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(54) **Device for reducing vibrations of sewing machines**

(57) The invention relates to the device for reducing vibrations of sewing machines induced by dynamic forces of the crank mechanism of needle bar (16) and the thread feeder (14) mechanism. At the same time the crank mechanism of needle bar (16) is coupled with the balancing eccentric mechanism (19), whose exit member (193) has a lift several times lower than the lift of needle

bar (16), and its weight is several times higher than the weight of moving parts of the crank mechanism of the needle bar (16) and of the thread feeder (14) mechanism. The vertical component of speed vector of exit member (193) of the balancing eccentric mechanism (19) has an opposite sense with respect to the speed vector of needle bar (16).

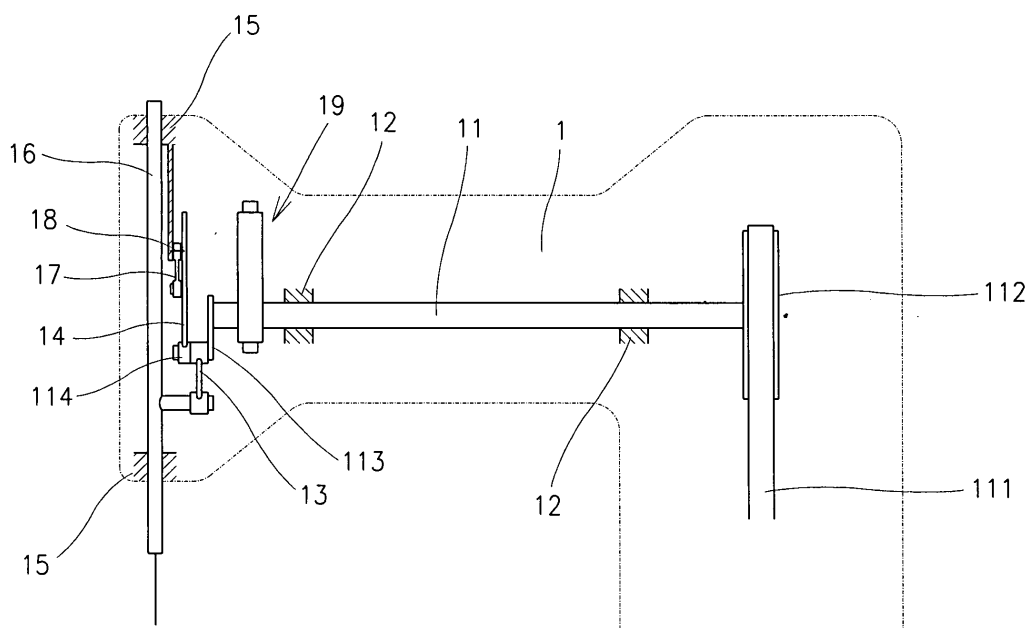


Fig. 1

Description

Technical field

[0001] The device for reducing vibrations of sewing machines induced by dynamic forces of the crank mechanism of needle bar and the thread feeder mechanism.

Background art

[0002] Needle bar of sewing machine is usually driven by a crank mechanism transferring the engine rotational motion driving the machine upper shaft to a straight-line reverse motion of needle bar. Due to high rotation speed of the upper shaft at the current sewing machines the bearing of upper shaft and the arm of sewing machine are loaded by considerable dynamic forces, which are transferred to the whole machine, causing its vibrations and increasing the operational noise of the machine. The dynamic forces are composed of harmonic components of various frequencies. Frequency of the first harmonic component is identical with frequency of rotation of the crank shaft, frequency of the second harmonic component has double value, etc. Balancing of sewing machines is commonly solved by counterweight on the crank shaft only balancing the centrifugal force and partially also the first harmonic component, nevertheless it results in creation of a similar harmonic component in direction being perpendicular to the direction of straight-line reverse motion of the needle bar. The higher harmonic components, whose frequencies are close to resonance frequency of machine arm, remain unbalanced.

[0003] Simple damping of induced vibrations is represented by a flexible mounting of upper shaft by means of spring rings arranged between the bearing outer ring of the upper shaft and the box of arm of the sewing machine according to the JP 8159153, which nevertheless only reduces the result of vibrations already being induced.

[0004] Some solutions in balancing of sewing machines use the principles used at the crank mechanisms of combustion engines.

[0005] According to the JP 7124361 the upper shaft of the sewing machine is coupled by means of toothed gearing with two counter-rotating auxiliary shafts provided with counterweights. According to the used gear ratio between the upper shaft and auxiliary shafts it is possible to balance the first (ratio 1 to 1), or the second harmonic component (ratio 1 to 2).

[0006] To balance the needle bar the JP 8038778 uses a counterweight positioned so that it is turned by 180° with respect to the position of the crank of needle bar mechanism and moreover of an absorbing means positioned in vicinity of the greatest radius of the sewing machine arm.

[0007] According to the JP 8071285 the upper shaft comprises the crankshaft throw turned by 180° with respect to the crank of crankshaft mechanism of needle

bar, while the pin of this throw is inserted in the groove of the damping swing arm rotatably mounted in the frame of sewing machine with pivot axis being parallel with the upper shaft.

[0008] According to the US 5839381 the toothed wheel connected with the upper shaft engages with the counter-rotating additional toothed wheel of the same dimension, while the counterweights of both wheels balance both the vertical inertia forces and the forces induced in the vertical plane being transversal to the upper shaft. This principle is similar to the JP 7124361.

[0009] The tuned vibration absorbers known for example from the sphere of crank mechanisms of combustion engines are effective only in a limited rotation speed range of machine and they partially balance only some harmonic components.

[0010] At many industrial sewing machines the effects of acting of high inertia forces must be reduced by using the machine arm of a high weight.

[0011] Mechanism of the thread feeder is usually formed of four-joint mechanism directly connected with the crank mechanism of needle bar. The main harmonic components of its motion are in motion direction of needle bar similar to harmonic components of needle bar.

[0012] The shortcoming at the known mechanisms for balancing the needle bar and the thread feeder is imperfect balancing or structurally complicated and thus in terms of space and price demanding solution. Due to this majority of sewing machines is produced without balancing devices, which has a negative impact to their operational properties and service life of the machines.

[0013] The goal of this invention is to eliminate the shortcomings of the present background art or to reduce them considerably.

Principle of the invention

[0014] The goal of the invention has been achieved through the device whose principle consists in that the crank mechanism of needle bar is coupled with balancing eccentric mechanism, whose exit member has a lift several times lower than the lift of needle bar and its weight is several times higher than the weight of moving parts of the crank mechanism of the needle bar and of the thread feeder mechanism, while the vertical component of speed vector of exit member of the balancing eccentric mechanism has an opposite sense with respect to the speed vector of needle bar.

[0015] The advantage of a short lift of exit member of the balancing eccentric mechanism lies in that this device is not demanding as to space and it can be guided by flexible members instead of a slide-way.

[0016] It is also advantageous if the balancing eccentric mechanism comprises the first eccentric connected with the upper shaft of sewing machine in a fixed manner and the second eccentric arranged rotatably on perimeter of the first eccentric and simultaneously rotatably mounted in a cavity of exit member of the balancing eccentric

mechanism. At the same time the eccentricity of the first eccentric is turned by 180° with respect to the crank of the needle bar crank mechanism.

[0017] This solution is not only undemanding as to space, but also its production is simple. The balancing means are situated in close vicinity of the needle bar being balanced and due to the fact that the centre of gravity of exit member of the balancing eccentric mechanism is moving in a plane perpendicular to the upper shaft, very good balancing of the thread feeder mechanism is achieved.

[0018] It is also advantageous, if exit member of the balancing eccentric mechanism is flexibly mounted with respect to the arm of the sewing machine by means of spring means. At the same time it is advantageous, if these spring means are formed of two parallel arranged flat springs, while exit member of the balancing eccentric mechanism is fastened between their free ends and their fixed ends are fastened to the frame of the sewing machine.

[0019] Such solution enables an exact guiding of the exit member without play. Moreover the lateral motion of exit member of the balancing eccentric mechanism caused by deformation of the flat springs contributes to balancing of horizontal inertia forces of the thread feeder mechanism.

Description of the drawing

[0020] Exemplary embodiment according to the invention is represented in the drawing where the Fig. 1 shows the side view to arrangement of the upper shaft, crank mechanism of the needle bar, thread feeder mechanism and balancing eccentric mechanism in arm of the sewing machine, the Fig. 2 front view to the crank mechanism of the needle bar, mechanism of the thread feeder and the balancing eccentric mechanism in arm of the sewing machine and the Fig. 3 geometric relations of crank mechanism of the needle bar and the balancing eccentric mechanism.

Examples of embodiment

[0021] The upper part of sewing machine is formed by the arm 1 of sewing machine in whose inner space in longitudinal direction is arranged the upper shaft 11 driven by the non-represented electro-motor by means of the belt 111 and belt pulley 112. The upper shaft 11 is rotatably mounted in bearings 12. On the side reversed from the belt pulley 112 on the upper shaft 11 is attached the crank 113, on whose crank journal 114 there is mounted the upper eye of the conrod 13 and the lower eye of the thread feeder 14. In vertical guiding bearings 15 displaceably is mounted the needle bar 16 with which the lower eye of the conrod 13 is connected rotatably. The upper eye of the thread feeder 14 is rotatably connected with one eye of the conrod 17 of the thread feeder 14 mechanism. The second eye of the conrod 17 is rotatably

mounted on the pin 18, which is firmly connected with frame of the arm 1 of sewing machine. Thus the conrod 17 forms a pitman of four-joint mechanism, whose further members are the frame of the arm 1 of sewing machine, the thread feeder 14 and the crank 113.

[0022] In exemplary embodiment between the bearing 12 of upper shaft 11 being adjacent to the needle bar 16 and the crank 113 the balancing eccentric mechanism 19 is arranged. To it belongs the first eccentric 191 firmly connected with upper shaft 11, while the centre s1 and thus the axis of the outer cylindric surface of the first eccentric 191 intersects the straight line p passing through the axis of the crank journal 114 and the axis of upper shaft 11 outside the join of axes of the crank journal 114 and axis of the upper shaft 11 behind the axis of the upper shaft 11.

[0023] The first eccentric 191 by its outer circumference is rotatably mounted in cylindric cavity of the second eccentric 192, which by its outer circumference is rotatably mounted in cylindric cavity of the exit member 193 of the balancing eccentric mechanism 19.

[0024] The eccentricity r of the first eccentric 191 is given by the distance of axis of the upper shaft 11 and the centre s1 of the first eccentric 191. The eccentricity e of the second eccentric 192 is given by the distance of the centre s2 of the second eccentric 192 and the centre s1 of the first eccentric 191. The eccentricity r of the first eccentric 191 is several times smaller than the length R of the crank 113. Similarly the eccentricity e of the second eccentric 192 is several times smaller than the length l of the conrod 13. In similar ratio the weight of the exit member 193 of the balancing eccentric mechanism 18 is greater than the weight of the needle bar 16.

[0025] The exit member 193 is formed of a flat square body to whose opposite external walls the ends of two flat springs 194 are fastened. Opposite ends of springs are firmly connected with frame of the arm 1 of sewing machine, thus also with frame of the sewing machine. At this solution deformation of the flat springs 194 arising as a result of the side motion of the exit member 193 of the balancing eccentric mechanism 18 may partially balance the horizontal inertia force of mechanism of the thread feeder 14.

[0026] In the not represented embodiment the exit member 193 of the balancing eccentric mechanism 18 is formed of a body of any spatially convenient shape arranged so that its centre of gravity is in direction of axis of the upper shaft 11 as close as possible to centre of gravity of the needle bar 16.

[0027] In another not represented embodiment the exit member 193 of the balancing eccentric mechanism 18 is guided in a straight-lined slide-way, at the same time in direction of this way it may be mounted in a spring manner between two pressure springs.

[0028] Upon rotating of the upper shaft 11 the needle bar 16 performs the working lifts. The size of a whole lift of the needle bar equals to double length of crank R of the crank 113, while the exit member 193 of the balancing

eccentric mechanism 18 performs a lift, which equals to double of eccentricity r of the first eccentric 191. At this activity the cyclic springy deformations of the flat springs 194 occur which the vertical motion of the exit member 193 of the balancing eccentric mechanism 19 enable through their elasticity. At the same time the flat springs 194 generate also the force which reduces the inertia forces between the eccentrics 191, 192 and the exit member 193 of the balancing eccentric mechanism 19.
[0029] The first eccentric 191 in principle balances the centrifugal force of the crank 113, the balancing eccentric mechanism 19 as a whole balances the inertia forces of the needle bar 16, of conrod 13 and partially also the inertia forces of thread feeder 14 mechanism.

[0030] The device for reducing vibrations of sewing machines induced by dynamic forces of the crank mechanism of needle bar 16 and of thread feeder 14 mechanism according to the invention creates an integral unit which can be easily built-in into an arm of the sewing machine 1 with assumption of low acquisition costs, good efficiency and reliability. It is advantageous that the centre of gravity of exit member 193 of the balancing eccentric mechanism 19 is situated in a minimum distance from the needle bar 16. At the same time this centre of gravity moves in a plane perpendicular to the upper shaft 11, through which a better balancing of the thread feeder 14 can be achieved. The balancing eccentric mechanism according to the invention also reduces forces exerting load to bearings of the upper shaft 11.

[0031] It is obvious that the exemplary embodiment does not restrict the scope of protection given by the patent claims. In compliance with the claims for example the external shape of individual parts of the mechanism, type of spring elements for guiding of exit member, geometric parameters, etc. may be modified.

[0032] The invention may be applied at all types of sewing machines using the crank or link mechanism for drive of needle bar. It is especially applicable at industrial high-speed sewing machines.

List of referential markings

[0033]

1	arm of sewing machine
11	upper shaft
111	belt
112	belt pulley
113	crank
114	crank journal
12	bearing
13	conrod
14	thread feeder
15	bearing
16	needle bar
17	conrod (of thread feeder)
18	pin
19	balancing eccentric mechanism

191	first eccentric
192	second eccentric
193	exit member (of balancing eccentric mechanism)
194	flat spring

Claims

1. The device for reducing vibrations of sewing machines induced by dynamic forces of the crank mechanism of needle bar and the thread feeder mechanism, **characterised in that the** crank mechanism of needle bar (16) is coupled with the balancing eccentric mechanism (19), whose exit member (193) has a lift several times lower than the lift of needle bar (16), and its weight is several times higher than the weight of moving parts of the crank mechanism of the needle bar (16) and of the thread feeder (14) mechanism, while the vertical component of speed vector of exit member (193) of the balancing eccentric mechanism (19) has an opposite sense with respect to the speed vector of needle bar (16).
2. The device according to the claim 1, **characterised in that** the balancing eccentric mechanism (19) comprises the first eccentric (191) connected with the upper shaft (11) of sewing machine in a fixed manner and the second eccentric (192) arranged rotatably on perimeter of the first eccentric (191) and simultaneously rotatably mounted in a cavity of exit member (193) of the balancing eccentric mechanism (19).
3. The device according to the claim 2, **characterised in that** the eccentricity (r) of the first eccentric (191) is turned by 180° with respect to the crank (113) of the needle bar (16) crank mechanism.
4. The device according to any of the previous claims, **characterised in that** the exit member (193) of the balancing eccentric mechanism (19) is flexibly mounted with respect to the arm (1) of the sewing machine by means of the spring means, while the size of the lift of the exit member (193) of the balancing eccentric mechanism (19) is within the range of elastic deformation of these spring means.
5. The device according to the claim 4, **characterised in that** the spring means for mounting of the exit member (193) of the balancing eccentric mechanism (19) are formed of parallel arranged flat springs (194), while the exit member (193) of the balancing eccentric mechanism (19) is fastened between their free ends and their fixed ends are fastened to the frame of arm (1) of the sewing machine.

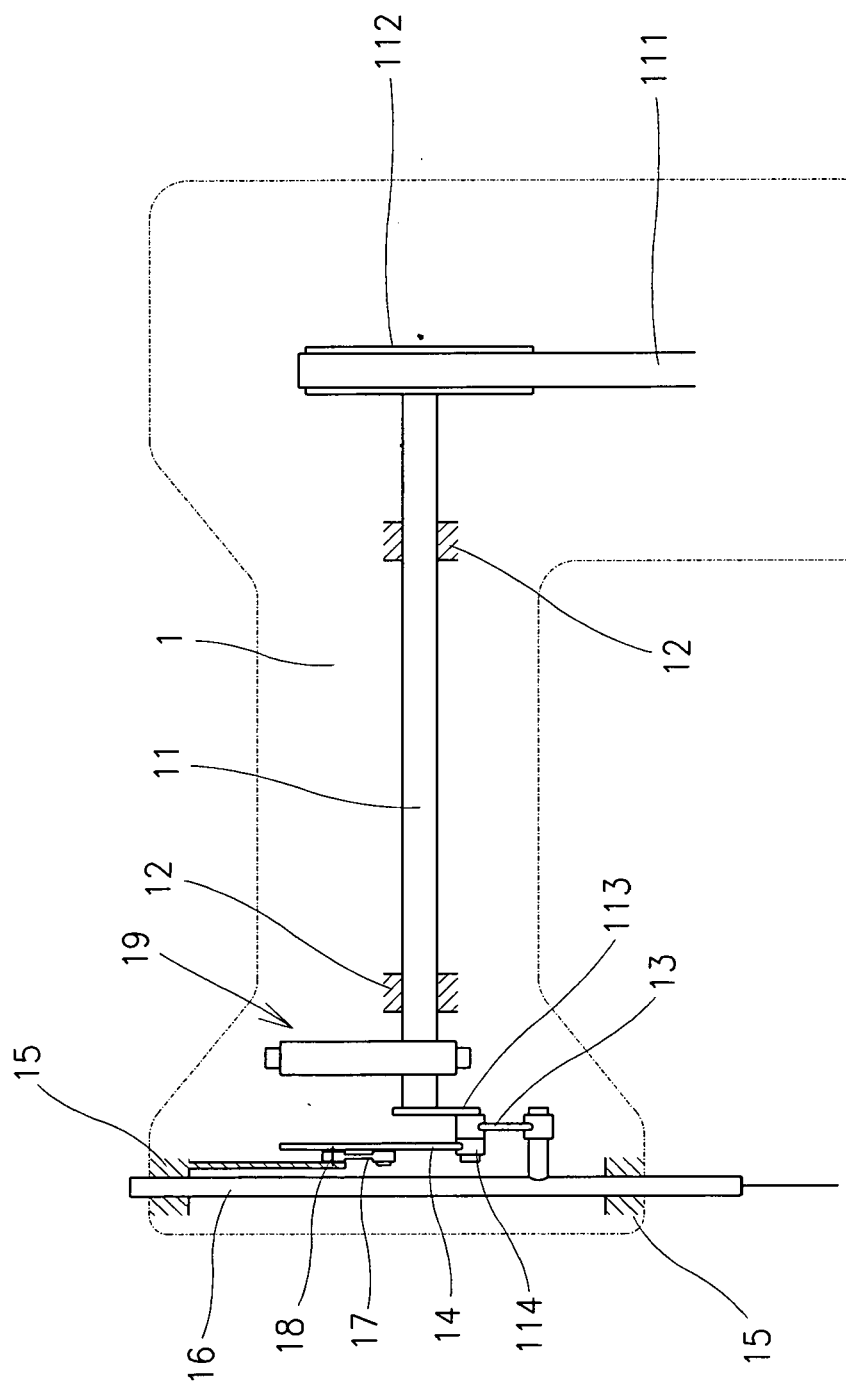


Fig. 1

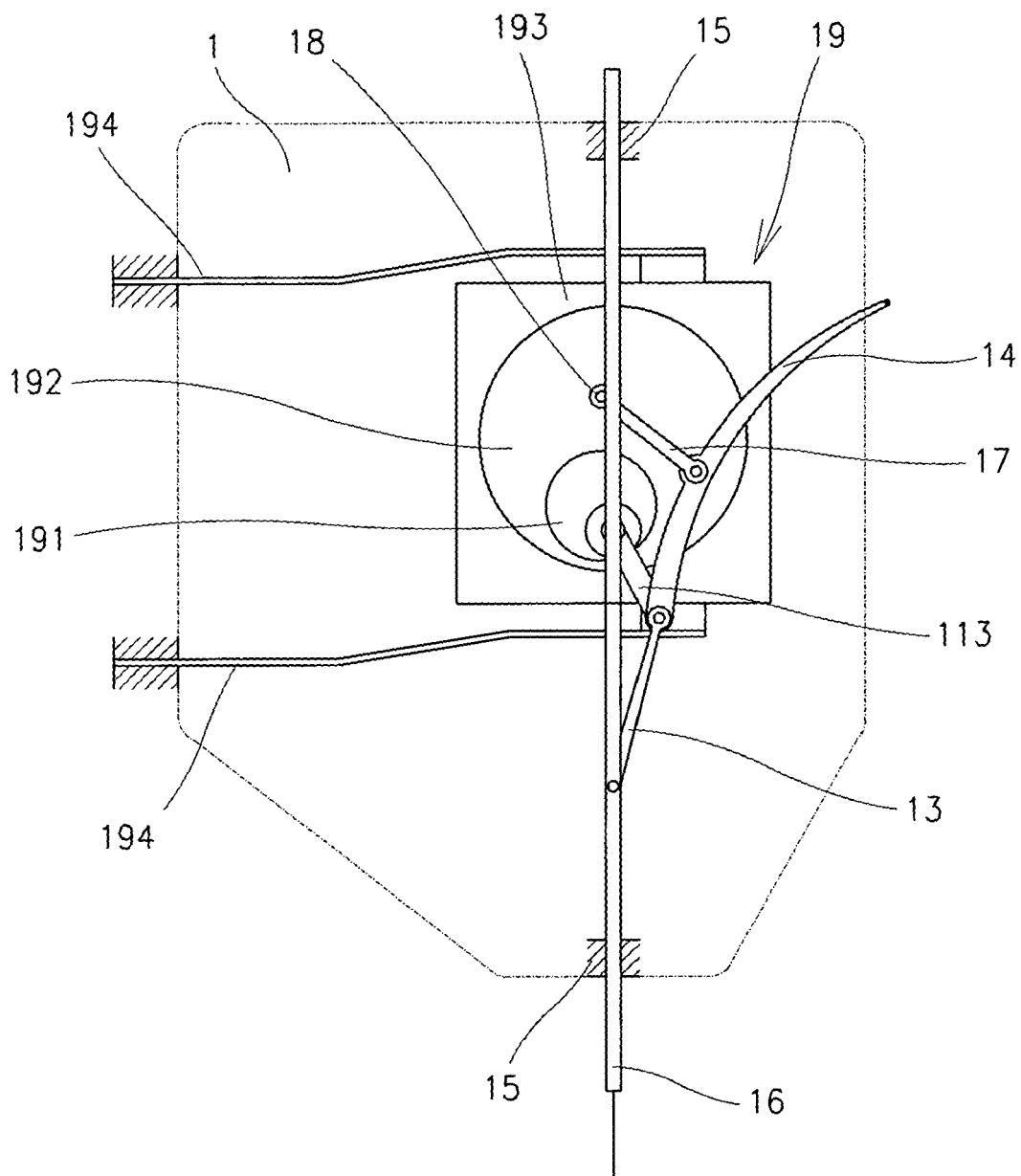


Fig. 2

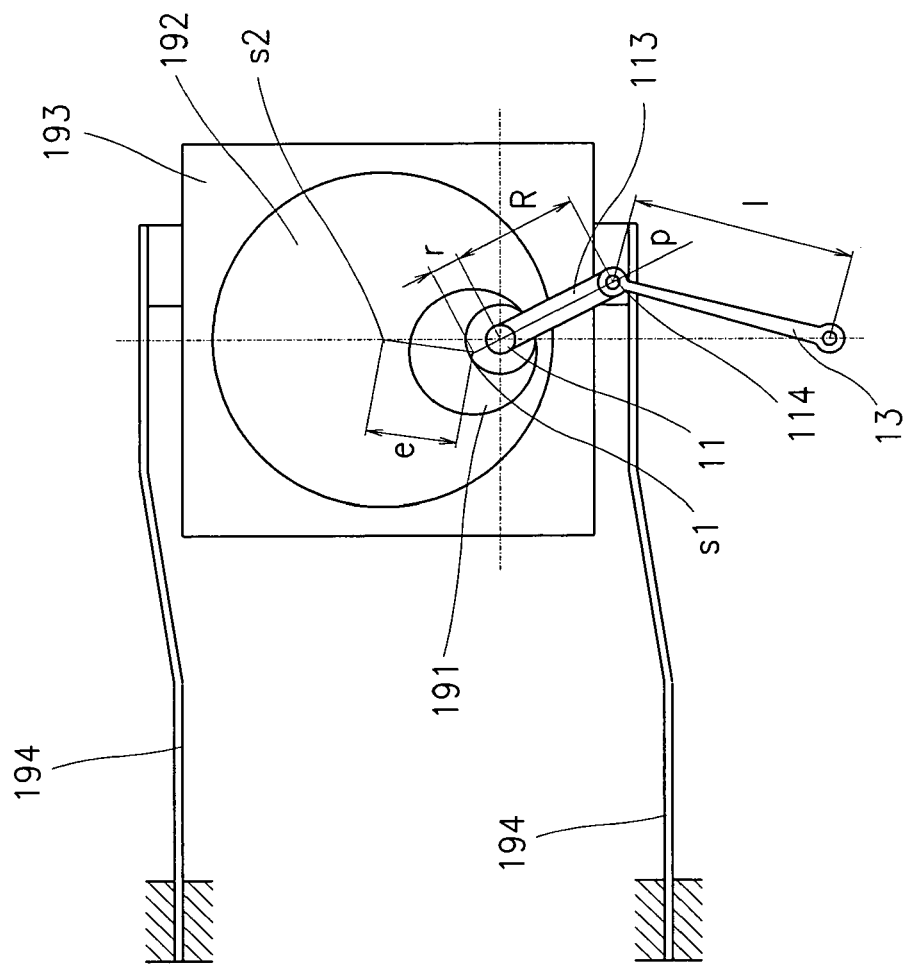


Fig. 3



EUROPEAN SEARCH REPORT

Application Number
EP 08 46 6025

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)
X	DE 43 25 116 C1 (PFAFF AG G M [DE]) 20 October 1994 (1994-10-20)	1-4	INV. D05B69/32
A	* column 3, line 9 - column 6, line 5; figures 1-6 *		
A	----- EP 1 388 601 A (HASHIMA KK [JP]) 11 February 2004 (2004-02-11) * paragraph [0014] - paragraph [0173]; figures 1-29 *	1-6	
P,A	----- EP 1 947 227 A (SUNSTAR PRECISION CO LTD [KR]) 23 July 2008 (2008-07-23) * paragraph [0019] - paragraph [0051]; figures 1-10 *	1-5	
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (IPC)
			D05B
Place of search		Date of completion of the search	Examiner
Munich		22 January 2009	Herry-Martin, D
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			

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EPO FORM 1503 03/82 (P04/C01)

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 08 46 6025

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22-01-2009

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
DE 4325116	C1	20-10-1994	NONE
EP 1388601	A	11-02-2004	CN 1485488 A 31-03-2004
		US 2004055521 A1	25-03-2004
EP 1947227	A	23-07-2008	NONE

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- JP 8159153 B [0003]
- JP 7124361 B [0005] [0008]
- JP 8038778 B [0006]
- JP 8071285 B [0007]
- US 5839381 A [0008]