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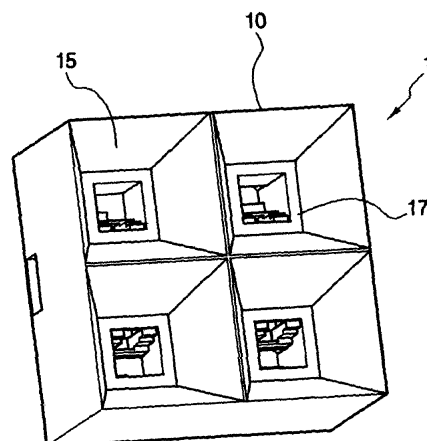
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(54) **Horn array antenna for dual linear polarization**

(57) A horn array antenna (1) for dual linear polarization receiving a first polarization wave and a second polarization wave comprises a plurality of horns (10) to which a mixed wave of the first polarization wave and the second polarization wave enters; a plurality of polarization filtering units (20) provided in each of the horns to separate the incident mixed wave into the first and second polarization waves; a first polarization guide (30) which guides the first polarization waves separated at the polarization filtering units; and a second polarization guide (50) which guides the second polarization waves separated at the polarization filtering units. An upper portion of each polarization filtering unit is formed as a quadrilateral space and each polarization filtering unit has four walls including a first, second, third and fourth walls. A stepped portion (25) is extended from a lower portion of the first wall to an interior of the polarization filtering unit, whereby a lower portion of the polarization filtering unit is formed as a quadrilateral space with a narrower width than that of the upper portion. An extended portion is formed on an upper portion of the stepped portion and a first polarization inlet is formed on the second wall opposite to the first wall to provide the first polarization wave to the first polarization guide.

FIG 2



DescriptionTechnical Field

5 **[0001]** The present invention relates to a horn array antenna for dual linear polarization; more particularly, to a horn array antenna for dual linear polarization for improving the antenna performance and reducing the size of antenna.

Background Art

10 **[0002]** Waves traveling higher than ultrahigh frequency have very short wavelengths and have characteristics similar to light. In order to effectively transmit or receive such waves, the technology has advanced itself to improve the directivity, applying optics theory or the theory that says a megaphone concentrates a sound wave. Such antennas, with enhanced directivity, are being manufactured in various shapes and configurations; they are known as horn antenna, parabola antenna, lens antenna, and slot antenna which have waveguides with holes formed thereon. And the use of these
15 antennas has now become wide.

[0003] Among these, the horn antenna is formed of a waveguide with one end formed in a horn shape and opened at both ends. The horn antenna radiates radio waves by vibrating one end of the waveguide and propagating radio waves along the waveguide. As the impedance between the waveguide and the air is not matching, it reflects a part of the radio wave, which means that the entire energy is not radiated through air. Therefore, a horn antenna is designed
20 to have its waveguide aperture to be gradually wider so that it matches the impedance between the air and the waveguide and allows it to maximally radiate energy through the aperture.

[0004] Fig. 1 is the cross-sectional view of a horn in a horn antenna according to the related art.

[0005] In Fig. 1, the horn antenna shows an external aperture 2 facing the air, and an internal aperture 3 at a side where the vibration starts. In such an antenna, the size of the external aperture 3 decides the performance. The wider
25 the size of the external aperture 3 is, the better the performance is provided. A ratio (S_2/S_1) of the size of the external aperture 2 and that of the internal aperture 3 influences the performance of the antenna. In other words, the difference between the external aperture 2, the internal aperture 3, and the gradient are important factors that decide the performance. So an antenna designed to perform better and to have a long horn usually has a larger size.

30 **[0006]** The present trend of the development of communication technology is towards compactness, and accordingly the demand persists that technology develop a method to reduce the size of an antenna while sustaining its performance.

DisclosureTechnical Problem

35 **[0007]** It is, therefore, an aspect of the present invention to provide a horn array antenna with dual linear polarization having an improved antenna performance and a small size.

40 **[0008]** Other objects and advantages of the present invention can be understood by the following description, which become apparent on reference to the embodiments of the present invention. To those skilled in the art, it is obvious to which the present invention pertains and how the objects and advantages measure up as claimed, and by means of combinations.

Technical Solution

45 **[0009]** In accordance with one aspect of the present invention, there is provided a horn array antenna for dual linear polarization includes a horn, a first polarization guide, and a second polarization guide. The horn guides inputting and outputting radio waves, and includes a inclined section tapered along a propagation direction of a radio wave and having an internal aperture formed at one end having a narrower width and at least one of ledges projected at the end toward an inside of the internal aperture. The first polarization guide is connected to the horn and guides a first polarization.
50 The second polarization guide is connected to the horn, disposed in parallel with the first polarization guide, and guides a second polarization having directivity perpendicular to the first polarization.

[0010] The horn may include: a inclined section formed to be tapered; and a polarization filtering unit connecting the aperture having the ledge of the inclined section with the first polarization guide.

55 **[0011]** A plurality of steps may be formed at one side of the polarization filtering unit so that the width of the polarization filtering unit is gradually narrowed in a direction to the first polarization guide and an aperture may be formed at the region of the plurality of steps to connect with the first polarization guide.

[0012] The ledge may be formed along a circumference of the aperture, and a shape of the ledge may be decided by a width of the ledge projected toward the aperture.

[0013] The shape of the aperture may be a square.

[0014] The first polarization guide may include: a first waveguide having a pair of apertures connected to a pair of the horns; a second waveguide having a pair of apertures connected to other pair of the horns, and disposed in parallel with the first waveguide; and a first mixing pipe disposed between the first waveguide and the second waveguide, connecting the first waveguide and the second waveguide, and having a first main aperture for inputting and outputting a first polarization.

[0015] Each aperture of the first waveguide may be connected to a pair of the polarization filtering units, a first ledge may be downwardly projected from an upper area of a central area of the first waveguide for changing a propagation direction of the first polarization, and a first horizontal layer may be upwardly projected from a lower area of the first ledge for separating or mixing the first polarization.

[0016] Each aperture of the second waveguide may be connected to the other pair of the polarization filtering units, a second ledge may be upwardly projected from a lower area of a central area of the second waveguide for changing a propagation direction of the second polarization, and a second horizontal layer may be downwardly projected at an upper area of the second ledge for separating and mixing the first polarization.

[0017] The first and second ledge may be formed long in a length direction of the first and second waveguides, and formed in a rectangular parallelepiped shape projected toward the inside of the first and second waveguides.

[0018] The first and second horizontal layers may be formed to have a width corresponding to a horizontal width of the first and second waveguides and to have a thickness thinner than a predetermined thickness.

[0019] The first mixing pipe may include: a first main aperture for inputting and outputting a first polarization; a first connecting pipe connected to the first waveguide; and a second connecting pipe connected to the second waveguide.

[0020] The first connecting pipe may be connected to an upper area of a central area of the first waveguide, and may be downwardly bended toward the first mixing pipe at a predetermined angle.

[0021] The second connecting pipe may be connected to a lower area of a central area of the second waveguide, and may be upwardly bended to the first mixing pipe at a predetermined angle.

[0022] A third horizontal layer may be projected in a perpendicular direction of a length direction of the first and second connecting pipe between the first and second connecting pipes of the first mixing pipe.

[0023] The first mixing pipe may include a fifth ledge projected at a predetermined area along a length direction toward an inside of the first mixing pipe so as to reduce a width of the first mixing pipe.

[0024] The second polarization guide may include: a third waveguide connected to a pair of the polarization filtering units for changing a propagation direction of a second polarization; a fourth waveguide connected to the other pair of the polarization filtering units and disposed in parallel with the third waveguide; and a second mixing pipe connected to the third and fourth waveguides and having a second main aperture for inputting and outputting a second polarization.

[0025] Both ends of the third waveguide may be upwardly opened and connected to the polarization filtering units, and a third ledge may be formed at an area penetrating the polarization filtering unit to change a propagation direction of the second polarization. Both ends of the fourth waveguide may be upwardly opened and connected to the polarization filtering units, and a fourth ledge may be formed at an area penetrating the polarization filtering unit and for changing a propagation direction of the second polarization.

[0026] A fourth horizontal layer may extend from a central area of the third waveguide toward the second mixing pipe as much as a predetermined width. A fifth horizontal layer may extend from a central area of the fourth waveguide toward the second mixing pipe as much as a predetermined width.

[0027] An inclined reflecting side may be formed at a side facing the third ledge in both ends of the third waveguide at a predetermined angle. An inclined reflecting side may be formed at a side facing the fourth ledge in the both end of the fourth waveguide at a predetermined angle.

[0028] A sixth horizontal layer may be projected between the third waveguide and the fourth waveguide of the second mixing pipe along a length direction of the third waveguide and the fourth waveguide.

[0029] A rib may be formed at an upper area of the horn to form at least two apertures at the upper are of the horn.

[0030] A ledge may be formed at an opposite side of the plurality of steps.

[0031] In accordance with another aspect of the present invention, there is provided a horn array antenna for dual linear polarization includes a first layer, a second layer, and a third layer. The first layer includes a plurality of horns therein, where each of the horns guides inputting and outputting radio waves, and has a inclined section tapered along a propagation direction of a radio wave and having an internal aperture formed at one end having a narrower width and at least one of ledges projected at the internal aperture toward an inside of the internal aperture. The second layer has a first polarization guide formed therein, where the first polarization guide is connected to the horn and guides a first polarization, and the third layer includes a second polarization guide formed therein, where the second polarization guide is connected to the horn, disposed in parallel with the first polarization guide, and guides a second polarization having a directivity perpendicular to the first polarization.

[0032] The horn array antenna for dual linear polarization may further include a first intermediate layer disposed between the first layer and the second layer and having a polarization filtering unit for connecting the aperture with the

ledge formed and the first polarization guide.

[0033] A width of the polarization filtering unit may be gradually narrowed in a direction to the first polarization guide by a plurality of steps formed at one side of the polarization filtering unit formed at the first intermediate layer. The polarization filtering unit may extend to the second layer so as to be connected to the aperture of the first polarization guide.

[0034] The first polarization guide formed at the second layer may include: a first waveguide having a pair of apertures connected to a pair of the horns; a second waveguide having a pair of aperture connected to the other pair of the horns, and disposed in parallel with the first waveguide; and a first mixing pipe disposed between the first and second waveguides for connecting the first and second waveguides and having a first main aperture for inputting and outputting a first polarization.

[0035] The first horizontal layer of the first waveguide for separating and mixing the first polarization may be formed and a second ledge of the second waveguide for changing a propagation direction of the first polarization may be formed in a side facing the first intermediate layer of the first layer.

[0036] A first ledge of the first waveguide for changing a propagation direction of the first polarization and a second horizontal layer of the second waveguide for separating and mixing the first polarization may be formed in the first intermediate layer.

[0037] A first connecting pipe connecting an upper area of a central area of the first waveguide and the first mixing pipe and downwardly bended to the first mixing pipe at a predetermined angle, and a second connecting pipe connecting an lower area of a central area of the second waveguide and the first mixing pipe and upwardly bended to the first mixing pipe at a predetermined angle are formed at the second layer; and wherein the first mixing pipe is formed at the second layer to be disposed between the first connecting pipe and the second connecting pipe.

[0038] The second polarization guide formed at the third layer may include: a third waveguide connected to a pair of the polarization filtering units and for changing a propagation direction of a second polarization; a fourth waveguide connected to the other pair of the polarization filtering units and disposed in parallel with the third waveguide; and a second mixing pipe connecting the third and fourth waveguides and having a second main aperture for inputting and outputting a second polarization.

[0039] A second intermediate layer having the polarization filtering unit formed therein may be disposed between the second and third layers.

Advantageous Effects

[0040] According to the present invention, the performance of the antenna can be improved while the size of the antenna is reduced.

Description of drawings

[0041] The above and other objects and features of the present invention will become apparent from the following description of the preferred embodiments given in conjunction with the accompanying drawings, in which:

Fig. 1 is the cross-sectional view of a horn in a horn antenna according to the related art;

Fig. 2 is the front view of a dual linear polarization horn array antenna;

Fig. 3 is the side view based on FIG 2;

Fig. 4 is a perspective view of a dual linear polarization horn array antenna according to another embodiment of the present invention;

Fig. 5 is a transparent view of a dual linear polarization horn array antenna shown in Fig. 4;

Fig. 6 is the perspective of a horn array antenna having a horn shown in Fig. 5 according to an embodiment of the present invention.

Fig. 7 is a side cross-sectional view of the horn array antenna;

Fig. 8 is a perspective view of a horn area of a horn array antenna as shown in Fig. 2 (tilted from top);

Fig. 9 is a plane view of a horn;

Figs. 10 and 12 are sectional perspective views of a horn;

Fig. 11 is a front perspective view of a horn.

Fig. 13 is a view of a horn according to another embodiment of the present invention;

Fig. 14 is a plane view of a horn shown in Fig. 13;

Fig. 15 is a side view of a horn shown in Fig. 13;

Fig. 16 is a sectional perspective view of a horn shown in Fig. 13;

Fig. 17 is a side cross sectional view of a horn as shown in Fig. 13;

Fig. 18 is a perspective view of a horn according to another embodiment of the invention;

Fig. 19 shows a schematic cross-sectional view of a horn according to the present embodiment;

Fig. 20 is the schematic side cross-sectional view of a horn having the same-sized external aperture and the same length of horn as shown in Fig. 19;

Fig. 21 is also a schematic side cross-sectional view of a horn having the same performance as shown in Fig. 19;

Fig. 22 is a schematic side cross-sectional view of a horn according to yet another embodiment;

Fig. 23 is a graph showing a parameter S11 of the horn shown in Fig. 19;

Fig. 24 is another graph showing a parameter S11 of the horn shown in Fig. 20;

Fig. 25 is still another showing a parameter S11 of the horn shown in Fig. 21;

Fig. 26 is a magnified perspective view of the polarization filtering unit of Fig. 2;

Fig. 27 shows the S11 parameter of a first port 1;

Fig. 28 shows the S21 parameter between the first port 1 and the second port 2;

Fig. 29 shows the S31 parameter between the first port 1 and the third port 3;

Figs. 30 to 32 are graphs showing S parameters of the second polarization of a polarization-filtering unit shown in Fig. 26;

Fig. 33 is a perspective view of a first polarization guide shown in Fig. 2;

Fig. 34 is a transparent view of a first polarization guide of Fig. 33;

Fig. 35 is the plane view of a first polarization guide of Fig. 33;

Fig. 36 is the side view of a first polarization guide shown in Fig. 33;

Fig. 37 is a perspective view of a first polarization guide connected to a polarization-filtering unit 20;

Fig. 38 is a transparent perspective view of a second waveguide and a second connecting pipe;

Fig. 39 is a perspective view of a first mixing pipe according to the embodiment of the present invention;

Fig. 40 is a perspective view of a first mixing pipe with the fifth ledge removed;

Fig. 41 is a schematic perspective view of a mixing pipe according to another embodiment of the present invention;

Fig. 42 is a schematic perspective view of a mixing pipe according to still another embodiment of the present invention;

Fig. 43 is a graph showing the S11 parameter of the first mixing pipe of Fig. 39;

Fig. 44 is a graph showing the S11 parameter of the first mixing pipe of Fig. 40;

Fig. 45 and Fig. 46 are graphs showing S11 parameter of Fig. 41, and S11 parameter of Fig. 42;

Figs. 47 and 48 are perspective views of a second polarization guide shown in Fig. 2;

Fig. 49 is a cross-sectional perspective view of a second polarization guide of Fig. 2;

Fig. 50 is a perspective view of a second polarization according to the related art;

Figs. 51 and 52 are perspective views of a first polarization guide connected with a second polarization guide according to an embodiment of the present invention;

Fig. 53 is a perspective view of third and fourth waveguides connected with a polarization filtering unit;

Fig. 54 shows radio wave bending units that change propagation direction of magnetic field and electric field at 90° according to another embodiment of the present invention;

Fig. 55 and 56 are diagrams for describing a radio wave bending unit of Fig. 54;

Fig. 57 is the graphical representation showing S11 parameter of Fig. 54;

Fig. 58 is an exploded perspective view of each layer of a dual linear polarization horn array antenna according to an embodiment of the present invention;

Fig. 59 is a perspective view of the first layer of dual linear polarization horn array antenna according to an embodiment of the present invention;

Fig. 60 is a plan view of a first layer shown in Fig. 58;

Fig. 61 is a rear view of a first layer shown in Fig. 58;

Fig. 62 is a perspective view of a first intermediate layer shown in Fig. 58;

Fig. 63 is a plane view of a first intermediate layer shown in Fig. 58;

Fig. 64 is a rear view of a first intermediate layer shown in Fig. 58;

Fig. 65 is a perspective view of a second layer shown in Fig. 58;

Fig. 66 is a plan view of a second layer shown in Fig. 58;

Fig. 67 is a rear view of a second layer shown in Fig. 58;

Fig. 68 is a perspective view of a second intermediate layer shown in Fig. 58;

Fig. 69 is a rear view of a second intermediate layer shown in Fig. 58;

Fig. 70 is a perspective view of a third layer shown in Fig. 58;

Fig. 71 is a plane view of a third layer shown in Fig. 58; and

Fig. 72 is a graphical view of the S11 parameter of a dual linear polarization horn array antenna according to an embodiment of the present invention.

Best Mode for the Invention

[0042] Other objects and aspects of the invention become apparent from the following description of the embodiments

referring to the drawings, set hereinafter.

[0043] A dual linear polarization horn array antenna according to an embodiment of the present invention performs a function of either receiving or transmitting radio waves. For convenience, the constituent elements of the dual linear polarization horn array antenna will be described based on a radio wave receiving function at first. Afterward, the constituent elements will be described based on a radio wave transmitting function thereof.

[0044] According to one embodiment of the present invention, a first polarization denotes a horizontal polarization 'H,' parallel to the equator of earth, and a second polarization denotes a vertical polarization 'V,' which is perpendicular to the equator of earth.

[0045] Fig. 2 is the front view of a dual linear polarization horn array antenna; Fig. 3 is the side view based on FIG 2; and Fig. 7 is a side cross-sectional view of the horn array antenna.

[0046] As shown in Figs. 2, 3 and 7, the dual linear polarization horn array antenna 1 includes a plurality of horns 10 for receiving radio waves, a first polarization guide 30 for guiding first polarization, and a second polarization guide 50 for guiding second polarization. Four of the plurality of horns 10, a first polarization guide 30, and a second polarization guide 50 form one antenna unit. Hereinafter, the dual linear polarization horn array antenna 1 is described based on an antenna unit.

[0047] The four horns 10 are opened toward a space with the first polarization guide 30 disposed under the horns 10, and the second polarization guide 50 disposed under the first guide 30. Herein, the horns 10, the first and the second polarization guides 30 and 50 are spaces for the radio wave to move. The shape of a frame for forming the horn 10, and the first and second polarization guides 30 and 50 will be described later.

[0048] Fig. 4 is a perspective view of a dual linear polarization horn array antenna according to another embodiment of the present invention, and Fig. 5 is a transparent view of a dual linear polarization horn array antenna shown in Fig. 4.

[0049] According to Figs. 4 and 5, a cross rib 401 is disposed at the upper portion of a horn 10, thereby forming four small aperture sides at the upper portion of the horn 10. By dividing the upper portion of the horn 10 to a plurality of aperture sides, the side lobe of an antenna is reduced, and the radiation efficiency increased.

[0050] Although the horn array antenna shown in Fig. 5 includes a horn shown in Fig. 22, it is obvious to those skilled in the art that the horn array antenna may include a horn shown in Fig. 19 or any other horn.

[0051] Fig. 6 is the perspective of a horn array antenna having a horn 10 shown in Fig. 5 according to an embodiment of the present invention. It also shows sixteen apertures are formed in one antenna unit.

[0052] Fig. 8 is a perspective view of a horn area of a horn array antenna as shown in Fig. 2 (tilted from top). Fig. 9 is a plane view of a horn; Figs. 10 and 12 are sectional perspective views, and Fig. 11 is a front perspective view of the horn.

[0053] The horn 10 includes a inclined section 15 formed in a quadrangular pyramid for guiding radio waves for the first polarization and the second polarization, perpendicular to each other, to input into an incident plane thereof, and a polarization filtering unit 20 formed at one end of the inclined section 15.

[0054] The inclined section 15 is tapered in a propagation direction of a radio wave. The inclined section 15 has both ends opened along the propagation direction of a radio wave, thereby forming both external and internal apertures. The internal aperture is formed at a narrower end of the inclined section 15, in a rectangular shape, and a ledge 17 is formed around the internal aperture, which is projected from the internal aperture toward the center area thereof. As shown in Fig. 9, the ledge 17 is projected along the internal aperture to have a predetermined width, forming a rectangular aperture.

[0055] Fig. 13 is a perspective view of a horn according to another embodiment of the present invention. Fig. 14 is a plane view of a horn shown in Fig. 13. Fig. 15 is a side view of a horn shown in Fig. 13. Fig. 16 is a sectional perspective view of a horn shown in Fig. 13, and Fig. 17 is a side cross sectional view of a horn as shown in Fig. 13.

[0056] Referring to Figs. 13 to 17, a horn 10 according to an embodiment of the present invention includes at least one of ledges 18a and 18b disposed at a tapered portion thereof, and a cross rib 401 forming four apertures. Also, a ledge 19 is formed on one side of the polarization filtering unit 20, thereby improving a parameter S11 of a vertical polarization.

[0057] In the present embodiment, the horn 10 contains two ledge 18a, 18b, 19 and a cross rib 401 for forming four apertures. However, the horn 10 is not limited thereto. The number of ledges 18a, 18b, 19 and apertures can change.

[0058] Fig. 18 is a perspective view of a horn according to another embodiment of the invention. Referring to Fig. 18, the horn holds at least one ledges 18a, 18b disposed at a tapered portion and a cross rib 401 for forming four apertures.

[0059] Fig. 19 shows a schematic cross-sectional view of a horn according to the present embodiment. Fig. 20 is the side cross-sectional view of a horn having the same-sized external aperture and the same length of horn as shown in Fig. 19. Fig. 21 is also a schematic side cross-sectional view of a horn having the same performance.

[0060] The length of the horn 110 shown in Fig. 20 and the horn 10 of present embodiment are each about 61.0 mm, and the length of the horn 210 shown in Fig. 21 is about 71.0 mm. The widths of the external apertures of each horn 10, 110, 210 are about 48.0 mm.

[0061] Table 1 shows results of comparing antenna gains of three horns 10, 110, 210 under conditions of the center frequency of 11.7GHz; the upper sideband of 12.75GHz, the lower sideband of 10.7GHz among a satellite broadcasting band KU band from about 10.7GHz to about 12.75GHz.

Table 1

	present embodiment	Fig. 20	Fig. 21
10.7GHz	14.8[dBi]	14.3[dBi]	14.8[dBi]
11.7GHz	15.8[dBi]	15.1[dBi]	15.8[dBi]
12.7GHz	16.1[dBi]	15.6[dBi]	16.1[dBi]

[0062] As shown in Table 1, the horn 10 according to the present embodiment and the horn 210 shown in Fig. 21 provide the same performance at all frequency bands. However, the horn having the same-sized external apertures and the same length horns 10 provide a smaller antenna gain than the horn 110 of Fig. 20 as much as about 0.5dBi at 10.7 GHz band, 0.7dBi at 11.7 GHz band, and 0.5dBi at 12.7GHz band. In case of 1dBi of the antenna gain difference, the antenna performance will improve at 33% in general. Therefore, the performance of the horn 10 is improved at about 18% compared with that of the conventional horn. The height also is reduced by 10 mm compared with a conventional horn having the same performance.

[0063] Fig. 22 is a schematic side cross-sectional view of a horn according to yet another embodiment.

[0064] Referring to Fig. 22, a pair of ledges '318a and 318b' is formed at the tapered portion of inside horn 310. With at least one of ledges '318a or 318b' formed, the height of the horn antenna can be reduced while sustaining the performance of a horn antenna. The length and the size of a horn as of Fig. 22 may differ from those of the horn in Fig. 19.

[0065] Fig. 23 is a graph showing a parameter S11 of the horn shown in Fig. 19; Fig. 24 is another graph showing a parameter S11 of the horn shown in Fig. 20, and Fig. 25 is still another showing a parameter S11 of the horn shown in Fig. 21.

[0066] The parameter S11 shows a tendency that a radio wave returns to an antenna after the radio wave is radiated from the antenna. The lower the parameter S11 is, the better the performance is. In general, the parameter S11 is allowable when the parameter S11 is lower than -10 dB.

[0067] As the horn 10 according to the present embodiment provides the parameter S11 lower than -40dB at about 11.6GHz, the parameter S11 of the horn 10 is in good condition. As such, the horn 10 provides the better parameter S11 than the horn shown in Fig. 20, which provides about -50dB of parameter S11 at 12.2GHz, or not worse than the horn shown in Fig. 21 providing about -30dB of S11 parameter.

[0068] As shown, by forming the ledge 17 at the internal aperture of the inclined section 15, the length of the horn 15 can be shortened not only while sustaining the width of the internal aperture and the width of the external aperture but also while not reducing the gain of the antenna 1.

[0069] The polarization filtering unit 20, connected to the internal aperture of the inclined section 15, passes only a predetermined polarization. As the first polarization cannot pass the polarization filtering unit 20, it is guided to the first polarization guide 30. The second polarization passes the area of a step difference 25 in the polarization filtering unit 20, thereby guiding to the second polarization guide 50.

[0070] Fig. 26 is a magnified perspective view of the polarization-filtering unit shown in Fig. 2.

[0071] Referring to Fig. 26, the polarization filtering unit 20 includes a first port 1 connected to the horn 10; a second port 2 connected to the first polarization guide 30; and a third port 3 connected to the second polarization guide 50.

[0072] The polarization filtering unit 20 extends from the internal aperture to the second polarization guide 50, and has one side with a plurality of steps 25 formed at a predetermined region thereon from the internal aperture. The region of the steps 25 makes the width of the filtering unit to be gradually narrower. The region of steps 25 separate the first and the second polarization passing the polarization-filtering unit 20 providing the first polarization to the first polarization guide 30 and the second to the second polarization guide 50. The first polarization, with an electric field direction identical to the 'wider width' of the polarization filtering unit 20, is given to the first polarization guide 30, and the second polarization, with an electric field direction identical to the 'narrow width' of the polarization filtering unit 20, is given to the second polarization guide 50 along the polarization-filtering unit 20. The number, the size, and the length of the step differences 25 may change according to the frequency of the second polarization guided along the second polarization guide 50.

[0073] Meanwhile, a passage 27, to be connected to the first polarization guide 30, is formed at the central area of the stepped region 25, gradually widening toward the first polarization 30 along the direction of length. The width, the length, and the height of the step difference, forming the passage 27, may change according to the frequency of the first polarization provided to the first polarization guide 30.

[0074] Figs. 27 to 29 are graphs showing S parameters of the first polarization of a polarization-filtering unit as in Fig. 26. Fig. 27 shows the S11 parameter of a first port 1; Fig. 28 shows the S21 parameter between the first port 1 and the second port 2; and Fig. 29 shows the S31 parameter between the first port 1 and the third port 3.

[0075] The first polarization, according to the graph, has about -24 dB of the S11 parameter at 10.7GHz, and has the

high S21 parameter identical to the S11 at the same frequency band. That is, according to the graphs, the first polarization inputs through the first port, and outputs through the second port.

[0076] Figs. 30 to 32 are graphs showing S parameters of the second polarization of a polarization-filtering unit shown in Fig. 26. Fig. 30 shows the S11 parameter of a first port 1, whereas Fig. 31 shows the S21 parameter between a first port 1 and a second port 2, and Fig. 29, the S31 parameter between the first port 1 and the third port 3.

[0077] As graph shows, the second polarization has the S11 parameter gradually decreasing as the frequency band increases, and that the S11 parameter of the second polarization lessens to more than -10 dB throughout the region of the satellite broadcasting. As the frequency band increases, the S31 parameter increases. That is, the second polarization inputs from the first port and outputs through the third port.

[0078] Fig. 33 is a perspective view of a first polarization guide shown in Fig. 2, and Fig. 34 is a transparent view of a first polarization guide of Fig. 33. Fig. 35 is the plane view of a first polarization guide of Fig. 33, and Fig. 36 is the side view of a first polarization guide shown in Fig. 33. Fig. 37 is a perspective view of a first polarization guide connected to a polarization-filtering unit, and Fig. 38 is a transparent perspective view of a second waveguide and a second connecting pipe.

[0079] As shown in Fig. 33, the first polarization guide 30 guides the first polarization inputted through the four horns 10, and outputs the first polarization to a first main aperture 46. The first polarization guide 30 has four apertures A, B, C, and D connected to the four polarization-filtering units 20,

[0080] The first polarization guide 30 includes a first waveguide 35 with a pair of apertures, and a second waveguide 40 with a pair of apertures arranged in parallel with the first waveguide 35. It also has a first mixing pipe 45 connected to the first waveguide 35 and the second waveguide 40 outputting the first polarization.

[0081] Apertures are formed at both ends of the first waveguide 35 and the second waveguide 40, each of them connected to the passage 27 of the polarization-filtering unit 30. In other words, the first polarization guide 30 is connected to the four polarization-filtering units 20 for receiving the first polarization inputting through the four inclined sections 15.

[0082] The first waveguide 35 includes a first ledge 36 and a first horizontal layer 37. The first ledge 36 is formed at the central area along the length direction, and the first horizontal layer 37 is formed for mixing the first polarizations inputted from both apertures. The first ledge 36, formed at the upper area of the first waveguide 35, has a rectangular parallel-piped shape along the length direction of the first waveguide 35. The first polarization inputted to the first waveguide 35, according to Fig. 36, has horizontal directivity components of aperture, making the first ledge 35 change the propagation direction of the first polarization inputting the first connecting pipe 48 to have up and down directivity components.

[0083] As shown in Figs. 34 and 36, the first horizontal layer 37 is upwardly projected from a corresponding location of the bottom side of the first waveguide 35, extending to the bottom of the first ledge 36. The width of the first horizontal layer 37 is identical to the width of the aperture, and the thickness thereof is thinner than a predetermined thickness.

[0084] As shown in Fig. 36, the first polarizations inputting through both the apertures reach the first horizontal layer 37, mixed with each other, changing the propagation direction thereof by the first ledge 36, and propagating toward the first mixing pipe 45.

[0085] The second waveguide 40 is formed in a shape of the first waveguide 35, turned upside down. The second waveguide 40 includes a second ledge 41 formed at a central area thereof and a second horizontal layer 42 for mixing the first polarizations inputted through both apertures. Unlike the first waveguide 35, the second ledge 41 is formed at the bottom area of the second waveguide 40, and the second horizontal layer 42 is formed at the upper area of the second waveguide 40. The structuring of the first waveguide 35 and the second waveguide 41 designed to be opposite in the up and down direction, as described above, prevents the phase of the first polarization from the first waveguide 35 from being opposite from the phase of the first polarization from the second waveguide 40. It also prevents the first polarization from the first waveguide 35 and the first polarization from the second waveguide 40 from being attenuated.

[0086] As shown Fig. 36, the first polarization inputting to the second waveguide 40 is mixed at the second horizontal layer 42, formed at the upper portion of the second waveguide 40, changing the propagation direction thereof by the second ledge 41 and propagating to the first mixing pipe 45.

[0087] The thickness and length of the first and second horizontal layers 37 and 42 as well as the thickness and length of the first and second ledges 36, and 41 is decided according to the frequency of the first polarization inputting to the first waveguide 35 and the second waveguide 40.

[0088] The first mixing pipe 45 has a first connecting pipe 48 connected to the first waveguide 35, a second connecting pipe 49 connected to the second waveguide 40, and a first main aperture 46 for outputting the first polarization from the first and second connecting pipes 48 and 49.

[0089] The first connecting pipe 48 is connected to the upper portion of the central area of the first waveguide 35, extending in parallel with the first waveguide 35 and bending downwardly to a third horizontal layer 47 of the first mixing pipe 45 at a predetermined angle. Meanwhile, the second connecting pipe 49 connected to the bottom of the central area of the second waveguide 40, extends in parallel with the second waveguide 40, and bends upwardly toward the third horizontal layer 47 of the first mixing pipe 45 at a predetermined angle.

[0090] The first mixing pipe 45 is formed in the horizontal direction, which is the length direction of the first and the second connecting pipes 48 and 49. The third horizontal layer 47 is projected along the length direction of the first mixing pipe 45 at one end adjacent to the first and second connecting pipes 48 and 49. Then, a pair of fifth ledges 44 is internally projected from both walls of the first mixing pipe 45 at a predetermined area thereof along the length direction of the first mixing pipe 45 to reduce the width of the first mixing pipe 45. When the first polarizations inputted from the first and the second connecting pipes 49 reach the first mixing pipe 45, the first polarizations mix together at the third horizontal layer 47 for outputting through the first main aperture 46.

[0091] According to the length and thickness of the third horizontal layer 37 and a pair of the fifth ledges 44, the center frequency of a signal inputted to the first mixing pipe 45 is decided. By controlling the length and thickness of the third horizontal layer 37 and the pair of fifth ledges 44, the center frequency of a signal inputted to the first mixing pipe 45 can be shifted. The performance of the first mixing pipe 45 depends on the presence or the non-presence of the pair of fifth ledges 44.

[0092] Hereinafter, a mixing pipe according to an embodiment of the present invention will be described with reference to Fig. 39 to 42. For convenience, a PORT 2-3 passage between a second port 2 to a third port 3 denotes a passage formed between the second port 2 and the third port 3 which face one another, and a PORT 1 passage denotes a passage formed between the first port 1 to the junction of the PORT 2-3 passage, as shown in Figs. 39, 40 and 41.

[0093] Fig. 39 is a perspective view of a first mixing pipe according to the embodiment of the present invention, and Fig. 40 is a perspective view of a first mixing pipe with the fifth ledge removed.

[0094] Referring to Fig. 39, a pair of fifth ledges 44 is projected to the inside of the first mixing pipe 45 from a predetermined area along the length direction of the PORT 1 passage in order to reduce the left-right width of the port 1 passage of the first mixing pipe 45, which is the width of the longer side of the PORT 1 passage of Fig. 39.

[0095] Fig. 43 is a graph showing the S11 parameter of the first mixing pipe of Fig. 39, and Fig. 44 is a graph showing the S11 parameter of the first mixing pipe of Fig. 40. Herein, a side connected to the first connecting pipe 48 and another side connected to the second connecting pipe 49 are defined as a second port and a third port, and a first port is defined as the first main aperture 46.

[0096] As shown in Fig. 43, the first mixing pipe 45 has about -29dB of S11 parameter at 11.75GHz. It denotes that the amount of reflecting a radio wave outputted or inputted through the first port 1 is less. As in Fig. 44, the first mixing pipe with a pair of fifth ledges 44 removed has about -18dB of the S11 parameter at the same frequency band. It denotes that the fifth ledges improve the performance of the first mixing pipe 45.

[0097] Fig. 41 is a schematic perspective view of a mixing pipe according to another embodiment of the present invention, and Fig. 42 is a schematic perspective view of a mixing pipe according to still another embodiment of the present invention. Fig. 45 and Fig. 46 are graphs showing S11 parameter of Fig. 41, and S11 parameter of Fig. 45.

[0098] Fig. 41 shows a pair of sixth ledges 51 projected from a predetermined area to the inside of the mixing pipe along the length direction of the PORT 1 passage, and that the pair is formed to reduce the width of the up-down side of the mixing pipe, that is, the width of the short side of the PORT 1 passage shown in Fig. 41. A pair of grooves 52 is also formed in the length direction of the PORT 2-3 passage, especially showing that it is externally concaved to be adjacent to the horizontal layer 47. Referring to Fig. 45, the mixing pipe of Fig. 41 according to an embodiment of the present invention has about -32 dB of the S11 parameter at 11.75GHz.

[0099] Referring to Fig. 42, seventh ledges 54a and 54b are formed at predetermined areas of the PORT 2-3 passage. More clearly, the seventh ledge 54a is projected from a predetermined area to the inside of the mixing pipe especially, in a direction that reduces the short direction of the PORT 2-3 passage. Whereas, the seventh ledge 54b is formed to be projected from an area adjacent to the junction of the PORT 1 passage including the PORT 2-3 passages into the inside of the mixing pipe. The seventh ledge 54b formed in that direction reduces the short side direction of the PORT 2-3 passage.

[0100] The mixing pipe, as shown in Figs. 39, 41, and 42, divides radio wave inputted from one port, i.e., the first port 1, into two ports, i.e., the second and third ports 2 and 3, or gathers radio waves inputted from two ports, i.e., the second and third ports 2 and 3, to one port, i.e., the first port 1. Therefore, the mixing pipe shown in Figs. 39, 41, and 42 is used as a function that receives two radio waves and gathers the received radio waves, or receives one radio waves and divides the received radio wave into two radio waves.

[0101] Figs. 47 and 48 are perspective views of a second polarization guide 50 shown in Fig. 2, Fig. 49 is a cross-sectional perspective view of a second polarization guide 50 of Fig. 2, and Fig. 50 is a perspective view of a second polarization guide 50 according to the related art.

[0102] The second polarization guide 50 is disposed in parallel with the first polarization guide 30. The second polarization guide 50 receives the second polarization received through the polarization filtering unit 20 and outputs the received second polarization.

[0103] The second polarization guide 50 includes a third waveguide 55 changing the propagation direction of the second polarization, a fourth waveguide 60 disposed in parallel with the third waveguide 55, and a second mixing pipe 65 having a second main aperture connected to the third and fourth waveguides 55 and 60 for outputting the second

polarization.

[0104] The second and fourth waveguides 55 and 60 have both ends upwardly opened and connected to the polarization-filtering unit 20. The third and fourth waveguides 55 and 60 are disposed both perpendicularly from the first and second waveguides 35 and 40 and in a direction to connect the first waveguide 35 and the second waveguide 40.

[0105] A third ledge 56 is formed at both ends of the third waveguide 55 where it communicates with the polarization-filtering unit 20. The third ledge 56 is formed in a rectangular parallel-piped shape along the length direction of the third waveguide 55, and projected upwardly from the bottom side of the third waveguide 55. The second polarization with the electric field direction along the narrow width of the polarization-filtering unit 20 reaches the third ledge 56, thereby changing the propagation direction.

[0106] A side facing the third ledge 56 is formed of a reflecting side 57 inclined at a predetermined angle. After the second polarization changes the propagation direction thereof at the third ledge 56, the second polarization is reflected by the reflecting side 57.

[0107] A fourth horizontal layer 58 extends from the central area of the third waveguide 55 in a horizontal direction of a length direction toward the second mixing pipe 65 as much as the predetermined width. The second polarizations reflected from the reflecting sides 57 at both ends of the third waveguide 55 are mixed at the fourth horizontal layer 58 and propagated to the second mixing pipe 65.

[0108] The fourth waveguide 60 is formed in a shape identical to the third waveguide 55. That is, a fourth ledge 61 is formed at both ends of the fourth waveguide 60 where it communicates with the polarization-filtering unit 20. A reflecting side 62 is formed at a side facing the fourth ledge 61 of the fourth waveguide 60. A fifth horizontal layer 63 extends from the central area of the fourth waveguide 60 in perpendicular to the length direction of the fourth waveguide 60 as much as a predetermined width.

[0109] A second polarization inputting to the fourth waveguide 60 changes the propagation direction thereof by the fourth ledge 61, and reflects from the reflecting side 62, thereby propagating to the fifth horizontal layer 63. Herein, the frequency of the second polarization inputted and outputted to/from the second polarization guide 50 can be controlled on the thickness and length of the fourth and fifth horizontal layers 58 and 63, and on the width and height of the reflecting sides 57 and 62.

[0110] Figs. 51 and 52 are perspective views of a first polarization guide connected with a second polarization guide from different angles.

[0111] As shown, the first polarization guide is vertically coupled to the second polarization guide.

[0112] Fig. 53 is a perspective view of third and fourth waveguides connected with a polarization filtering unit.

[0113] As shown, the polarization-filtering unit 20 is formed in a rectangular passage, and the second polarization is formed in an electric field direction along a narrow width of the polarization-filtering unit 20. The cross-sections of the third and fourth waveguides 55 and 60 connected to the polarization filtering unit 20 are formed in a narrow rectangular shape. Accordingly, the second polarization shifts the electric direction into top and bottom directions when the second polarization meets the third and the fourth ledges 56, and 61. The propagation direction usually changes at 90°. Therefore, the part shown in Fig. 53 is called a radio wave bending unit.

[0114] Meanwhile, the second mixing pipe 65 is formed between the third waveguide 55 and the fourth waveguide 60 parallel to the third and fourth waveguides 55 and 60, and the second mixing pipe 65 is disposed at the right angle to the first mixing pipe 45. A second main aperture 66, therefore, formed at one end of the second mixing pipe 65 is at the right angle to the first main aperture 46. A sixth horizontal layer 67 is formed at one end facing the second main aperture 66 of the second mixing pipe 65, projecting along the length direction of the third and fourth waveguides 55 and 60. The second polarizations from the third and fourth waveguides 55 and 60 get mixed at the sixth horizontal layer 67, and the mixed second polarization propagates toward the second main aperture 66.

[0115] Similar to the first mixing pipe 45, the second mixing pipe 65 can change the frequency band of an inputting and outputting signal according to the length and thickness of the sixth horizontal layer 67 and a pair of ledges 64. Since the second polarization guide 50 includes the ledge 53, the antenna performance can be improved as shown in S11 parameter of Fig. 43.

[0116] According to Fig. 50, the conventional second polarization guide has a narrow horizontal width compared to the height thereof. The conventional second polarization guide, on the other hand, is formed to comparatively have a higher height. The second polarization guide 50 according to the present embodiment shown in Fig. 47 has a lower height compared to a horizontal width. For example, the second polarization guide 50 according to the present embodiment has 50% of the height of the conventional second polarization guide. Therefore, the height of the second polarization guide 50 can be reduced, and the overall size of the antenna 1 can be miniaturized.

[0117] Fig. 54 shows radio wave bending units that change propagation direction of magnetic field and electric field at 90° according to another embodiment of the present invention. Fig. 55 is a diagram for describing a radio wave bending unit of Fig. 54, and Fig. 57 is the graphical representation showing S11 parameter of Fig. 54.

[0118] The radio wave bending unit as shown Fig. 54 can be used at the junction area of both ends of the third and fourth waveguides 55 and 60 and the polarization-filtering unit 20. The unit can also be used to change the magnetic

field and the electric field at 90°. Referring to Fig. 57, the radio wave bending unit has good S11 parameter.

[0119] The structures shown in Fig. 55 and 56, as mentioned earlier, can change the electric field at 90° and the magnetic field at 90° respectively, according to the present embodiment.

[0120] Hereinafter, the operations of the Dual Linear Polarization Horn Antenna, with the structures for separating and receiving the first polarization and the second polarization, will be described.

[0121] At first, when the horn 10 receives the radio wave, it guides the radio wave along the inclined section 14, through the ledge 17, and to the polarization-filtering unit 20. Then, the plurality of step differences 25 gradually narrows the one side of the polarization-filtering unit 20. Therefore, the first polarization having an electric field direction identical to the long width of the polarization filtering unit 20 cannot pass through the polarization filtering unit 20, thereby propagating to the first polarization guide 30 through an aperture facing the first polarization guide 30 of the polarization filtering unit 20. The second polarization having an electric field direction identical to the short width of the polarization filtering unit 20 downwardly propagates along the polarization filtering unit 20, inputting to the second polarization guide 50.

[0122] Among radio waves inputted through four horns 10, the first polarization inputs to each aperture of the first and second waveguides 35, and 40 of the first polarization guide 30. In the first waveguide 35, the first polarizations input through each aperture reach the first horizontal layer 37 and get mixed together. Then, the electric field direction of the first polarizations changes to the up and down direction at the first ledge 36. In the second waveguide 40, the first polarizations input through each aperture are mixed together at the second horizontal layer 42. The electric field direction thereof changes to an up and down direction at the second ledge 41. The first polarizations from the first and second waveguides 35 and 40 propagate along the first and second connecting pipes 48 and 49, and enter the first mixing pipe 45. In the first mixing pipe 45, the first polarizations from the first and second waveguides 35 and 40 mix at the third, horizontal layer 47 and reenter the first main aperture.

[0123] The second polarization guided to the second polarization guide 50 through the polarization filtering unit 20 holds an electric field direction identical to a short width of the polarization filtering unit 20. The propagation direction of the second polarization changes by the third and fourth ledges 56 and 61 formed at the third and fourth waveguides 55 and 60. The second polarizations reflected from the reflecting sides 57 and 62 of the third and fourth waveguides 55 and 60 propagate to the fourth and fifth horizontal layers 58 and 63 resulting in the mixing together at the fourth and fifth horizontal layers 58 and 63. The mixed second polarization propagates to the second mixing pipe 65. On the sixth horizontal layer 67 of the second mixing pipe 65, the second polarizations from the third and fourth waveguides 55 and 60 mix together, and the mixed the second polarization consequentially enter through the second main aperture 66 of the second mixing pipe 65.

[0124] Following is the description of the operation on transmitting a first and a second polarization in the dual linear polarization horn array antenna 1 according to an embodiment of the present invention.

[0125] The second polarization input to the second mixing pipe 65 through the second main aperture 66 is separated at the sixth horizontal layer 67 and guided to the third and fourth waveguides 55 and 60. In the third and fourth waveguides 55 and 60, the second polarization is separated again by the fourth and fifth horizontal layers 58 and 63. The separated polarizations are then reflected from the reflecting sides 57 and 62, and provided to the third and fourth ledges 56 and 61. The second polarization changes the propagation direction to the polarization filtering unit 20 with the help of the third and fourth ledges 56 and 61 elevating to the polarization-filtering unit 20.

[0126] The first polarization input to the first mixing pipe 45 through the first main aperture 46 is separated at the third horizontal layer 47, and the separated first polarizations are transferred to the first and second waveguides 35 and 40 through the first and second connecting pipes 48 and 49. In the first and second waveguides 35, and 40, the propagation direction of the first polarization changes at the first and second ledges 36 and 41, and the first polarization propagates to each aperture by the first and second horizontal layers 37 and 42. The first polarizations so outputted to the each polarization filtering unit 20 through each aperture are mixed with the second polarization from the second polarization guide 50, and the mixed polarization is radiated to the space through the inclined section 15.

[0127] A configuration for manufacturing the dual linear polarization horn array antenna 1 according to the present embodiment will be described in an antenna unit.

[0128] Fig. 58 is an exploded perspective view of each layer of a dual linear polarization horn array antenna according to an embodiment of the present invention. Fig. 59 is a perspective view of the first layer of dual linear polarization horn array antenna according to an embodiment of the present invention, and Fig. 60 is a plan view of a first layer shown in Fig. 58. Fig. 61 is a rear view of a first layer shown in Fig. 58.

[0129] The dual linear polarization horn array antenna according to the present embodiment includes a first layer 100, a first intermediate layer 150, a second layer 200, a second intermediate layer 250, and a third layer 300.

[0130] In the first layer 100, a inclined section 15 of a horn 10 and a ledge 17 are formed. Accordingly, the inclined section 15 is formed at the front side of the first layer 100, and the internal aperture is formed at the rear side of the first layer 100.

[0131] Fig. 62 is a perspective view of a first intermediate layer shown in Fig. 58; Fig. 63 is a plane view of a first intermediate layer shown in Fig. 58; and Fig. 64 is a rear view of a first intermediate layer shown in Fig. 58.

[0132] The polarization filtering unit 20, connected to an internal aperture formed at the first layer 100, is formed at the first intermediate layer 150, and the polarization filtering unit 20 is formed to penetrate areas adjacent to each corner of the first intermediate layer 150. The rear side of the first intermediate layer 150 includes the upper portion of the first and second waveguides 35 and 40 of the first polarization guide 30, and the upper portion of the first mixing pipe 45.

[0133] Fig. 65 is a perspective view of a second layer shown in Fig. 58; Fig. 66 is a plan view of a second layer shown in Fig. 58; and Fig. 67 is a rear view of a second layer shown in Fig. 58.

[0134] The second layer 200 includes a lower area of the first polarization guide 30 and the polarization filtering unit 20. That is, the second layer 200 includes the first horizontal layer 37 of the first waveguide 35, the second ledge 41 of the second waveguide 40, and the remained portion of the third horizontal layer 47 of the first mixing pipe 45. The polarization filtering unit 20 is formed at each aperture of the first and second waveguides 35 and 40 of the first polarization guide 30 to penetrate the second layer 200. Accordingly, the polarization filtering unit 20 is only formed at the rear side of the second layer 20.

[0135] Fig. 68 is a perspective view of a second intermediate layer shown in Fig. 58, and Fig. 69 is a rear view of a second intermediate layer shown in Fig. 58.

[0136] The polarization filtering unit 20 is formed at the second intermediate layer 250 to penetrate therethrough, as well as a predetermined upper portion of the second polarization guide 50 at the rear side of the second intermediate layer 250. The fourth and fifth horizontal layers 58 and 63 of the third and fourth waveguides 55 and 60, and the sixth horizontal layer 67 of the second mixing pipe 65 are formed at the rear side of the second intermediate layer 250.

[0137] Fig. 70 is a perspective view of a third layer, and Fig. 71 is a plan view of a third layer.

[0138] The lower portion of the second polarization guide 50 is formed at the third layer 300. The third layer 300 forms the second polarization guide 50 with the second intermediate layer 250 and includes the third and fourth waveguides 55 and 60, and the second mixing pipe 65 as well. The third layer 300 further includes the fourth and fifth horizontal layers 58 and 63, along with the sixth horizontal layer 67, and the third and fourth ledges 56 and 61.

[0139] The horn array antenna according to the present embodiment was described based on an antenna unit formed with four horns. With an antenna gain that stands higher than 27 dB, it is preferably assumed that the horn array antenna has an enhanced output. Popular approval goes with the antenna that has greater gain than 31dB. To improve in antenna performance, a horn array antenna is designed to have one antenna unit with four separate antenna units in vertical direction and in horizontal directions, ultimately forming one set of 16 antenna units. To manufacture one according to the present embodiment, the upper area should likely have 390 mm x 390 mm, and the height at 61mm.

[0140] Table 2 shows the antenna gain of a horn array antenna formed of one antenna unit according to an embodiment of the present invention.

Table 2

	10.7GHz	11.7GHz	12.7GHz
First polarization	20.6dBi	21.3dBi	21.4dBi
Second polarization	20.5dBi	21.2dBi	21.3dBi

[0141] The antenna gain of the first polarization guide 30 is obtained when the radio wave inputs through the first main aperture 46 and outputs through the inclined section 15. The horn array antenna according to the present embodiment has a gain higher than 20 dBi at each frequency band of satellite broadcasting. The antenna gain of the second polarization guide 50 is a gain obtained when the radio wave inputs through the second main aperture 66 and outputs through the inclined section 15. As in the first polarization guide 30, the horn antenna has a gain of higher than 20 dBi at each frequency band of satellite broadcasting.

[0142] Table 3 shows the antenna gains of a horn array antenna formed of 16 antenna units.

Table 3

	10.7GHz	11.7GHz	12.7GHz
First polarization	33.0dBi	33.7dBi	34.0dBi
Second polarization	33.0dBi	33.6dBi	33.9dBi

[0143] The antenna gain of the first polarization guide 30 is higher than 33dBi at each frequency band of satellite broadcasting, and gain of the second polarization guide 50 is higher than 33dBi at each frequency band of satellite broadcasting.

[0144] As shown in Table 3, the horn array antenna formed of antenna units on the present embodiment of invention

has the superior antenna performance.

[0145] Fig. 72 is a graphical view of the S11 parameter of a dual linear polarization horn array antenna according to an embodiment of the present invention. As shown, the S11 parameter graph of the horn 10 shows the operating frequency formed around the center frequency of 11.4GHz. The operating frequency having the S11 parameter of about -10 dB also appears in a range from 10 GHz to 13 GHz. Accordingly, the dual linear polarization horn array antenna 1 is operated within a frequency band range 10.7GHz to 12.75GHz, which are the existing frequency band of the satellite broadcasting. As the S11 parameter of the operating frequency band is less than -10dB, the dual linear polarization horn array antenna 1 based on the present embodiment has superior performance.

[0146] In the dual linear polarization horn array antenna 1, the height of the horn 10 can be reduced while sustaining the antenna efficiency by forming the ledges 17 at the horn 10. The height of the second polarization guide 50 can also be reduced by the horizontal width of the second polarization guide 50 to be wider than the height thereof. Furthermore, the overall size of the dual linear polarization horn array antenna 1 can be reduced. Although it is reduced in size, the dual linear polarization horn array antenna 1 is compact and has an improved antenna performance as FIGd in Table 3.

[0147] Although the first and second polarizations were described based on electric field, they can be applied to magnetic field. The configurations for manufacturing the horn 10, the first polarization guide 30, and the second polarization guide 50 shown in Figs. 20 to 58 are only examples of the present invention. According to needs, at least two of the horn 10, the first polarization guide 30, and the second polarization guide 50 can be manufactured at once through injection molding. The manufacturing of the horn 10, the first polarization guide 30, and the second polarization guide 50 is not limited to the number of layers illustrated in Figs. 58 to 71.

[0148] According to certain embodiments of the present invention, the performance of the antenna can be improved while the size of the antenna is reduced.

[0149] While this invention has been described in connection with what is presently considered to be practical exemplary embodiments, it is to be understood that the invention is not limited to the disclosed embodiments, but, on the contrary, is intended to cover various modifications and equivalent arrangements included within the spirit and scope of the appended claims.

Claims

1. A horn array antenna for dual linear polarization receiving a first polarization wave and a second polarization wave, the horn array antenna comprising:

a plurality of horns to which a mixed wave of the first polarization wave and the second polarization wave, enters;
a plurality of polarization filtering units provided in each of the horns to separate the incident mixed wave into the first and second polarization waves;

a first polarization guide which guides the first polarization waves separated at the polarization filtering units; and
a second polarization guide which guides the second polarization waves separated at the polarization filtering units,

wherein an upper portion of each polarization filtering unit is formed as a quadrilateral space,
each polarization filtering unit has four walls including a first, second, third and fourth walls, and a stepped portion is extended from a lower portion of the first wall to an interior of the polarization filtering unit, whereby a lower portion of the polarization filtering unit is formed as a quadrilateral space with a narrower width than that of the upper portion,

an extended portion is formed on an upper portion of the stepped portion, and

a first polarization inlet is formed on the second wall opposite to the first wall to provide the first polarization wave to the first polarization guide.

2. The horn array antenna for dual linear polarization of claim 1, wherein the quadrilateral space of the upper portion of each polarization filtering unit may be a square space, and the quadrilateral space of the lower portion of each polarization filtering unit may be a rectangular space.

3. The horn array antenna for dual linear polarization of claim 1, wherein the stepped portion is formed at a predetermined distance downwardly from an uppermost end of the first wall.

4. The horn array antenna for dual linear polarization of claim 1, wherein the lower portion of the polarization filtering unit is narrowed to a predetermined direction, whereby a lower surface of the polarization filtering unit is formed in a rectangular shape.

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5. The horn array antenna for dual linear polarization of claim 1, wherein each horn includes a square outer aperture open to outside, and a square inner aperture open to the polarization filtering unit, and the square inner aperture includes an extended portion extending toward a central area.

5 6. The horn array antenna for dual linear polarization of claim 5, wherein walls of the square outer aperture are in parallel with walls of the square inner aperture.

7. The horn array antenna for dual linear polarization of claim 6, wherein the extended portion extends from, and along an edge of the square inner aperture to a predetermined width.

10 8. The horn array antenna for dual linear polarization of claim 1, wherein the stepped portion includes a plurality of uneven surfaces.

15 9. The horn array antenna for dual linear polarization of claim 8, wherein the plurality of uneven surfaces is so formed that a width of the polarization filtering unit gradually decreases toward a lower portion of the polarization filtering unit.

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50

55

FIG 1

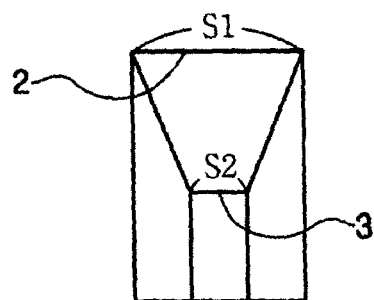


FIG 2

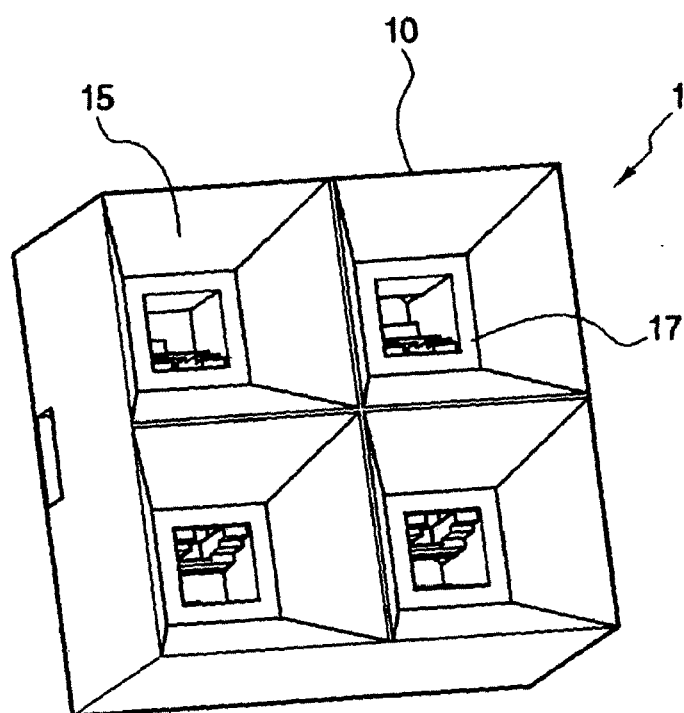


FIG 3

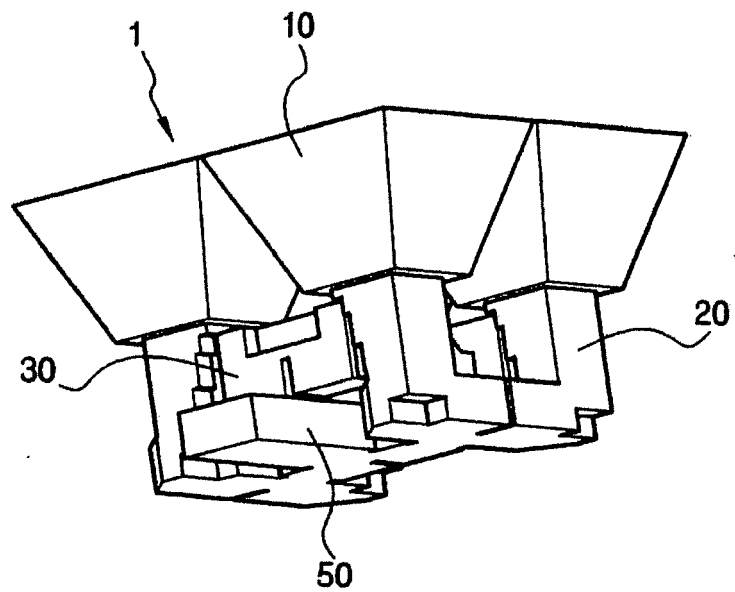


FIG 4

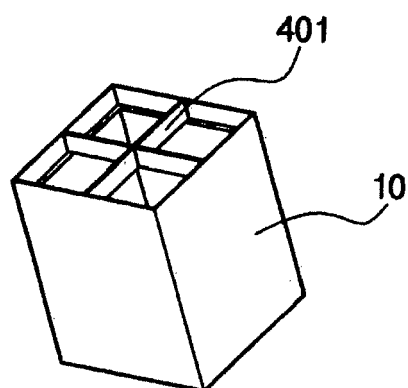


FIG 5

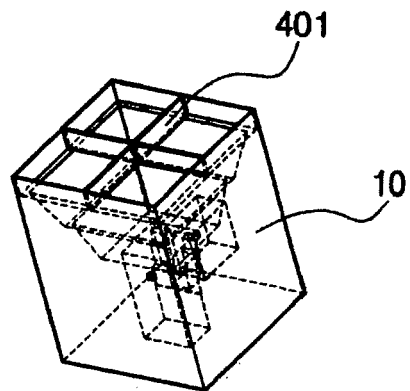


FIG 6

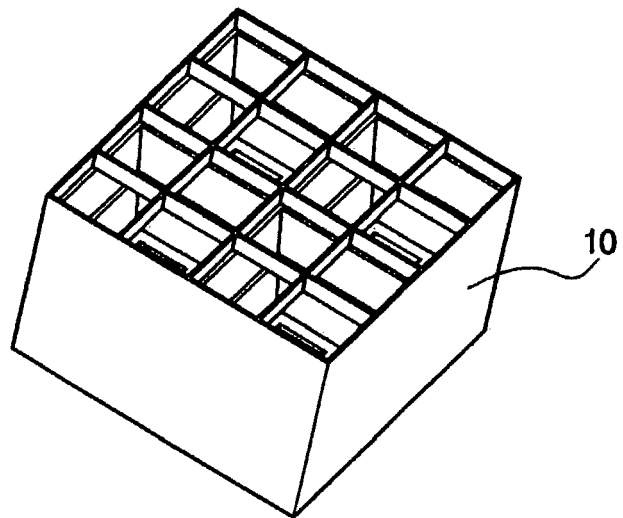


FIG 7

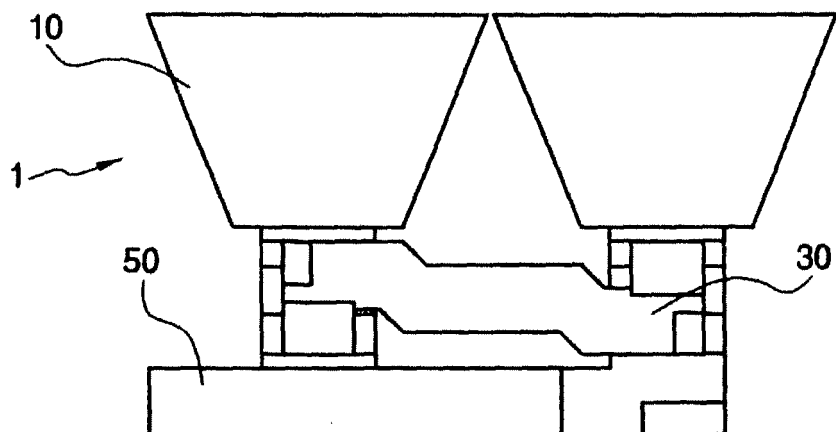


FIG 8

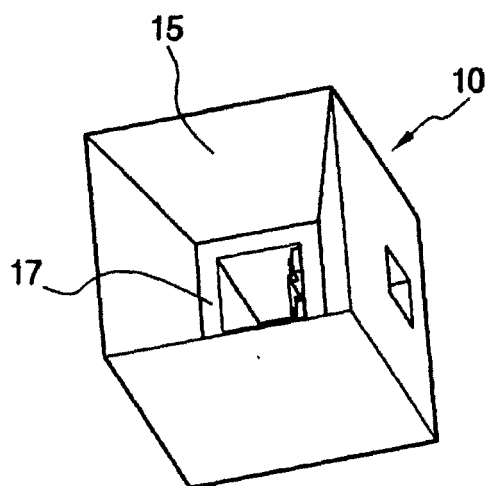


FIG 9

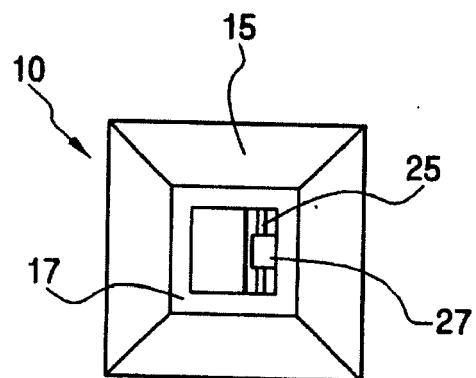


FIG 10

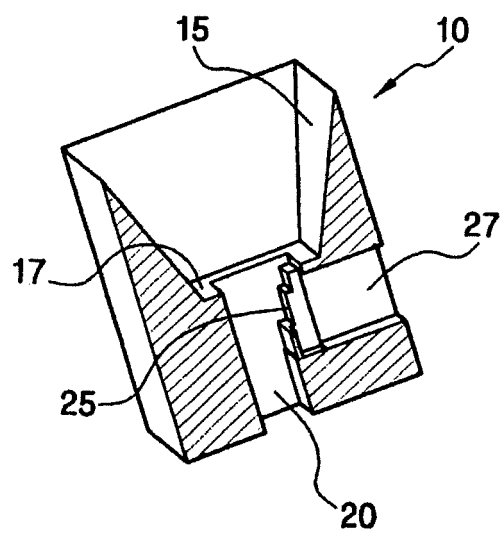


FIG 11

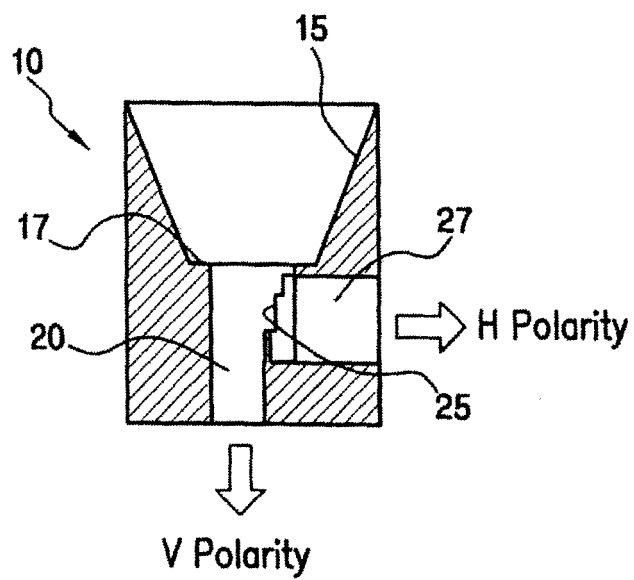


FIG 12

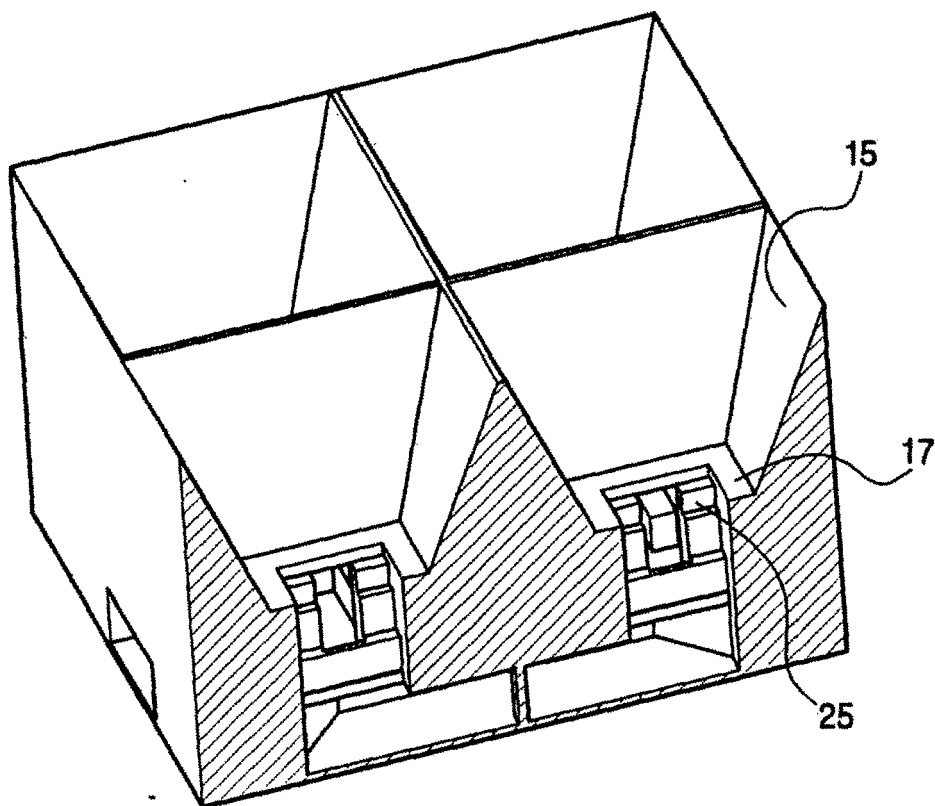


FIG 13

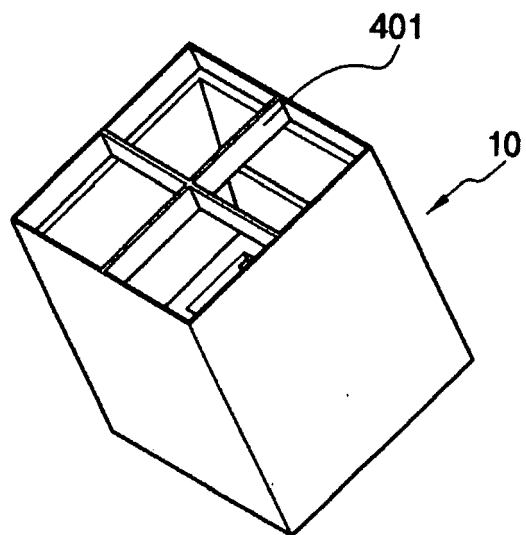


FIG 14

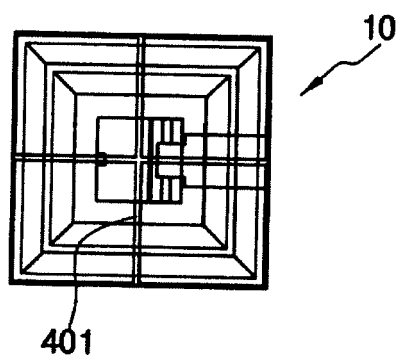


FIG 15

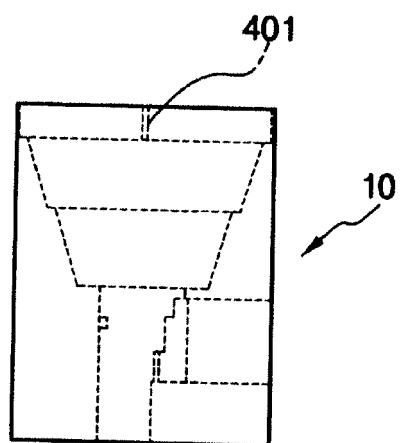


FIG 16

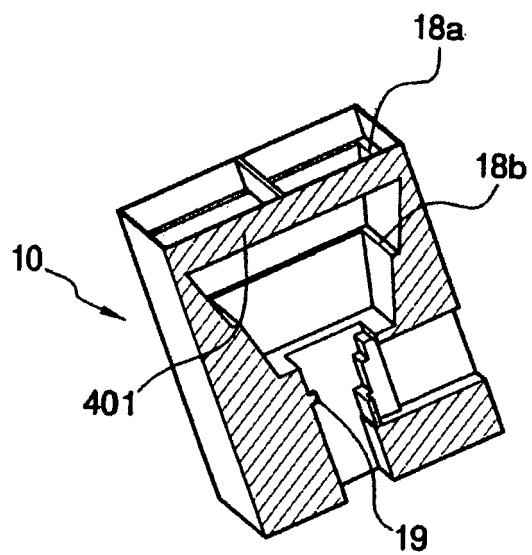


FIG 17

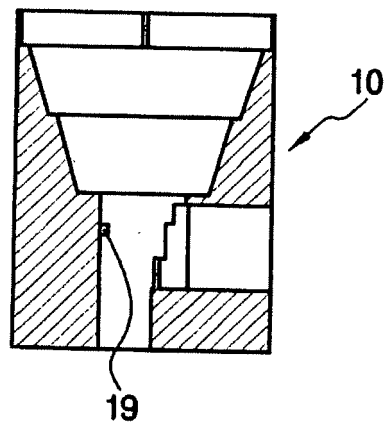


FIG 18

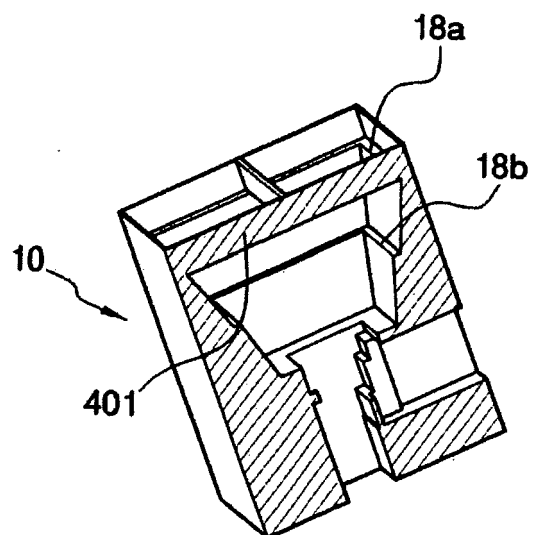


FIG 19

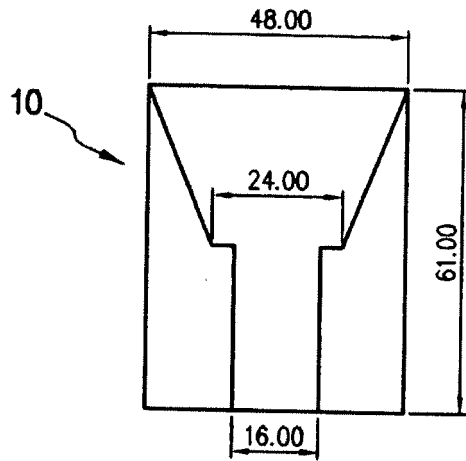


FIG 20

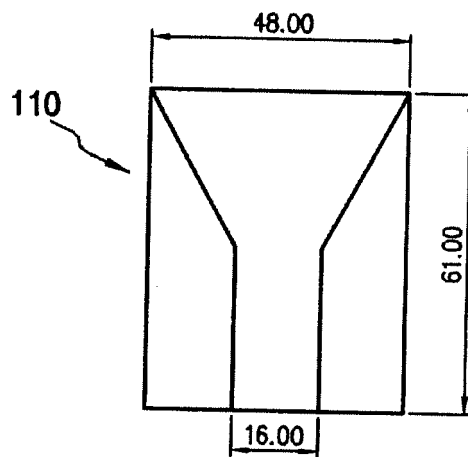


FIG 21

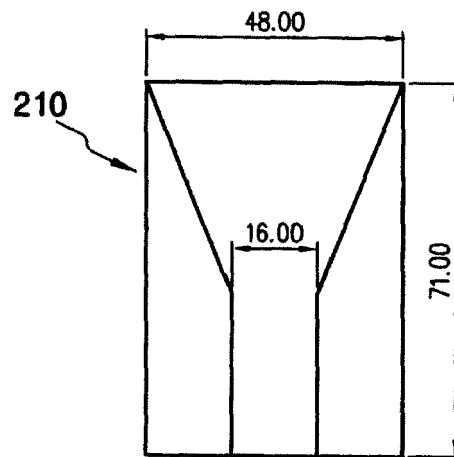


FIG 22

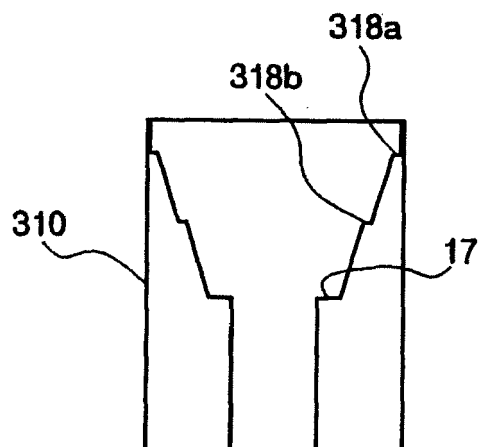


FIG 23

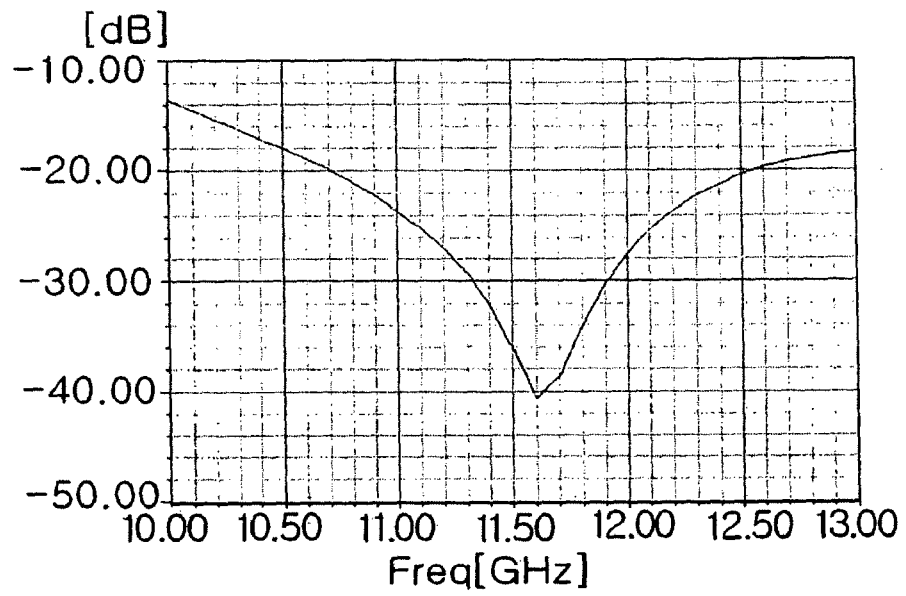


FIG 24

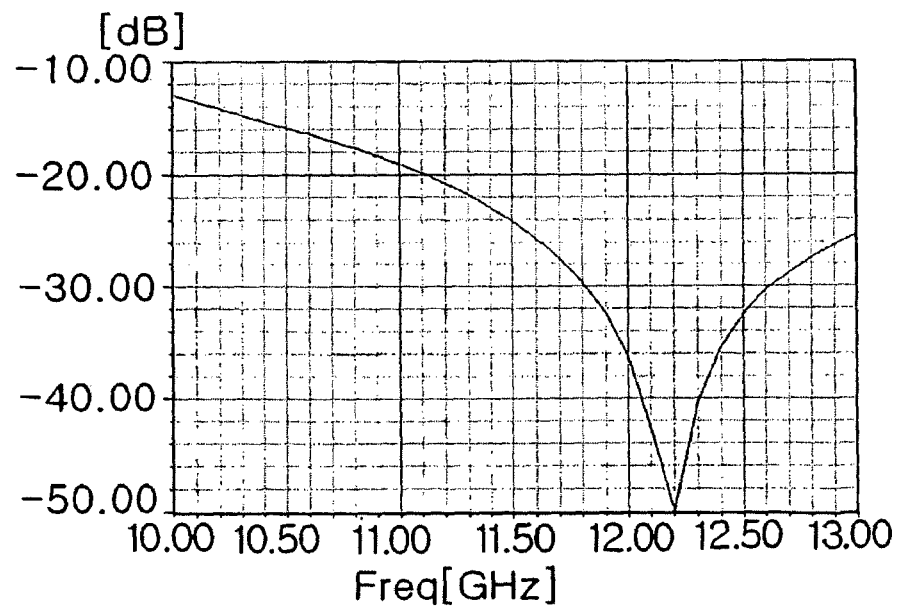


FIG 25

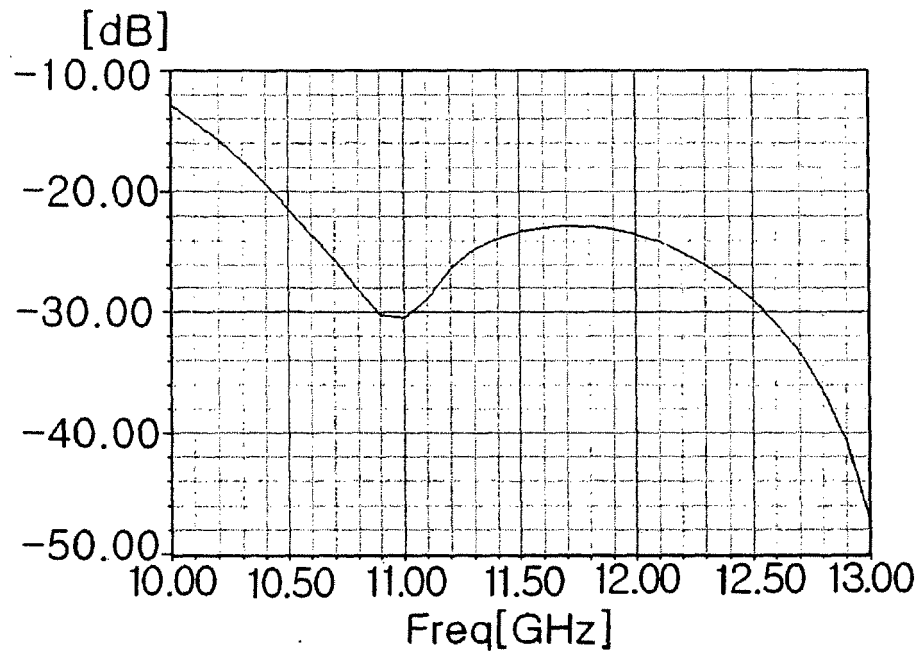


FIG 26

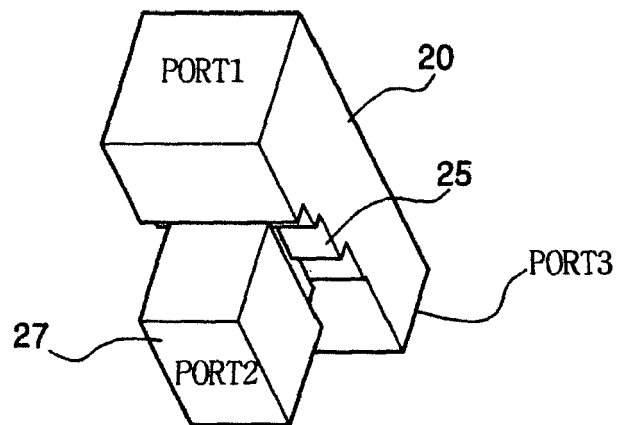


FIG 27

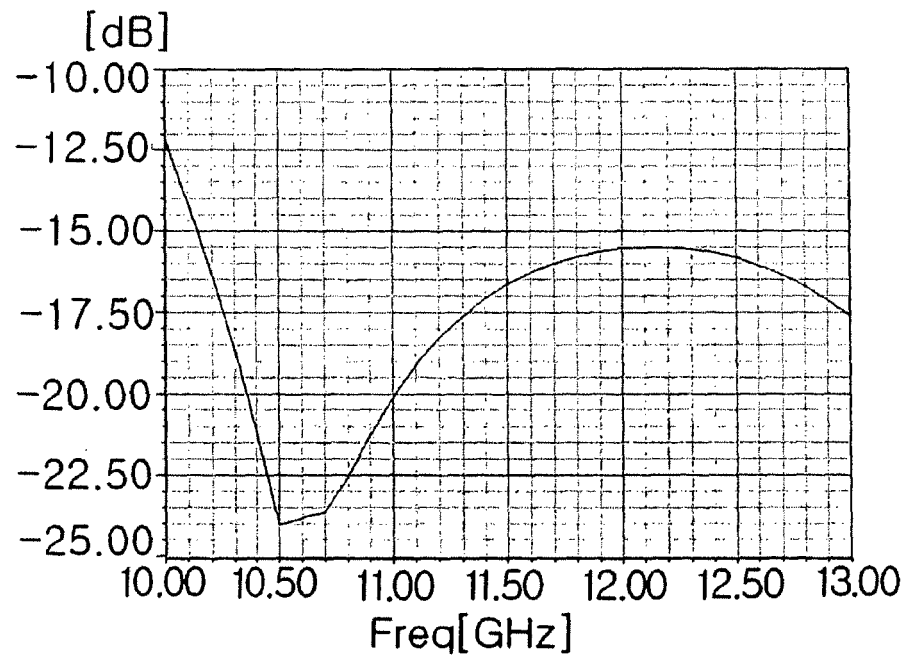


FIG 28

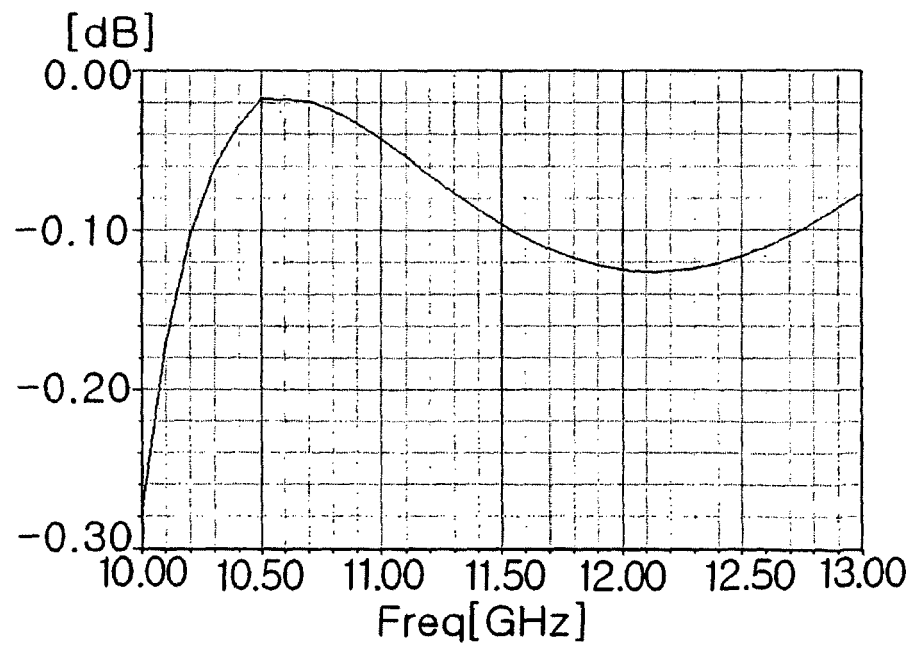


FIG 29

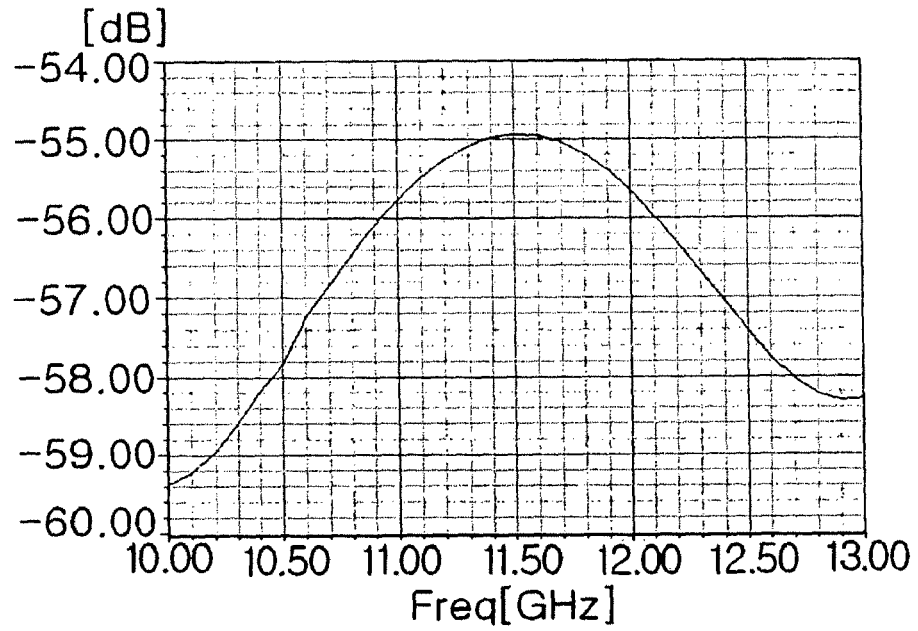


FIG 30

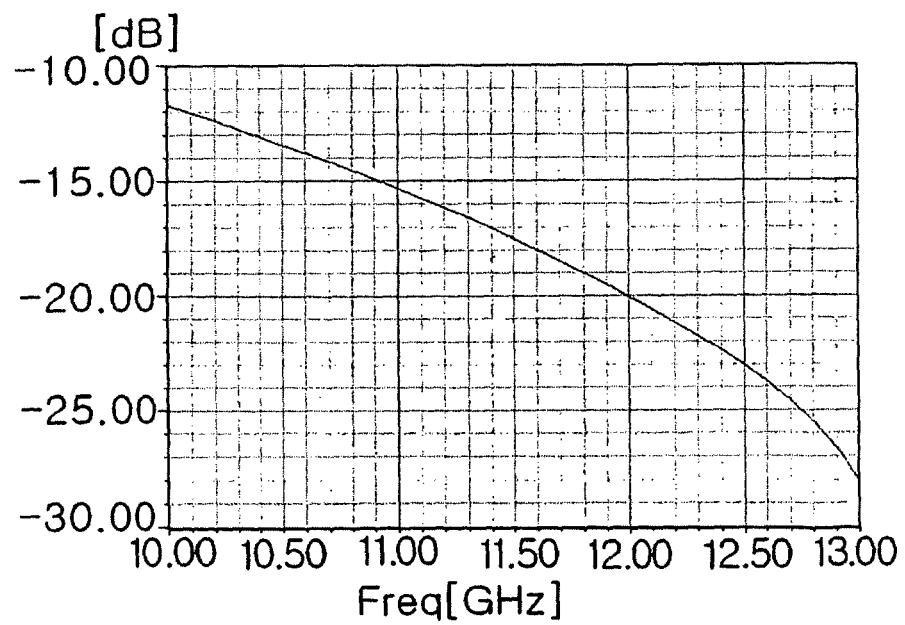


FIG 31

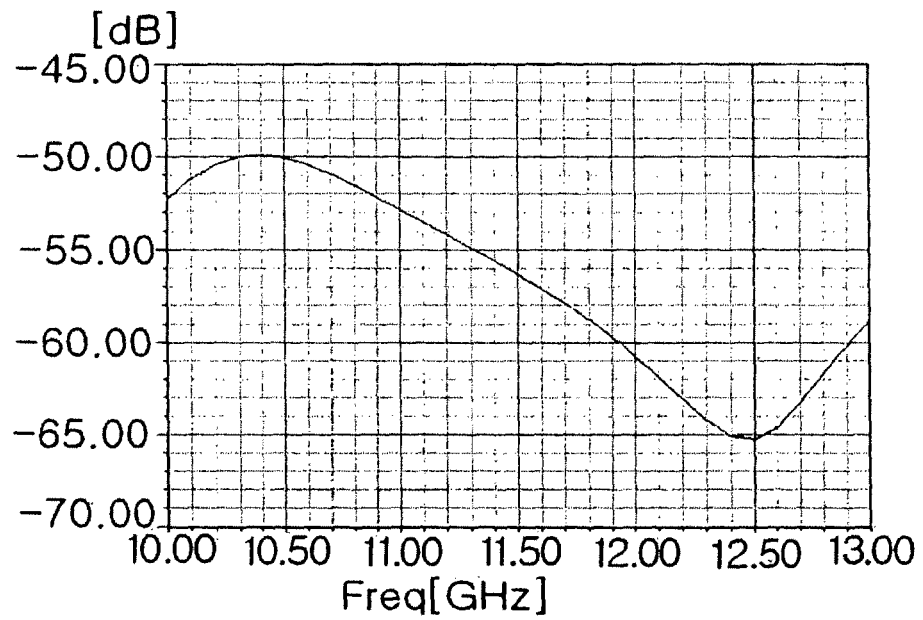


FIG 32

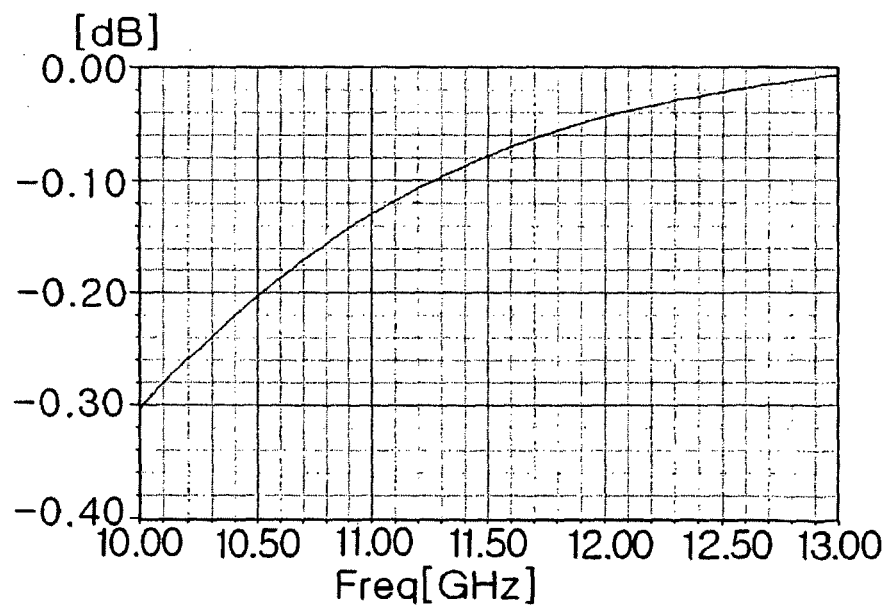


FIG 33

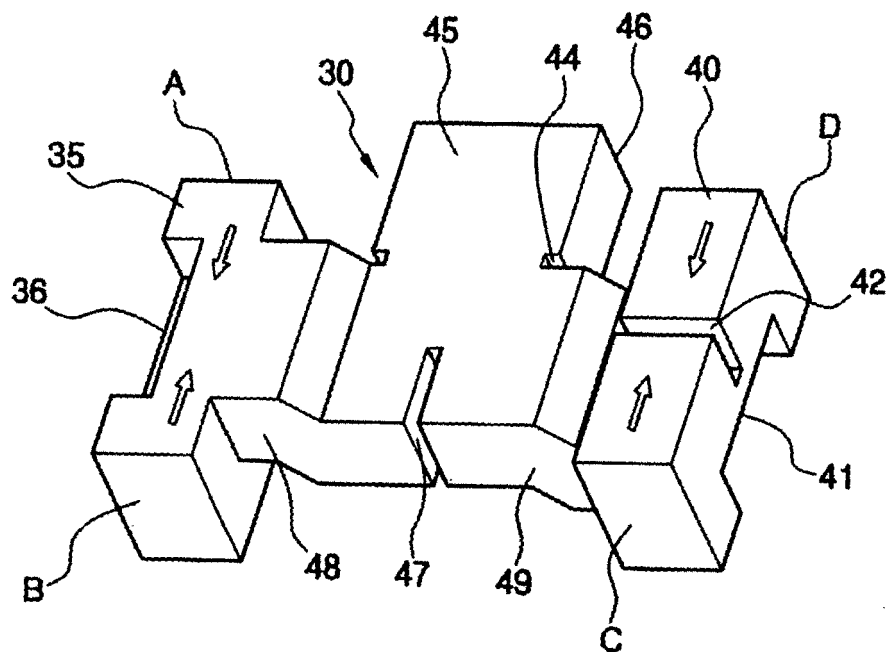


FIG 34

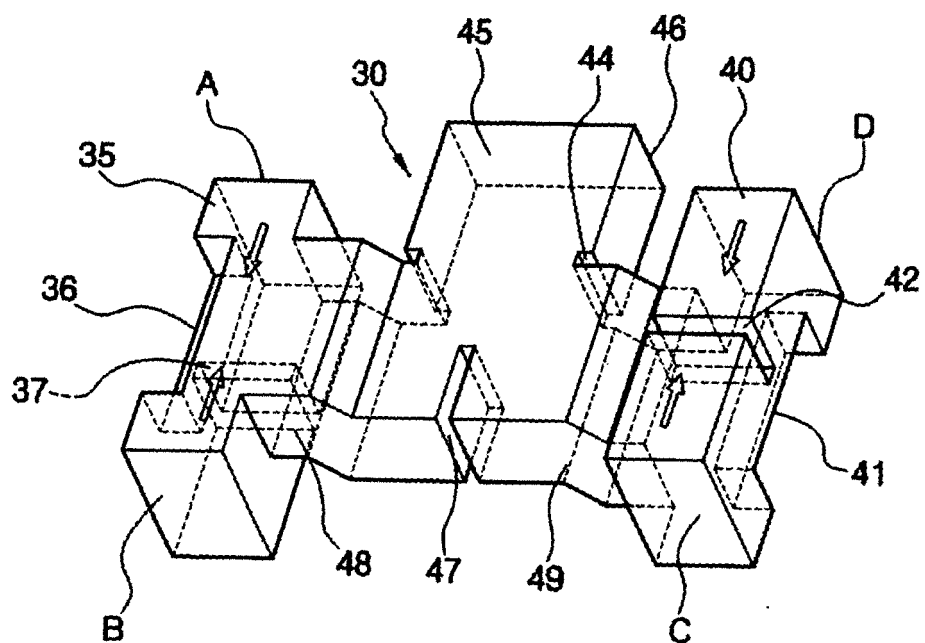


FIG 35

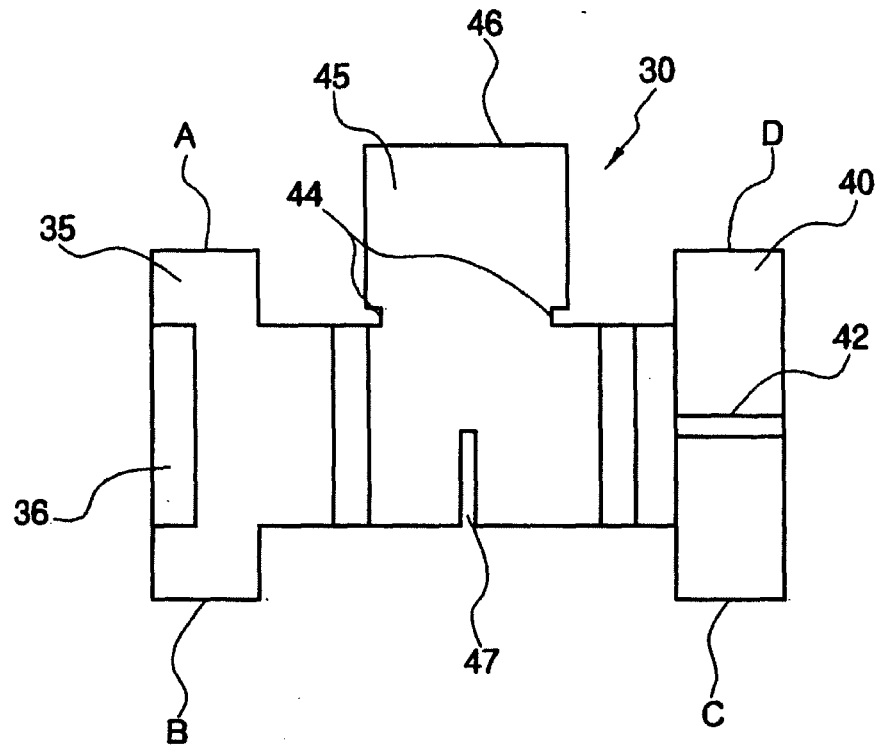


FIG 36

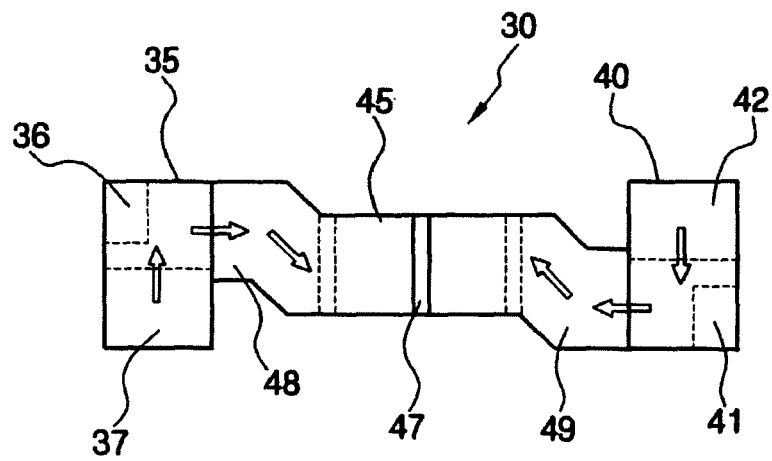


FIG 37

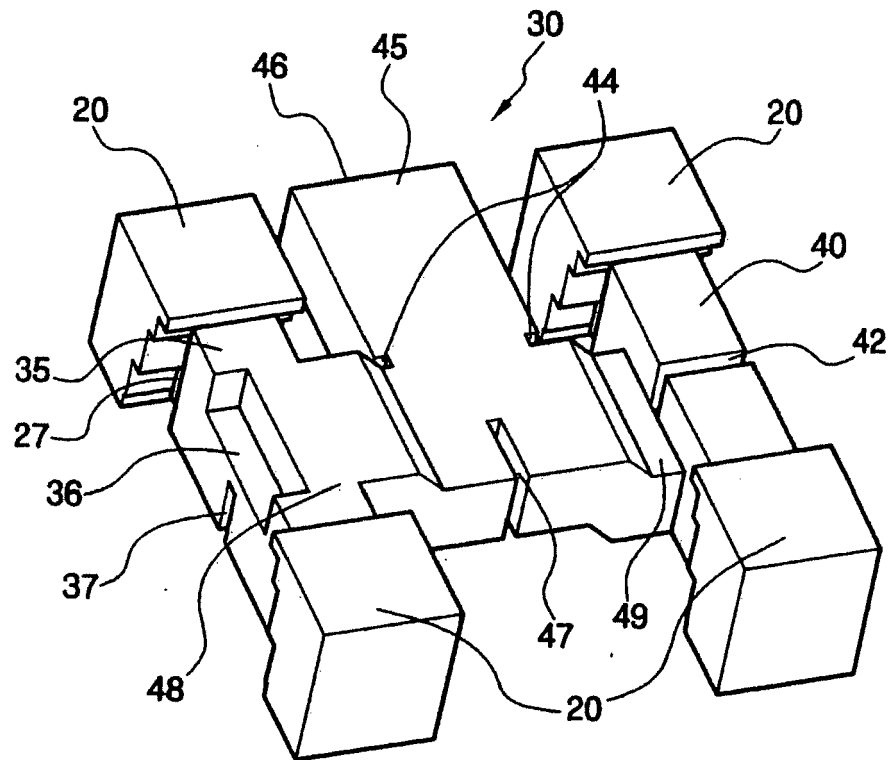


FIG 38

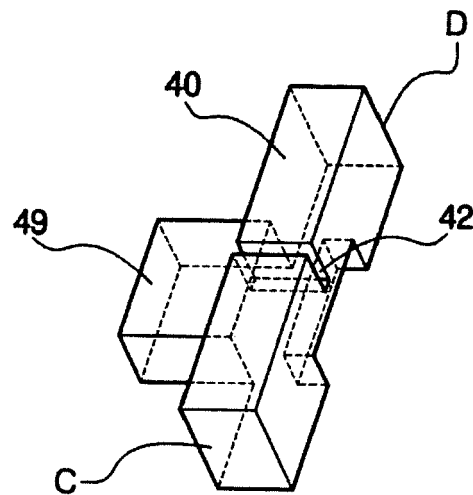


FIG 39

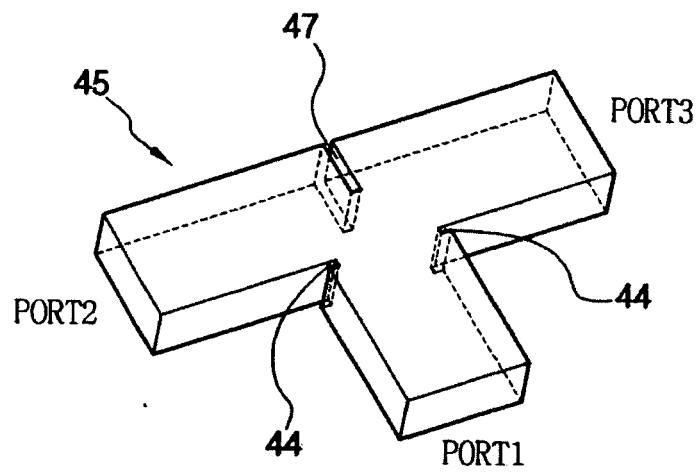


FIG 40

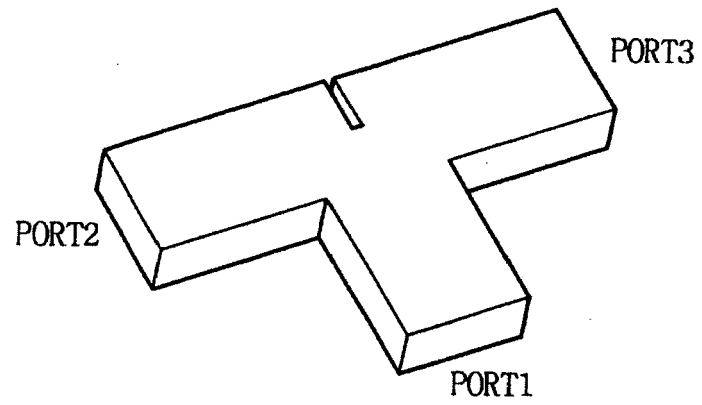


FIG 41

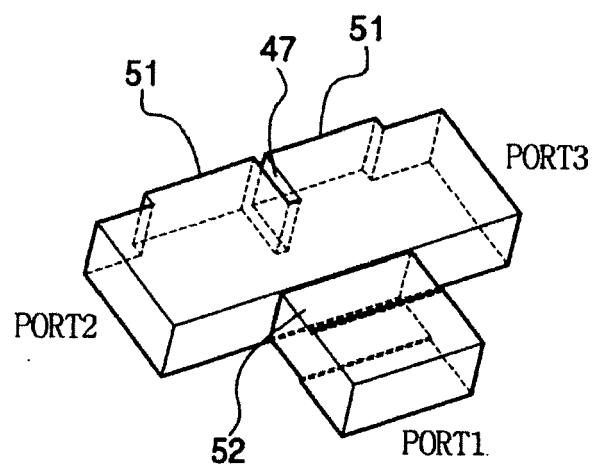


FIG 42

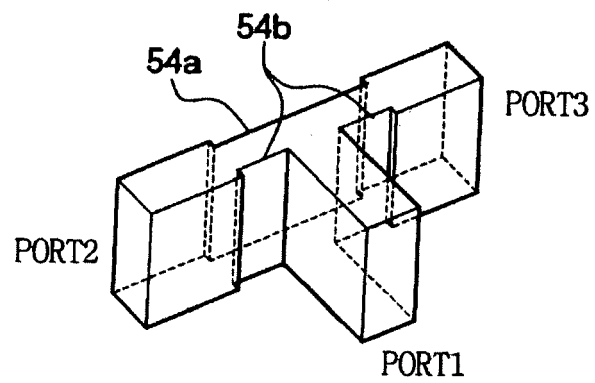


FIG 43

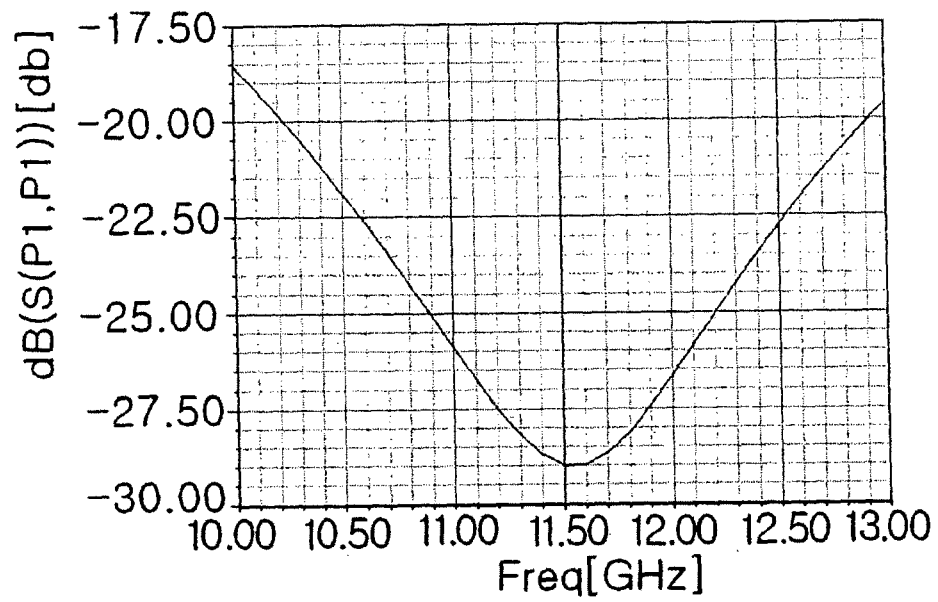


FIG 44

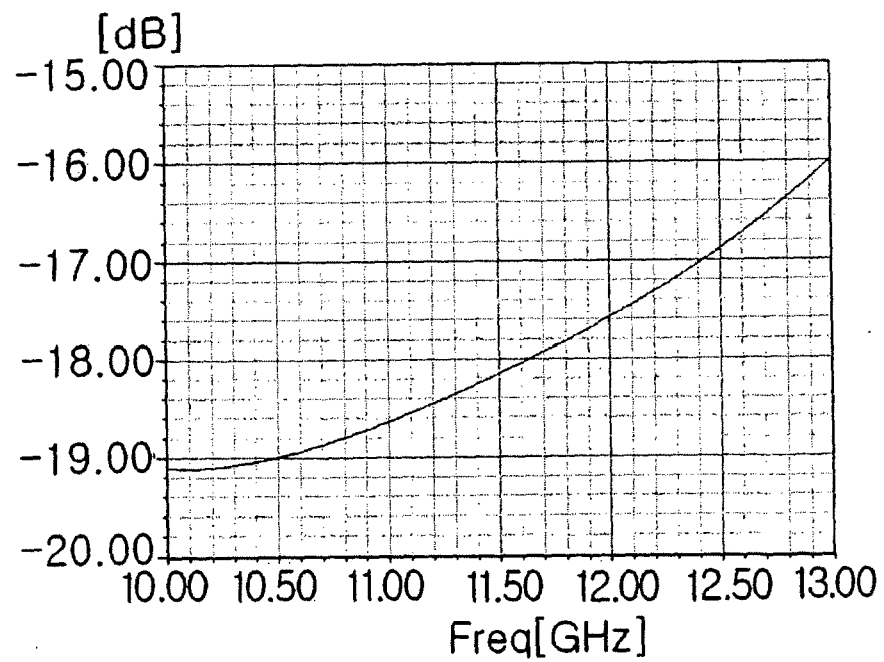


FIG 45

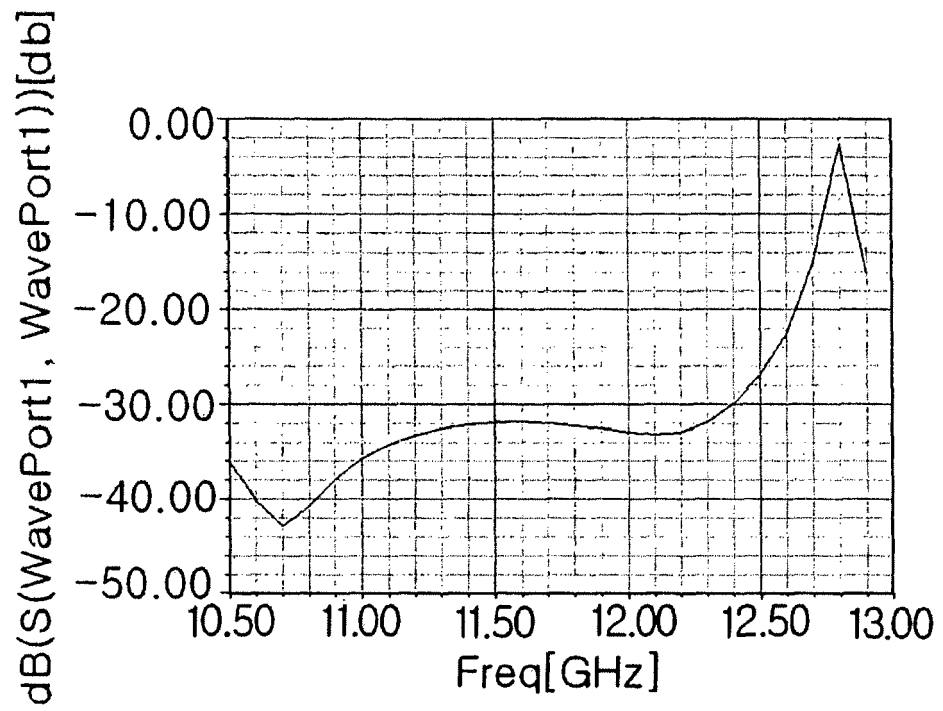


FIG 46

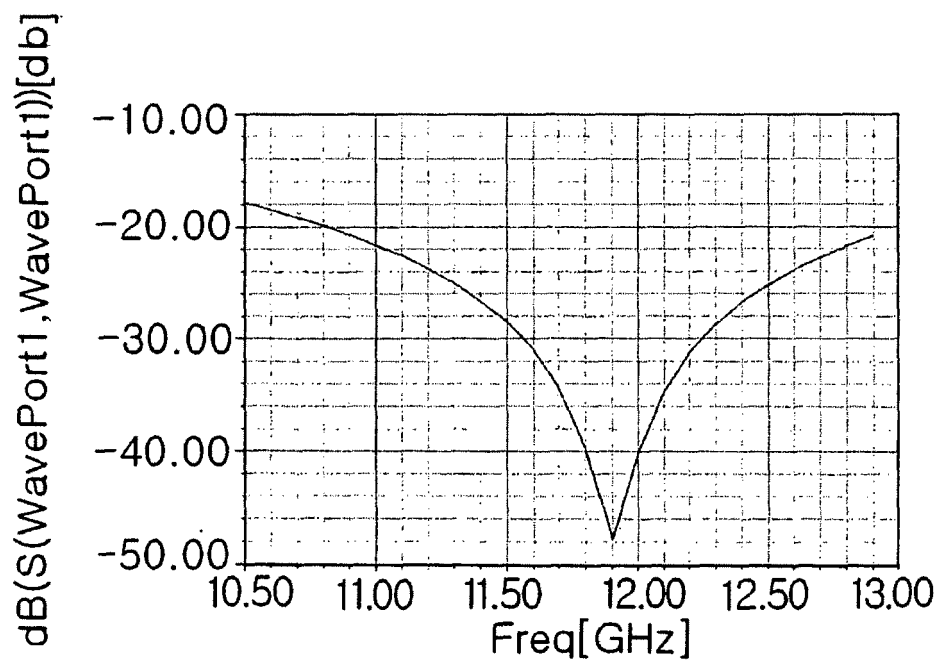


FIG 47

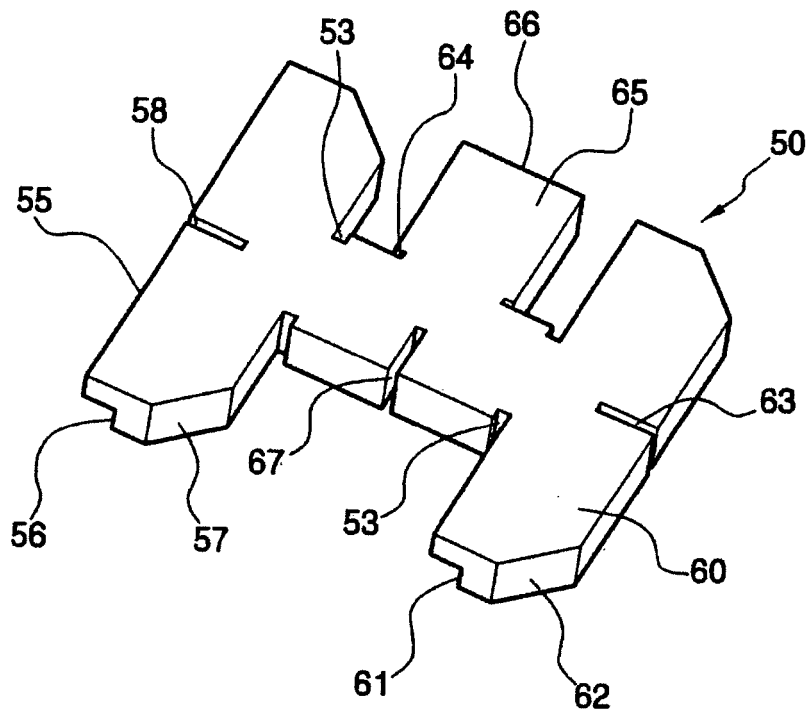


FIG 48

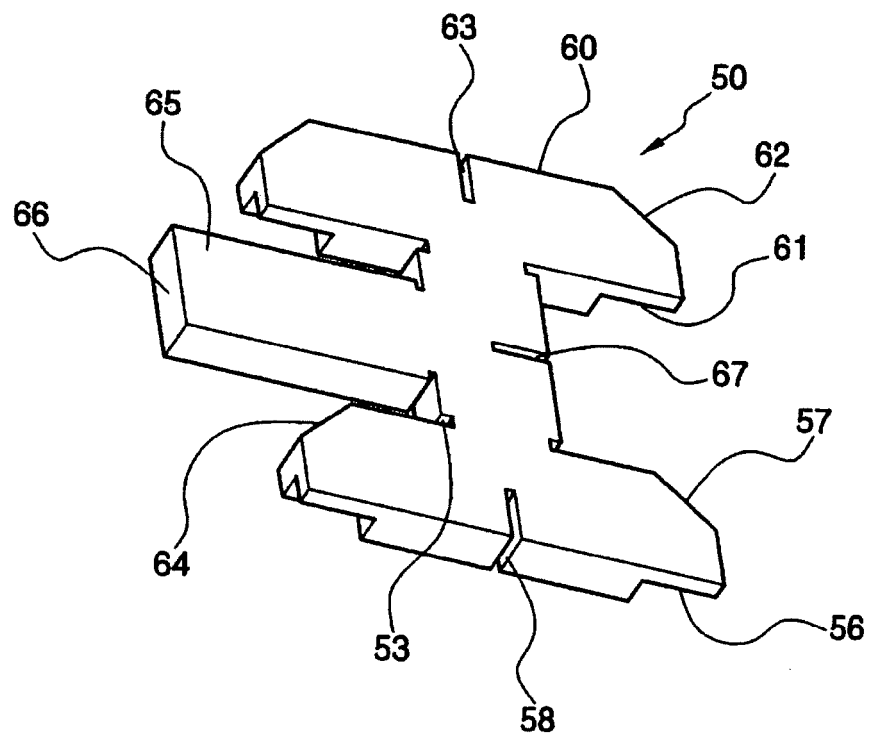


FIG 49

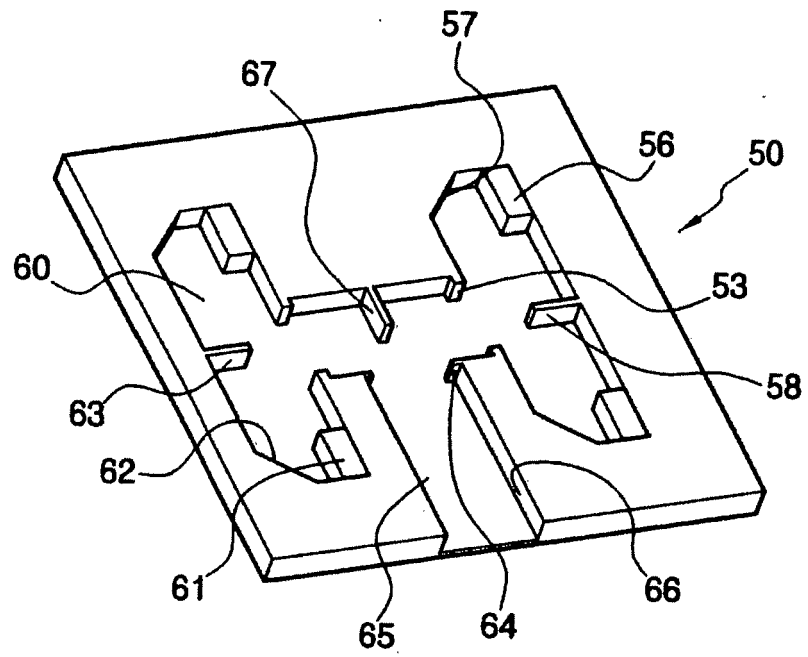


FIG 50

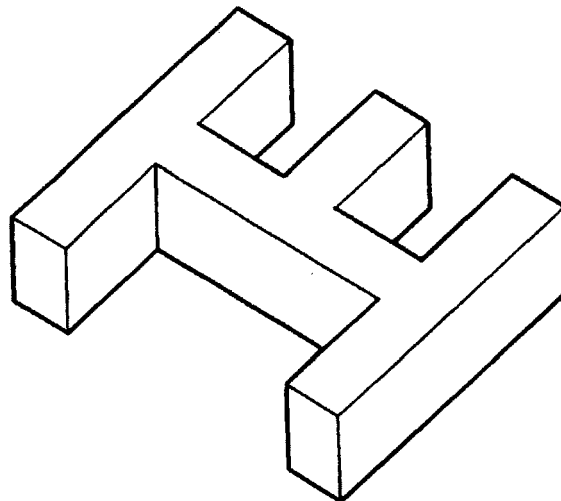


FIG 51

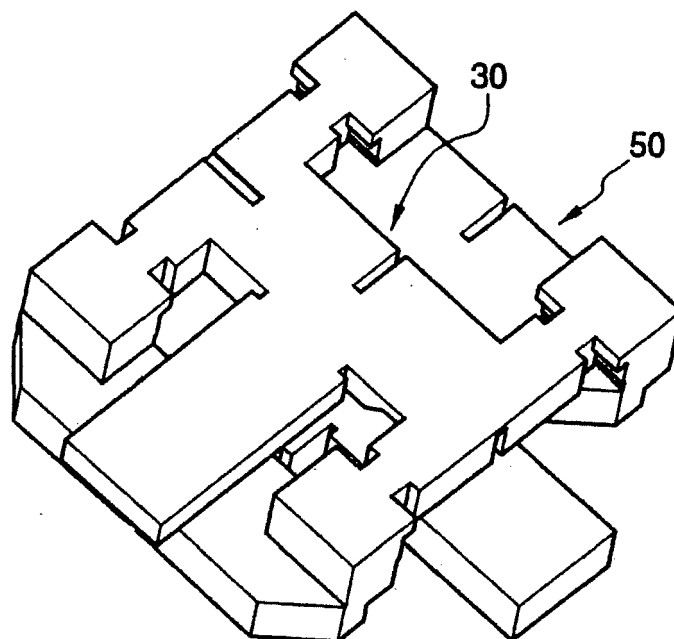


FIG 52

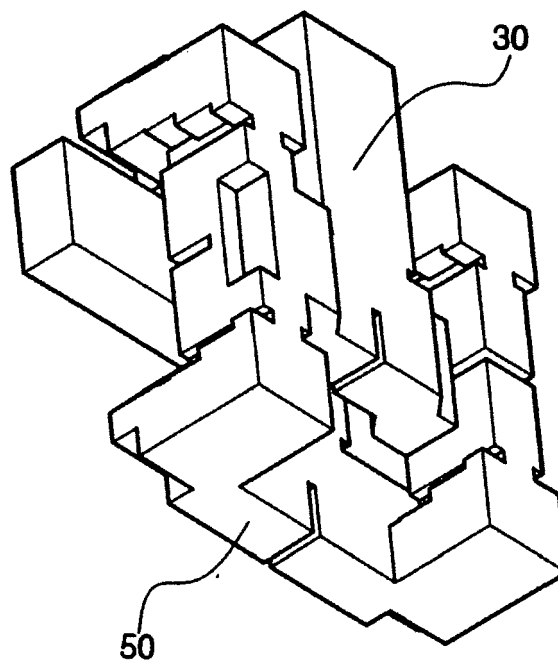


FIG 53

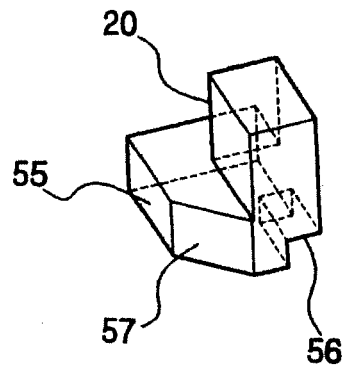


FIG 54

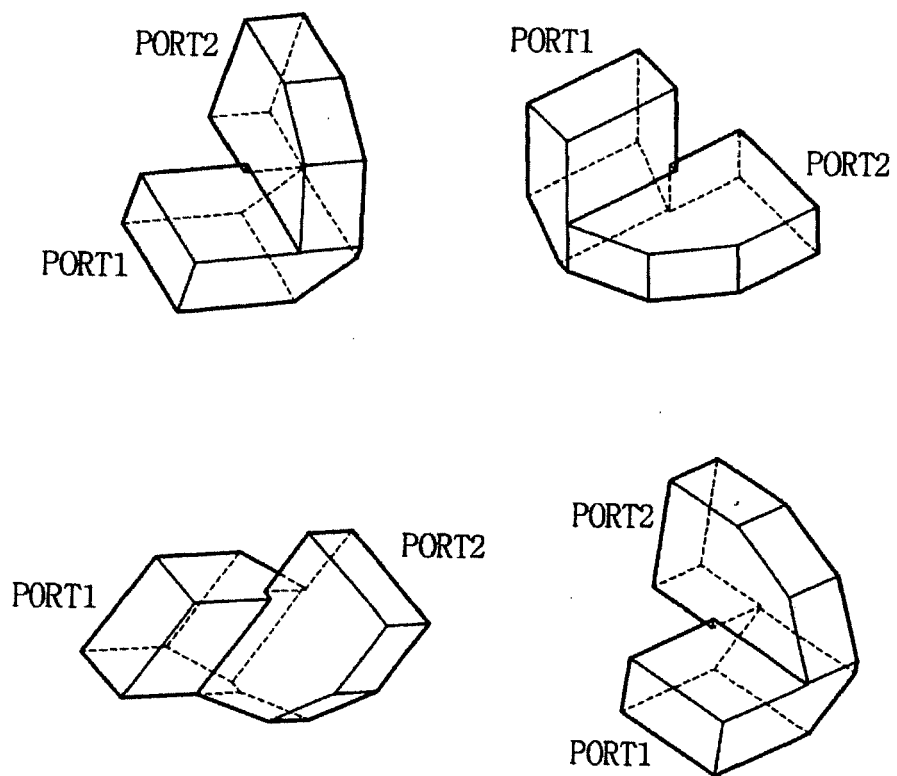


FIG 55

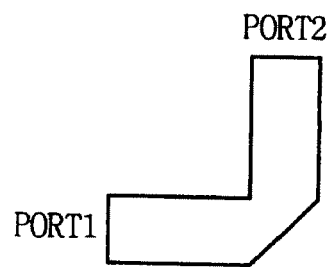


FIG 56

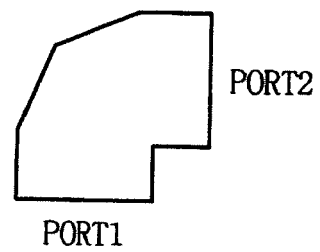


FIG 57

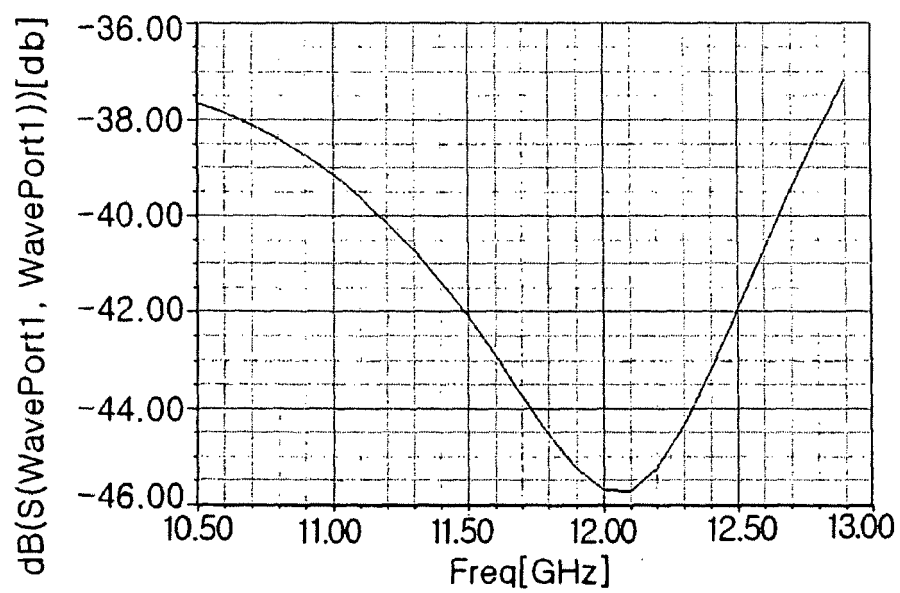


FIG 58

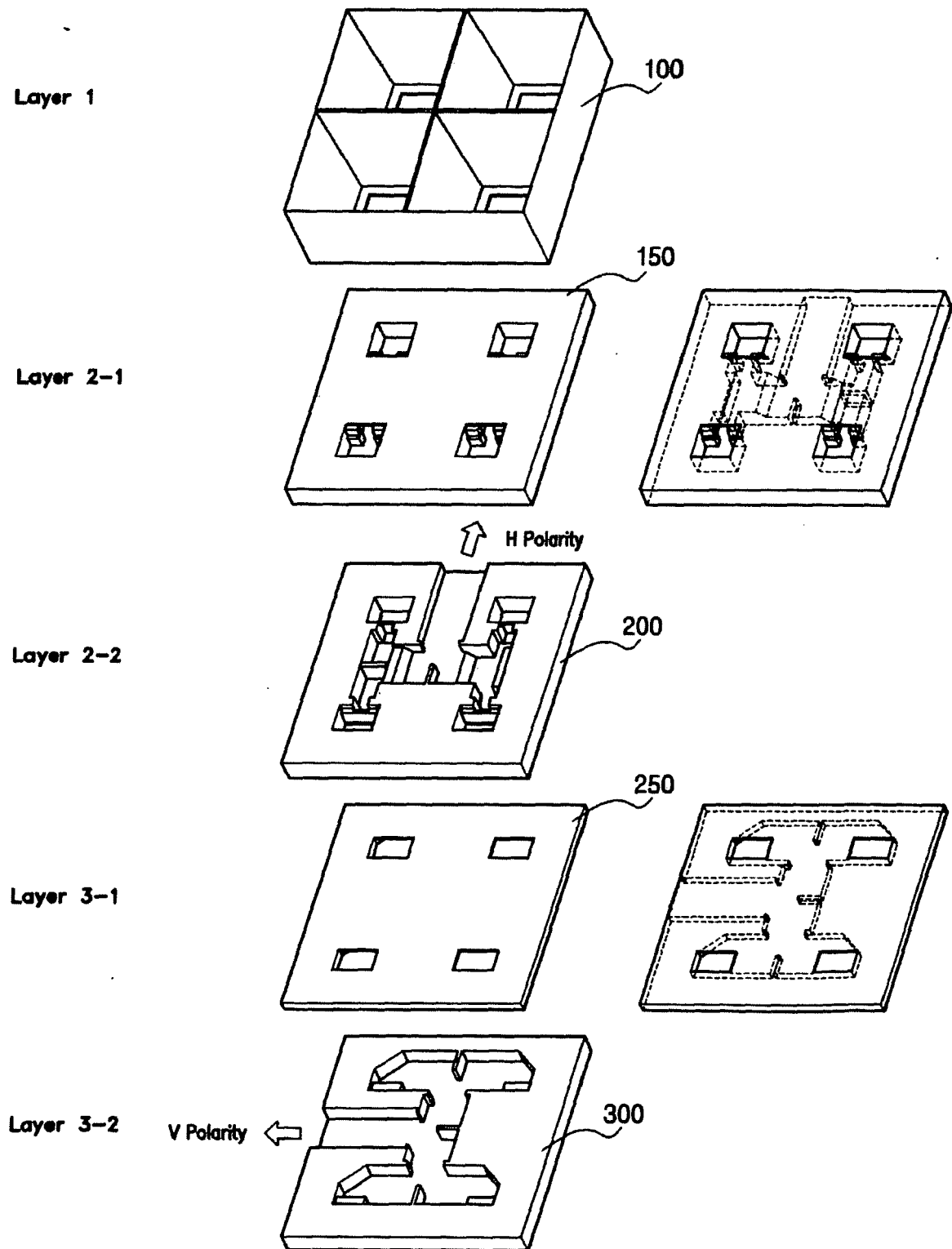


FIG 59

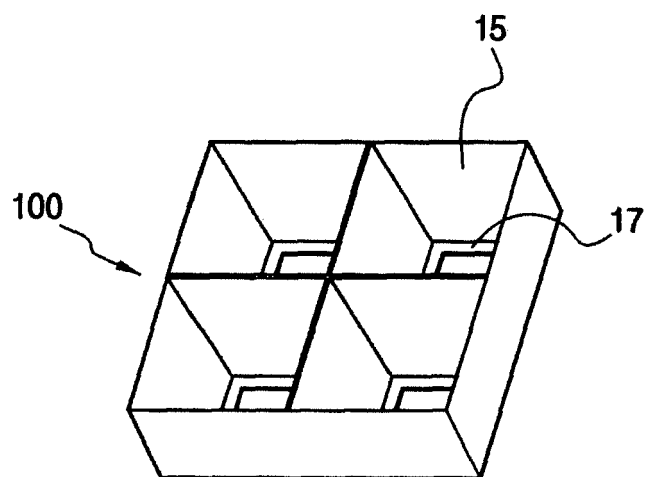


FIG 60

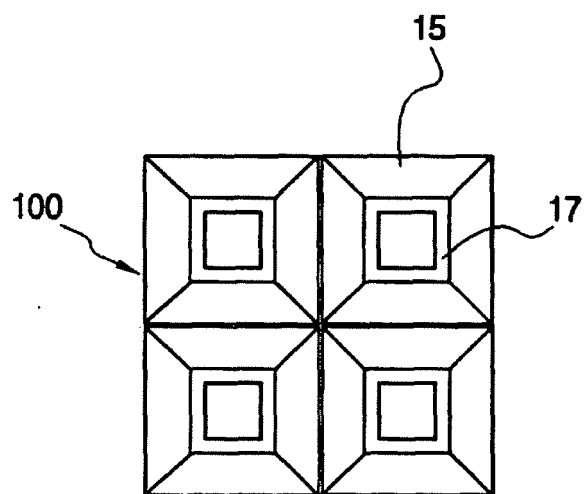


FIG 61

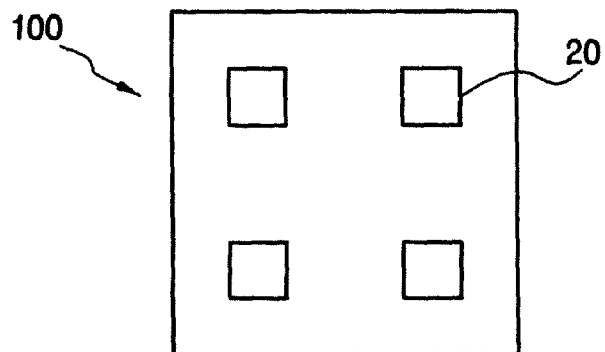


FIG 62

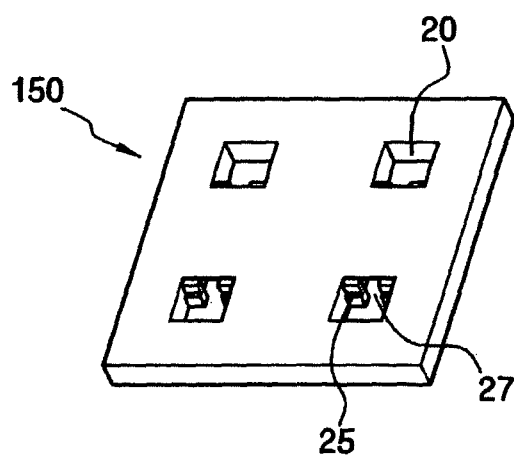


FIG 63

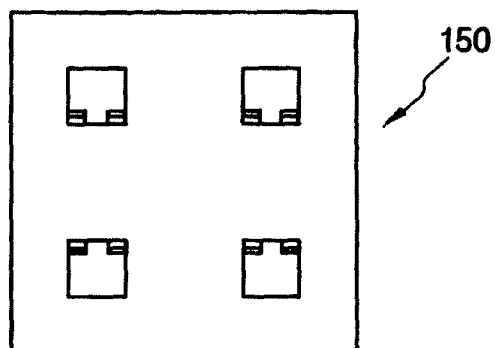


FIG 64

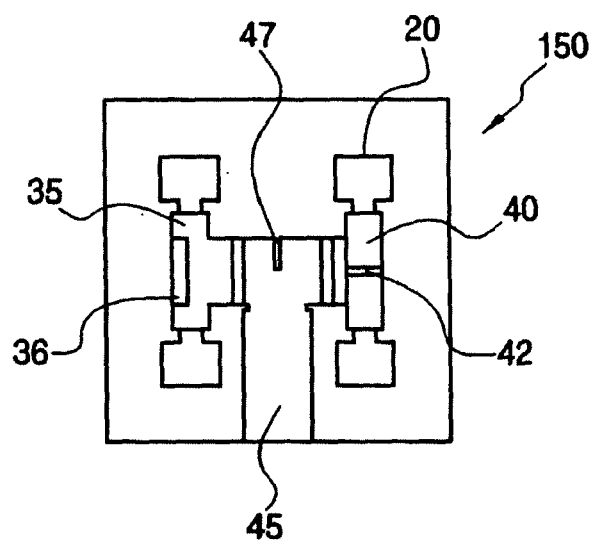


FIG 65

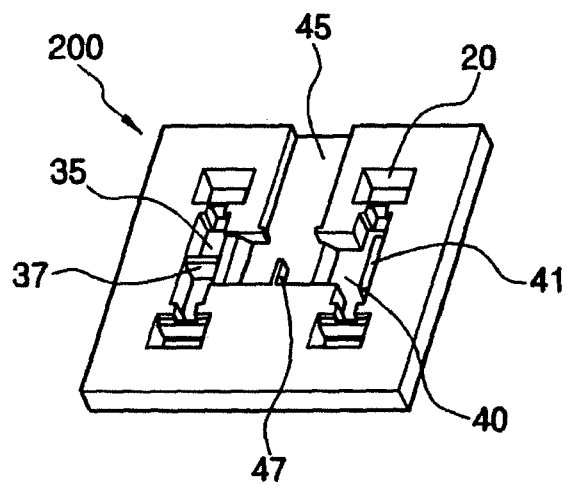


FIG 66

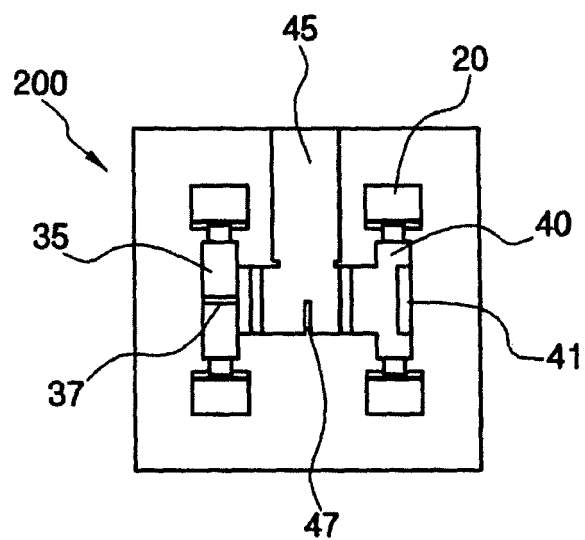


FIG 67

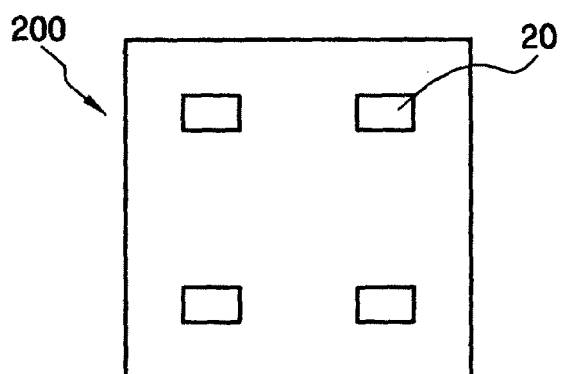


FIG 68

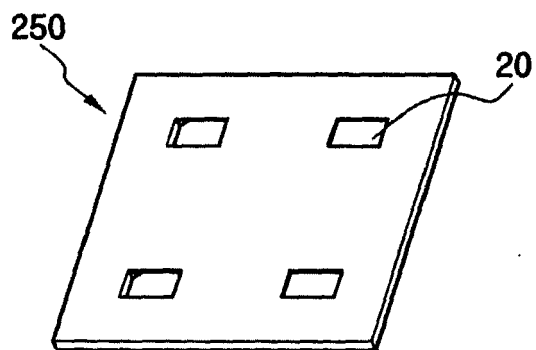


FIG 69

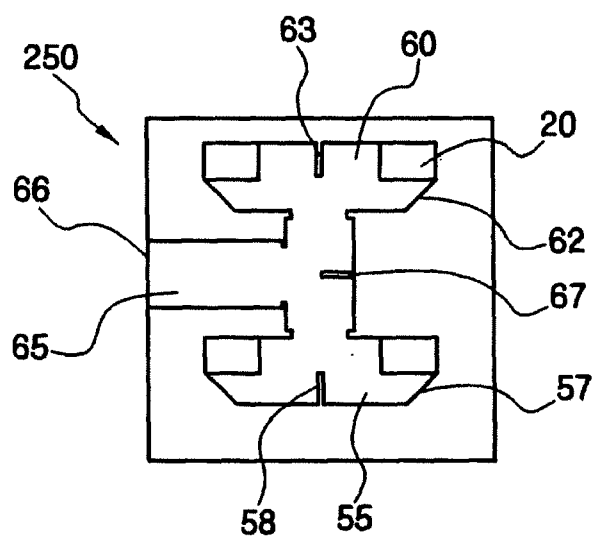


FIG 70

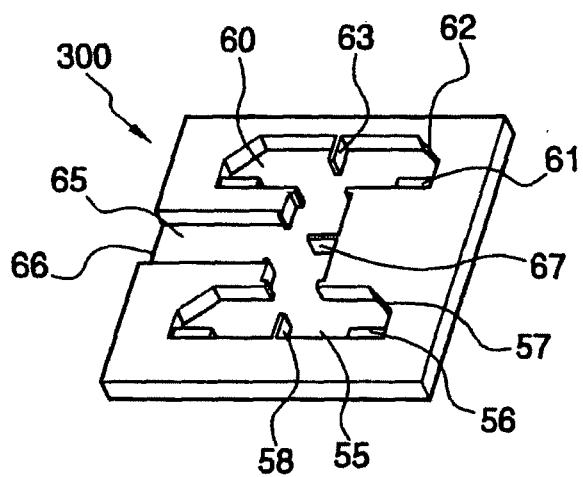


FIG 71

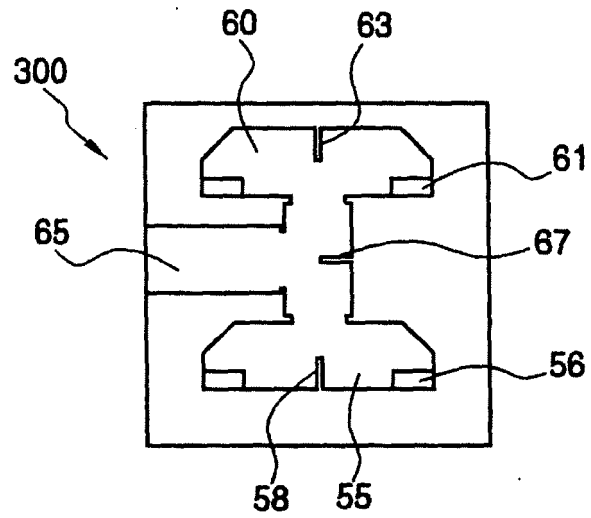
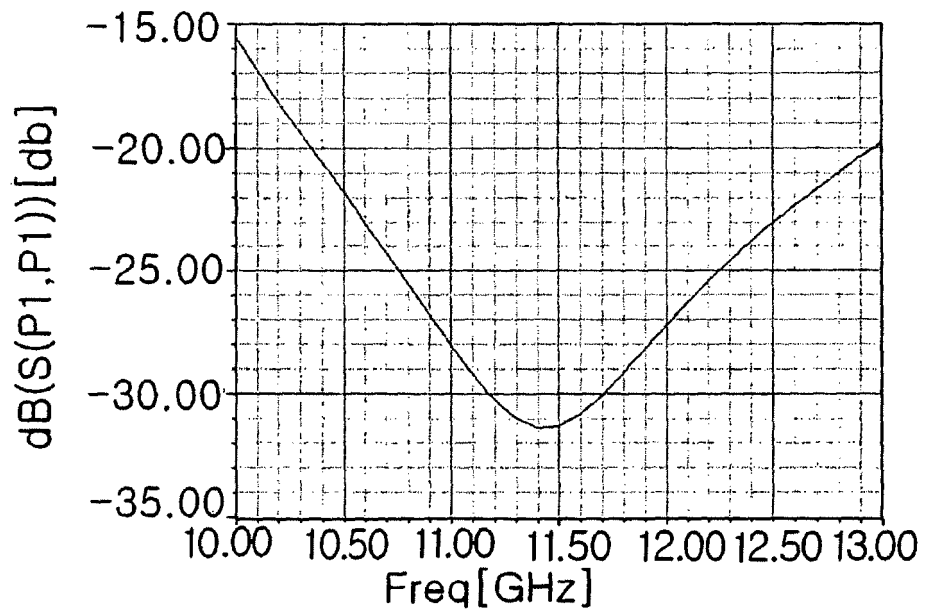


FIG 72





EUROPEAN SEARCH REPORT

Application Number
EP 10 18 8071

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)
X	WO 95/23440 A1 (FORTEL TECHNOLOGY LTD [GB]; COLLINS JOHN LOUIS FREDERICK C [GB]) 31 August 1995 (1995-08-31) * the whole document *	1-9	INV. H01Q13/02 H01Q21/00 H01Q21/06 H01Q21/24 H01P1/161 H01P3/123
X	EP 0 812 029 A1 (HUGHES AIRCRAFT CO [US] HUGHES ELECTRONICS CORP [US]) 10 December 1997 (1997-12-10) * abstract * * column 3, line 45 - column 4, line 8 *	1-9	
X	DE 44 25 048 A1 (SIEMENS AG [DE]) 18 January 1996 (1996-01-18) * the whole document *	1-9	
			TECHNICAL FIELDS SEARCHED (IPC)
			H01Q H01P
The present search report has been drawn up for all claims			
Place of search Munich		Date of completion of the search 23 December 2010	Examiner van Norel, Jan
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document</p>			

1
EPO FORM 1503 03.82 (P04C01)

**ANNEX TO THE EUROPEAN SEARCH REPORT
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EP 10 18 8071

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

23-12-2010

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