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(71) Applicant: BAE SYSTEMS plc London SW1Y 5AD (GB)

(72) Inventor: The designation of the inventor has not yet been filed

(74) Representative: BAE SYSTEMS plc

**Group IP Department** 

P.O. Box 87

**Warwick House** 

**Farnborough Aerospace Centre** 

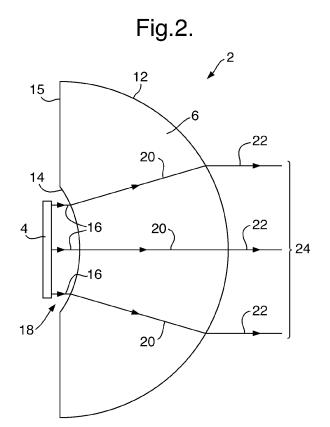
**Farnborough** 

Hampshire GU14 6YU (GB)

#### (54)Antenna system

(57)An antenna system, comprising: a phased array antenna (4); and a dielectric lens arrangement (6), for example a single solid dielectric lens (6) comprising a substantially spherical convex surface (12) and a concave surface (14); wherein the dielectric lens arrangement (6) is arranged to magnify the effective aperture of the phased array antenna (4). The concave surface (14)

is positioned within the near field of the phased array antenna (4). The phased array antenna (4) is operated at a frequency greater than or equal to 50GHz. The antenna system retains some ability to electronically scan the beam. The antenna system may be for transmission and/or reception. The antenna system may be used for example for communication between two vehicles.



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#### FIELD OF THE INVENTION

**[0001]** The present invention relates to wireless antenna systems and arrangements, in particular systems and arrangements including one or more phased array antennas.

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### **BACKGROUND**

**[0002]** Phased array antennas are well known, and are used for example to provide wireless links. One or more phased array antennas may provide transmission and one or more phased array antennas may provide reception.

**[0003]** Signal processing arrangements for modulating and otherwise providing suitable transmission signals, and for receiving and demodulating received signals, are also well known.

**[0004]** Phased array antennas and signal processing arrangements are provided in many variations for many different uses. In many applications, frequencies of less than 10GHz are employed, requiring relatively large antenna sizes. For a given phased array antenna, there will be limitations on its useful range (i.e. distance between transmitter and receiver) of operation. Conventionally, to increase range, antenna size and/or power must be increased.

#### SUMMARY OF THE INVENTION

**[0005]** The present inventors have realised it would be desirable to provide an antenna system or arrangement that gives a required range of operation by a solution other than that of increasing antenna size and/or power. The present inventors have realised this would be particularly desirable in a context of achieving ranges of, say, 100m, with small equipment sizes, as such a solution could efficiently be deployed in applications where larger equipment would be less suitable, for example as a wireless communication system between vehicles, e.g. between vehicles.

**[0006]** In a first aspect, the present invention provides an antenna system, comprising: a phased array antenna; and a dielectric lens arrangement; wherein the dielectric lens arrangement is arranged to magnify the effective aperture of the phased array antenna.

**[0007]** The dielectric lens arrangement may be a single solid dielectric lens.

**[0008]** The solid dielectric lens may comprise a convex surface and a concave surface.

[0009] The convex surface may be substantially spherical.

**[0010]** The side of the dielectric lens arrangement closest to the phased array antenna may be positioned within the near field of the phased array antenna.

[0011] The phased array antenna may be adapted to

be operated at a frequency greater than or equal to 50GHz.

**[0012]** The dielectric lens may be of a material having a dielectric constant greater than or equal to 2.

**[0013]** The dielectric lens may be of a material having a dielectric constant greater than or equal to 5.

**[0014]** The antenna system may be arranged such that the antenna system retains some ability to electronically scan the beam provided by and/or being received by the antenna system.

**[0015]** The antenna system may be adapted to be used as a transmission antenna system.

**[0016]** The antenna system may be adapted to be used as a reception antenna system.

**[0017]** In a further aspect, the present invention provides a wireless communication system comprising, as a transmission antenna system, at least one antenna system according to any of the above aspects.

**[0018]** In a further aspect, the present invention provides a wireless communication system comprising, as a reception antenna system, at least one antenna system according to any of the above aspects.

[0019] In a further aspect, the present invention provides a wireless communication system comprising, as a transmission antenna system, at least one antenna system according to any of the above aspects, and further comprising, as a reception antenna system, at least one antenna system according to any of the above aspects.

[0020] In a further aspect, the present invention provides a use of one or more antenna systems according to any of claims 1 to 9 for communication between two vehicles.

## BRIEF DESCRIPTION OF THE DRAWINGS

### [0021]

Figure 1 is a schematic illustration (not to scale) of a wireless system;

Figure 2 is a schematic illustration (not to scale) showing an antenna system of the wireless system of Figure 1;

Figure 3 is a schematic illustration (not to scale) showing certain dimensional details of the antenna system of Figure 2;

Figure 4 is a diagram illustrating aspects of refraction by a spherical lens;

Figure 5 is a schematic illustration (not to scale) of grooves which are provided at both surfaces of a dielectric lens forming part of the antenna system of Figure 2; and

Figure 6 is a schematic illustration (not to scale) of a phased array antenna 4 forming part of the antenna

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system of Figure 2.

#### **DETAILED DESCRIPTION**

[0022] Figure 1 is a schematic illustration (not to scale) of a first embodiment of a wireless system 1. The wireless system 1 comprises two antenna systems 2, which in this embodiment are the same as each other. Each antenna system 2 comprises a phased array antenna 4 and a dielectric lens 6. The phased array antenna 4 is placed in front of, and spaced apart, from the dielectric lens 6. [0023] The phased array antenna 4 of a first of the antenna systems 2 (which may be termed the transmission antenna system) is electrically coupled to a transmission module 8. The phased array antenna 4 of the other of the antenna systems 2 (which may be termed the reception antenna system) is electrically coupled to a reception module 10.

**[0024]** The phased array antennas 4 are placed close to the respective dielectric lenses 6 so that in operation, in the case of transmission, millimetre waves emitted from the phased array antenna 4 pass through the dielectric lens 6 before continuing onwards away from the phased array antenna, and in the case of reception, external millimetre waves falling on the dielectric lens 6 pass through the dielectric lens 6 before continuing on to fall on the phased array antenna 4.

[0025] The transmission antenna system is positioned remote from the reception antenna system. For example, the transmission antenna system may advantageously be placed on a first vehicle, and the reception antenna system may be placed on a second vehicle. In operation, when the transmission antenna system and the reception antenna system are sufficiently aligned, i.e. in effect sufficiently pointed at each other (within angular ranges that will be described in more detail later below), signals generated/modulated by the transmission module 8 are transmitted from the transmission antenna system 2, received by the reception antenna system, and demodulated/otherwise processed by the reception module 10. [0026] In other embodiments, only one of the antenna systems, e.g. either the transmission antenna system or the reception antenna system, is as described above, and the other antenna system is a conventional antenna system comprising a phased array antenna but without a dielectric lens.

[0027] In yet further embodiments, either one, or both, of the above described antenna systems are coupled to both a transmission module and a reception module, and may individually be used for transmission and/or reception, as opposed to only transmission or only reception.

[0028] In yet further embodiments, any of the above described arrangements are modified by using plural antenna systems for either or both of the functions of transmission and reception.

**[0029]** It will also be appreciated that, as well as the overall wireless system 1 being an embodiment of the invention, paired arrangements of one or more transmis-

sion antenna systems with one or more reception antenna systems also represent embodiments of the present invention; and moreover, a single antenna system 2 (i.e. a phased array antenna with a dielectric lens 2), with a transmission and/or reception module represents an embodiment of the present invention; and also a single antenna system 2 (i.e. a phased array antenna with a dielectric lens 2), without a transmission and/or reception module represents in itself an embodiment of the present invention.

[0030] Figure 2 is a schematic illustration (not to scale) showing the antenna system 2, comprising the phased array antenna 4 and the dielectric lens 6, in further detail. In this embodiment, the dielectric lens 6 is a solid spherical lens, comprising a convex curved outer surface 12 and a concave curved inner surface 14, where the curved outer surface 12 is the surface further away from the phased array antenna 4 and the curved inner surface 14 is the surface closer to the phased array antenna 4. The curved outer surface 12 is larger than the curved inner surface 14. As a consequence, a further extent of surface exists between the curved inner surface 14 and the curved outer surface 12, which for convenience will be termed the remaining inner surface 15.

[0031] In overview, in operation, the dielectric lens 6 effectively acts as a magnifying lens, in the standard way for such a lens, as follows. (For convenience, certain optical terminology is used in the following summary of the effect of the lens, and likewise for convenience certain properties of the millimetre waves employed are simplified or schematised to allow the effect of the lens to be most readily appreciated.) The operation will be described in terms of transmission. It will be appreciated that the reverse operations occur in the case of reception. In operation, the phased array antenna 4 emits electromagnetic waves (in this embodiment millimetre waves) 16 that initially, in the so-called near field, may be considered as being nominally parallel to each other, i.e. providing a nominally parallel beam 18. The curved inner surface 14 of the dielectric lens 6 is positioned relative to the phased array antenna 4 such that the distance there between is smaller than the extent of the near-field, i.e. smaller than the Rayleigh distance. Thus the nominally parallel rays 16 of the nominally parallel beam 18 reach the curved inner surface 14 where they are diverged to provide diverged rays 20. The diverged rays 20 then pass through the dielectric lens 6 to reach the outer curved surface 12, where they are converged to be parallel to each other again and thereby provide a nominally parallel beam 24 exiting the dielectric lens 6 at the curved outer surface 12. The nominally parallel beam 24 is magnified compared to the original nominally parallel beam 18 that was emitted by the phased array antenna 4 and passed into the dielectric lens 6 through the inner curved surface 14, and hence is hereinafter referred to as the magnified nominally parallel beam 24. In other words, the dielectric lens 6 has in effect magnified the effective radiating aperture of the phased array antenna 4 (in the case of reception the dielectric lens 6 in effect magnifies the effective reception aperture of the phased array antenna 4).

**[0032]** Figure 3 is a schematic illustration (not to scale) showing certain dimensional details of the antenna system 2.

**[0033]** In this embodiment, the curved outer surface is substantially a spherical shaped surface, with a radius R of approximately 0.035m (35mm). The centre of the emission surface of the phased array antenna is approximately placed at the centre of the sphere defining the spherical shaping of the outer curved surface 12.

[0034] In this embodiment, the inner curved surface 14 is substantially elliptical shaped with a focal point behind the phased array antenna. More details of the functional effect of this will be described later below with reference to Figure 4. In this embodiment, the focal point is at a distance of approximately 17mm.

**[0035]** In this embodiment, the separation s between the centre of the radiating surface of the phased array antenna and the axially aligned point (i.e. closest point or central point) on the inner curved surface 14 of the dielectric lens 6 is approximately 0.005m (5mm).

**[0036]** In this embodiment, the phased array antenna 4 is approximately square shaped, with sides of length I approximately equal to 0.015m (15mm).

[0037] In this embodiment, the dielectric lens is made of solid nylon, with a dielectric constant  $\varepsilon_r$  approximately equal to 3. However, in other embodiments, other materials with other dielectric constant values may be used. Preferably a dielectric constant equal to or greater than 2 is used. For example, PTFE with dielectric constant of approximately 2 may be used. Also for example, in other embodiments a material called "Eccostock" (trademark) HIK 500F, available from Emerson & Cuming Microwave Products N.V., Nijverheidsstraat 7A, B-2260 Westerlo, Belgium, is used. In this embodiment, this material has a dielectric constant of approximately 5. The effect of different dielectric constant values of the material of the dielectric lens 6 will be discussed later below. Other examples of materials with dielectric constant of approximately  $\varepsilon_r$  = 5, and which advantageously have relatively low loss at 60GHz, are boron nitride and a material called "Macor" (trademark) available from Corning Incorporated Lighting & Materials, Houghton Park CB-08, Corning, New York 14831.

[0038] In other embodiments, other types of lens arrangements (for example multi-lens telescope arrangements such as a Keplerian refractor or a Galilean telescope arrangement) may be used instead of the above described dielectric lens of this embodiment. However, compared to other such possibilities, the use in this embodiment of the dielectric lens 6 described above, i.e. a single solid lens of a relatively high dielectric material and with a shape based on a spherical surface, advantageously provides a reasonable amount of gain i.e. magnification, whilst only requiring a relatively small physical size.

The operation of the antenna system 2 of this embodiment, and in particular the operation of the dielectric lens 6, can further be understood by considering Figure 4, which is a diagram illustrating aspects of refraction by a spherical lens. Figure 4 shows a theoretical spherical lens surface (indicated in Figure 4 by reference numeral 40) of radius R with a centre point indicated in Figure 4 by reference numeral 41, considered in terms of a reference diameter direction (indicated in Figure 4 by reference numeral 42). For any given point (indicated in Figure 4 by reference numeral 44) on the spherical lens surface 40, a height from that point to the reference diameter 42 is termed h; for a ray originating from the centre of the sphere 41 and falling on the surface point 44, the angle between the original direction of that ray and the output (refracted) ray is termed  $\theta$ ; the distance between the focal point of the lens (indicated in Figure 4 by reference numeral 46) and the surface point 44, i.e. the focal length, is termed f; and the angle between the line from the focal point 46 to the surface point 44 and the radius to the surface point 44 is termed  $\xi$ .

**[0040]** A spherical lens of constant dielectric constant brings a bundle of incident rays to an approximate focus. The location of the focal point for paraxial rays depends only on the dielectric constant of the sphere (see Figure 4). Using the small angle approximation, the focal length f is given in terms of the radius of the sphere R by

$$f = \frac{R\sqrt{\varepsilon}}{\sqrt{\varepsilon} - 1}$$

. When, for example, the dielectric constant is  $\epsilon$  = 4, the focus lies on the circumference. As the dielectric constant is increased, the focus approaches but never reaches the centre of the sphere.

**[0041]** By virtue of the phased array antenna 4 being positioned behind the concave curved inner surface 14 at the centre of the sphere, the operation is similar to that of a Galilean telescope, i.e. the rays are approximately directed as illustrated in, and described above with reference to, Figure 2.

**[0042]** The concave curved inner surface 14 is preferably designed to convert the cone of rays from the convex outer surface 12 to a parallel bundle. The magnification m available for such an arrangement is

$$m = \frac{f}{f - R} = \sqrt{\varepsilon}$$

and therefore depends only on the dielectric constant. For example, (as per one preferred embodiment) a magnification of 2.236 is achieved by the use of the above mentioned material with a dielectric constant equal to 5. By providing a magnification of 2.236 (in both azimuth

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and elevation), the useful range of the antenna system 2 is, to a first approximation, increased by a factor of 2.236<sup>2</sup> i.e. approximately 5. Thus, in approximate terms, although using a phased array antenna with a useful range of approximately 20m (as is the case for the phased array antenna 4 of this embodiment, which will be described in more detail later below with reference to Figure 6), the overall antenna system 2 provides a useful range of approximately 100m. (Note each lens increases the effective aperture in both azimuth and elevation dimensions.)

**[0043]** In other embodiments, the radius R of the lens can be freely chosen within reason, but preferably it should be larger than the magnified image of the array. However, if it is too small, diffraction may dominate.

[0044] By using a spherical shape for the convex outer curved surface 12 of the dielectric lens 6, distortion or deviation arising from the different swept angles involved in the operation of the phased array antenna 4 is reduced or avoided. However, in other embodiments, this advantage may be traded off with improved gain at specific angles by using shapes other than spherical, for example by using elliptical or hyperbolic shaped surfaces. It will also be appreciated that the whole of the outer surface need not be fully in compliance with the basic operational shape of the surface. For example, the surface may be truncated with a cylinder shape at the rear to aid mounting of the lens. Also for example, grooves or notches or ridges (in addition to the grooves to be described later below with reference to Figure 5) may be included for the purposes of fixing the dielectric lens mechanically to clamps or the like. Depending on their positions or size, such variations may degrade performance but only to a limited extent compared to the overall magnification and uniformity achieved by the lens, or may, if located sufficiently radially distant from the magnified image of the antenna, have no, or at least negligible, interplay with the magnification process.

**[0045]** By using an elliptical shape for the concave inner curved surface 14, "optical" performance tends to be optimised. However, since a shallow curvature is preferable, the exact details of the curved surface shape are not very significant, i.e. in other embodiments other shapes may be used for the concave curved inner surface.

[0046] In this embodiment the inner curved surface 14 and the outer curved surface 12 are both provided with (i.e. the surfaces comprise a further detail of shaping) with concentric grooves for the purpose of providing, at least to some extent, impedance matching, i.e. the grooves function as an anti-reflection measure. The grooves represent a way of minimising the mismatch between the high dielectric constant of the lens and that of free space. Figure 5 is a schematic illustration (not to scale) of the grooves which are provided at both surfaces. The dotted line indicated by reference numeral 52 represents a hypothetical smooth form of the respective curved surfaces. The grooves 50 are provided by virtue

of troughs 54 and ridges 56. The grooves are preferably at less than half-wavelength pitch, which in the case of operation at 60GHz means a pitch of 2.5mm or less is desirable. In this embodiment, a pitch of 1.5mm is provided, with the ridges 56 and the troughs 54 each being 0.75mm wide. The height or depth of the grooves is 0.85mm. The optimum values depend upon the intended frequency to be used.

**[0047]** In other embodiments, anti-reflection properties may instead be provided by the use of antireflection coatings applied to the curved surfaces, or by any other appropriate means.

**[0048]** In the above described embodiments, the shape of the dielectric lens 6 may be provided by any suitable manufacturing process, for example by machining a solid block of the material or by casting.

[0049] Further details of the phased array antenna 4 of this embodiment will now be described. Figure 6 is a schematic illustration (not to scale) of the phased array antenna 4. In this embodiment the phased array antenna 4 comprises a total of fifty-two dipole-like antenna elements 60 arranged in eight alternating columns of six and seven elements. The overall size of the antenna is approximately 0.015m x 0.015m (15mm x 15mm). The phased array antennas 4 of this embodiment provide thirty-six beams with wide elevation and azimuth scan angular ranges to allow for non line of sight operation. These are commercial units sold by AboCom Systems Inc. (trademark) of No.77, Yu-Yih Road, Chu-Nan Chen, Miao-Lih Hsuan, Taiwan, R.O.C. that are provided for the WirelessHD standard market (i.e. digital video data).

**[0050]** In this embodiment the phased array antenna is operated in the frequency range of 57 to 66GHz.

**[0051]** Beam-forming electronics are used to drive the array to produce a fixed set of beams using phase shifters. These may be positioned directly behind the radiating array, or may be provided in a separate module, for example being provided as part of the transmission module 8. (In the case of reception, the corresponding electronics serves to perform the receive signal amplification and beamforming function). This reception electronics may be positioned directly behind the radiating array, or may be provided in a separate module, for example being provided as part of the reception module 10.)

[0052] In this embodiment, as mentioned above, the phased array antenna 4 operating on its own, i.e. without the dielectric lens 6, can generate a beam that covers a wide azimuth and elevation scan angular range. The angular range of the antenna system 2, i.e. the effect of the dielectric lens 6, is that the angular output range is reduced. In this embodiment, the reduction in angular range is related to the reduction in the beamwidth. In general the improvement in distance range is at a cost of angular range. However, there are many applications where such a trade-off is either irrelevant or at least bearable, for example in a vehicle to vehicle communications application as mentioned earlier. Also, in some applications the relative positioning and directionality between

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the transmission antenna system and the reception antenna system can be fixed, in which case relatively narrow angular range can be tolerated (and may even be advantageous). In yet further embodiments, the achievable azimuth angle can be traded off with the achievable elevation angle, for example by use of asymmetrical lens shapes.

**[0053]** It will be appreciated that an advantage of the above described embodiments is that increased distance range is achieved whilst retaining at least a significant extent of the ability to electronically scan the beam.

**[0054]** In the above described embodiments the phased array antenna is operated at a frequency between 57 to 66GHz. By using such a relatively high frequency, the physical size of the dielectric lens can be kept small. Thus, in preferred embodiments, the phased array antenna is operated at frequencies greater than or equal to 50GHz. However, in other embodiments other frequencies may be used.

**[0055]** In the above described embodiments the phased array antenna is as described with reference to Figure 6. However, this need not be the case, and in other embodiments other implementations or details of phased array antenna may be used instead, for example different sizes, different angular output, different numbers of antenna elements, different numbers of beams, different beam properties, and so on.

**[0056]** Likewise, some or all of the various dimensions of the various elements employed in the above described embodiments, e.g. sizes of the dielectric lens and the phased array antenna, and spacing between the various elements employed in the above described embodiments, may be different in other embodiments.

## **Claims**

1. An antenna system, comprising:

a phased array antenna (4); and a dielectric lens arrangement (6);

wherein the dielectric lens arrangement (6) is arranged to magnify the effective aperture of the phased array antenna (4).

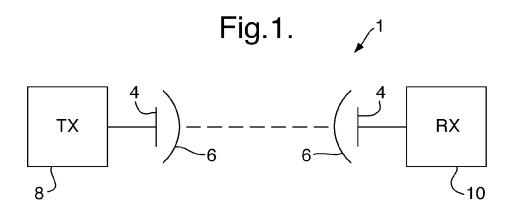
- 2. An antenna system according to claim 1, wherein the dielectric lens arrangement (6) is a single solid dielectric lens (6).
- **3.** An antenna system according to claim 2, wherein the solid dielectric lens (6) comprises a convex surface (12) and a concave surface (14).
- **4.** An antenna system according to claim 3, wherein 55 the convex surface (12) is substantially spherical.
- 5. An antenna system according to any of claims 1 to

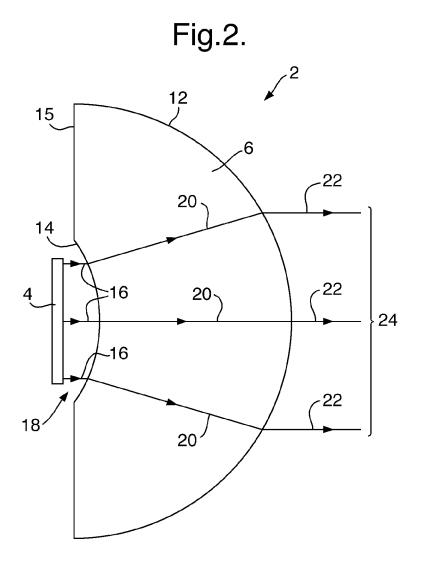
4, wherein the side (14) of the dielectric lens arrangement (6) closest to the phased array antenna (4) is positioned within the near field of the phased array antenna (4).

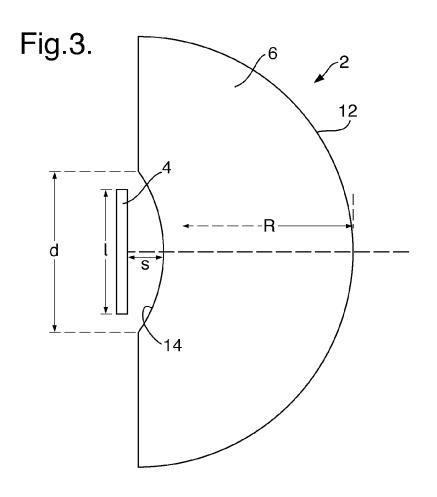
**6.** An antenna system according to any of claims 1 to 5, wherein the phased array antenna (4) is adapted to be operated at a frequency greater than or equal to 50GHz.

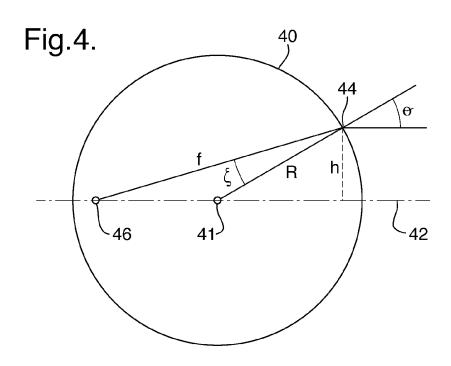
- 7. An antenna system according to any of claims 2 to 6, wherein the dielectric lens (6) is of a material having a dielectric constant greater than or equal to 2.
- 15 8. An antenna system according to claim 7, wherein the dielectric lens (6) is of a material having a dielectric constant greater than or equal to 5.
  - 9. An antenna system according to any of claims 1 to 8, arranged such that the antenna system retains some ability to electronically scan the beam provided by and/or being received by the antenna system.
  - **10.** An antenna system according to any of claims 1 to 9, adapted to be used as a transmission antenna system.
  - An antenna system according to any of claims 1 to 10, adapted to be used as a reception antenna system
  - **12.** A wireless communication system comprising, as a transmission antenna system, at least one antenna system according to any of claims 1 to 9.
  - **13.** A wireless communication system comprising, as a reception antenna system, at least one antenna system according to any of claims 1 to 9.
- 40 14. A wireless communication system comprising, as a transmission antenna system, at least one antenna system according to any of claims 1 to 9, and further comprising, as a reception antenna system, at least one antenna system according to any of claims 1 to 9.
  - **15.** Use of one or more antenna systems according to any of claims 1 to 9 for communication between two vehicles.

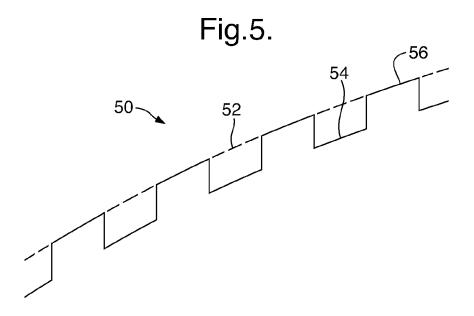
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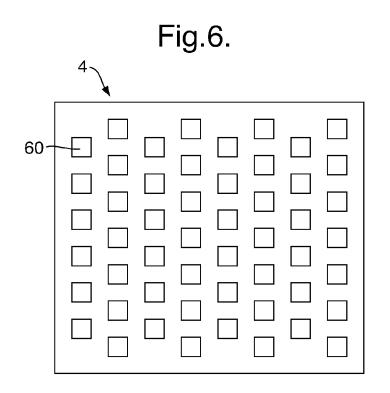














# **EUROPEAN SEARCH REPORT**

**Application Number** EP 10 27 5017

Category	Citation of document with indic of relevant passage		Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)	
Y	WO 2007/136289 A1 (IN ALAMOUTI SIAVASH M [LALEXANDROV) 29 November page 4, line 30 - per page 10, line 5 - per page 13, line 7 - per figures 2A, 2B, 4A,	US]; MALTSEV ÄLEXANDER Der 2007 (2007-11-29) Dage 8, line 24 * Dage 11, line 6 * Dage 14, line 9 *	1-7,9-14 8,15	INV. H01Q3/30 H01Q15/08 H01Q19/06 H01Q21/06	
X Y	EP 0 773 598 A2 (DENS CORP) 14 May 1997 (19 * column 5, line 1 - * figures 1, 2 *	997-05-14)	1,2,6, 9-14 15		
X Y	GB 2 189 650 A (GEN E 28 October 1987 (1987 * page 1, line 6 - li * page 1, line 85 - p * figures 1, 2 *	7-10-28) ine 10 *	1,2,5, 9-11 15		
Y	JORGE R COSTA ET AL: Double-Shell Integrat Antenna" IEEE ANTENNAS AND WIF LETTERS, IEEE, PISCAT vol. 7, 1 January 200 781-784, XP011237329 ISSN: 1536-1225 * page 782, right-har line 41 *	ed Scanning Lens RELESS PROPAGATION FAWAY, NJ, US, 08 (2008-01-01), pages	8	TECHNICAL FIELDS SEARCHED (IPC)	
Y	WO 2005/107181 A1 (PH PROPERTY [DE]; KONINK NV [NL) 10 November 2 * abstract * * page 3, line 29 - p * figures 1, 2 *	KL PHILIPS ELECTRONICS 2005 (2005-11-10)	15		
	The present search report has bee	n drawn up for all claims			
	Place of search Munich	Date of completion of the search 28 April 2010	Kön	Examiner pe, Maro	
CATEGORY OF CITED DOCUMENTS  X: particularly relevant if taken alone Y: particularly relevant if combined with another document of the same category A: technological background O: non-written disclosure P: intermediate document		T : theory or principl E : earlier patent doc after the filing dat D : document cited in L : document cited fo	T: theory or principle underlying the invention E: earlier patent document, but published on, or after the filing date D: document cited in the application L: document cited for other reasons  &: member of the same patent family, corresponding		



# **EUROPEAN SEARCH REPORT**

Application Number EP 10 27 5017

- 1	DOCUMENTS CONSIDEREI				
ategory	Citation of document with indication of relevant passages	n, where appropriate,	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)	
	apRhys T L: "The homoge millimeter-wave lens" In: "Fourth Internation Propagation Symposium" 1966, IEEE , New York , pages 59-66 * the whole document *	al Antennas and	1-4,6	TECHNICAL FIELDS SEARCHED (IPC)	
	The present search report has been di	•		Examine-	
Place of search  Munich		Date of completion of the search  28 April 2010	Кöр	Examiner Köppe, Maro	
CATEGORY OF CITED DOCUMENTS  X: particularly relevant if taken alone Y: particularly relevant if combined with another document of the same category A: technological background O: non-written disclosure		T : theory or principle E : earlier patent doo after the filling date D : document cited in L : document cited for	T: theory or principle underlying the invention E: earlier patent document, but published on, or after the filling date D: document oited in the application L: document oited for other reasons  8: member of the same patent family, corresponding		

## ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 10 27 5017

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

28-04-2010

CN 101427422 A 06-05-20 CN 101427420 A 06-05-20 EP 2025045 A1 18-02-20 EP 2022135 A1 11-02-20 EP 2022188 A1 11-02-20 JP 2009538034 T 29-10-20 WO 2007136292 A1 29-11-20 US 2009219903 A1 29-11-20 US 2009219903 A1 24-12-20 US 2009315794 A1 24-12-20 US 2009315794 A1 24-05-1997 JP 9191213 A 22-07-19 GB 2189650 A 28-10-1987 FR 2717312 A1 15-09-19 WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20 US 20095107181 A1 10-11-2005 JP 2007536860 T 10-11-2005 J	CN 101427422 A 06-05-20 CN 101427420 A 06-05-20 EP 2025045 A1 18-02-20 EP 2022135 A1 11-02-20 EP 2022188 A1 11-02-20 JP 2009538034 T 29-10-20 WO 2007136292 A1 29-11-20 US 2009219903 A1 29-11-20 US 2009219903 A1 24-12-20 US 2009315794 A1 24-12-20 US 2009315794 A1 24-05-1997 JP 9191213 A 22-07-19 GB 2189650 A 28-10-1987 FR 2717312 A1 15-09-19 WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20 US 20095107181 A1 10-11-2005 JP 2007536860 T 10-11-2005 J	Patent document cited in search report		Publication date		Patent family member(s)		Publication date
GB 2189650 A 28-10-1987 FR 2717312 A1 15-09-19 WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20	GB 2189650 A 28-10-1987 FR 2717312 A1 15-09-19 WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20	WO 2007136289	A1	29-11-2007	CN CN EP EP JP WO WO	101427422 101427420 2025045 2022135 2022188 2009538034 2007136292 2007136293 2009219903	A A1 A1 A1 T A1 A1 A1	06-05-20 06-05-20 06-05-20 18-02-20 11-02-20 29-10-20 29-11-20 29-11-20 03-09-20 24-12-20
WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20	WO 2005107181 A1 10-11-2005 JP 2007536860 T 13-12-20	EP 0773598	A2	14-05-1997	JР	9191213	Α	22-07-19
		GB 2189650	Α	28-10-1987	FR	2717312	A1	15-09-19
		WO 2005107181	A1	10-11-2005				13-12-20 23-08-20

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