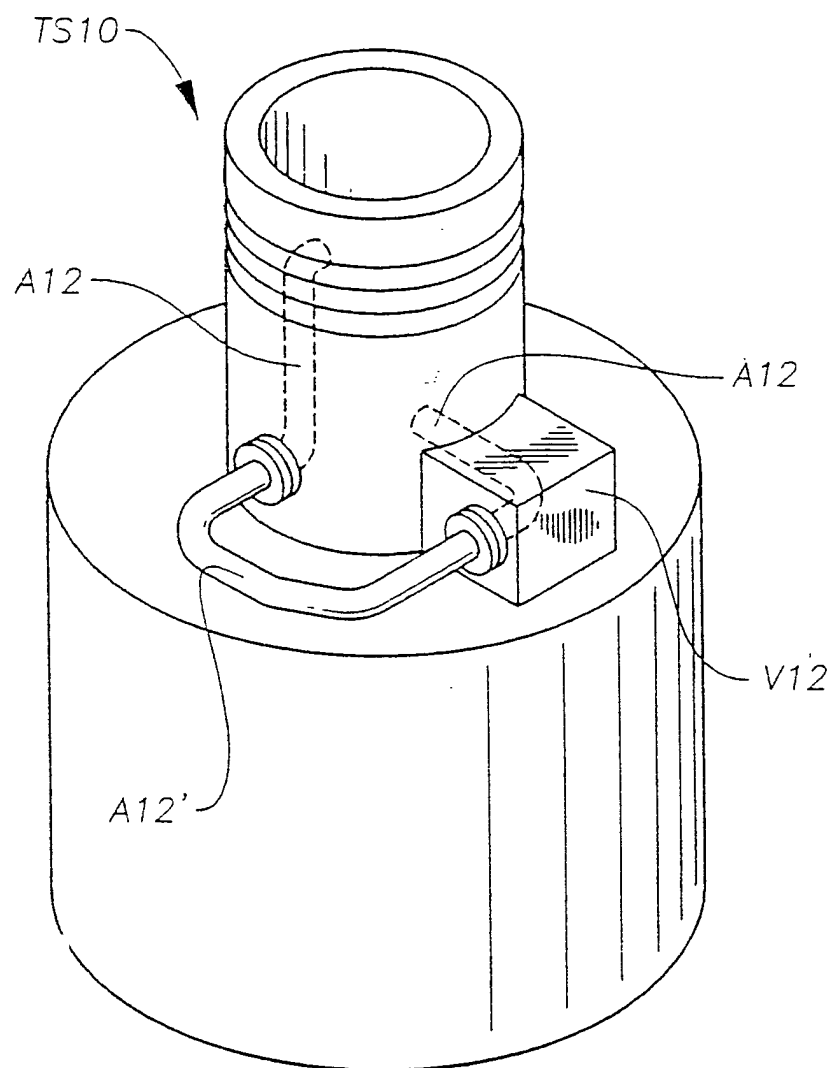


Fig. 12B

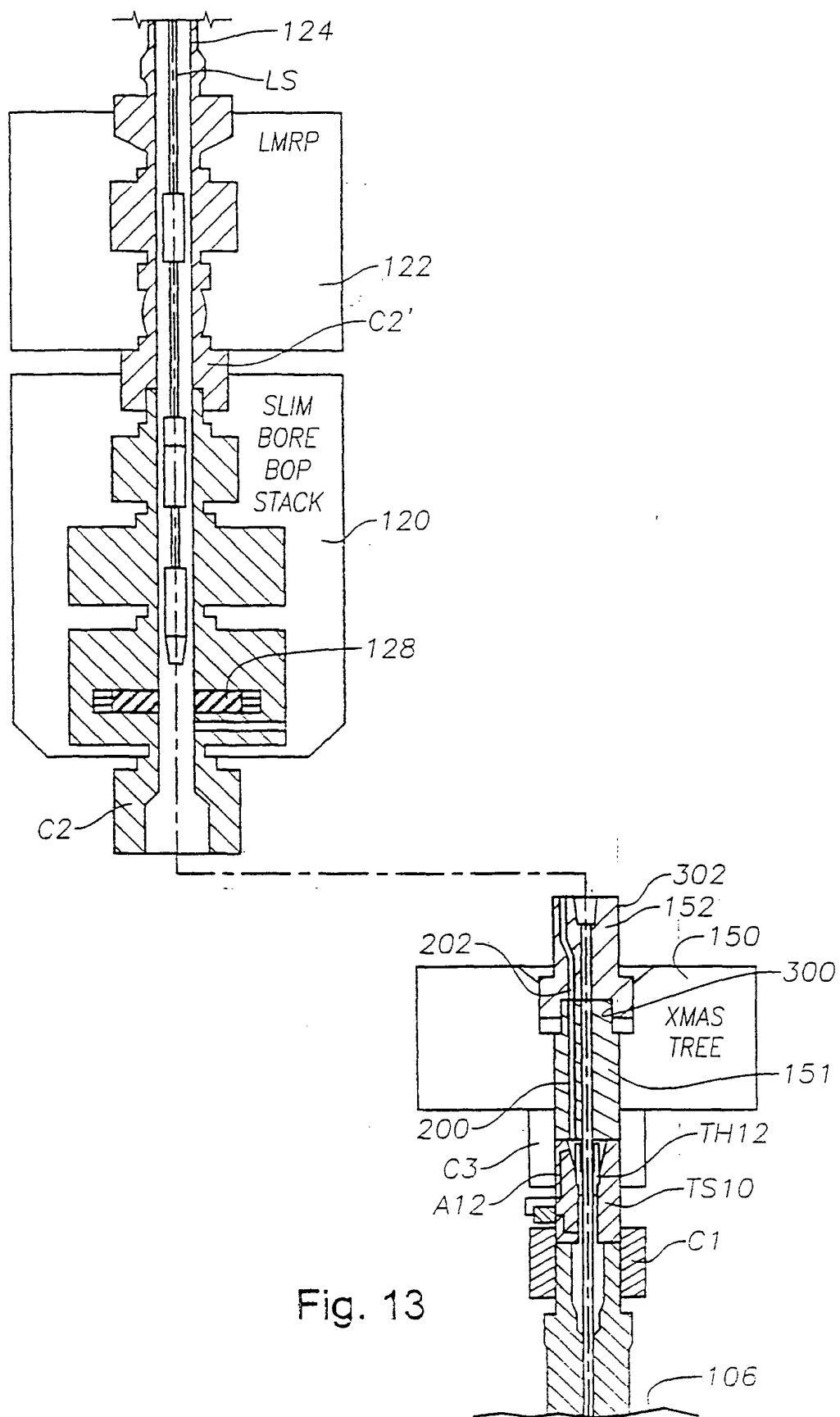


Fig. 13

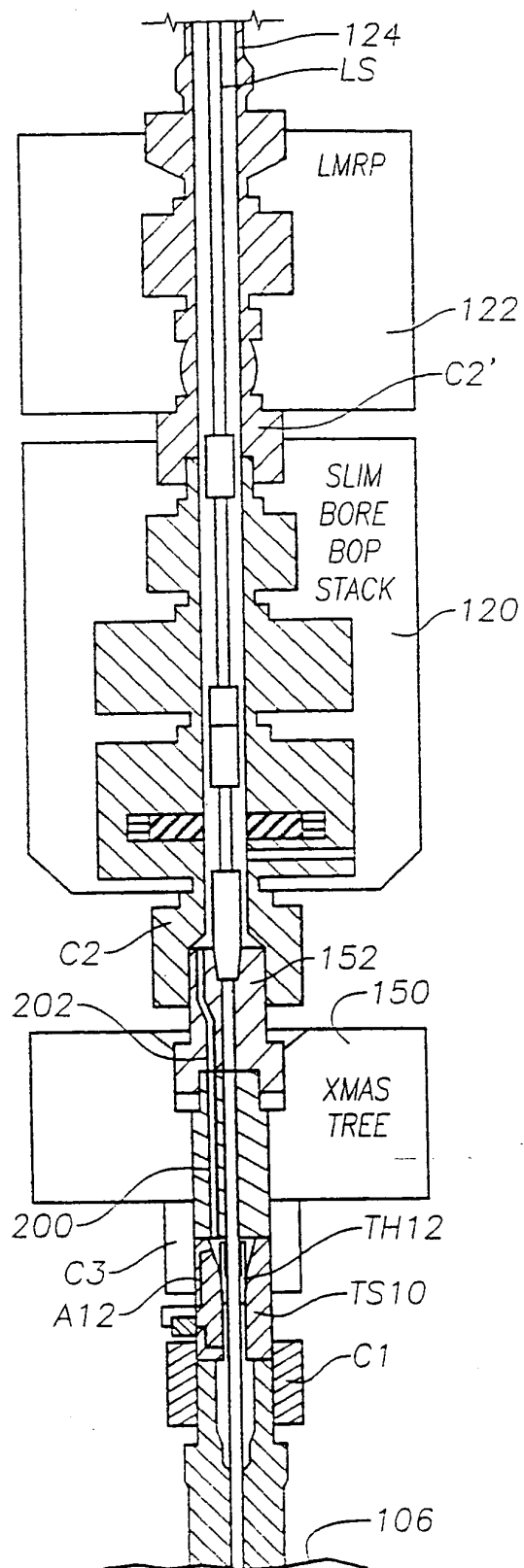


Fig. 14

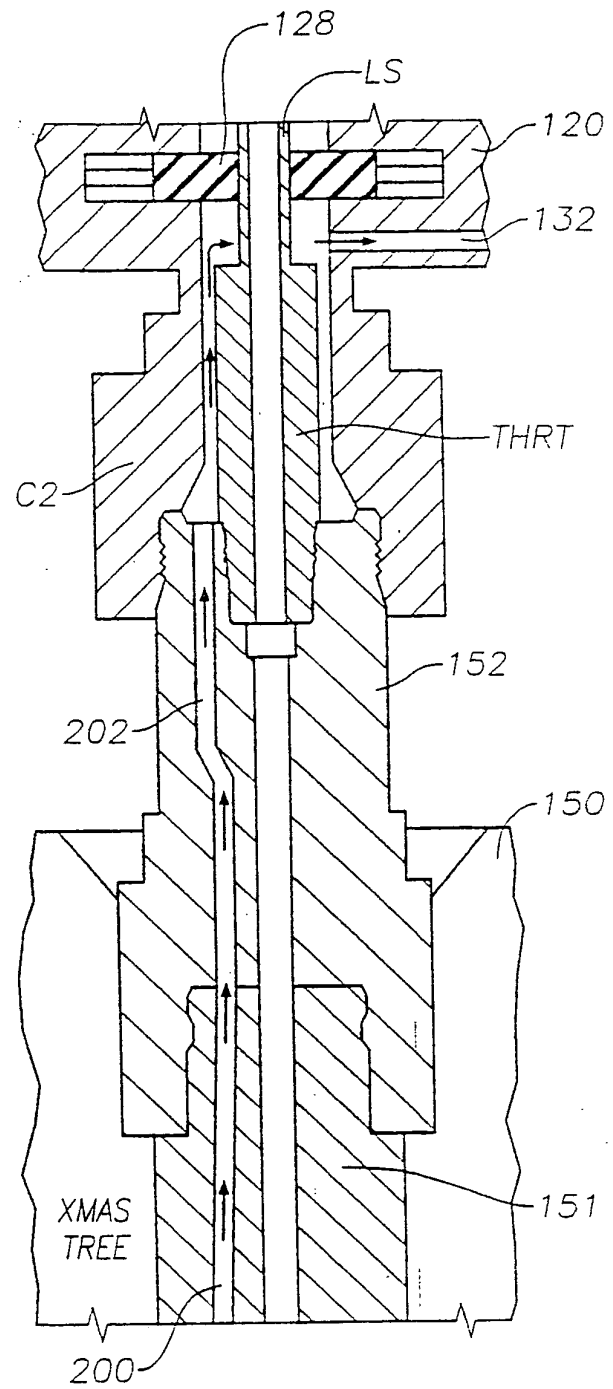


Fig. 14A

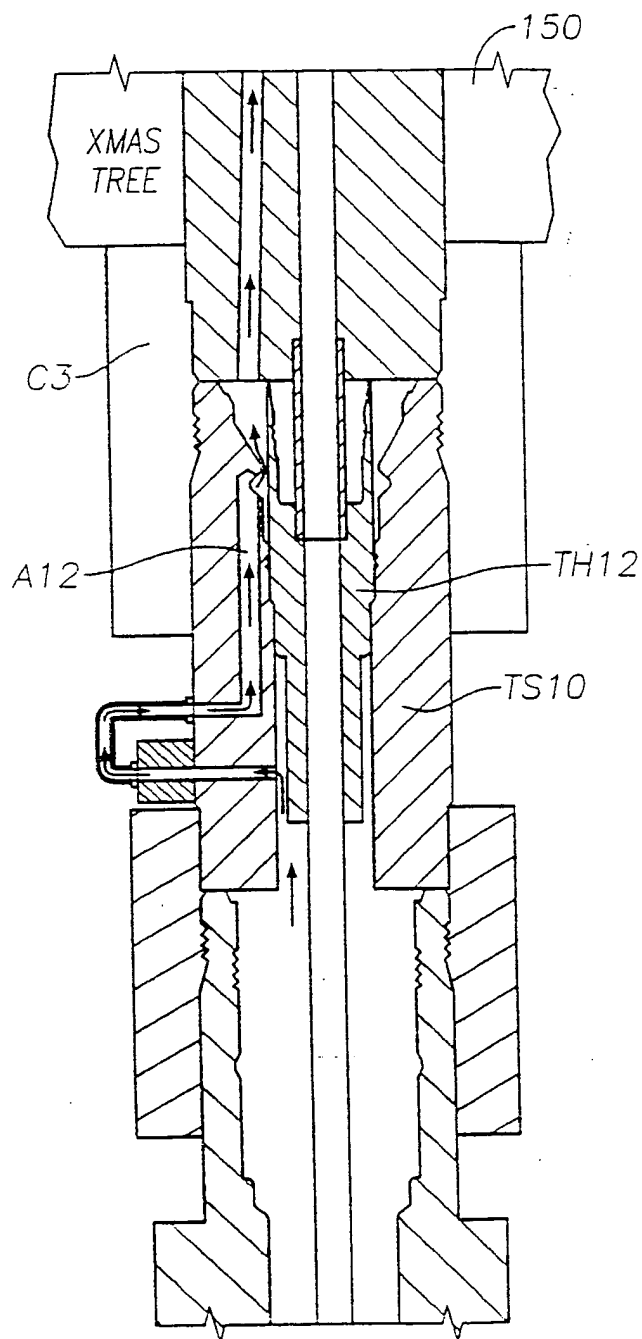


Fig. 14B

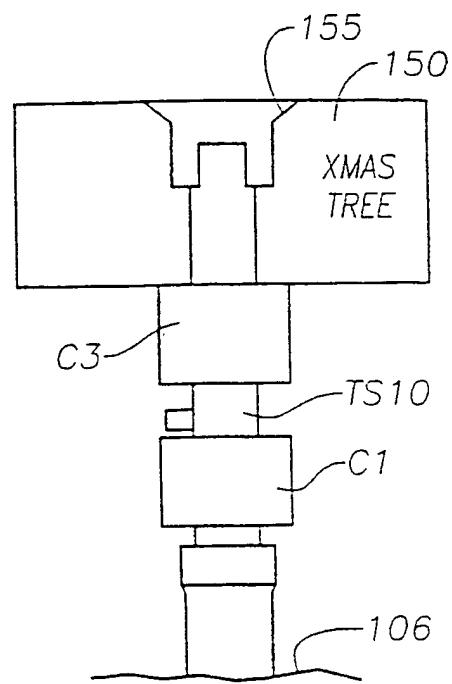


Fig. 15

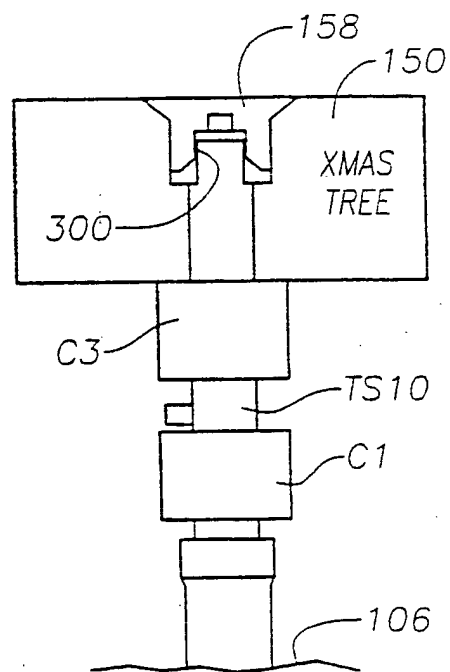


Fig. 16

