



(11)

EP 1 726 876 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:

29.11.2006 Bulletin 2006/48

(21) Application number: 05253289.2

(22) Date of filing: 27.05.2005

(51) Int Cl.:

F23G 5/05 (2006.01)

F23L 1/02 (2006.01)

F23N 3/00 (2006.01)

F23G 5/16 (2006.01)

F23L 9/02 (2006.01)

(84) Designated Contracting States:

AT BE BG CH CY CZ DE DK EE ES FI FR GB GR
HU IE IS IT LI LT LU MC NL PL PT RO SE SI SK TR

Designated Extension States:

AL BA HR LV MK YU

(71) Applicant: TAKUMA CO., LTD.

Kita-ku

Osaka (JP)

(72) Inventors:

• Kataoka, Shizuo

Amagasaki-shi

Hyogo (JP)

• Aso, Tomonori

Amagasaki-shi

Hyogo (JP)

• Akiyama, Jin

Amagasaki-shi

Hyogo (JP)

• Sameshima, Ryoji

Amagasaki-shi

Hyogo (JP)

(74) Representative: Faulkner, Thomas John et al

fJ Cleveland,

40-43 Chancery Lane

London WC2A 1JQ (GB)

(54) Improved method of combusting solid waste

(57) The present invention discloses a method of combusting waste (W) with a stoker-type waste incinerator (1), in which a significant reduction in discharging toxic matters and also substantial improvements in heat recovery have been achieved together with limited feeding of combustion air for efficient, combustion of waste (W).

More particularly, with the present method of combusting waste (W), adjustments can be made such that the volume of the primary combustion air (A1) becomes 0.8~1.0 as the air ratio, the volume of the secondary combustion air (A2) 0.3~0.4 as the air ratio and the total air volume less than 1.3 as the air ratio respectively. A reduction zone (B) of 0.8~1.0 as the air ratio in the combustion chamber is formed by drawing the re-circulating combustion gas (G') from the primary combustion chamber (7) in the zone where the burnout stoker (4c) is positioned with respect to the outside, and injecting the re-circulating combustion gas (G') into the combustion chamber on the upstream side of the feeding position of the secondary combustion air (A2). Furthermore, a combustion control system comprising a steady state control part (D) to combust the waste (W) in a steady, stable state and a fuzzy control part (E) to restore an abnormal combustion state of waste (W) to a steady, stable state can be incorporated.

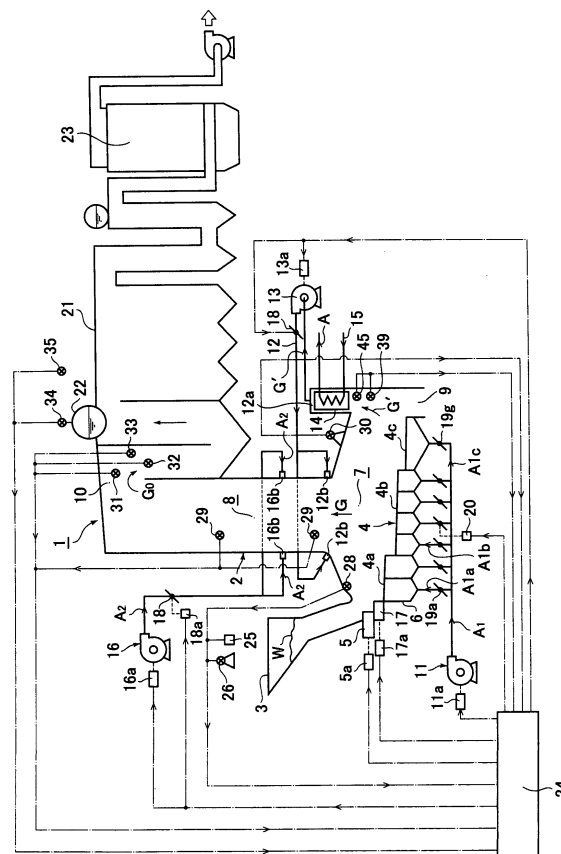


Fig. 1

Description

Field of the Invention

[0001] The present invention relates to improvements to a method of combusting municipal solid waste such as industrial waste, household solid waste and the like (hereinafter called waste) with a stoker-type waste incinerator. In particular, the present invention concerns improvements in such a method of combusting waste by using a stoker-type waste incinerator at a low air ratio. This enables the stoker-type waste incinerator to combust waste efficiently and perfectly whilst using a reduced amount of fed combustion air, to substantially reduce generation of toxic substances, to improve heat recovery efficiency, and to downsize the dimensions of both the stoker-type waste incinerator and exhaust gas treatment facilities.

Background of the Invention

[0002] In most instances, disposal of municipal solid waste is performed by combusting it with waste incinerators. Waste incinerators commonly used include either stoker-type waste incinerators or fluidized bed-type waste incinerators, with the stoker-type waste incinerator being the most popular type.

[0003] Figure 5 illustrates one example of a stoker-type waste incinerator. Said stoker-type waste incinerator 50 comprises a furnace 51, a waste hopper 52, a feeder pusher 53, a stoker 54, an under-stoker hopper 55, a primary combustion chamber 56, a secondary combustion chamber 57, a primary combustion air duct 58, a secondary combustion air duct 59, an ash discharge chute 60, an exhaust gas outlet 61 and the like. The stoker 54 consists of a drying stoker 54a, a combustion stoker 54b and a burnout stoker 54c, to feed the primary combustion air A1 from underneath the stoker 54 to stokers 54a, 54b and 54c.

[0004] The waste W fed into the waste hopper 52 is fed onto the drying stoker 54a in succession with a feeder pusher 53, and then heated and dried with primary combustion air A1 fed from underneath the drying stoker 54a and also with radiant heat from the upper-positioned primary combustion chamber 56 at elevated temperatures. Thus, moisture and volatile components in the waste W are evaporated and unburned gas (reduction gas) such as CO (carbon oxides), HC (hydrocarbon) and the like are released.

[0005] Dried waste W is conveyed from the drying stoker 54a to the combustion stoker 54b, and burned in flames with primary combustion air A1b fed from its underneath thereon. It reaches the burnout position just at the end part on the downstream side of the combustion stoker 54b. Then, the waste W burned out in proximity to the end part of the downstream side of the combustion stoker 54b is conveyed onto the burnout stoker 54c. Next, after so-called embers are burnt with primary combustion

air Alc fed from underneath the burnout stoker 54c, the incineration residues (having typically unburned combustibles content of 5% or less) are discharged from the ash discharge chute 60 downward.

[0006] On the other hand, primary combustion gas G, containing the unburned gas and unburned combustibles, which were generated while drying and burning the waste W, flows into the second combustion chamber 57 that is installed above the primary combustion chamber 50. It is, then, discharged from the exhaust gas outlet 61 to the outside after so-called secondary combustion has been performed in the secondary combustion chamber 57 by feeding the secondary combustion air A2, to achieve complete combustion.

Object of the Invention

[0007] There is a strong demand for waste incineration using a stoker-type waste incinerator in which (1) complete combustion can be achieved surely, automatically and at ease by using an incinerator small in size and with high efficiency, (2) toxic substances are not discharged to the outside when the waste is incinerated, and (3) the purification treatment of the secondary combustion gas is simply performed with a small-type purification treatment device.

[0008] On the other hand, with the above-mentioned stoker-type waste incinerator 50 shown in Figure 5, it is found that compositions and temperatures of the combustion gas generated while waste W is combusted differ depending on where it is combusted. Thus, generally a zone is formed where the combustion gas containing a large quantity of the unburned gas such as CO and the like is generated, a further zone is formed where the combustion gas containing a large quantity of NO_x is generated with intensive burning, and a yet a further zone is formed where the low temperature combustion gas of 500~700° C containing the residual oxygen of more than 15% with the excess air, thus making the combustion gas inside the primary combustion chamber 56 to be in such a state that the distribution of compositions and temperatures is found not to be uniform.

[0009] Therefore, with stoker-type waste incinerator 50, it has been imperative that the unevenly distributed primary combustion gas is mixed and stirred in order to make the combustion gas uniform enough for the unburned gas to be burned completely.

[0010] To mix and stir the above-mentioned primary combustion gas, a method has been utilized (1) with which part of the exhaust combustion gas is blown into the waste incinerator as a re-circulating combustion gas after the complete combustion and purification treatment, and for (2) with which the secondary combustion air (or the temperature adjusting air) is injected, and/or (3) with which blow-in of the re-circulating combustion gas and blow-in of the secondary combustion gas are combined.

[0011] With the above-mentioned methods, there has typically been the problem that the amount of exhaust

combustion gas discharged from the incinerator inevitably increases because either the re-circulating combustion gas or air, or both, are blown in a large volume into the incinerator, thus resulting in the facilities used, such as the exhaust gas treatment device installed downstream of the stoker-type waste incinerator 50, being made bulky.

Furthermore, with the waste combustion for which a conventional stoker-type incinerator is employed, the generation of NOx increases when the feeding volume of the primary combustion air is raised to control the generation of the unburned gas such as CO and the like in order that a lesser amount of toxic substances, such as dioxins, is discharged. Conversely, the generation of dioxins increases, when the feeding volume of the primary combustion air is lowered in order to suppress the generation of NOx, because a greater volume of unburned gas such as CO and the like is discharged. Thus, there remain many unsolved difficulties with such combustion control.

[0012] For example, with a waste incinerator equipped with a power generating unit, it is strongly required that (a) heat recovery can be achieved efficiently in a boiler, (b) the steam flow rate of the boiler and temperatures inside the waste incinerator remain in the set range, and (c) the combustion control of waste is performed to suppress the generation of dioxins, NOx and the like.

To meet these requirements, generally the steam flow rate of the boiler, temperatures inside the furnace, O₂, CO and NOx concentration in the secondary combustion gas are detected such that, the volume of the primary and secondary combustion air, the distribution of the primary combustion air to the stokers and the operating velocity of the stokers can be adjusted.

However, with the above-mentioned conventional method of combustion control, so-called real time combustion control is impossible, thus causing the delay in control because the values detected at the position on the downstream side of the waste combusted are used for controlling the waste combustion.

[0013] Furthermore, with a stoker-type waste incinerator, when a state of combustion turns out to be a so-called non-steady state, due to the substantial fluctuation in the composition and excess or insufficient supply of waste, automatic combustion control does not function because the responsibility of combustion control varies vastly from steady state combustion.

[0014] It is an object of the present invention to solve the afore-mentioned problems with regard to methods of combusting waste using a conventional stoker-type waste incinerator, such as (1) the difficulty in combusting the waste while reducing the generation of toxic substances together with the use of the least amount of combustion air, (2) the difficulty in downsizing a purification treatment unit for the secondary combustion gas, because the volume of the secondary combustion gas from the waste incinerator increases when the primary combustion gas is mixed and stirred by re-circulating the secondary combustion gas and the like, and (3) the difficulty

in holding the waste combustion promptly in a more desirable state of combustion by responding to the fluctuation of the composition and form of the waste on the stokers.

5 Further, it is also an object of the present invention to provide a method of combusting waste at a low air ratio with a stoker-type waste incinerator with which stable, complete combustion of the waste can be performed at a low air ratio regardless of the fluctuation in the quality of the waste whilst achieving a substantial reduction in discharging toxic matters. This is to be obtained in a manner that combustion gas with high oxygen concentration can be drawn from the range where the burnout stoker in the primary combustion chamber of the stoker-type waste incinerator, and the combustion gas drawn is fed to the primary combustion gas underneath the feeding position of the secondary combustion air, that is, on the upstream side. Thus a mixing, stirring and reduction zone of the primary combustion gas is formed. Further, blowing in the least amount of the secondary air to achieve complete combustion. And for the combustion control of waste, a steady state control part mainly responsible at least for the combustion control in normal operating conditions including the control of heat inputs of the waste fed, the control of the combustion-center and burnout position and the real time control of the secondary combustion air and a fuzzy control part responsible for restoring the abnormal combustion to the steady state of combustion when the abnormal combustion of waste happens can be employed.

Method of Achieving the Objects

[0015] To achieve the object of the afore-mentioned invention, the present invention in one aspect provides a method of combusting waste according to claim 1.

[0016] Preferred features are shown in the accompanying subsidiary claims.

The present invention will now be illustrated by way of the following nonlimiting example, with reference to the accompanying drawings, in which:

Brief Description of the Drawings

[0017] Figure 1 is a whole block diagram of a stoker-type waste incinerator employed in one embodiment of the present invention;

Figure 2 is a system diagram to illustrate the outline of the measurement of the heat input of the waste and the control of waste feeding with the stoker-type waste incinerator according to one embodiment of the present invention;

Figure 3 is a system diagram to illustrate the outline of the control of combustion center burnout points with the stoker-type waste incinerator according to one embodiment of the present invention;

Figure 4 is a block diagram to illustrate the basic

constitution of the combustion control system with the stoker-type waste incinerator according to one embodiment of the present invention; and Figure 5 is an explanatory drawing of a conventional stoker-type waste incinerator as an example of the prior art.

List of Reference Characters and Numerals

[0018]

W	Waste
G	Primary combustion gas
Go	Secondary combustion gas
G'	Re-circulating combustion gas (Combustion gas in a zone on the downstream side of a stoker)
A1	Primary combustion air
A2	Secondary combustion air
A	Preheated fresh air
B	Reduction zone
D	Steady state control part
E	Fuzzy control part
1	Stoker-type waste incinerator
2	Furnace body
3	Waste hopper
4	Stoker
4a	Drying stoker
4b	Combustion stoker
4d	Burnout stoker
5	Waste feeder
5a	Waste feeder controller
6	Under-stoker hopper
7	Primary combustion chamber
8	Secondary combustion chamber
9	Ash discharge chute
10	Exhaust gas outlet
11	Primary combustion air blower
12	Duct of re-circulating combustion gas
12a	Suction chamber
12b	Blowing nozzle of re-circulating combustion gas
13	Fan
13a	Driving part of the fan
14	Heat exchanger
15	Air duct
16	Secondary combustion air blower
16a	Driving part of the secondary combustion air blower
16b	Blowing nozzle of secondary combustion air
17	Stoker driving device
17a	Stoker driving device controller
18	Damper
18a	Damper controller
19a~19g	Dampers
20	Damper controller
21	Heat recovery boiler
22	Boiler drum

23	Exhaust gas treatment equipment
24	Automatic combustion control unit
25	Waste scale
26	Scanning laser-type level meter
28	Waste layer thickness meter
29	Gas thermometer
30	Scanning-type infrared radiation thermometer
31	NOx analyzer
32	O ₂ analyzer
33	CO analyzer (Dioxins precursor analyzer)
34	Steam pressure gauge and thermometer
35	Steam flow meter
36	Waste quality and heat inputs computation part
37	Waste feeding control part
38	Waste forwarding control part
39	O ₂ analyzer
40	Image processing part
41	Total air volume computation part
42	Zone temperature distribution assessment part
43	Distribution air volume computation part
44	Air adjustment device control part
45	Gas thermometer
46	Combustion gas control part
47	Boiler steam flow rate control part
48	Total air supplying volume control part
49	Combustion center control part

Detailed Description of Best Mode of the Invention

[0019] Figure 1 illustrates an example of a stoker-type waste incinerator 1 for carrying out the method according to the present invention. Said stoker-type waste incinerator 1 comprises a furnace body 2 formed with a furnace wall, a waste hopper 3 in which waste W is fed, a stoker 4 for burning waste W, a waste feeder 5 to feed waste W onto the stoker 4, an under-stoker hopper 6 installed underneath the stoker 4, a combustion chamber (reference number omitted) consisting of a primary combustion chamber 7 formed above the stoker 4 and a secondary combustion chamber 8 formed above the primary combustion chamber 7, an ash discharge chute 9 for discharging incineration ashes. A exhaust gas outlet 10 is present for discharging the secondary combustion gas Go, a primary combustion air blower 11 feeds the primary combustion air A1 into the primary combustion chamber 7 from beneath the stoker 4, a duct of re-circulating combustion gas 12 leads the re-circulating combustion gas G', drawn from the primary combustion chamber 7 on the downstream side of the stoker 4, to the outside of the primary combustion chamber 7, into the combustion chamber on the upstream side of the blow-in position of the secondary combustion air A2. A fan 13 is located within the duct of re-circulating combustion gas 12, a heat exchanger 14 is provided in the duct of re-circulating com-

bustion gas 12 on the upstream side of the fan 13. An air duct 15 is connected to the heat exchanger and the like to take out fresh air A preheated by the heat exchanger, a secondary combustion air blower 16, a stoker driving device 17 to actuate the stoker 4, and dampers 18, 19a~19g.

[0020] Referring again to Figure 1, 5a designates a driving part of the waste feeder(waste feeder controller), 11a a driving part of the primary combustion air blower (primary combustion air blower controller), 13a a driving part of the fan, 16a a driving part of the secondary combustion air blower(secondary combustion air blower controller), 17a a stoker driving device controller, and 18a, 20 damper controllers.

Also, referring to Figure 1, 21 designates a waste heat recovery boiler, 22 a boiler drum, 23 an exhaust gas treatment equipment, and 24a an automatic combustion control unit.

Furthermore in Figure 1, 25 designates a waste scale, 26 a scanning laser-type level meter, 28 a waste layer thickness meter, 29 a gas thermometer, 30 a scanning-type infrared radiation thermometer, 31 a NOx analyzer, 32 an O₂ analyzer, 33 a CO analyzer, 34 a steam pressure gauge and thermometer and 35 a steam flow meter.

[0021] The above-mentioned stoker 4 comprises a drying stoker 4a, a combustion stoker 4b and a burnout stoker 4c, and an under-stoker hopper 6 is located underneath the stokers 4a, 4b and 4c respectively. These stoker 4a, 4b and 4c are formed with both conventionally known travelling grates (not illustrated), and fixed grates (not illustrated), which are arranged in alternating order. The waste W on the stoker 4 is moved forward from the upstream side to the downstream side while stirring it in a reciprocating motion of travelling grates back and forth with a certain pitch by the stoker driving device 17.

Above the stoker 4, there is provided a primary combustion chamber 7 for drying and combusting the waste W while it moves forward on the stoker 4 with primary combustion air A1a~A1c fed from underneath the stoker 4. Also provided therewith is a secondary combustion chamber 8 for combusting the unburned gas such as CO and the like and unburned combustibles generated in the primary combustion chamber with secondary combustion air A2.

[0022] The above-mentioned primary combustion air blower 11 which is for supplying the primary combustion air A1 to the lower part of the stokers 4a, 4b and 4c through the under-stoker hoppers 6 under the stoker 4, is equipped with a plural number of air volume adjusting dampers 19a~19g. Further, damper controllers 20 control the opening/closing of these dampers 19a~19g with which the amount of the primary combustion air A1 fed to the lower part of the stoker 4a, 4b and 4c is adjusted.

[0023] According to this embodiment, the amount of the primary combustion air A1 fed from underneath the stoker 4 is controlled, typically the primary air ratio (the amount of the primary combustion air/the amount of the theoretical combustion air) being 0.8~1.0. And, usually

approximately 70~80% of the primary combustion air A1 is fed from the combustion stoker 4b, to form the reduction zone containing the unburned gas, such as CO, HC and the like above the combustion stoker 4b, so that the space above the combustion stoker 4b is made to be the atmosphere inhibiting to the generation of NO_x. Meanwhile approximately 20% of the primary combustion air A1c is fed from the burnout stoker 4c, to achieve complete combustion of the unburned combustibles in the ashes.

[0024] The distribution amount and temperature of the primary combustion air A1a~A1c fed to the lower part of stokers 4a, 4b and 4c and the amount of waste forwarded by the stokers are controlled so that the residual oxygen in the re-circulating combustion gas G' is typically found to be more than 15%, and the temperatures above the burnout stoker 4c to be a value set generally between 600~800°C.

[0025] The above-mentioned duct of re-circulating combustion gas 12 is for leading the re-circulating combustion gas G' on the upper part on the downstream side of the stoker 4 (the upper part of the burnout stoker 4c) being drawn to the outside of the primary combustion chamber 7 into the combustion chamber on the upstream side of the blow position of the secondary combustion air A2. In particular, by forming a suction chamber 12a on the furnace wall above the burnout stoker 4c to draw out the combustion gas G' above the burnout stoker 4, the re-circulating combustion gas G' above the burnout stoker 4c is sucked into the suction chamber 12a by using fan 13, and the re-circulating combustion gas G' is blown into the combustion chamber at high velocity from the blowing nozzle of re-circulating combustion gas 12b on the upstream side of the blow-in position of the secondary combustion air A2.

[0026] The re-circulating combustion gas G' above the burnout stoker 4c is drawn to the outside of the furnace, and the drawn re-circulating combustion gas G' is blown into the combustion chamber on the upstream side of the blow-in position of the secondary combustion air A2 to mix and stir the primary combustion gas G generated inside the primary combustion chamber 7. In this way a slightly reducing atmosphere (reduction zone B) where the composition and temperatures of the primary combustion gas G become uniform is formed at a region of the combustion chamber upstream of the blow-in position of the secondary combustion air A2 to prevent the generation of NO_x, and to combust unburned gas and the like completely by supplying the minimum amount of secondary combustion air A2 thereafter.

[0027] According to the present embodiment, the retention time of the afore-mentioned primary combustion gas G is such that at the reduction zone B (i.e. the time required to pass the reduction zone B) is typically 0.5 seconds or longer, and generally it can retain in the high temperature zone of higher than 850°C for 1.5 seconds or longer after supplying secondary combustion air.

[0028] The above-mentioned heat exchanger 14 is provided in the duct of re-circulating combustion gas 12

on the upstream side of the fan 13 (with this example, inside the suction chamber 12a) to reduce the temperature of the re-circulating combustion gas G'. An economizer, deaeration heater, boiler, air heater and the like can typically be employed as such a heat exchanger 14.

[0029] Corrosive gases such as HCl, SOx and the like, in the afore-mentioned primary combustion gas, are generated when plastics such as polyvinyl chloride and the like, contained in waste W, are combusted. Plastics are mainly burned on the combustion stoker 4b because they are decomposed and are generally burned at temperatures of 350°C~500°C at a relatively high velocity of combustion. Accordingly, corrosive gases are mainly generated on the combustion stoker 4b, and found in the primary combustion gas G above the combustion stoker 4b and drying stoker 4a, while the re-circulating combustion gas G' above the burnout stoker 4c has a lesser concentration of corrosive gas and dust, thus allowing the afore-mentioned heat exchanger 14 to be provided inside the suction chamber 12a so as to draw the re-circulating combustion gas G' above the burnout stoker 4c. And, there are caused no problems such as corrosion and the like even when the re-circulating combustion gas G' which temperatures are reduced to 200°C~300°C is blown into the secondary combustion chamber 8 by the fan 13.

[0030] The afore-mentioned secondary combustion air blower 16 is for supplying the secondary combustion air A2 to the blowing nozzles of secondary combustion air 16b formed on the furnace wall of the secondary combustion chamber 8.

[0031] The volume of the secondary combustion air A2 blown into the secondary combustion chamber 8 is adjusted by means of a damper 18. In this embodiment, the volume of the secondary combustion air A2 fed into the secondary combustion chamber 8 is set at 0.3~0.4 as its secondary air ratio (the secondary combustion air volume/the theoretical combustion air volume), and the total volume of the primary combustion air A1 and secondary combustion air A2 is set at 1.3 as its air ratio. Accordingly, the oxygen concentration of the secondary combustion gas Go is continuously measured at real time by the laser-type oxygen analyzer 32 and the volume of the secondary combustion air is controlled to make the oxygen concentration to be approximately 5% (dry).

[0032] Figure 2 is a schematic system diagram that illustrates a heat input measuring device and a waste feeding controller for which a below mentioned waste scale 25 and a scanning laser-type level meter 26 are employed.

The waste scale 25 can be used for measuring the weight of waste picked up by a crane C, and the measured data are inputted to the waste quality and heat input computation part 36.

The data on the waste volume in the waste hopper 3 obtained by the scanning laser-type level meter 26 installed above the waste hopper 3 is also inputted to the waste quality and heat input computation part 36.

[0033] In the waste quality and heat input computation

part 36, the waste quality (heat value) is estimated based on the specific gravity of the waste computed by both afore-mentioned inputted volume and weight of the waste and stored each time the waste is fed.

Also, changes in the total volume of the waste per unit time are computed from the total volume of the waste stored in the waste hopper 3, and the moving volume of the waste (that is, the fluctuation rate of the volume of the waste in the hopper) is determined by the changes in the total volume of the waste per unit time, thus the heat input of the waste per unit time is computed from the moving volume and the heat value predicted from the afore-mentioned specific gravity.

[0034] Data regarding the heat input of the waste is inputted to the waste feeding control part 37 which controls the waste feeder controller 5a of the waste feeder 5. The waste feeder 5 and stoker driving device 17 are controlled by the waste feeding control part 37 to make the heat input of the waste fed into the stoker-type waste incinerator constant at the setting value.

[0035] Figure 3 is a schematic system diagram that illustrates the control of burning center and burnout points.

The information on the incineration occurring inside the furnace from scanning-type infrared radiation thermometer 30 is inputted to an image processing part 40, which constitutes a automatic combustion control unit 24. Similarly, detecting signals obtained by an O2 analyzer 32 and the like, a gas thermometer 29 and a layer thickness meter 28 and the like are also inputted to the total air volume computation part 41 and burning center control part 49 of the automatic combustion control unit 24.

The information data regarding the inside of the furnace processed at the afore-mentioned image processing part 40 is inputted to the zone temperature distribution assessment part 42, where the temperature distribution, burning center position (the position of the highest temperature) and burnout point inside the furnace are assessed.

[0036] Further, the distribution volume of the primary combustion air A1 is computed at the distribution air volume computation part 43 based on the temperature distribution inside the furnace obtained at the zone temperature distribution assessment part 42, and so the temperature distribution inside the furnace can be adjusted to the temperature distribution set in advance by making the dampers 19a~19g open or close through the air-adjusting device control part 44.

Furthermore, based on signals outputted from the waste layer thickness meter 28 and the afore-mentioned burning center position, the waste feeder 5 and stoker driving device 17 are adjusted respectively through the burning center control part 49, waste forwarding control part 38 and waste feeding control part 37. Thus the waste forwarding velocity and waste feeding volume can be controlled, so that the waste layer level on the drying stoker 4a and burning center position on the combustion stoker 4b are positioned within a set range.

[0037] The automatic combustion control unit 24 is equipped with the afore-mentioned waste quality and heat input computation part 36, combustion gas control part 36, boiler steam flow rate control part 47, total air feeding control part 48 and the like as shown in Figure 2.

[0038] Further, detecting signals from the boiler steam pressure gauge and thermometer 34 and steam flow meter 35 are inputted to the boiler steam flow rate control part 47, to compute the volume of steam generated, and the heat input of the waste required to generate steam. Thus, operating signals are transmitted to the devices 5, 17, 11 and the like from the waste feeding control part 37, waste forwarding control part 38, total air feeding control part 48 and the like to acquire the heat input needed.

[0039] In addition, the above-mentioned combustion gas control part 46 is for controlling the operation of the fan 13 to draw the re-circulating combustion gas G' fed into the combustion chamber. With the signals from the O₂ analyzer 39, the volume of the primary combustion air A1 c fed to the burnout stoker 4c is controlled so that the re-circulating combustion gas G' having oxygen concentration of 15% or more can be fed to the blowing nozzle of re-circulating combustion gas 12b.

[0040] Furthermore, the temperature of the above-mentioned re-circulating combustion gas G' is continuously detected with the gas thermometer 45, and it is controlled to keep setting between 600~800°C by adjusting both the volume of the primary combustion air A1c fed underneath the burnout stoker 4c and waste feed rate of the stoker 4.

[0041] Though not shown in Figure 3, the volume of the primary combustion air AC 1 fed underneath the burnout stoker 4c and the waste feed rate of the stoker 4 can be adjusted by measuring at least one of O₂ concentration, CO concentration and HCl concentration in the re-circulating combustion gas G', thus making the measured value remain in the range of concentration set in advance.

[0042] In addition, the volume of the above-mentioned re-circulating combustion gas G' is usually adjusted so that the NO_x concentration in the secondary combustion gas Go is less than 60ppm at any time with the detecting signals coming from NO_x analyzer 31. If the NO_x concentration exceeds 60ppm, the feeding volume of the re-circulating combustion gas G' is increased to enhance the ability of mixing and stirring the re-circulating combustion gas G' in the reduction zone B.

[0043] The operation of the above-mentioned secondary combustion air blower 16 is controlled by the total air volume computation part 41 and total air supplying volume control part 48, with the detecting signals from the O₂ analyzer 32 provided at the combustion chamber outlet, so that the oxygen concentration of the secondary combustion gas Go typically comes to approximately 5%, and the total volume of the primary combustion air A1 and secondary combustion air A2 has been adjusted to the air volume of 1.3 as the air ratio.

[0044] Taking into consideration both the mixing capability of the primary combustion gas G and the sec-

ondary combustion of incombustibles, it is necessary to supply a certain volume of the above-mentioned secondary combustion air A2. Namely, when the feeding volume of the secondary combustion air A2 is reduced to 0.2 or less as the air ratio, complete secondary combustion cannot be performed because of its insufficient mixing with the primary combustion gas G. Accordingly, in order to solve this problem, even when the oxygen concentration in the secondary combustion gas Go exceeds 5%, the feeding volume of the secondary combustion air A2 should not be less than 0.2 as the air ratio.

[0045] Figure 4 is a basic block diagram that illustrates the combustion control system of the stoker-type waste incinerator employed with this embodiment. The combustion control system comprises a steady state control part D and a fuzzy control part E.

That is, the steady state control part D controls stable combustion conditions in a steady state of the stoker-type waste incinerator, while the fuzzy control part E controls abnormal combustion conditions under non-steady state of the incinerator, to restore the abnormal combustion back to the steady state.

[0046] As shown in Figure 4, the major elements that constitute the above-mentioned steady state control part D include waste heat input control D1, combustion center position control D2, burnout point control D3, air-waste ratio control D4, boiler steam flow rate control D5, secondary combustion air real time control D6, re-circulating combustion gas control D7, and the like.

[0047] Namely, waste heat input control D1 controls the velocity of the waste feeder 5 and stoker 4 to hold the volume of the waste (the waste heat input) fed into the furnace body to the set value. The air-waste ratio control D4 corrects the incorrect balance between the volume of the primary combustion air A1 and the waste volume by adjusting the velocity of the stoker 4. Furthermore, the boiler steam flow rate control D5 adjusts the volume of the primary combustion air A1, and the operating velocity of the waste feeder 5, the stoker 4 and the like in order that the boiler steam generation rate is held at the set value. The secondary combustion air real time control D6 adjusts the volume of the secondary combustion air A2 so that the value measured by the oxygen analyzer installed at the combustion chamber outlet is constant to the set value. The combustion center position control D2 and burnout point control D3 correct the incorrect combustion center and burnout position by adjusting both the volume of the primary combustion air A1 and the velocity of the stoker, or at least by adjusting one of them.

The re-circulating combustion gas control D7 adjusts the volume of the re-circulating combustion gas G' drawn from the space above the burnout stoker 4c to keep NO_x concentration of furnace outlet gas less than 60 ppm and correct the temperature of re-circulating combustion gas G', oxygen concentration, and the like.

[0048] On the other hand, the above-mentioned fuzzy control part E checks the state of combustion by a plural

number of parameters when the combustion becomes a so-called non-steady state due to the substantial and abrupt changes in the quantity and quality of the waste, and performs the restoration control of the non-steady state of combustion back to the steady state by outputting the control signal to correct the volume of combustion air and waste feed rate depending on the abnormal state by applying fuzzy-logical inferences with multivariable logics.

[0049] Concretely, for example, the above-mentioned waste heat input control D1 and air-waste ratio control D4 are capable of dealing with a certain fluctuation of the quantity and quality of the waste. However, when the extreme changes happen, it is necessary to control volume of the combustion air and the velocity of the stoker extremely fast and widely by using the fuzzy control part E.

[0050] Next, a method of waste combustion at the low air ratio by employing the stoker-type waste incinerator 1 according to the present embodiment is explained. Referring to Figure 1 to Figure 4 inclusive, whilst the waste W fed into the furnace from the waste hopper 3 is gasified and combusted while it moves forward on the drying stoker 4a, combustion stoker 4b and burnout stoker 4c in succession, with supplying the primary combustion air A1 which is fed into the primary combustion chamber 7 through the stokers 4a, 4b and 4c from the primary combustion air blower 11.

[0051] Thus, the waste W in the waste hopper 3 is continuously fed by the waste feeder 5 onto the drying stoker 4a on which the waste W is dried with the primary combustion air A1 fed from beneath the drying stoker 4a and radiation heat of the high-temperature combustion gas G generated with the combustion on the combustion stoker 4b in the next stage. Also, some combustion contents of the waste W on the drying stoker 4a starts gasification and combustion. Moisture in the waste W is evaporated, and unburned gas such as CO, HC and the like are released herewith.

[0052] The dried waste W forwarded from the drying stoker 4a onto the combustion stoker 4b in succession is combusted with flames with the primary combustion air A1b fed from underneath the combustion stoker 4b, and burned out at the end part on the downstream side of the stoker 4b.

The waste W burned out at the end part on the downstream side of the combustion stoker 4b is forwarded onto the burnout stoker in succession. Then, after so-called embers burning with the primary combustion air A1c fed from underneath the burnout stoker 4c, the waste W is discharged from the ash discharge chute 9 as incinerated ashes not containing almost no unburned combustibles at all.

[0053] With the stoker-type waste incinerator 1, the volume of the primary combustion air A1 fed underneath the stoker 4 is made to be 0.8~1.0 as the air ratio, and approximate 70%~80% of the total primary combustion air A1 is fed from underneath of the combustion stoker

4b, to form a reduction zone containing the unburned gas such as CO, HC and the like. Then, approximately 20% of the primary combustion air A1 is fed from underneath of the burnout stoker 4c to combust the unburned combustible contents of ash completely.

[0054] According to the invention, the re-circulating combustion gas G' (temperature: 600°C~800°C) above the burnout stoker 4c is sucked into the suction chamber 12a by the fan 13, and the re-circulating combustion gas G' which temperature is reduced by the heat exchanger (temperature: 200°C~300°C) is blown into the combustion chamber on the upstream of the blow-in position of the secondary combustion air A2 (the combustion chamber on the lower side of the blowing nozzle of secondary combustion air gas 20b) from the blowing nozzle of re-circulating combustion gas 12b at high velocity (higher than 50m/s). By doing so, the primary combustion gas G that has ascended from the primary combustion chamber 7 is mixed and stirred, thus the inside of the upstream of the blow-in position of the secondary combustion air A2 becomes a reduction zone B containing a weak reducing atmosphere. Then, the secondary combustion air A2 is blown into the secondary combustion chamber 8 through the secondary combustion air nozzle 20b from the secondary combustion air blower 16.

By controlling the volume of the secondary combustion air A2 to keep oxygen concentration of secondary combustion gas which is measured at real time with a laser type oxygen analyser, the total air ratio of the primary air A1 and secondary air A2 is kept 1.3.

[0055] The primary combustion gas G containing the unburned gas and unburned combustibles is mixed and stirred twice with the re-circulating combustion gas G' blown in from the blowing nozzle of re-circulating combustion gas 12b and with the secondary combustion air A2. That is, the primary combustion gas G having varied components generated from the stokers 4a, 4b and 4c is mixed and stirred twice with the re-circulating combustion gas G' and secondary combustion air A2, thus making its composition and temperature distribution uniform, and sufficient mixing with the secondary combustion air A2 also being achieved. Accordingly, the unburned gas and unburned combustibles in the primary combustion gas G are completely combusted without a large volume of combustion air being blown into the furnace, and the generation of CO, dioxins, NOx and the like are sufficiently suppressed. (CO at the furnace outlet <10ppm, DXN<0.5ngTEQ/m³ N, NOx<60ppm).

[0056] The re-circulating combustion gas G' drawn from above the burnout stoker 4c contains more than 15% oxygen. The residual oxygen can effectively be utilized by blowing it into the primary combustion gas G. Because of low concentration of dust, HCl and the like which are corrosive, the heat exchanger 14 provided at the suction chamber 12a and fan 13 are not damaged by corrosion.

[0057] After the primary combustion gas G containing the unburned gas and unburned combustibles is burned

completely with the re-circulating combustion gas G' blown into the combustion chamber on the upstream of the blow-in position of the secondary combustion air A2 and with the secondary combustion air A blown into the secondary combustion chamber 8, it is discharged from the exhaust gas outlet 10 as the secondary combustion gas, and released in the atmosphere through the boiler, exhaust gas treatment facility and the like.

[0058] In the above-mentioned embodiment, the suction chamber 12a is provided with an air heater to be used as a heat exchanger 14. However, it can be replaced by an economizer, deaeration heater or superheater.

[0059] Also, in the above-mentioned embodiment, a heat exchanger 14 is provided in the suction chamber 12a. However, the place where the heat exchanger 14 may be installed can be chosen, as desired.

Effects of the Invention

[0060] In the combustion method according to the present invention the volume of the primary combustion air to be fed from underneath the stoker can be set as 0.8~1.0 as the primary air ratio, and the combustion chamber can be made to be a strongly reducing atmosphere by drawing the re-circulating combustion gas G' having high oxygen concentration above on the downstream of the stoker to the outside, and the inside of the combustion chamber on the upstream side of the blow-in position of the secondary combustion air A2 can be made to be a mildly reducing atmosphere (a reduction zone B), in which the composition and temperature distribution of the primary combustion gas can be made uniform by blowing the re-circulating combustion gas G' having high oxygen concentration into the combustion chamber on the upstream of the blow-in position of the secondary combustion air A2. Furthermore, the unburned gas and unburned combustibles in the primary combustion gas G are typically burned over the 3 completely by blowing the secondary combustion air A2 into the secondary combustion chamber on the downstream of the afore-mentioned reduction zone B. It follows that the waste can be burned completely with the 3 stage combustion under a state of 1.3 or less as the total air ratio

[0061] As a result, complete combustion of the unburned gas, unburned combustibles, and the like has been achieved with the small volume of combustion air of 1.3 as the total air ratio, thus resulting in substantial reduction of the secondary combustion gas Go and in downsizing of the exhaust gas treatment facilities, and the like. Further, CO, NOx and dioxins are remarkably reduced because the unburned gas and unburned combustibles are completely combusted. Furthermore, heat loss of exhaust gas is also lowered because the volume of the exhaust gas is reduced, thus enhancing the heat recovery efficiency.

[0062] In addition, according to the present invention, the combustion of waste is achieved by using a stoker-

type waste incinerator equipped with a combustion control system comprising a steady state control part and fuzzy control part, hence not only achieving stable waste combustion in a steady state, but also being able to restore the abnormal state back to the steady state by the combustion control of the fuzzy control part, which responds to the case of abnormality promptly when abnormal situations such as substantial fluctuation in the quality and quantity of waste and the like occur.

Claims

1. A method of combusting waste (W) with a stoke-type waste incinerator (1) at a low air ratio; **characterized in that** said waste (W) is shifted from a drying stoker (4a) to a combustion stoker (4b), to a burnout stoker (4d), in succession for the primary combustion of said waste (W), said waste (W) being placed on stokers (4) of said incinerator, said combustion effected by feeding primary combustion air (A1) from underneath said stokers (4) to a primary combustion chamber (7) above said stokers (4), said combustion being effected also for the unburned gas and unburned combustibles contained in the primary combustion gas (G) flowing in from said primary combustion chamber (7) being combusted by feeding secondary combustion air (A2) into a secondary combustion chamber (8) placed above the primary combustion chamber (7); further **characterized in that** the volume of said primary combustion air (A1) fed from beneath said stokers (4) is held to allow the air ratio to be 0.8~1.0, re-circulating combustion gas (G') having oxygen concentration of 15% or more is drawn to the outside from said primary combustion chamber (7) in the zone where said burnout stoker (4d) is positioned, and said drawn re-circulating combustion gas (G') is blown into said primary combustion gas (G) flowing in from said primary combustion chamber (7) at the upstream of a feeding position of said secondary combustion air (A2) for mixing and stirring said primary combustion gas (G) with the re-circulating combustion gas (G') blown in, thus forming a high-temperature reduction zone with an air ratio of 0.8~1.0 and also with a uniform distribution of composition and temperature of gas flow; and furthermore **characterized in that** the feeding volume of said secondary combustion air (A2) is held to allow the air ratio to be 0.3~0.4, the oxygen concentration of the secondary combustion gas (Go) at the outlet of said secondary combustion chamber (8) being measured continuously at real time, by using a laser-type oxygen analyzer, to control the feeding amount of said secondary combustion air (A2) so that the measured value of said oxygen concentration becomes substantially 5%, thus achieving a complete combustion of waste (W) with a total air ratio of less than 1.3; and yet further **characterized in that** the

combustion control system comprises a steady state control part (D) responsible for the stable combustion control in normal operating conditions including at least: the control of the heat input of the waste (W), the control of the burning-center and burnout points and the real time control of the secondary combustion air (A2), and a fuzzy control part (E) responsible for restoring the state of abnormal combustion to the stable, steady conditions when abnormal combustion of waste (W) has occurred, thus achieving complete combustion of said waste (W).

2. A method as claimed in Claim 1, wherein said temperatures of the re-circulating combustion gas (G') drawn from the primary combustion chamber (7) to the outside are reduced to approximately 200°C~300°C by using a heat exchanger (14) consisting of either one or more than two of a deaeration heater, economizer, boiler or air heater.
3. A method as claimed in Claim 1, wherein said primary combustion gas (G) flowing in from the primary combustion chamber (7) to said reduction zone (B) is retained in said reduction zone (B) for more than 0.5 seconds, and said secondary combustion gas (Go) after the secondary combustion air (A2) was blown in is retained in the high temperature zone of higher than 850°C for more than 1.5 seconds.
4. A method as claimed in Claim 1, **characterized by** that said distribution volume and said temperature of the primary combustion air (A1) fed to the lower part of the stoker (1) and said rate of waste(w) to be forwarded by the stoker (1) are so controlled such that the temperature of the re-circulating combustion gas (G') above the burnout stoker (4d) becomes constant with temperatures set between 600°C~800°C, or at least one of oxygen concentration, CO concentration or HCl concentration of the re-circulating combustion gas (G') remains within the range of concentration set in advance.
5. A method as claimed in Claim 1, wherein said volume of the re-circulating combustion gas (G') drawn from the upper part of the burnout stoker (4d) to the outside and blown into the combustion chamber on the upstream side of the blow-in position of the secondary combustion air is so controlled such that NOx (31) contained in the secondary combustion gas (Go) discharged from the waste incinerator (1) becomes less than 60ppm.
6. A method as claimed in Claim 1, wherein said weight of the waste (W) fed into a waste hopper (3) by the waste crane is measured and the waste level in the waste hopper is continuously measured to compute the volume of the waste fed in and compute the specific gravity of the waste (W) with the said weight and

volume of the waste (W), and also the volume of the waste (W) continuously fed into the stoker-type waste incinerator (1) is computed, and the heat input of the waste is computed from said feeding volume of the waste (W) and the said specific gravity of the waste so that the waste feeder is controlled to make constant said heat input of the waste (W), and furthermore, the quality of the waste (W) such as the heat value is estimated with the said computed specific gravity and the distribution volume of the primary combustion air (A1) fed underneath the stokers (4) is controlled based on said quality of the waste (W).

7. A method as claimed in claim 1, wherein a scanning-type infrared radiation thermometer (30) equipped above the stokers (4) detects the temperature distribution on the waste surface in the direction of the flow of the waste (W) on the stokers (4) continuously so that the burning center position of the waste (W) is determined from the detected highest temperature on the waste surface while the burn out position of the waste (w) on the stoker (4) is determined from the greatest drop rate of the temperature on the waste surface and the velocity of the stokers (4) and the distribution volume of the primary combustion air (A1) are controlled to maintain the burning center position and burn out position of the waste (W) on the stokers (4) at the set positions.
8. A method as claimed in Claim 1, wherein said control of the heat input of the waste (W), the control of the burning center and burnout positions and the control of the secondary combustion air (A2) at real time are integrated as one system.
9. A method as claimed in Claim 1, wherein even if the value of oxygen concentration in the secondary combustion gas (Go) at the outlet of the secondary combustion chamber (8) detected by the laser-type oxygen analyzer exceeds 5%, the feeding volume of the secondary combustion air (A2) is controlled at least more than 0.2 for the air ratio to hold the blow-in velocity of the secondary combustion air (A2) higher than the set value.
10. A method as claimed in Claim 1, wherein the feed rate of the waste(W) is adjusted with the fuzzy control when the burning center and burnout positions of the waste on the stokers are out of normal operations or substantially fluctuated.

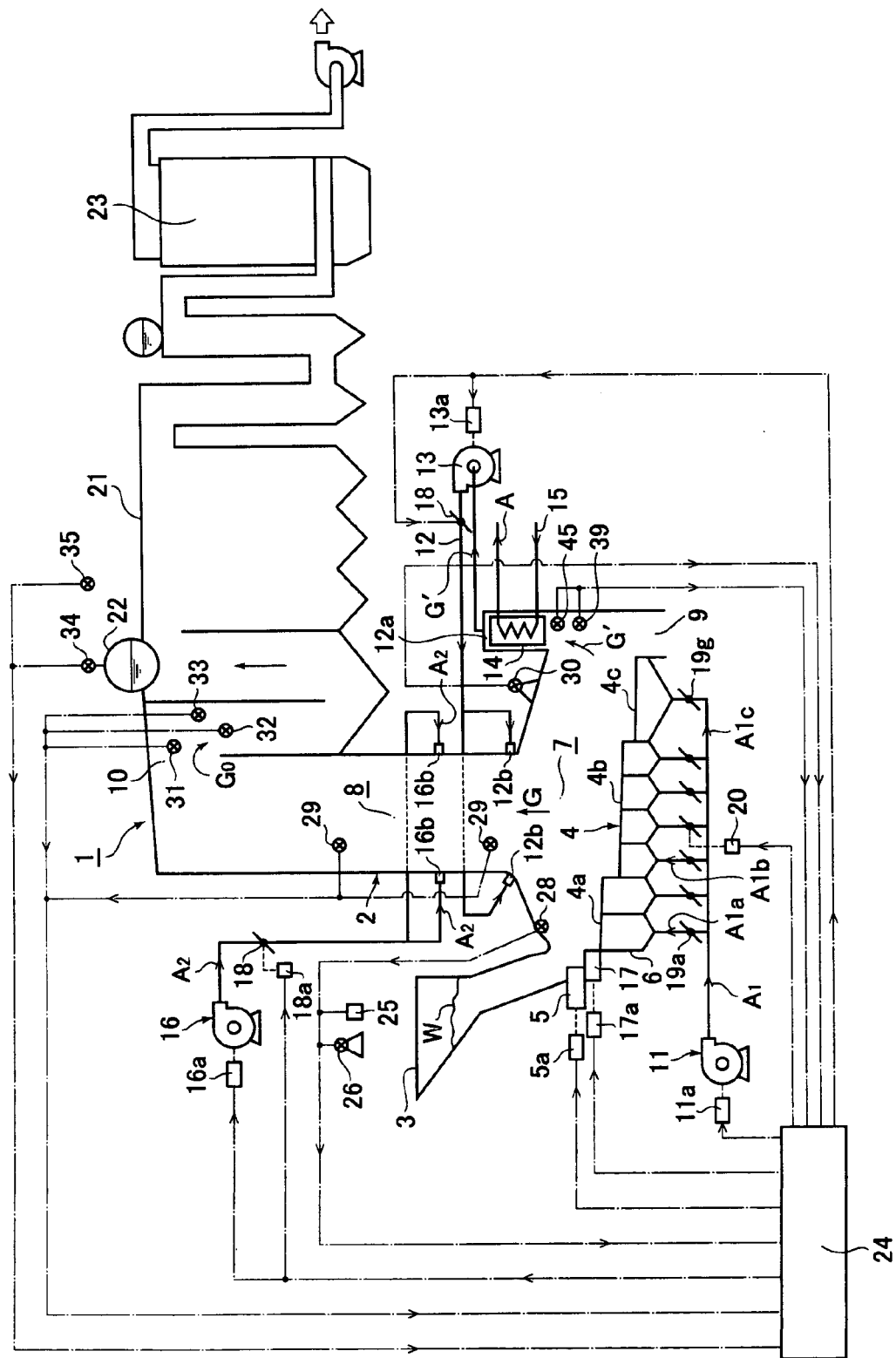


FIG. 1

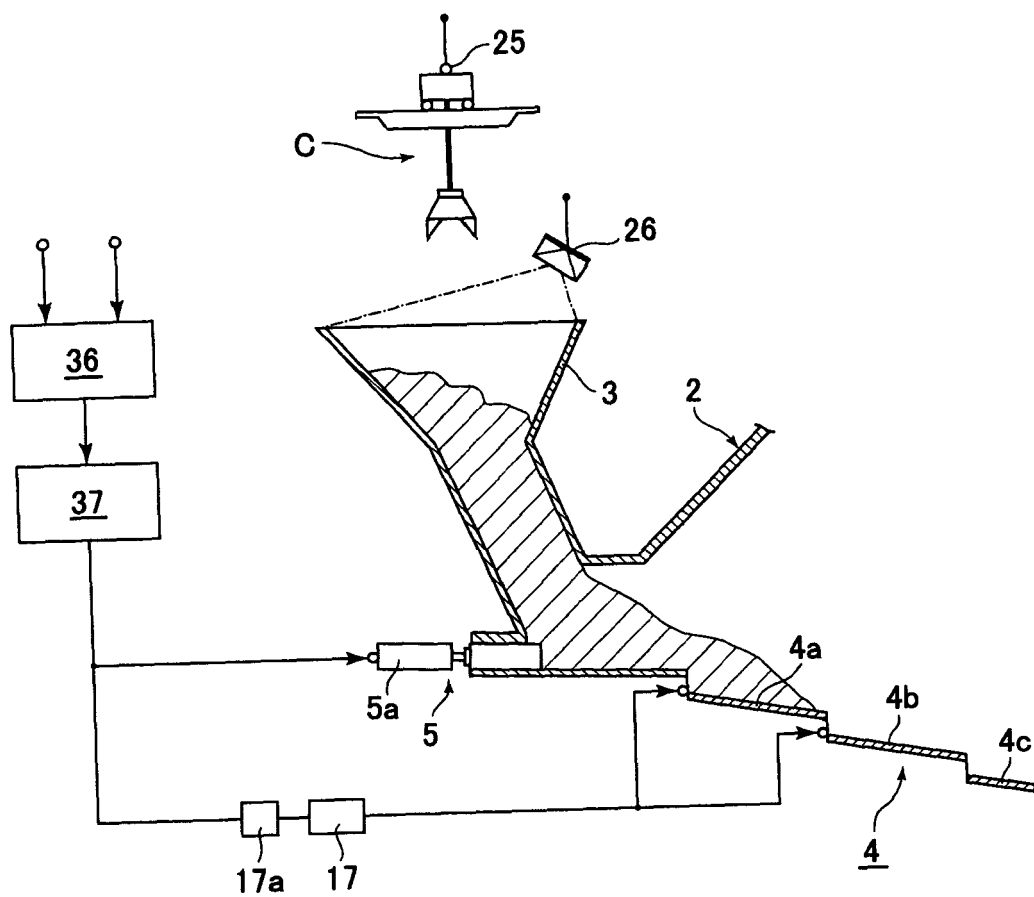


FIG. 2

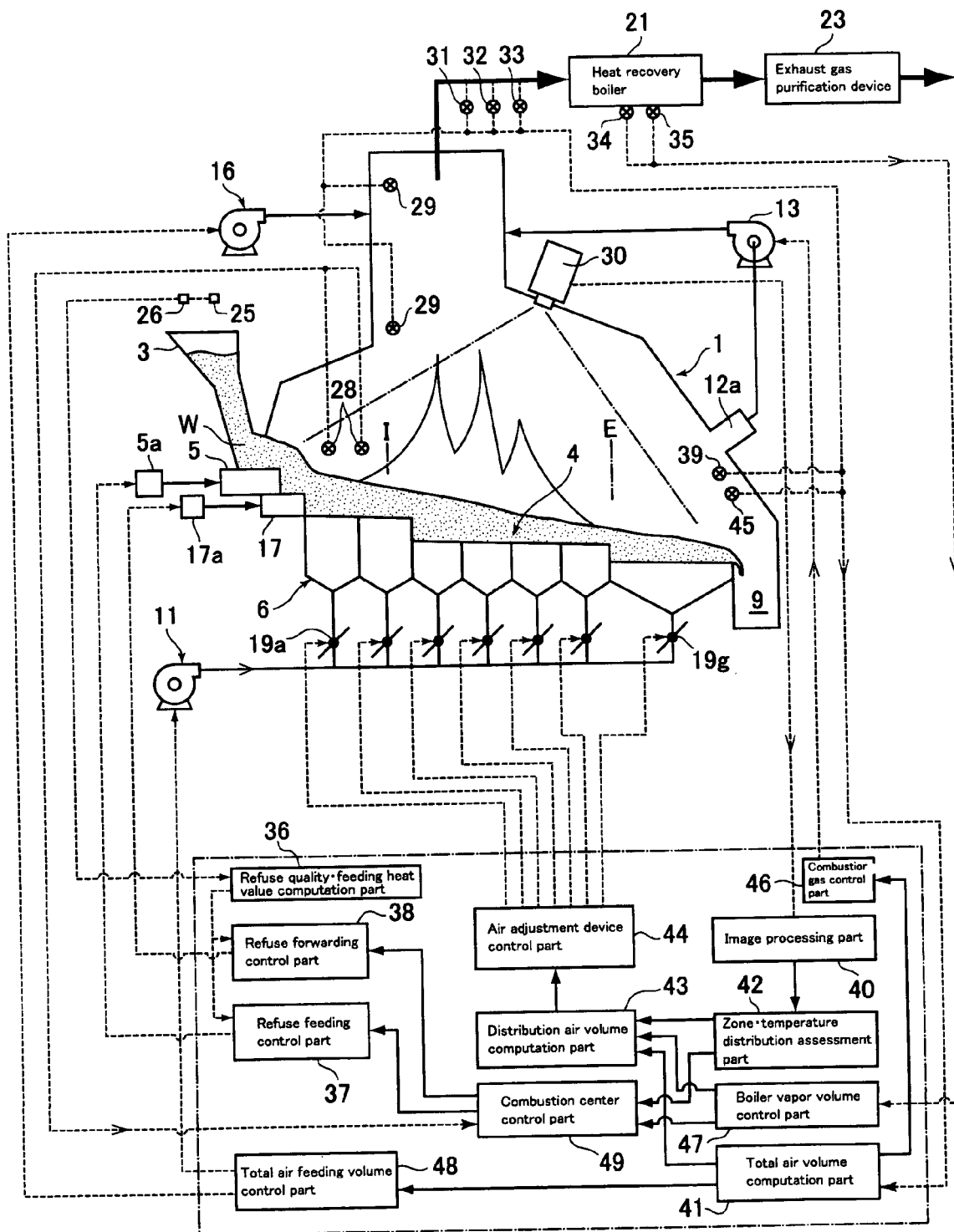


FIG. 3

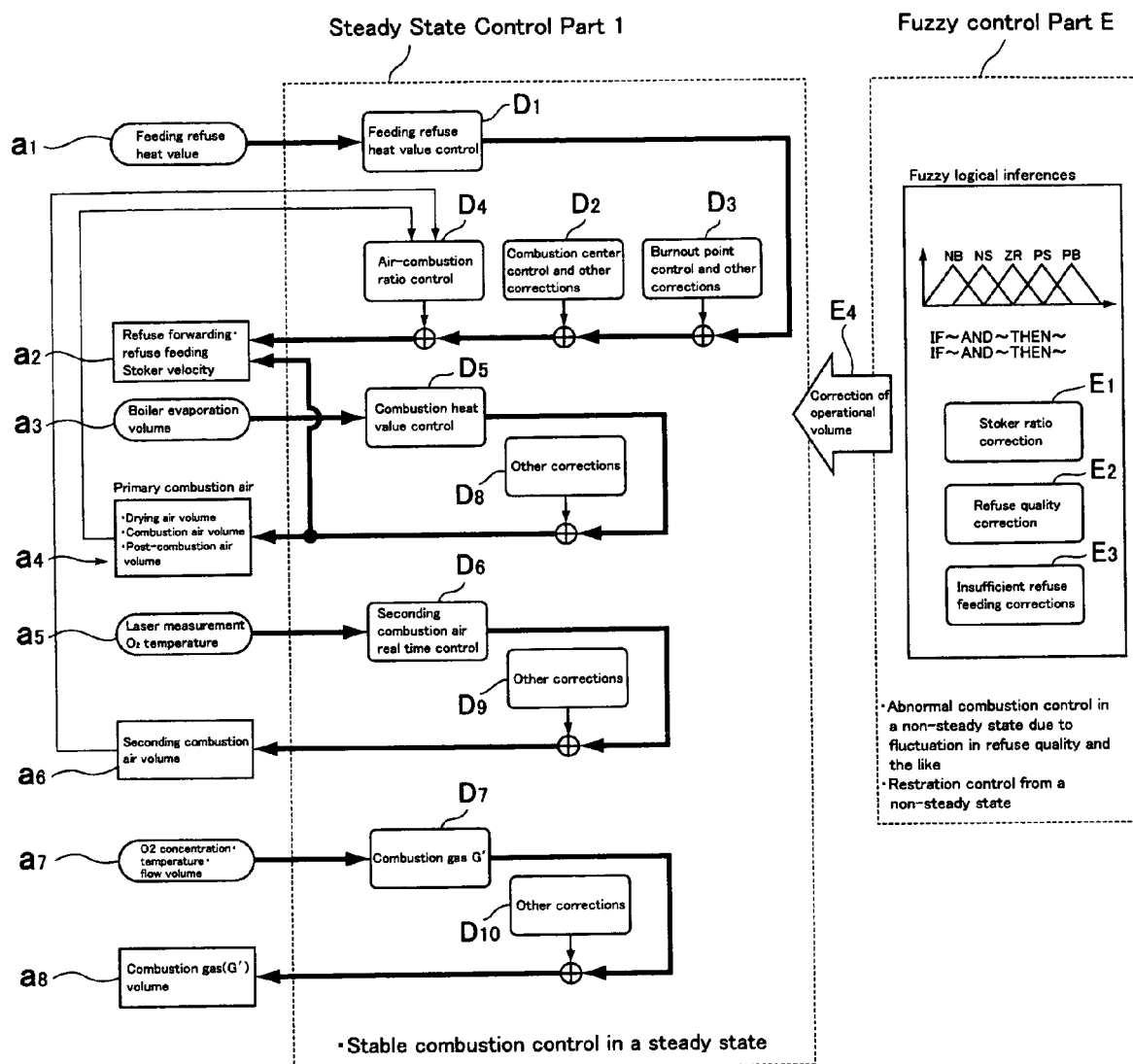


FIG. 4.

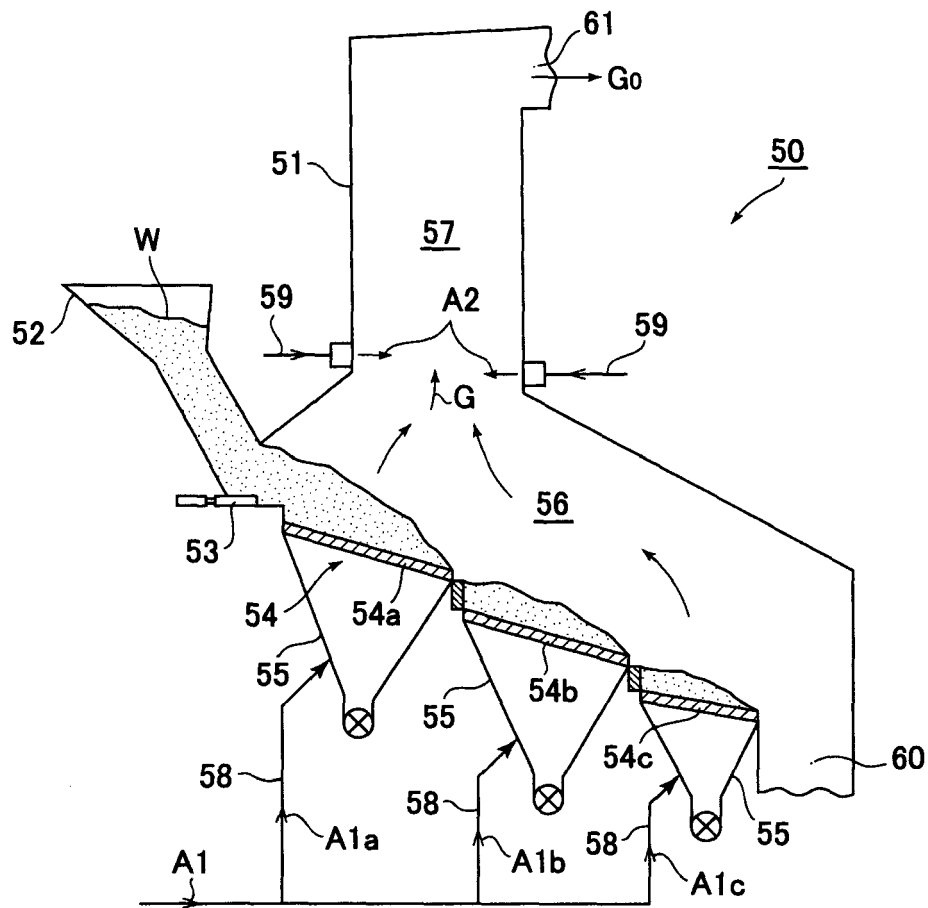


FIG. 5



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 05 25 3289

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
Y	EP 0 621 448 A (MARTIN GMBH FUER UMWELT-UND ENERGIETECHNIK) 26 October 1994 (1994-10-26) * column 10, line 11 - column 13, line 6 * * column 14, line 19 - line 50 * * figures 1,2,5,6 *	1,7,9	F23G5/05 F23G5/16 F23L1/02 F23L9/02 F23N3/00
Y	EP 0 770 820 A (HITACHI ZOSSEN CORPORATION) 2 May 1997 (1997-05-02) * column 3, line 18 - line 24 * * column 4, line 30 - line 44 * * column 8, line 28 - column 9, line 4 * * figures 1,7,8 *	1,7,9	
A	EP 0 805 307 A (KURIHARA KOGYO CO., LTD; SAITOH, SHIGERU) 5 November 1997 (1997-11-05) * column 1, line 12 - line 28 * * column 4, line 22 - column 6, line 55; figures 1,2 *	1,3	
A	US 4 510 873 A (SHIGAKI ET AL) 16 April 1985 (1985-04-16) * column 2, line 64 - column 3, line 4 * * column 3, line 37 - column 4, line 24; figure 1 *	1	TECHNICAL FIELDS SEARCHED (Int.Cl.7) F23G F23L F23N
A	GB 2 348 270 A (* NKK CORPORATION) 27 September 2000 (2000-09-27) * page 24, paragraph 5 - page 25, paragraph 2 * * page 30, last paragraph - page 32, paragraph 2; figures 3,4,15 *	1	
The present search report has been drawn up for all claims			
Place of search Munich		Date of completion of the search 11 October 2005	Examiner Gavriliu, C
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

EPO FORM 1503 03.82 (P04C01)



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 05 25 3289

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
A	PATENT ABSTRACTS OF JAPAN vol. 005, no. 076 (M-069), 20 May 1981 (1981-05-20) & JP 56 025609 A (TAKUMA CO LTD), 12 March 1981 (1981-03-12) * abstract * -----	1	
			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
The present search report has been drawn up for all claims			
Place of search Munich		Date of completion of the search 11 October 2005	Examiner Gavriliu, C
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

1
EPO FORM 1503 03.82 (P04C01)

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 05 25 3289

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

11-10-2005

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
EP 0621448	A	26-10-1994	AT 158396 T	15-10-1997
			BR 9401541 A	22-11-1994
			CA 2121295 A1	21-10-1994
			DE 4312820 A1	27-10-1994
			DK 621448 T3	27-04-1998
			ES 2107703 T3	01-12-1997
			JP 3347463 B2	20-11-2002
			JP 6313534 A	08-11-1994
			RU 2101610 C1	10-01-1998
			SG 47890 A1	17-04-1998
EP 0770820	A	02-05-1997	AT 206196 T	15-10-2001
			CN 1154160 A	09-07-1997
			DE 69615494 D1	31-10-2001
			DE 69615494 T2	08-05-2002
			DK 770820 T3	26-11-2001
			WO 9636837 A1	21-11-1996
			US 5862762 A	26-01-1999
EP 0805307	A	05-11-1997	WO 9719295 A1	29-05-1997
			JP 2712017 B2	10-02-1998
			JP 9145035 A	06-06-1997
			KR 216426 B1	16-08-1999
US 4510873	A	16-04-1985	JP 1685179 C	31-07-1992
			JP 3046725 B	17-07-1991
			JP 59180213 A	13-10-1984
GB 2348270	A	27-09-2000	WO 0031470 A1	02-06-2000
JP 56025609	A	12-03-1981	JP 1449050 C	11-07-1988
			JP 62055053 B	18-11-1987