(11) **EP 2 374 568 A1**

(12) EUROPEAN PATENT APPLICATION

(43) Date of publication: 12.10.2011 Bulletin 2011/41

(51) Int Cl.: **B23K 20/02** (2006.01)

C23C 14/34 (2006.01)

(21) Application number: 11173006.5

(22) Date of filing: 25.02.2005

(84) Designated Contracting States:

AT BE BG CH CY CZ DE DK EE ES FI FR GB GR

HU IE IS IT LI LT LU MC NL PL PT RO SE SI SK TR

(30) Priority: **27.02.2004 US 548790 P 20.08.2004 US 603528 P 22.02.2005 US 62777**

(62) Document number(s) of the earlier application(s) in accordance with Art. 76 EPC: 05714100.4 / 1 727 643

- (71) Applicant: **HOWMET CORPORATION Cleveland, Ohio 44105 (US)**
- (72) Inventors:
 - Butzer, Greg A.
 Whitehall, MI Michigan 49461 (US)

- Huizenga, Robert H.
 North Muskegon, MI Michigan 49445 (US)
- Mussman, Steven D.
 North Muskegon, MI Michigan 49445 (US)
- (74) Representative: Hoeger, Stellrecht & Partner Patentanwälte
 Uhlandstrasse 14c
 70182 Stuttgart (DE)

Remarks:

This application was filed on 07-07-2011 as a divisional application to the application mentioned under INID code 62.

- (54) Billet or bar for a sputtering target with Molybdenum; Corresponding sputtering target
- (57) A billet or bar is provided for a sputtering target and having a first powder preform comprising molybdenum and a second powder preform comprising molyb-

denum bonded together at a diffusion bond that corresponds to a location where a powder layer comprising molybdenum formerly resided between the first and second preforms.

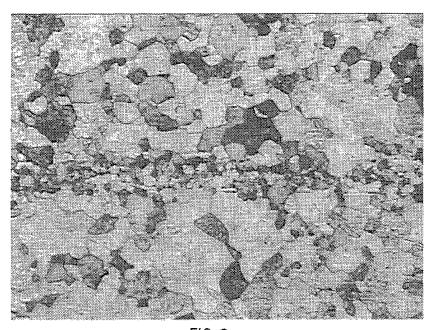


FIG. 2

25

40

Cross Reference to Related Applications

[0001] This application claims benefits and priority of provisional application Serial No. 60/548,790 filed February 27, 2004, and provisional application Serial No. 60/603,528 filed August 20, 2004.

1

Field of the Invention

[0002] The present invention relates to a method of making a large billet or bar comprising molybdenum (Mo) for a sputtering target and to the billet and sputtering target produced by the method.

Background of the Invention

[0003] The current method of making a large molybdenum sputtering target is to cold isostatic press (CIP) Mo powder, sinter to reduce the oxygen content and then hot roll to a plate length/width/thickness desired. The plate then is machined to final tolerance. Mo sputtering targets made using the CIP, sinter and roll process are disadvantageous due to the sputter yield of the target and of the etching characteristics of the deposited thin film. This is related to the plate microstructure that is formed during the rolling process.

Summary of the Invention

[0004] The present invention provides in an illustrative embodiment a method of making a billet or bar comprising molybdenum (Mo) for a sputtering target wherein two or more sintered powder metal bodies (e.g. ingot bodies) comprising Mo are placed adjacent one another (e.g. stacked one on the other) with powder metal comprising Mo present at joints between adjacent bodies. The adjacent bodies are hot isostatically pressed to form a diffusion bond at each metal-to-powder metal layer-to-metal joint between adjacent bodies.. This forms a billet or bar that can be machined or otherwise formed to provide a large sputtering target. The number and dimensions of the bodies placed adjacent one another are selected to yield a desired large size billet or bar suitable for the sputtering target. For example, a billet or bar having a length of over 3000mm and cross-section of 225mm by 225mm can be provided by practice of the invention.

[0005] In another illustrative embodiment of the present invention, a method is provided for making a billet or bar comprising molybdenum (Mo) for a sputtering target wherein two or more sintered powder metal bodies comprising Mo are diffusion bonded together at one or more metal-to-metal joints therebetween in a first hot isostatic pressing operation to form a preform. Two or more preforms then are placed adjacent one another (e.g. stacked one on the other) with a powder metal layer comprising Mo present at joints between the adjacent pre-

forms. The adjacent preforms are hot isostatically pressed in a second hot isostatic pressing operation to form a diffusion bond at each metal-to-powder metal layer-to-metal joint between adjacent preforms to form a billet or bar that can be machined or otherwise formed to provide a large sputtering target. The number and dimensions of the preforms placed adjacent one another are selected to yield a desired large size the billet or bar suitable for the sputtering target.

[0006] The billet or bar for the sputtering target exhibits a microstructure comprising equiaxed grains of desired small grain size (e.g. about 30 microns or less) and exhibits a low oxygen content of less than about 100 ppm (part per million by weight) as a result of use of low oxygen sintered Mo powder metal bodies. The billet or bar for the sputtering target includes a density greater than 99% of theoretical density and one or more diffusion bond joints where the metal powder was formerly present at the joints between adjacent bodies or preforms.

[0007] Other advantages, features, and embodiments of the present invention will become apparent from the following description.

Brief Description of the Drawings

[0008] Figure 1 is a photomicrograph at 100X of a metal-to powder metal layer-to-metal diffusion bond joint between sintered Mo powder metal ingot bodies.

[0009] Figure 2 is a photomicrograph at 100X of a metal-to-metal diffusion bond joint between plate-shaped sintered Mo powder metal bricks.

Description of the Invention

[0010] The present invention provides a method of making an elongated body, such as a large billet or bar, comprising molybdenum (Mo) for a sputtering target. For purposes of illustration and not limitation, the method can be used to make a billet or bar for the sputtering target having a bar length of 3000mm and above and bar cross-sectional dimensions of 225mm by 225mm (mm is millimeters) and less, although practice of the invention is not limited to any particular size billet/bar as any size may be made suitable for an intended target application.

45 The billet or bar for the sputtering target exhibits a microstructure comprising equiaxed grains of desired small grain size (e.g. about 30 microns or less) and exhibits a low oxygen content of less than about 100 ppm (part per million by weight) as explained below. The billet or bar for the sputtering target includes a density of greater than 99% of theoretical density.

[0011] An illustrative embodiment of the method of the invention starts with sintered powder metal plate-shaped ingot bodies comprising Mo having an oxygen content of less than about 100 ppm (parts per million by weight). The ingot bodies are made by cold isostatic pressing (CIP) of commercially available Mo powders in a suitable rubber container to produce a pressed ingot body and

20

35

40

then sintering the ingot body in a designated atmosphere (e.g. hydrogen) to reduce the oxygen content thereof to less than about 100 ppm by weight and increase the theoretical density thereof to greater than 94%. For purposes of illustration and not limitation, commercially available Mo powder having a particle size of 3 to 10 microns, purity of 99.95% by weight, and oxygen content typically of less than 1000 ppm by weight is loaded into a rubber bag and steel die to produce a near net shape ingot body when the rubber bag and steel die package with Mo powder therein are cold isostatically pressed (CIP) at room temperature at appropriate pressure (e.g. 15 to 30 ksi gas pressure), although other CIP parameters may be used. The near net shape ingot body exhibits a density greater than 60% of theoretical density. An illustrative ingot body after CIP for one particular sputtering target application may have a size of 220mm by 210mm with about 600mm thickness, although practice of the invention is not limited to any particular size CIP'ed ingot body as any size may be made suitable for an intended target application. For example, another illustrative ingot body after CIP may have a size of 220mm by 210mm with about 200mm thickness. The CIP ingot body then is sintered. For purposes of illustration and not limitation, the CIP ingot body is induction sintered at an appropriate temperature and time in an appropriate atmosphere (e.g. at 1800 degrees C for 18-24 hours in a partial hydrogen atmosphere) effective to reduce oxygen content of the CIP'ed ingot body to less than 100 ppm by weight, although other sintering parameters may be employed. The sintered Mo powder metal ingot body exhibits a density greater than 94% of theoretical density and 99.95% purity by weight basis with the above dimensions for purposes of illustration and not limitation. Such low oxygen ingot bodies can be purchased from H.C. Starck, Coldwater, Michigan, in various shapes and dimensions suitable to make a desired sputtering target.

[0012] The next step in the method embodiment of the invention involves HIP'ing two or more of the ingot bodies under special joint conditions in a hot isostatic pressing operation to form a relatively large billet or bar for the sputtering target. For example, two ingot bodies described above have their outer top and bottom major side surfaces machined and cleaned. A HIP can of low carbon steel is provided having internal dimensions of 225mm by 225mm with a height of 2300mm. One ingot body is placed in the HIP can with its machined major side surface facing sideways. A second ingot body is placed in the HIP can with its machined major side surface facing the major machined side of the first ingot body. A gap of approximately 6mm is left between the ingot bodies. This process is repeated until the HIP can is full of ingot bodies arranged side-by-side. Then, commercially available Mo metal powder is sprinkled on the upwardly facing machined major side surface of, as well as optionally around edges, of the first preform in the HIP can. For purposes of illustration and not limitation, the Mo metal powder is placed as a layer in the gaps between the adjacent ingot bodies in the HIP can. The oxygen content of the commercially available Mo powder metal filling the gaps typically is less than 1000 ppm by weight.

[0013] Additional Mo metal powder may be placed about the edges of the ingot bodies to fill up any gaps between the HIP can and the ingot bodies. This process continues until all gaps have been filled. The remaining sidewall of the HIP can having an evacuation stem then is welded to the HIP can to seal it.

[0014] Before the HIP'ing operation, the HIP can is leak tested using helium gas through the stem on the welded sidewall. Several of the leak-tested HIP cans each with CIP'ed and sintered ingot bodies therein are placed in a degas oven and heated to an appropriate temperature (e.g. 600 degrees F) while evacuating the HIP cans (e.g. to less than 10-5 torr) via the stems until an appropriate leak rate (e.g. less than 100 microns per minute) is attained. The HIP can is then placed in a conventional HIP vessel and HIP'ed at a temperature, pressure and time (e.g. 1236 degrees C at a gas pressure of 1034 bar for 300 minutes) to effect diffusion bonding of the metal (Mo)-to-powder metal (Mo) layer-to-metal(Mo) at the joints between the adjacent ingot bodies to form a billet or bar, although other HIP parameters may be used. The number and dimensions of the ingot bodies HIP'ed are selected to yield a desired large size the billet or bar suitable for the sputtering target.

[0015] The final HIP'ed billet or bar for the sputtering target exhibits a microstructure comprising equiaxed grains of desired small grain size (e.g. about 30 microns or less) and exhibits a low oxygen content of less than about 100 ppm (part per million by weight) as a result of use of low oxygen sintered Mo powder metal ingot bodies and of the HIP process effecting diffusion of oxygen from the commercially available Mo powder metal at each joint between adjacent ingot bodies. For example, it is through the HIP process that the oxygen from the commercially available Mo powder metal joint diffuses into the low oxygen (less than 100 ppm O) ingot bodies, reducing the oxygen content in the joint to less than 100 ppm by weight. Figure 1 shows the diffusion bond joint achieved at an initial metal (Mo)-to-powder metal(Mo) layer-to-metal (Mo) joint by the procedure set forth above. The billet or bar for the sputtering target thereby includes one or more diffusion bond joints where the Mo powder layer was formerly present in the gaps between the adjacent ingot bodies in the HIP can.

[0016] Pursuant to another method embodiment of the invention, two or more sintered Mo powder metal bricks (ingot bodies) of the type described above are diffusion bonded together at one or more metal-to-metal joints therebetween in a first hot isostatic pressing operation to form two or more preforms. The preforms then are placed adjacent one another (e.g. stacked one on the other) with a Mo powder layer present at joint(s) between adjacent preforms. The adjacent preforms are hot isostatically pressed in a second hot isostatic pressing operation to form a diffusion bond at each joint between the

15

20

25

adjacent preforms to form a billet or bar that can be machined or otherwise formed to provide a large sputtering target. The number and dimensions of the preforms placed adjacent one another are selected to yield a desired large size billet or bar suitable for the sputtering target.

[0017] For purposes of illustration and not limitation, to form the preforms, two plate-shaped Mo powder bricks made as described above have their mating flat major side surfaces (i.e. largest area surfaces) machined to 180 to 220 RMS (root mean square) surface finish and cleaned to insure adequate metal-to-metal contact when the major side surfaces are placed in contact to form a metal-to-metal joint therebetween. Typically, the sintered bricks are stacked one atop the other in the form of a sandwich with a metal(Mo)-to-metal(Mo) joint between the major side surfaces thereof. The stacked sintered bricks are placed in a mild steel HIP can for hot isostatic pressing (HIP'ing). For example, the stacked sintered bricks can be placed on one end cover of the HIP can. Then, the top end cover of the HIP can is placed atop the Stacked sintered bricks followed by placement of a sidewall of the HIP can between the top and bottom covers about the stacked sintered bricks. The sidewall then is welded in position to the top and bottom covers of the HIP can.

[0018] Before HIP'ing, the HIP can is leak tested using helium gas using stems welded on one end cover. Several of the leak-tested HIP cans each with the stacked sintered plate-shaped bricks therein are placed in a degas oven and heated to an appropriate temperature (e.g. 600 degrees F) while evacuating the HIP cans (e.g. to less than 10-5 torr) via the stems until an appropriate leak rate (e.g. less than 100 microns per minute) is attained. The HIP cans then are placed in a conventional HIP vessel and HIP'ed at a temperature, pressure and time (e.g. 1400 degrees C at a gas pressure of 1034 bar for 240 minutes) to effect metal(Mo)-to-metal(Mo) diffusion bonding between the machined major side surfaces of the Mo powder metal bricks, although other HIP temperatures, pressures, and times can be used.

[0019] For purposes of illustration and not limitation, each HIP may have internal dimensions of 225 mm by 225 mm by 625 mm. Each HIP can is coated with alumina internally as a release agent. The HIP treatment produces a HIP'ed preform comprising a sandwich of two plateshaped bricks diffusion bonded together at their inner mating major surfaces. Figure 2 shows the diffusion bond achieved at the metal-to-metal joint of the plate-shaped bricks by the procedure set forth above.

[0020] The HIP'ed preforms are removed from the HIP vessel followed by machining of the outer flat major side surfaces of each preform sandwich to 180 to 220 RMS surface finish for purposes of illustration and not limitation. These outer flat major side surfaces correspond to outer top and bottom surfaces of the preform sandwich when it placed on a horizontal surface with the diffusion bonded inner surfaces parallel with the surface.

[0021] The next step in this method embodiment of the invention involves HIP'ing two or more preforms under special joint conditions in a second hot isostatic pressing operation to form a relatively large billet or bar for the sputtering target. For example, two preforms described above having their outer top and bottom major side surfaces machined and cleaned are placed in a HIP can as follows. A HIP can of low carbon steel sans top can cover is provided having internal dimensions of 225 mm by 225 mm with a height of 2300 mm. One preform is placed in the HIP can (sans top can cover) with its machined major side surface facing upwardly. Then, commercially available Mo metal powder is sprinkled on the upwardly facing machined major side surface of, as well as optionally around edges, of the first preform in the HIP can. For purposes of illustration and not limitation, the Mo metal powder is placed as a layer of uniform depth of about 3 mm on the first preform in the HIP can. The Mo powder metal forming the layer typically has an oxygen content of less than 1000 ppm by weight.

[0022] Then the second preform is placed in the HIP can (sans top can cover) with its machined major side surface facing downwardly toward the machined major side surface of the first preform with the Mo powder metal layer thereon so that the machined major side surface of the second preform contacts the Mo powder metal layer. Additional Mo metal powder is placed about the edges of the second (top) preform. This process continues with placement of additional preforms in the HIP can until the HIP can is full. The top cover of the HIP can having an evacuation stem then is welded to the can sidewall.

[0023] Before the second HIP'ing operation, the HIP can is leak tested using helium gas using stems welded on each end cover. Several of the leak-tested HIP cans each with the stacked performs therein are placed in a degas oven and heated to an appropriate temperature (e.g. 600 degrees F) while evacuating the HIP cans (e.g. to less than 10⁻⁵ torr) via the stems until an appropriate leak rate (e.g. less than 100 microns per minute) is attained. The HIP can then are placed in a conventional HIP vessel and HIP'ed at temperature, pressure and time (e.g. 1236 degrees C lower than the HIP temperature of the first HIP'ing operation) at a gas pressure of 1034 bar for 300 minutes) to effect diffusion bonding of the metal (Mo)-to-powder metal (Mo) layer-to-metal(Mo) at the joints between the preforms to form a billet or bar, although other HIP parameters may be used. The number and dimensions of the preforms HIP'ed in the second HIP'ing operation are selected to yield a desired large size the billet or bar suitable for the sputtering target.

[0024] The final HIP'ed billet or bar for the sputtering target exhibits a microstructure comprising equiaxed grains of desired small grain size (e.g. about 30 microns or less) and exhibits a low oxygen content of less than about 100 ppm (part per million by weight) as a result of use of low oxygen sintered Mo powder metal bodies and of the second HIP operation effecting diffusion of oxygen from the commercially available Mo powder metal at each

50

joint between adjacent ingot bodies. For example, it is through the second HIP operation that the oxygen from the commercially available Mo powder metal joint diffuses into the low oxygen (less than 100 ppm O) ingot bodies, reducing the oxygen content in the joint to less than 100 ppm by weight. Figure 1 shows the diffusion bond joint achieved at an initial metal(Mo)-to-powder metal (Mo) layer-to-metal(Mo) joint by the procedure set forth above. The billet or bar for the sputtering target thereby includes a diffusion bond joint where the Mo powder layer was formerly present at the preform joint.

[0025] Although certain embodiments of the invention have been described above, those skilled in the art will appreciate that the invention is not limited to these embodiments and that modifications and changes can be made therein without departing from the spirit and scope of the invention as set forth in the appended claims.

In accordance with a first embodiment, it is provided a method of making a billet or bar comprising molybdenum, comprising diffusion bonding adjacent bodies comprising Mo together at a metal-to-powder metal layer-to-metal joint therebetween in a hot isostatic pressing operation wherein the powder metal layer comprises Mo.

In accordance with a second embodiment, which is related to the first embodiment, it is provided the method wherein the powder metal layer has an oxygen content of less than about 1000 ppm by weight.

In accordance with a third embodiment, which is related to the first embodiment, it is provided the method wherein the bodies have an oxygen content of less than about 100 ppm by weight.

In accordance with a fourth embodiment, which is related to the first embodiment, it is provided the method including machining the billet or bar to form a sputtering target. In accordance with a fifth embodiment, which is related to the first embodiment, it is provided the method wherein the bodies each comprises a preform made by diffusion bonding adjacent sintered Mo powder metal bodies together at a metal-to-metal joint in a first hot isostatic pressing operation to form each preform.

In accordance with a sixth embodiment, which is related to the fifth embodiment, it is provided the method wherein the sintered Mo powder metal bodies have an oxygen content of less than about 100 ppm by weight.

In accordance with a seventh embodiment it is provided a method of making an elongated billet or bar comprising molybdenum, comprising placing bodies comprising Mo adjacent one another, providing a metal powder comprising Mo between the adjacent bodies, and diffusion bonding the adjacent bodies with the metal powder therebetween in a hot isostatic pressing operation.

In accordance with an eighth embodiment, it is provided a billet or bar for a sputtering target made by the process of any one of the first to seventh embodiments.

In accordance with a ninth embodiment, it is provided a sputtering target made by the process of any one of the first to seventh embodiments.

In accordance with a tenth embodiment, it is provided a

billet or bar for a sputtering target having a HIP'ed microstructure comprising equiaxed grains of grain size of about 30 microns or less and an oxygen content of less than 100 ppm by weight.

In accordance with an eleventh embodiment, which is related to the tenth embodiment, it is provided the billet or bar having a diffusion bond joint where Mo powder metal formerly resided.

Claims

15

20

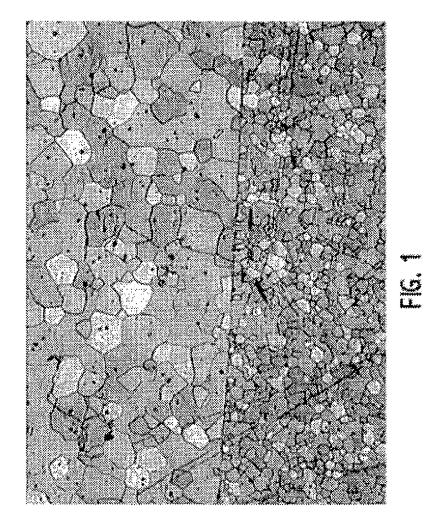
25

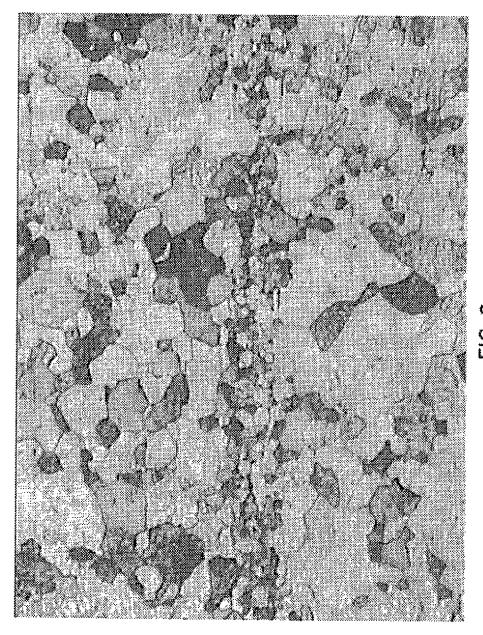
30

45

- A billet or bar for a sputtering target and having a first powder preform comprising molybdenum and a second powder preform comprising molybdenum bonded together at a diffusion bond that corresponds to a location where a powder layer comprising molybdenum formerly resided between the first and second preforms.
- A sputtering target comprising a first powder preform comprising molybdenum and a second powder preform comprising molybdenum bonded together at a diffusion bond that corresponds to a location where a powder layer comprising molybdenum formerly resided.
- 3. A billet or bar for a sputtering target having a HIP'ed microstructure comprising equiaxed grains of grain size of about 30 microns or less and an oxygen content of less than 100 ppm by weight having a diffusion bond where a powder layer comprising molybdenum formerly resided.
- 35 4. The billet or bar of claim 1 or 3 having the diffusion bond joint where commercially available Mo powder metal having an oxygen content higher than 100 ppm by weight formerly resided.
- 40 5. The target of claim 2 wherein the diffusion bond corresponds to a location where a layer of commercially available molybdenum powder formerly resided but having a lower oxygen content than commercially available molybdenum powder.
 - **6.** The target of claim 2 or 5 having a HIP'ed microstructure comprising equiaxed grains of grain size of about 30 microns or less.
- 7. The billet or bar of claims 1, 3 or 4 wherein the first powder preform and the second powder preform comprise sintered powder bodies comprising Mo.
 - **8.** The target of claims 2, 5 or 6 wherein the first powder preform and the second powder preform comprise sintered powder bodies comprising Mo.

55





TE N



EUROPEAN SEARCH REPORT

Application Number EP 11 17 3006

	DOCUMENTS CONSIDERI	D TO BE RELEVANT	•	
Category	Citation of document with indicat of relevant passages	tion, where appropriate,	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)
X A	JP 2003 129232 A (HITA 8 May 2003 (2003-05-08 * abstract; figures *	3)	1,2,4,7 3,5,6,8	INV. B23K20/02 C23C14/34
.,	* paragraphs [0412] - [0018]; example 1 *			
X	JP 2003 342720 A (NIPF 3 December 2003 (2003- * abstract; table 1 *		1-8	
X	JP 6 264233 A (NIKKO k 20 September 1994 (199 * abstract * * paragraph [0017] *		1-8	
X	US 3 714 702 A (J.P. F 6 February 1973 (1973- * column 4, line 63 - table *	02-06)	1,2,7	
A	US 6 199 747 B1 (M.A. 13 March 2001 (2001-03	COHN ET AL)	1-8	TECHNICAL FIELDS SEARCHED (IPC)
	* column 1, line 49 claims 1-4 *	column 2, line 52;		B23K C23C C22C B22F
	The present search report has been	drawn up for all claims		
	Place of search	Date of completion of the search		Examiner
	Munich	25 August 2011	Jeg	ggy, Thierry
X : part Y : part docu A : tech	ATEGORY OF CITED DOCUMENTS icularly relevant if taken alone cularly relevant if combined with another iment of the same category nological background	E : earlier patent of after the filing of D : document cited L : document cited	d in the application d for other reasons	shed on, or
O : non P : inte	-written disclosure rmediate document	& : member of the document	same patent family	r, corresponding

ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 11 17 3006

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

25-08-2011

	Patent document ed in search report		Publication date		Patent family member(s)	Publication date
JP	2003129232	Α	08-05-2003	JP	3748221 B2	22-02-200
JP	2003342720	Α	03-12-2003	NONE		
JP	6264233	Α	20-09-1994	NONE		
US	3714702	Α	06-02-1973	NONE		
US	6199747	B1	13-03-2001	NONE		
			icial Journal of the Euro			

EP 2 374 568 A1

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

• US 60548790 B [0001]

US 60603528 B [0001]