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(54) **Method for making a processless lithographic printing plate**

(57) According to the present invention a method is
disclosed for making a negative-working, heat-sensitive
printing plate precursor capable of switching from a hy-
drophilic state into a hydrophobic state upon exposure
to heat and/or infrared light, comprising the steps of (i)

providing a support having a surface comprising titanium,
(ii) modifying said surface by producing an oxide of tita-
nium following the steps of (1) etching said support and
(2) anodizing said etched support.

EP 1 887 424 A1

Description

FIELD OF THE INVENTION

5 **[0001]** The present invention relates to a method for making a negative-working, heat-sensitive printing plate precursor which is suitable for making a lithographic printing plate by direct-to-plate recording.

BACKGROUND OF THE INVENTION

10 **[0002]** Lithographic printing presses use a so-called printing master such as a printing plate which is mounted on a cylinder of the printing press. The master carries a lithographic image on its surface and a print is obtained by applying ink to said image and then transferring the ink from the master onto a receiver material, which is typically paper. In conventional, so-called "wet" lithographic printing, ink as well as an aqueous fountain solution (also called dampening liquid) are supplied to the lithographic image which consists of oleophilic (or hydrophobic, i.e. ink-accepting, water-repelling) areas as well as hydrophilic (or oleophobic, i.e. water-accepting, ink-repelling) areas. In so-called driographic printing, the lithographic image consists of ink-accepting and ink-abhesive (ink-repelling) areas and during driographic printing, only ink is supplied to the master.

15 **[0003]** Printing masters are generally obtained by the image-wise exposure and processing of an imaging material called plate precursor. In addition to the well-known photosensitive, so-called pre-sensitized plates, which are suitable for UV contact exposure through a film mask, also heat-sensitive printing plate precursors have become very popular in the late 1990s. Such thermal materials offer the advantage of daylight stability and are especially used in the so-called computer-to-plate method wherein the plate precursor is directly exposed, i.e. without the use of a film mask. The material is exposed to heat or to infrared light and the generated heat triggers a (physico-)chemical process, such as ablation, polymerization, insolubilization by cross linking of a polymer, heat-induced solubilization, or by particle coagulation of a thermoplastic polymer latex.

25 **[0004]** The most popular thermal plates form an image by a heat-induced solubility difference in an alkaline developer between exposed and non-exposed areas of the coating. The coating typically comprises an oleophilic binder, e.g. a phenolic resin, of which the rate of dissolution in the developer is either reduced (negative working) or increased (positive working) by the image-wise exposure. During processing, the solubility differential leads to the removal of the non-image (non-printing) areas of the coating, thereby revealing the hydrophilic support, while the image (printing) areas of the coating remain on the support. Typical examples of such plates are described in e.g. EP-A 625728, 823327, 825927, 864420, 894622 and 901902. Negative working embodiments of such thermal materials often require a pre-heat step between exposure and development as described in e.g. EP-A 625,728.

30 **[0005]** Some of these thermal processes enable plate making without wet processing and are for example based on ablation of one or more layers of the coating. At the exposed areas the surface of an underlying layer is revealed which has a different affinity towards ink or fountain than the surface of the unexposed coating; the image (printing) and non-image or background (non-printing) areas are obtained.

35 **[0006]** US 5,605,780 discloses a lithographic printing plate comprising an anodized aluminum support and provided thereon an image-forming layer comprising an IR absorbing agent and a cyanoacrylate polymer binder. The image-forming layer is removed by laser-induced thermal ablation whereby the underlying hydrophilic support is revealed.

40 **[0007]** EP-A 580,393 discloses a lithographic printing plate directly imageable by laser discharge, the plate comprising a topmost first layer and a second layer underlying the first layer wherein the first layer is characterized by efficient absorption of infrared radiation and the first and second layer exhibit different affinities for at least one printing liquid.

45 **[0008]** EP 1,065,051 discloses a negative-working heat-sensitive material for making lithographic plates comprising in the order given a lithographic base having a hydrophilic surface, an oleophilic imaging layer and a cross-linked hydrophilic upper layer. The heat generated during exposure in the light-sensitive layer removes the hydrophilic upper layer by ablation.

50 **[0009]** Most ablative plates generate ablation debris which may contaminate the electronics and optics of the exposure device and which needs to be removed from the plate by wiping it with a cleaning solvent, so that ablative plates are often not truly processless. Ablation debris which is deposited onto the plate's surface may also interfere during the printing process and result in for example scumming.

[0010] Other thermal processes which enable plate making without wet processing are for example processes based on a heat-induced hydrophilic/ oleophilic conversion of one or more layers of the coating so that at exposed areas a different affinity towards ink or fountain is created than at the surface of the unexposed coating.

55 **[0011]** US 5,855,173, US 5,839,369 and 5,839,370 describe a method relying on the image-wise hydrophilic-hydrophobic transition of a ceramic such as a zirconia ceramic and the subsequent reverse transition in an image erasure step. This image-wise transition is obtained by exposure to infrared laser irradiation at a wavelength of 1064 nm at high power which induces local ablation and formation of substoichiometric zirconia. US 5,893,328, US 5,836,248 and US

5,836,249 disclose a printing material comprising a composite of zirconia alloy and α -alumina which can be imaged using similar exposure means to cause localized "melting" of the alloy in the exposed areas and thereby creating hydrophobic/oleophilic surfaces. A similar printing material containing an alloy of zirconium oxide and Yttrium oxide is described in US 5,870,956. The high laser power output required in these prior art methods implies the use of expensive exposure devices.

[0012] EP 1,002,643 discloses a printing plate comprising an anodized titanium metal sheet which becomes hydrophilic or ink-repellent upon image-wise exposure to actinic light. Said printing plate can be regenerated after printing by first cleaning the plate and subsequently subjecting the plate to a heat-treatment step whereby the plate surface becomes evenly oleophilic or ink-accepting.

[0013] EP 958,941 discloses a plate precursor having a surface layer comprising Si_3N_4 and/or BN on which an image can be formed after image-wise exposure of the layer to light.

[0014] US 6,240,091 discloses a method of producing a lithographic printing plate by image-wise irradiation of a printing plate precursor which comprises a support having a hydrophilic, metallic compound layer with photo-catalytic properties and light-heat convertible minute particles onto said layer, whereby the polarity of the metallic layer is converted and a hydrophobic area is obtained.

[0015] EP 903,223 discloses a lithographic printing method using a printing plate precursor comprising a surface having a thin layer of TiO_2 , ZnO or a compound selected from the group consisting of RTiO_3 wherein R represents an alkaline earth metal atom, $\text{AB}_{2-x}\text{C}_x\text{D}_{3-x}\text{E}_x\text{O}_{10}$ wherein A represents a hydrogen atom or an alkali metal atom; B represents an alkaline earth metal atom or a lead atom; C represents a rare earth atom; D represents a metal atom of the group 5A of the Periodic Table; E represents a metal atom of the group 4A of the Periodic Table; and x represents a number from 0 to 2, SnO_2 , Bi_2O_3 and Fe_2O_3 . The exposure step with actinic light through a film mask renders the surface hydrophilic at the exposed areas and subsequent heating results in a hydrophilic/hydrophobic conversion.

[0016] US 6,455,222 discloses a lithographic printing plate precursor comprising fine hydrophilic light-heat convertible particles such as inorganic metal oxides including TiO_x ($x=1.0-2.0$), SiO_x ($x=0.6-2.0$) and AlO_x ($x=1.0-2.0$) which are converted from a hydrophilic state into a hydrophobic state by the action of heat.

[0017] A major problem associated with the prior art materials based on metal oxides is that these materials require exposure with high power laser light and/or the use of expensive exposure devices. Other plates based on metal oxides have to undergo a photo-reduction reaction prior to their use to induce a hydrophobic/hydrophilic conversion. This photo-reduction reaction can be initiated by for example a pre-heat treatment step and/or a flood UV-exposure step which have to be performed by the end-user. Such pre-treatment steps make plate making a cumbersome process.

SUMMARY OF THE INVENTION

[0018] It is an object of the present invention to provide a method for making a negative-working, heat-sensitive lithographic printing plate precursor which requires no processing step and which can be directly exposed to heat and/or light by means of a laser with low power output and without the need for a flood UV-exposure pre-treatment.

[0019] According to the present invention there is provided a method for making a negative-working, heat sensitive lithographic printing plate precursor comprising the steps of

- (i) providing a support having a surface comprising titanium,
- (ii) modifying said surface by producing a hydrophilic oxide of titanium by the steps of

- 1) etching said surface and
- 2) anodizing said etched surface,

wherein said oxide of titanium is capable of switching from a hydrophilic state into a hydrophobic state upon exposure to heat and/or infrared light.

[0020] According to the present invention there is further provided a method for making a lithographic printing plate comprising the steps of

- (i) providing a lithographic printing plate precursor according to the present invention;
- (ii) image-wise exposing the precursor to heat and/or infrared light whereby the surface of the precursor switches from a hydrophilic state to a hydrophobic state at exposed areas.

[0021] According to the present invention there is further provided a method of printing comprising the steps of

- (i) providing a lithographic printing plate carrying on the surface a lithographic image according to the method described above;

- (ii) producing a plurality of printed copies by supplying ink to the printing plate and transferring the ink to paper;
 (iii) optionally cleaning the printing plate by removing the ink from the plate;
 (iv) erasing the lithographic image by flood-exposing the printing plate to UV light thereby converting hydrophobic areas of the surface to a hydrophilic state;
 (v) re-using the precursor thus obtained in a next cycle comprising the steps (i) to (iv).

[0022] Preferred embodiments of the present invention are defined in the dependent claims.

DETAILED DESCRIPTION OF THE INVENTION

[0023] According to the method of the present invention, a printing plate precursor having a support with a surface comprising titanium is converted from a hydrophobic state into a hydrophilic state by first etching said support followed by an anodizing step. By irradiation of the hydrophilized surface with heat and/or infrared light, a switch from a hydrophilic state into a hydrophobic state is obtained.

[0024] The support of the printing plate precursor having a surface comprising titanium is preferably a titanium metal sheet. Alternatively, the support is a base onto which a thin layer of titanium metal is applied.

[0025] The titanium metal sheet may be a commercially available titanium metal sheet having preferably a 99.5 %wt to 99.9 %wt purity. Also suitable is an alloy of titanium containing about 4 %wt to 5 %wt of for example aluminium, vanadium, manganese, iron, chromium and molybdenum. The thickness of the titanium metal sheet is not critical: it may be between 0.05 mm to 0.6 mm, preferably from 0.05 mm to 0.4 mm, more preferably from 0.1 mm to 0.3 mm.

[0026] The base onto which a thin layer of titanium is applied may be a metal sheet including for example aluminium, stainless steel, nickel, and copper. Also suitable as a base is a flexible plastic support such as polyester or cellulose ester, waterproof paper, polyethylene-laminated paper, or polyethylene-impregnated paper. The support can also be a laminate comprising an aluminum foil and a plastic layer, e.g. polyester film.

[0027] When a metal sheet is used as a base for the titanium layer, the surface of the metal base may have been roughened by any of the known methods. The surface roughening may be conducted by mechanical means, electrochemical means and chemical etching means, or by combinations of these methods.

[0028] A particularly preferred lithographic support is an electrochemically grained and anodized aluminum support. The grained and anodized aluminum support is preferably grained by electrochemical graining, and anodized by means of anodizing techniques employing phosphoric acid or a sulphuric acid/phosphoric acid mixture. Methods of both graining and anodization of aluminum are very well known in the art.

[0029] By varying the type and/or concentration of the electrolyte and the applied voltage in the graining step, different type of grains can be obtained.

[0030] By anodizing the aluminium support, its abrasion resistance and hydrophilic nature are improved. The micro-structure as well as the thickness of the Al_2O_3 layer are determined by the anodizing step, the anodic weight ($\text{g/m}^2 \text{Al}_2\text{O}_3$ formed on the aluminium surface) varies between 1 and 8 g/m^2 .

[0031] The thin layer of titanium present on the base may be applied by known methods such as for example vapor deposition, spray pyrolysis, sputtering, or electrodeposition. The thickness of the deposited titanium metal layer is preferably from 0.01 μm to 10 μm , more preferably from 0.05 μm to 1.0 μm , most preferably the thickness varies between 0.10 μm and 0.30 μm .

[0032] The titanium sheet or the base provided with a titanium layer may be subjected to a surface roughening step treatment prior to the etching step. Preceding the surface-roughening step, a degreasing step may be conducted with for example a surfactant, an organic solvent or an aqueous alkali solution.

[0033] The surface roughening treatment of the titanium sheet or the base provided with a titanium layer can be conducted by various methods; examples thereof include mechanically roughening (e.g. grinding with balls, brushing, blasting, or buffing), electrochemical dissolution (e.g. surface roughening in an electrolytic solution with application of an AC or DC current) or chemical dissolution (e.g. immersing the metal in an aqueous solution of one or more alkaline salts selected from sodium hydroxide, sodium carbonate, sodium silicate or sodium pyrophosphate). These methods may be used alone or in combination.

[0034] According to a preferred method of the present invention, the anodization of titanium is performed by treatment of the surface comprising titanium with an aqueous electrolyte solution at a concentration of 0.001 mol/l to 5 mol/l, preferably from 0.005 mol/l to 3 mol/l, a liquid temperature of 5°C to 70°C, preferably from 15°C to 30°C, a DC voltage of 1 V to 100 V, preferably 5 V to 50 V, more preferably 10 V to 30 V, and an electrolysis period of 10 seconds to 10 minutes, preferably 1 minute to 8 minutes.

[0035] More preferably, the surface of the support is anodized in an aqueous electrolyte solution containing at least one of the following chemicals:

- an inorganic acid selected from sulfuric acid, phosphoric acid, nitric acid or boric acid;

- hydrogen peroxide in addition to one or more of these inorganic acids;
- an alkali metal salt and/or an alkaline earth metal salt of these inorganic acids;
- an organic acid selected from oxalic acid, tartaric acid, citric acid, acetic acid, lactic acid, succinic acid, glutamic acid, sulfosalicylic acid or naphthalenedisulfonic acid;
- an alkali metal salt and/or an alkaline earth metal salt of these organic acids.
- hydroxides and/or water-soluble carbonates of sodium, potassium, calcium, lithium, and magnesium and/or aqueous alkali solutions such as ammonium hydroxide solution;
- glycerophosphoric acid and the alkali metal salt and/or the alkaline earth metal salt thereof and/or acetic acid and the alkali metal salt and/or the alkaline earth metal salt thereof.

[0036] These aqueous electrolyte solutions may be used alone or in combination. The concentration of the solutions depends on the kind of the electrolyte used for the anodization process.

[0037] In a most preferred embodiment the electrolyte solution comprises oxalic acid at a concentration of 0.6 mol/l, and the anodizing reaction is carried out at room temperature using 20 V DC for a period of 5 minutes.

[0038] Doping the anodized surface with a metal such as platinum, palladium, gold, silver, copper, nickel, iron, or cobalt or a mixture thereof may be advantageous.

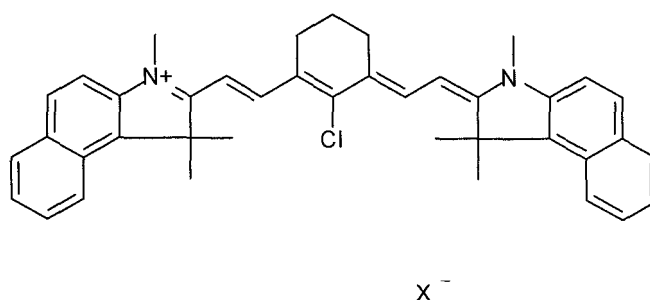
[0039] According to the method of the present invention, prior to the anodization step, the support is etched. Etching of metal surfaces can be done in many ways. For example, aqueous solutions comprising one or more alkaline salts can be used. In a preferred embodiment a mixture comprising H_2O_2 and NaOH is used wherein the concentration of H_2O_2 varies between 0.05 mol/l and 1 mol/l, more preferably between 0.1 mol/l and 0.8 mol/l and the concentration of NaOH varies between 0.1 mol/l and 5 mol/l, more preferably between 0.5 mol/l and 3.5 mol/l. The etching temperature varies preferably between 50 °C and 100 °C, more preferably between 60 °C and 80 °C and the reaction time varies preferably between 0.5 minute and 10 minutes, more preferably between 0.5 minute and 5 minutes. Alternatively, the etching and anodizing step may be carried out in one step. The etched and anodized printing plate precursor may optionally undergo further post-treatments such as chemical reducing treatments e.g. annealing at reduced pressure as defined in the first method, or photolytic reduction e.g. UV-treatment.

[0040] The lithographic printing plate precursor comprising an etched and anodized support thus obtained, may be rinsed with water, with a liquid containing a surfactant or with a desensitizing liquid (so called gum solution) containing gum arabic or a starch derivative, or with combinations thereof.

[0041] The surface of the printing plate precursor is hydrophilic and upon image-wise exposure to heat and/or light, the exposed areas become ink accepting. This conversion from a hydrophilic to a hydrophobic state can for example be characterized by an increase of the contact angle for water measured on the surface: the contact angle for water increases after the treatment of the support indicating a hydrophilic/hydrophobic conversion. The contact angle is defined as the angle between the tangent of the edge of the water droplet at the contact zone between the support and the droplet.

[0042] A layer which comprises a compound capable of absorbing light and converting the absorbed energy into heat may optionally be coated onto the etched and anodized support. The compound capable of absorbing light and converting it into heat is preferably an infrared absorbing agent. Preferred IR absorbing compounds are dyes such as cyanine, merocyanine, indoaniline, oxonol, pyrilium and squarilium dyes or pigments such as carbon black. Examples of suitable IR absorbers are described in e.g. EP-As 823327, 978376, 1029667, 1053868, 1093934; WO 97/39894 and 00/29214.

A preferred compound is the following cyanine dye IR-A:



wherein X^- is a suitable counter ion such as tosylate.

[0043] The coating may in addition to the layer comprising the infrared absorbing agent also contain one or more additional layer(s) such as i.e. a protective layer or an adhesion-improving layer between the layer comprising the infrared absorbing agent and the support.

[0044] Optionally, the layer comprising a compound capable of absorbing light or an optional other layer may further

contain additional ingredients. For example binders, surfactants such as perfluoro surfactants, silicon or titanium dioxide particles or colorants may be present.

[0045] According to the present invention, the heat-sensitive printing plate precursor thus obtained is then image-wise exposed directly with heat or indirectly with infrared light, preferably near infrared light. The infrared light is preferably converted into heat by an IR light absorbing compound as discussed above. The printing plate precursor is not sensitive to ambient light so that it can be handled without the need for a safe light environment.

[0046] The printing plate precursor can be exposed to infrared light by means of e.g. LEDs or an infrared laser. Preferably, the light used for the exposure is a laser emitting near infrared light having a wavelength in the range from about 700 nm to about 1500 nm, e.g. a semiconductor laser diode, a Nd:YAG or a Nd:YLF laser.

[0047] The exposure step may optionally be followed by a rinsing step and/or a gumming step. The gumming step involves post-treatment of the heat-sensitive printing plate with a gum solution. A gum solution is typically an aqueous liquid which comprises one or more surface protective compounds that are capable of protecting the lithographic image of a heat-sensitive material or printing plate against contamination or damaging. Suitable examples of such compounds are film-forming hydrophilic polymers or surfactants.

[0048] According to the present invention, the heat-sensitive printing plate is then ready for printing without an additional development step. The exposed plate can be mounted on a conventional, so-called wet offset printing press in which ink and an aqueous dampening liquid are supplied to the material. The non-image areas hold the dampening water and the image areas withhold the ink.

[0049] Another suitable printing method uses so-called single-fluid ink without a dampening liquid. Suitable single-fluid inks have been described in US 4,045,232; US 4,981,517 and US 6,140,392. In a most preferred embodiment, the single-fluid ink comprises an ink phase, also called the hydrophobic or oleophilic phase, and a polyol phase as described in WO 00/32705.

[0050] Alternatively, the printing plate is first mounted on the printing cylinder of the printing press and then image-wise exposed directly on the press by means of an integrated image-recording device. Subsequent to exposure, the plate is ready for printing.

[0051] The printing plate can be regenerated after printing. After printing, the printing plate is subjected to a flood exposure with UV light whereby hydrophobic areas are converted to a hydrophilic state and recover sensitivity to infrared light and/or heat irradiation. Optionally, before the flood exposure step, a cleaning step may be performed to remove the adherent ink. Suitable solvents that can be used for cleaning include hydrophobic petroleum solvents such as aromatic hydrocarbons commercially available as printing ink solvents: kerosine, benzol, toluol, xylol, acetone, methyl ethyl ketone, and mixtures thereof.

[0052] The regenerated printing plate precursor thus obtained can be used for a next printing operation involving image-wise exposure and printing.

Examples

Example 1.

[0053] A Ti-foil (Goodfellow TI000380 99,6%, 125 μ m foil) was cleaned by ultrasound treatment in isopropanol and was subsequently rinsed with water.

[0054] In a first step, samples of the cleaned Ti-foil (size: 19 cm x 5,5 cm) were etched at 70°C following the various conditions listed in Table 1.

[0055] After the etching step, the different printing plate precursors were anodized at room temperature utilizing a DC voltage of 20 V (Table 1). A titanium counter electrode was used and the distance between the two electrodes was 2.4 cm.

Table 1: Etching and anodizing conditions.

Printing plate precursor (PPP) nr.	Etching conditions			Anodizing conditions	
	Conc. H ₂ O ₂ mol/l	Conc. NaOH Mol/l	Etching time min	Conc. Oxalic acid mol/l	Anodizing time min
PPP 1	-	-	-	0.6	1
PPP 2	-	-	-	0.6	5
PPP 3	0.5	0.5	1	0.6	1
PPP 4	0.1	3.0	4	0.6	1

(continued)

	Etching conditions			Anodizing conditions	
Printing plate precursor (PPP) nr.	Conc. H ₂ O ₂ mol/l	Conc. NaOH Mol/l	Etching time min	Conc. Oxalic acid mol/l	Anodizing time min
PPP 5	0.5	3.0	4	0.6	1
PPP 6	0.5	0.5	1	0.6	5
PPP 7	0.5	3.0	1	0.6	5

[0056] The printing plate precursors 4 - 10 were subsequently exposed with a single beam IR laser diode at 830 nm with a pitch of 7 μ m at different powers and drum speeds. The resulting energy densities are given in Table 2.

Table 2: Energy densities.

Laser Setting	Power MW	Drum speed m/s	Energy density mJ/cm ²
6	280	4	1000
7	200	4	714
8	140	4	500
9	280	8	500
10	200	8	357

[0057] After the laser exposure, the plates were immediately mounted on a ABDick 360 wet offset printing press. Van SON 167 ink (trademark of Van Son) was used together with a fountain solution of 5% G671 (trademark of Agfa-Gevaert) in water. A non-compressible rubber blanket was used and 250 copies were printed on 80 g offset paper. The ink density on the prints were measured using a Gretag Macbeth D19C densitometer (available from Gretag Macbeth AG) and are summarized Table 3 (ink density after 50 prints) and Table 4 (ink density after 250 prints).

Table 3: Ink density after 50 prints.

Printing plate (PP) nr.	Density after 50 prints at laser setting*					
	6	7	8	9	10	Unexposed
PP 1 <i>Comparative</i>	1.15	1.15	1.15	1.15	1.15	1.15
PP 2 <i>Comparative</i>	1.15	1.15	1.15	1.15	1.15	1.15
PP 3 <i>Invention</i>	0.25	0.20	0.15	0.20	0.04	0.02
PP 4 <i>Invention</i>	0.29	0.12	0.05	0.06	0.01	0.005
PP 5 <i>Invention</i>	1.15	1.10	1.15	1.10	1.00	0.04
PP 6 <i>Invention</i>	0.16	0.11	0.08	0.16	0.09	0.05
PP 7 <i>Invention</i>	0.55	0.55	0.5	0.35	0.20	0.015
*: laser setting see Table 2.						

Table 4: Ink density after 250 prints.

Printing plate (PP) nr.	Density after 250 prints at laser setting*					
	6	7	8	9	10	Unexposed
PP 1 <i>Comparative</i>	1.15	1.15	1.15	1.15	1.15	1.15
PP 2 <i>Comparative</i>	1.15	1.15	1.15	1.15	1.15	1.15
PP 3 <i>Invention</i>	0.15	0.15	0.10	0.15	0.03	0.02

(continued)

Printing plate (PP) nr.	Density after 250 prints at laser setting*					
	6	7	8	9	10	Unexposed
PP 4 <i>Invention</i>	0.08	0.01	0.005	0.02	0	0
PP 5 <i>Invention</i>	0.95	0.9	1.05	0.85	0.5	0
PP 6 <i>Invention</i>	0.14	0.07	0.06	0.13	0.06	0.015
PP 7 <i>Invention</i>	0.45	0.35	0.2	0.35	0.01	0
*: laser setting see Table 2.						

[0058] Tables 3 and 4 show that an etching step followed by an anodization step results in a support having a surface with hydrophilic properties. Upon exposure to infrared light, the ink density values increase. The best results are obtained by the "strongest" etching condition i.e. longest reaction time and highest concentration of H₂O₂ and NaOH (see invention printing plate 5). When no etching step is carried out (only an anodization step), the support has a surface with hydrophobic properties (ink density value ≥ 1 ; see comparative printing plates 1 and 2).

Example 2.

[0059] After the printjob, printing plate 5 was cleaned by removing the ink from the plate; the plate cleaner Howson Normakleen RC910 (trademark of Howson Normakleen) was used.

[0060] Subsequently, the plate was irradiated for 24 hours with a mercury lamp emitting at 254 nm at 0.5 mW/cm².

[0061] After the UV-treatment, half of the plate was irradiated with the IR-laser according to Table 2.

[0062] After the laser exposure, the plates were immediately mounted on an ABDick 360 wet offset printing press. Van SON 167 ink was used together with a fountain solution of 5% G671 (trademark of Agfa Graphics NV) in water. A non-compressible rubber blanket was used and the copies were printed on 80 g offset paper.

[0063] The part of the plate which was not irradiated with the IR-laser showed at print 50 ink density values varying between 0.05 and 0.15. The part of the plate which was irradiated with the IR-laser showed ink density values of 1.0. The ink density values were measured using a Gretag Macbeth D19C densitometer (available from Gretag Macbeth). This example shows that flood exposure of the printing plate with UV-light results in a precursor which can be reused in a next cycle of imaging and printing.

Claims

1. A method for making a negative-working, heat sensitive lithographic printing plate precursor comprising the steps of

- (i) providing a support having a surface comprising titanium,
- (ii) modifying said surface by producing a hydrophilic oxide of titanium by the steps of

- 1) etching said surface and
- 2) anodizing said etched surface,

wherein said oxide of titanium is capable of switching from a hydrophilic state into a hydrophobic state upon exposure to heat and/or infrared light.

2. A method according to claim 1 wherein the etching step is carried out by immersing the surface in an aqueous solution comprising one or more alkaline salts for a period of 0.5 to 10 minutes at a temperature between 50 °C and 100 °C.

3. A method according to claims 1 and 2 wherein the anodizing step is carried out by subjecting the surface at room temperature for a period of 1 to 8 minutes in an aqueous electrolyte solution at a concentration of 0.005 mol/l to 3 mol/l to a DC voltage of 10 V to 30 V.

4. A method according to any of the preceding claims further comprising the following step:

(iii) applying onto the etched and anodized support a layer comprising a compound capable of absorbing infrared light and converting the absorbed energy into heat.

5. A method for making a lithographic printing plate comprising the steps of

- (i) providing a lithographic printing plate precursor obtained according to the method of any of the preceding claims;
- (ii) image-wise exposing the precursor to heat and/or infrared light whereby the surface of the precursor switches from a hydrophilic state to a hydrophobic state at exposed areas, thereby producing a lithographic image on said surface.

6. A method according to claim 5 wherein the exposure step is carried out with a laser emitting near infrared light having a wavelength in the range from about 700 nm to about 1500 nm.

7. A lithographic printing method comprising the steps of

- (i) providing a lithographic printing plate according to the method of claim 6;
- (ii) producing a plurality of printed copies by supplying ink to the printing plate and transferring the ink to paper;
- (iii) optionally cleaning the printing plate by removing the ink from the plate;
- (iv) erasing the lithographic image by flood-exposing the printing plate to UV light thereby converting hydrophobic areas of the surface to a hydrophilic state;
- (v) re-using the precursor thus obtained in a next cycle comprising steps (i) to (iv).



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 07 11 8445

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)
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Place of search Munich		Date of completion of the search 17 December 2007	Examiner Vogel, Thomas
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4

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