



(11)

EP 1 669 697 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
14.06.2006 Bulletin 2006/24

(51) Int Cl.:
F25B 25/00 (2006.01) F25B 9/00 (2006.01)

(21) Application number: **04257654.6**

(22) Date of filing: **09.12.2004**

(84) Designated Contracting States:
**AT BE BG CH CY CZ DE DK EE ES FI FR GB GR
HU IE IS IT LI LT LU MC NL PL PT RO SE SI SK TR**
Designated Extension States:
AL BA HR LV MK YU

(72) Inventor: **Nacer, Achaichia**
1429 Luxembourg (LU)

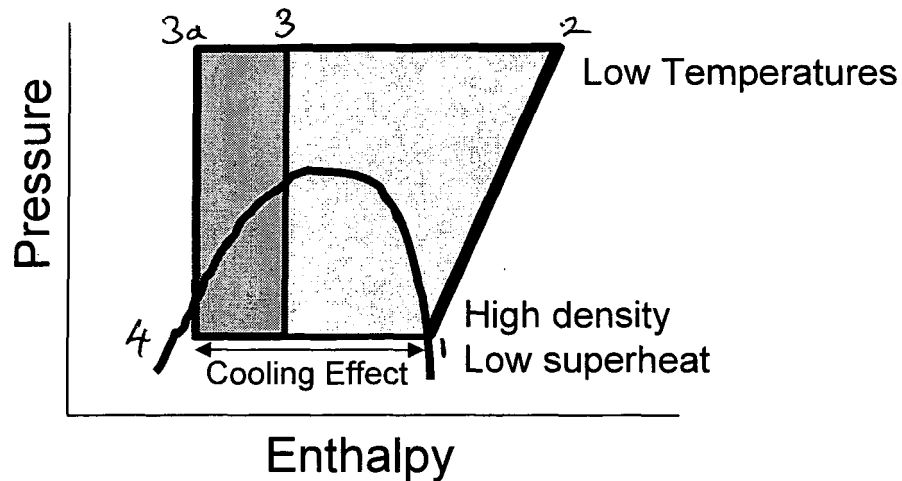
(74) Representative: **Waller, Stephen et al**
Murgitroyd & Company,
165-169 Scotland Street
Glasgow G5 8PL (GB)

(71) Applicant: **Delphi Technologies, Inc.**
Troy, MI 48007 (US)

(54) Thermoelectrically enhanced CO₂ cycle

(57) Figure 1c illustrates a vapour compression cycle according to the present invention wherein a thermoelectric device is used to sub-cool the refrigerant exiting the gas cooler from point 3a to point 3, thus increasing the cooling effect of the evaporator/heat exchanger be-

tween points 4 and 1 without the detrimental increase in the temperature of the refrigerant at the suction inlet of the compressor that occurs in known systems through the use of an internal heat exchanger. The thermoelectric device may be provided at the outlet of the gas cooler or may be incorporated into the gas cooler.



c) CO₂ Cycle with thermoelectric sub-cooling

Fig.-1- Transcritical Cycles

Description

[0001] The present invention relates to a refrigeration system for an air conditioner and to an improved transcritical vapour compression cycle and in particular to a refrigeration system and cycle using carbon dioxide as the refrigerant.

[0002] Carbon dioxide refrigerant is being considered as a replacement refrigerant for use by the automotive industry for air conditioning, as well as in other applications, mainly due to the low toxicity of such refrigerant. However, carbon dioxide based systems have many challenges resulting from the fact that such systems operates in transcritical mode leading to high pressures and high compressor outlet temperatures. Other challenges are the low critical temperature and the shape of the isotherms around the critical point. The performance of the gas cooler is therefore limited by the ambient air temperature.

[0003] In order to improve the performance of such carbon dioxide systems it is important to have additional cooling at the exit from the gas cooler. This is usually achieved in the prior art through an internal heat exchanger, where cold refrigerant at exit from the evaporator is used to further cool down the refrigerant leaving the gas cooler. This method, although achieving the goal of improving the cooling capacity, has the drawback that it will increase drastically the amount of superheat going into the compressor and therefore results in lower refrigerant density at the compressor suction inlet and higher compressor outlet temperature, which can shorten the life of the compressor and require the gas cooler to be made from special heat resistant materials.

[0004] The object of the present invention is to avoid the need to have high superheat and high compressor outlet temperature whilst improving the efficiency and performance of the system.

[0005] According to the present invention there is provided a refrigeration system for an air conditioner comprising a compressor for compressing a refrigerant, a gas cooler downstream of the compressor for cooling the refrigerant, an expansion valve downstream of the gas cooler for reducing the pressure of the refrigerant and a heat exchanger or evaporator downstream of the expansion valve for evaporating the refrigerant, characterised by the provision of thermoelectric means for reducing the temperature of the refrigerant at the inlet of the expansion valve.

[0006] Preferably the refrigerant is carbon dioxide.

[0007] In one embodiment the thermoelectric means may be provided at or adjacent the outlet of the gas cooler. In an alternative embodiment the thermoelectric means be incorporated within the gas cooler to cool the refrigerant at the outlet of the gas cooler.

[0008] According to a further aspect of the present invention there is provided a transcritical vapour compression cycle for carbon dioxide refrigerant comprising the steps of compressing a superheated refrigerant to in-

crease the temperature, pressure and enthalpy of the refrigerant into the supercritical region, cooling the refrigerant in a gas cooler at a substantially constant pressure, expanding the refrigerant through an expansion valve to a temperature and pressure below the critical values, evaporating the refrigerant in an evaporator/heat exchanger whereby the refrigerant absorbs heat from a cooled space, characterised by the further step using thermoelectric means to further cool the refrigerant exiting the gas cooler thereby reducing the temperature of the refrigerant at the inlet of the expansion valve.

[0009] Two embodiments of the present invention will now be described by way of example only, and with reference to the accompanying drawings in which:

Figure 1a is a pressure-enthalpy diagram of a typical transcritical vapour compression cycle using carbon dioxide as a refrigerant without the use of an internal heat exchanger;

Figure 1b is a pressure-enthalpy diagram of a typical transcritical vapour compression cycle using carbon dioxide as a refrigerant, the cycle including an internal heat exchanger, to improve system performance;

Figure 1c is a pressure-enthalpy diagram of a vapour compression cycle according to the present invention;

Figure 2a is a schematic view of a gas cooler and thermoelectric sub-cooler according to a first embodiment of the present invention;

Figure 2b is a schematic view of a gas cooler and thermoelectric sub-cooler according to a second embodiment of the present invention.

[0010] Figure 1a illustrates a typical transcritical vapour compression cycle for carbon dioxide. Carbon dioxide vapour enters a compressor at point 1. The compressor compresses the vapour whereby its pressure, temperature and enthalpy are increased, using power from a vehicle engine in the case of a vehicle air conditioning system, until it leaves the compressor at point 2 located in the supercritical region. Next the carbon dioxide refrigerant enters a gas cooler, usually water or air cooled, whose function is to transfer heat from the fluid to a coolant (for example air or water) to cool the refrigerant at a constant pressure. The cooled refrigerant leaves the gas cooler at point 3. The refrigerant then undergoes a substantially constant enthalpy expansion process through an expansion valve to reach point 4 in the mixed liquid-vapour region. Finally the refrigerant is vapourised in an evaporator/heat exchanger whereby it absorbs heat from a space to be cooled, for example the vehicle cabin in a vehicle air conditioning system until it enters the compressor again at point 1 and repeats the cycle. The cooling effect of the cycle is represented by

the line between points 4 and 1.

[0011] As can be seen from Figure 1a, the cooling effect could be increased by further reducing the temperature/enthalpy of the refrigerant in the gas cooler to move point 3 further to the left.

[0012] Figure 1b illustrates a typical vapour compression cycle for carbon dioxide refrigerant using internal heat exchange to further cool the supercritical refrigerant at the outlet of the gas cooler using refrigerant from the outlet of the evaporator/heat exchanger. The internal heat exchanger cools the refrigerant between points 3a and 3, this heat being transferred to the refrigerant between points 4a and 1 downstream of the compressor.

[0013] The heat removed from the refrigerant at the outlet of the gas cooler by the internal heat exchanger provides an increased cooling effect but since such heat is transferred to the refrigerant at the outlet of the evaporator/heat exchanger, this increases the temperature of the refrigerant and reduces its density at the suction inlet of the compressor, further increasing the temperature of the refrigerant at the outlet of the compressor at point 2. This has an impact on the compressor durability, lubrication characteristics and gas cooler material selection. Analysis of the cycle performance characteristics will show an operating condition point at which the system, operates at optimum cycle efficiency. Away from this point the system efficiency deteriorates.

[0014] Figure 1c illustrates a vapour compression cycle according to the present invention wherein a thermoelectric device is used to sub-cool the refrigerant exiting the gas cooler from point 3a to point 3, thus increasing the cooling effect of the evaporator/heat exchanger between points 4 and 1 without the detrimental increase in the temperature of the refrigerant at the suction inlet of the compressor that occurs in known systems through the use of an internal heat exchanger.

[0015] Thermoelectric cooling devices utilise semiconductor materials to remove heat through the use of electrical energy by the Peltier effect, the theory that there is a heating or cooling effect when electric current passes through two conductors. A voltage applied to the free ends of two dissimilar materials creates a temperature difference. With this temperature difference, Peltier cooling will cause heat to move from one end to the other. A typical thermoelectric cooler will consist of an array of p- and n- type semiconductor elements that act as the two dissimilar conductors. As an electric current passes through one or more pairs of elements, there is a decrease in temperature at the junction ("cold side") resulting in the absorption of heat from the environment. The heat is carried through the cooler by electron transport and released on the opposite ("hot") side as the electrons move from a high to low energy state.

[0016] In an automotive air conditioning system the electrical power for the thermoelectric device can be provided by the vehicle's electrical system, such as alternator and battery, or fuel cell system.

[0017] A first embodiment of the invention is shown in

Figure 2a, wherein a thermoelectric device is incorporated into the gas cooler to sub-cool the refrigerant at the exit thereof. The heat exchanger details are shown for information only and other geometrical and design concepts are envisaged.

[0018] A second embodiment of the invention is shown in Figure 2b, wherein the refrigerant passes through a separate thermoelectric sub-cooler downstream of the gas cooler.

[0019] A control device can be provided controlling the operation of the thermoelectric device to provide the level of cooling required to achieve a desired cooling effect or system performance, thus providing a simple and effective control arrangement for the air conditioning system.

[0020] Current transcritical carbon dioxide refrigerant cycles make use on an internal heat exchanger to improve system efficiency and cooling capacity, resulting in drawbacks in terms of excessive compressor outlet temperature and lower refrigerant density at the compressor inlet.

[0021] The present invention, through the use of thermoelectric means in order to cool down the refrigerant leaving the gas cooler, leads to lower compressor outlet temperature, lower refrigerant specific volume at suction point leading to much higher refrigerant mass flow rate and better volumetric efficiency. Furthermore, the use of thermoelectric cooling of the refrigerant enables the degree of refrigerant sub-cooling to be controlled to a desired amount depending on system parameters, ambient conditions, and refrigeration requirements. The present invention also provides improved compressor durability due to the lower temperature of the refrigerant and improved oil quality therein due to the more favourable operating conditions, and also eliminates the impact of high pressure and temperature on the choice of gas cooler material and strength. The present invention also offers the possibility to optimise the use of the thermoelectric element depending on system or performance needs, fan operation, and ambient condition.

Claims

1. A refrigeration system for an air conditioner comprising a compressor for compressing a refrigerant, a gas cooler downstream of the compressor for cooling the refrigerant, an expansion valve downstream of the gas cooler for reducing the pressure of the refrigerant and a heat exchanger or evaporator downstream of the expansion valve for evaporating the refrigerant, **characterised by** the provision of thermoelectric means for reducing the temperature of the refrigerant at the inlet of the expansion valve.
2. A refrigeration system as claimed in claim 1, wherein the refrigerant is carbon dioxide.
3. A refrigeration system as claimed in any preceding

claim, wherein the thermoelectric means is provided at or adjacent the outlet of the gas cooler.

4. A refrigeration system as claimed in claim 1 or claim 2, wherein the thermoelectric means is incorporated within the gas cooler to cool the refrigerant at the outlet of the gas cooler. 5
5. A refrigeration system as claimed in any preceding claim, wherein control means are provided for controlling the degree of cooling provided by the thermoelectric means to optimise the cooling effect depending on system or performance needs, gas cooler performance, and ambient conditions. 10
15
6. A transcritical vapour compression cycle for carbon dioxide refrigerant comprising the steps of compressing a superheated refrigerant to increase the temperature, pressure and enthalpy of the refrigerant into the supercritical region, cooling the refrigerant in a gas cooler at a substantially constant pressure, expanding the refrigerant through an expansion valve to a temperature and pressure below the critical values, evaporating the refrigerant in an evaporator/heat exchanger whereby the refrigerant absorbs heat from a cooled space, **characterised by** the further step using thermoelectric means to further cool the refrigerant exiting the gas cooler thereby reducing the temperature of the refrigerant at the inlet of the expansion valve. 20
25
30

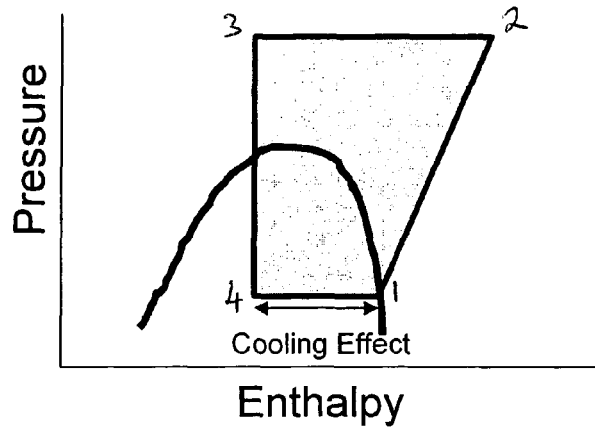
35

40

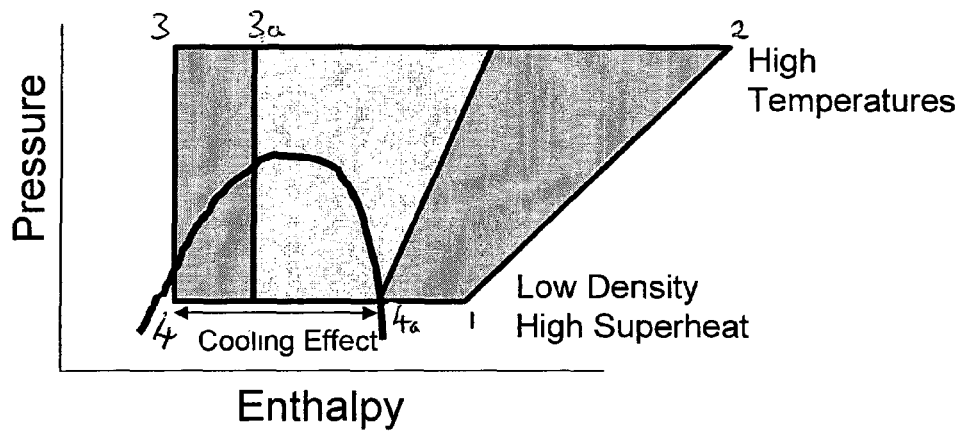
45

50

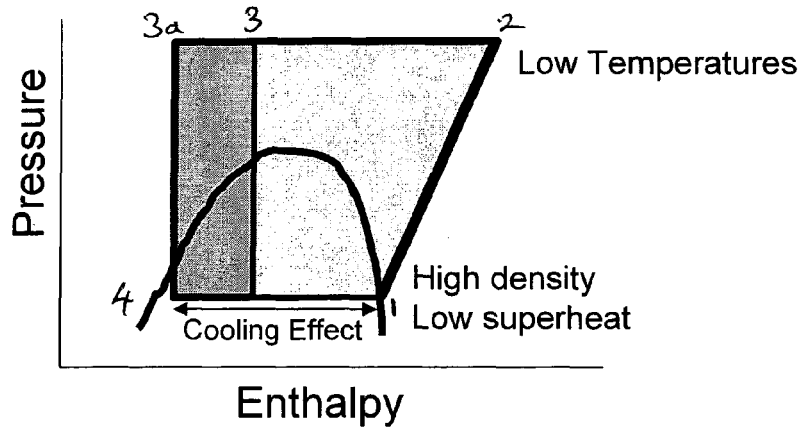
55



a) CO₂ Cycle without internal heat exchanger

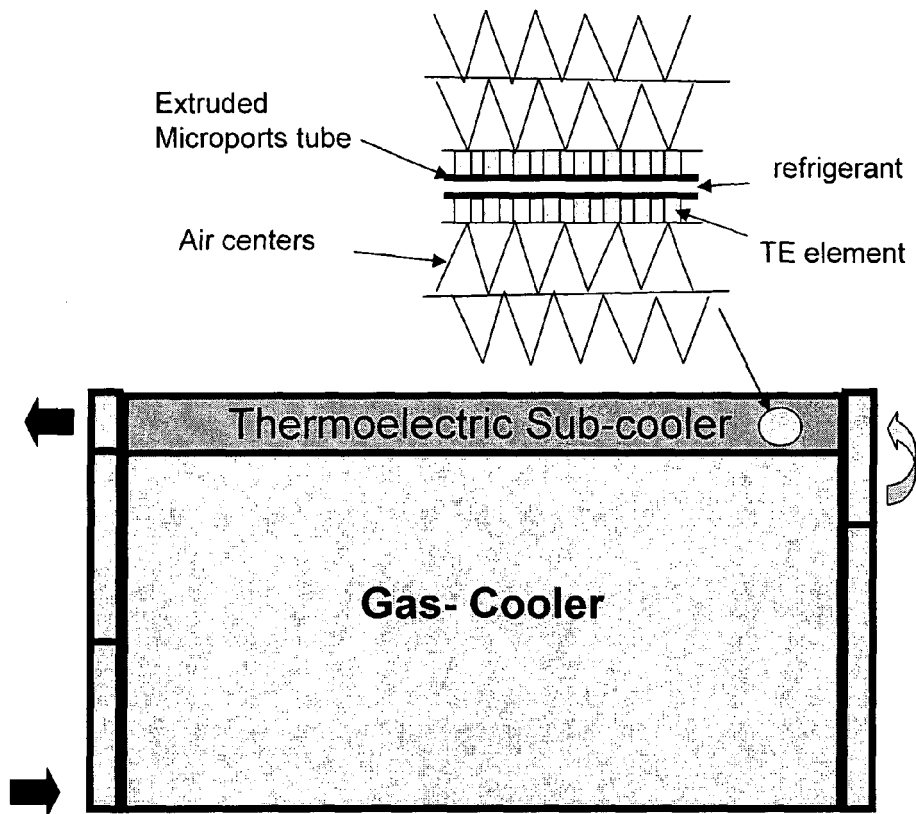


b) CO₂ Cycle with internal heat exchanger

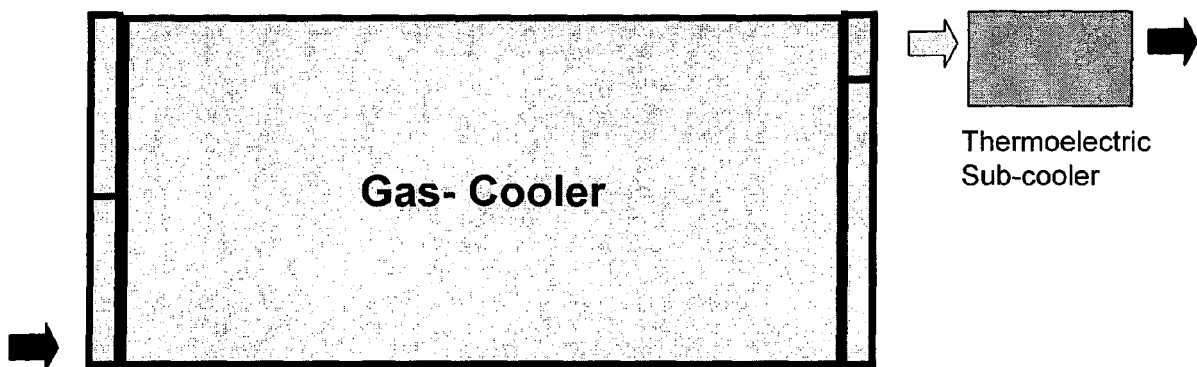


c) CO₂ Cycle with thermoelectric sub-cooling

Fig.-1- Transcritical Cycles



a) Sub-cooler integrated into the gas-cooler



b) Remote sub-cooler. Water or air cooled

Fig.-2- Thermoelectric Sub-cooling concepts



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 04 25 7654

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
X	PATENT ABSTRACTS OF JAPAN vol. 1998, no. 06, 30 April 1998 (1998-04-30) -& JP 10 035270 A (ZEXEL CORP), 10 February 1998 (1998-02-10) * the whole document *	1,3-5	F25B25/00 F25B9/00
Y	* the whole document *	2,6	
Y	DE 100 60 114 A1 (VALEO CLIMATISATION, LA VERRIERE) 13 June 2001 (2001-06-13) * the whole document *	2,6	
X	PATENT ABSTRACTS OF JAPAN vol. 2000, no. 14, 5 March 2001 (2001-03-05) -& JP 2000 329414 A (FUJITSU GENERAL LTD), 30 November 2000 (2000-11-30) * the whole document *	1-5	
X	US 6 351 950 B1 (DUNCAN GERALD DAVID) 5 March 2002 (2002-03-05) * the whole document *	1,3,5	
X	PATENT ABSTRACTS OF JAPAN vol. 1998, no. 06, 30 April 1998 (1998-04-30) -& JP 10 038409 A (MANDO MACH CO LTD), 13 February 1998 (1998-02-13) * the whole document *	1,3-5	TECHNICAL FIELDS SEARCHED (Int.Cl.7) F25B
X	US 5 361 587 A (HOFFMAN ET AL) 8 November 1994 (1994-11-08) * the whole document *	1,3-5	
X	US 3 266 258 A (ROSENFELD LEV MARKOVICH ET AL) 16 August 1966 (1966-08-16) * the whole document *	1	
		-/--	
The present search report has been drawn up for all claims			
Place of search The Hague		Date of completion of the search 27 April 2005	Examiner De Graaf, J.D.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

3
EPO FORM 1503 03.82 (P04C01)



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 04 25 7654

DOCUMENTS CONSIDERED TO BE RELEVANT				
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)	
A	PATENT ABSTRACTS OF JAPAN vol. 2003, no. 12, 5 December 2003 (2003-12-05) -& JP 2004 144399 A (MATSUSHITA ELECTRIC IND CO LTD), 20 May 2004 (2004-05-20) * the whole document *	1,2,6		
A	HIRATA T ET AL: "IMPROVEMENT OF MOBILE AIR CONDITIONING SYSTEM FROM POINT OF GLOBAL WARMING PROBLEMS" IIR - GUSTAV LORENTZEN CONFERENCE ON NATURAL WORKING FLUIDS. PROCEEDINGS, 2 June 1998 (1998-06-02), pages 314-323, XP001169058 * the whole document *	6		
A	US 4 825 667 A (BENEDICT ET AL) 2 May 1989 (1989-05-02)			
A	PATENT ABSTRACTS OF JAPAN vol. 2000, no. 25, 12 April 2001 (2001-04-12) -& JP 2001 227840 A (DAIKIN IND LTD), 24 August 2001 (2001-08-24) * abstract *			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
A	STOCKHOLM MM J ET AL: "UTILISATION DE LA THERMOELECTRICITE DANS LE VEHICULE AUTOMOBILE PERSPECTIVES TECHNICO-ECONOMIQUES ACTUELLES" INGENIEURS DE L'AUTOMOBILE, RAIP. BOULOGNE, FR, no. 687, 1 March 1994 (1994-03-01), pages 10-11, XP000435028 ISSN: 0020-1200			
A	US 4 819 451 A (HINGST ET AL) 11 April 1989 (1989-04-11)			
The present search report has been drawn up for all claims				
Place of search The Hague		Date of completion of the search 27 April 2005	Examiner De Graaf, J.D.	
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document				

3
EPO FORM 1503 03/82 (P04C01)



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 04 25 7654

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
A	US 5 063 747 A (JONES ET AL) 12 November 1991 (1991-11-12) -----		
A	US 4 697 425 A (JONES ET AL) 6 October 1987 (1987-10-06) -----		
A	US 3 148 511 A (GABLE GERALD K) 15 September 1964 (1964-09-15) -----		
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
The present search report has been drawn up for all claims			
Place of search The Hague		Date of completion of the search 27 April 2005	Examiner De Graaf, J.D.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

3
EPO FORM 1503 03.82 (P04C01)

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 04 25 7654

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

27-04-2005

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
JP 10035270	A	10-02-1998	NONE	
DE 10060114	A1	13-06-2001	FR 2802291 A1 JP 2001191786 A	15-06-2001 17-07-2001
JP 2000329414	A	30-11-2000	NONE	
US 6351950	B1	05-03-2002	AU 9010598 A EP 1012514 A1 WO 9913277 A1	29-03-1999 28-06-2000 18-03-1999
JP 10038409	A	13-02-1998	KR 189334 B1	01-06-1999
US 5361587	A	08-11-1994	NONE	
US 3266258	A	16-08-1966	DE 1254652 B FR 1390899 A	23-11-1967 26-02-1965
JP 2004144399	A	20-05-2004	NONE	
US 4825667	A	02-05-1989	NONE	
JP 2001227840	A	24-08-2001	NONE	
US 4819451	A	11-04-1989	DE 3642683 A1 GB 2199399 A ,B	16-06-1988 06-07-1988
US 5063747	A	12-11-1991	NONE	
US 4697425	A	06-10-1987	NONE	
US 3148511	A	15-09-1964	NONE	