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(54) Method for reducing negative effects of natural pitch contaminants in both pulping and papermaking operations

(57) The instant invention relates to a method for inhibiting pitch deposition on pulping and papermaking equipment or machinery comprising adding to a pulp slurry containing pitch an effective amount of polymer dispersion comprising a component A and a component B, wherein component A being a homopolymer and/or copolymer of acrylic acid and/or its alkyl esters, or methacrylic acid and/or its alkyl esters, styrene and/or methylstyrene, vinyl acetate, itaconic acid, glycidyl methacrylate, 2-hydroxyalkyl (meth)acrylate, methacrylamide, N-

hydroxyethyl(meth)acrylamide, dimethacrylate monomers, 1,3-butylene glycol dimethacrylate, ethylene glycol dimethacrylate, propylene glycol dimethacrylate, dipropylene glycol dimethacrylate, dipropylene glycol dimethacrylate, 4-methyl-1,4-pentanediol dimethacrylate, divinylbenzene and/or trivinylbenzene, and component B being an aqueous solution of a styrene copolymer with acrylic acid, maleimide and/or maleic anhydride.

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Description

[0001] The invention relates to resin and pitch control agents, which are aqueous, non-film forming, polymer dispersions and to a process for preventing the deposition of pitch particles in cellulosic pulp suspensions, by use of such polymer dispersions.

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[0002] Cellulosic pulps contain a considerable proportion of organosoluble matter which is generally referred to as resin or pitch. The resins are extracted from the wood during the pulping process and constitute a significant nuisance in cellulosic suspensions because the resin particles are sticky, tend to agglomerate and form adherent deposits on the pulping and papermaking machinery. The removal of water during papermaking is normally carried out using a type of fabric mesh, commonly referred to as machine wires or felts. Resin or pitch deposits clog and block the small openings in the fabrics inhibiting drainage and causing sheet defects, such as holes in the finished paper. Deposits which accumulate on the internal surfaces of pulp and backwater chests can suddenly be released and displayed as resin lumps in the paper sheet. Larger lumps can break the paper sheet in the machine, leading to loss of production.

[0003] For years there have already been products supplied as passivating agents for treating pulp contaminants such as resin or pitch. These dissolved products are intended to make the surface of the tacky impurities more hydrophilic and hence keep them more wettable, thereby reducing the affinity for hydrophobic surfaces. Hydrophobic surfaces are present on, for example, wires, felts and rollers; hydrophobizing is boosted further by coating, with sizing agent or defoamer, for example, thereby further promoting the attachment of pitch.

[0004] In certain cases, resins and pitch do not cause any problems in papermaking, if they do not agglomerate. To prevent agglomeration, various methods are known for chemically modifying the pitch particles that have remained in the stock stream and the adsorption thereof on support materials, such as machine wires.

[0005] In the context of these problems, the procedures below have been adopted in practice, but lead only to partial success.

[0006] On the one hand, dispersion may take place, with the aim of changing the charge on the pitch by means of anionic and nonionic dispersants. This forms colloidal, anionically charged or nonionic particles which counteract agglomeration and deposition. The wetting properties of the dispersant are very important in this case, since the pitch is hydrophobic.

[0007] Alternatively, according to the literature, the tack of the pitch can be reduced in the following ways:

 Fixing of the strongly anionic contaminants by means of strongly cationic fixatives (formation of what are called polyelectrolyte complexes; the reaction product then adsorbs on the anionic fiber).

- Absorption on pigments of high specific surface area (e.g., talc, modified clay, mica, smectite, bentonite), often with subsequent flocculation by means of polymers in order to bind separable macroflocs.
- Enveloping (masking) with nonionic hydrophilic polymers (polyvinyl alcohol) or zirconium compounds, more particularly zirconium acetate and ammonium zirconium carbonate.

[0008] Known strongly cationic fixatives include polyethyleneimine (PEI) , polydiallyldimethylammonium chloride (polyDADMAC) , polyvinylamine (PVAm) , polyaluminum chloride (PAC) , polyacrylamide (PAAM) , polyamine, etc. The sphere of action of fixatives extends from about 1 nm to 50 micrometers in terms of the particle size of the pitch, depending on the nature and modification of the chemicals used.

[0009] Materials with a low surface energy (wires, felts, roller surfaces) exhibit a more hydrophobic behaviour and therefore possess a high affinity for hydrophobic compounds, such as resins and pitch, thereby resulting in contamination of the wires and hence to defects and/or reduction in the dewatering performance of felts.

[0010] Adsorbents used are, in particular, various types of talc with specific surface modifications and particle-size distribution, which on account of their hydrophobic and organophilic surface are capable of attaching to adhesive constituents and entraining them with the paper. Particles of adhesive encapsulated in this way have less of a tendency to deposit on hot machinery parts.

[0011] Protein solutions are also employed as agents for masking sticky impurities.

[0012] The pitch agglomerates tend to deposit on machinery parts, wires, cloths, drying cylinders, and this consequently leads to marks, holes, and instances of web sticking, and consequently to breakages in the wet section and drying section in the course of winding and rewinding or in the course of printing.

[0013] 2009DE002 by Clariant discloses a method for reducing negative effects of adhesive synthetic contaminants in systems of substances comprising waste paper. In waste paper the main problem are the pitch agglomerates (stickies) which lead to a deposit on the machinery parts.

[0014] In contrary in the process for producing cellulosic pulp suspensions the negative effects are caused by natural pitch contaminants in both pulping and papermaking operations. These contaminants tend to deposit during the production on the cellulosic material and lead to ugly black spots.

[0015] In order to prevent resin deposits talc has been known in the prior art to prevent and control pitch deposits. Using talc to control pitch deposits, however, has certain disadvantages. For instance, the system is highly sensitive to shear. Talc, moreover, has poor retention properties and frequently causes clogging of the felts.

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Talc may adversely affect resin sizing, and stabilizes foam. The two inorganic products, talc and bentonite, require laborious dispersion.

[0016] There continues to be a need for improvement in reducing the tackiness of natural pitch and resin particles.

[0017] Surprisingly, the tackiness of pitch can be reduced considerably through the use of specific polymer dispersions.

[0018] The invention provides an aqueous polymer dispersion and the use thereof in a method for reducing sticky contaminants in the processing of wood pulp and in the papermaking procedure, which involves adding an aqueous polymer dispersion comprising a component A and a component B for passivating and detackifying the pitch particles, component A being a homopolymer and/or copolymer of acrylic acid and/or its alkyl esters, more particularly its methyl, ethyl, butyl, isobutyl, propyl, octyl, decyl, 2- ethylhexyl esters;

or methacrylic acid and/or its alkyl esters, more particularly its methyl, ethyl, butyl, isobutyl, propyl, octyl, decyl, 2- ethylhexyl esters;

styrene and/or methylstyrene;

vinyl acetate;

itaconic acid;

glycidyl methacrylate;

2- hydroxyalkyl (meth) acrylate;

methacrylamide;

N- hydroxyethyl (meth) acrylamide

dimethacrylate monomers, such as, for example, 1, 4-butylene glycol dimethacrylate, 1, 3- butylene glycol dimethacrylate, ethylene glycol dimethacrylate, diethylene glycol dimethacrylate, propylene glycol dimethacrylate, dipropylene glycol dimethacrylate, 4- methyl- 1, 4-pentanediol dimethacrylate;

divinylbenzene and/or trivinylbenzene

and component B being an aqueous solution of a styrene copolymer with acrylic acid, maleimide and/or maleic anhydride.

[0019] Component A is a hydrophobic homopolymer and/or copolymer of the above-stated monomers having a very high glass transition temperature or softening temperature (Tg), preferably methyl methacrylate or styrene. The glass transition temperature of A is preferably above 70°C, more particularly above 90°C, very preferably above 100°C.

[0020] Component B is a styrene copolymer with (meth)acrylic acid, maleimide and/or maleic anhydride. Component B is preferably a copolymer of styrene and acrylic acid. Component B preferably has a molecular weight of between 3000 g/mol and 15 000 g/mol, more particularly 3000 and 7000 g/mol.

[0021] Particularly preferred is an aqueous dispersion with particle sizes of less than 150 nm, preferably less than 120 nm.

[0022] The aqueous polymer dispersion may be applied in combination with calcium and or magnesium salts, often naturally occurring in the processing water.

Hardness salts insolubilise component B, leading to the de-stabilisation of the tiny emulsion particles. The agglomerated emulsion particles are now more hydrophobic and associate readily and preferentially with any pitch particles in the pulp. The harder emulsion particles reduce the tackiness of the pitch and increase the softening temperature. Hard agglomerates show much less tendency to deposit on machinery.

[0023] Where water hardness levels are very low, there may not be sufficient electrolyte to initiate de-stabilisation of the emulsion particles. The aqueous polymer dispersion may therefore be optionally applied in combination with component C, a cationic fixative, which promotes coagulation of the emulsion particles in the cellulosic fibre slurry. Component C is preferably selected from the following group: polyethyleneimine (PEI) , polydiallyldimethylammonium chloride (polyDADMAC) , polyvinylamine (PVAm) , polyaluminum chloride (PAC) , zirconium salts, polyacrylamide (PAAM) , polyamine and polyamideamine.

[0024] In order to boost the efficiency of the polymer dispersion of the invention and its stability, it is further possible to add a further component D optionally in the form of a surfactant.

[0025] Further to components A, B, and/or D, the polymer dispersion comprises water (component E).

[0026] In one preferred embodiment the aqueous dispersion comprises

2 % to 50 %, preferably 5 % to 30 % of component A, 1 % to 30 %, preferably 3 % to 10 % of component B, 0 % to 0.3 %, preferably 0 % to 0.2 % of component D, and 96 % to 17.7 %, preferably 90 % to 45 % of water (component E).

[0027] All percentages here relate to % by weight.

[0028] In the presence of Ca²⁺, the aqueous dispersion constitutes a self-coagulating nanodispersion. The polymer dispersion of the invention attaches to the hydrophobic sticky particles, incorporating them into the precipitating polymer dispersion and thus detackifying them.

Examples:

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Example 1 (version with methyl methacrylate)

[0029] A 2 I reactor with stirrer and reflux condenser was charged with 739.5 g of deionized water and 419.3 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0030] Feed stream I:

384.8 g of methyl methacrylate

[0031] Feed stream II:

1.9 g of ammonium peroxodisulfate 136.3 g of deionized water

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[0032] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318.2 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μm .

[0033] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$D = 53 \text{ nm}$$

Example 2 (version with methyl methacrylate + crosslinker)

[0034] A 2 I reactor with stirrer and reflux condenser was charged with 739.5 g of deionized water and 419.3 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0035] Feed stream I:

370.9 g of methyl methacrylate 19.5 g of glycidyl methacrylate

[0036] Feed stream II:

1.9 g of ammonium peroxodisulfate 136.3 g of deionized water

[0037] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318.2 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μ m.

[0038] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$SC = 24.9 \%$$

$$D = 40 \text{ nm}$$

Example 3 (version with methyl methacrylate + second crosslinker)

[0039] A 2 I reactor with stirrer and reflux condenser was charged with 740 g of deionized water and 419 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0040] Feed stream I:

370 g of methyl methacrylate19 g of ethylene glycol dimethacrylate

[0041] Feed stream II:

2 g of ammonium peroxodisulfate 136 g of deionized water

[0042] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μ m.

[0043] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$SC = 25 \%$$

$$D = 40 \text{ nm}$$

Example 4 (version with styrene)

[0044] A 2 I reactor with stirrer and reflux condenser was charged with 739.5 g of deionized water and 419.3 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0045] Feed stream I:

384.8 g of styrene

[0046] Feed stream II:

1.9 g of ammonium peroxodisulfate136.3 g of deionized water

[0047] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318.2 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μm .

[0048] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$SC = 24.5 \%$$

$$D = 61 \text{ nm}$$

Example 5 (version with colloid + surfactant)

[0049] A 2 I reactor with stirrer and reflux condenser was charged with 1111 g of deionized water, 310 g of 25 % strength solution of styrene-acrylic acid copolymer, and 3 grams of lauryl sulfate, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere. [0050] Feed stream I:

387 g of methyl methacrylate

[0051] Feed stream II:

2 g of ammonium peroxodisulfate 88 g of deionized water

[0052] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 80 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μm .

[0053] The characterization of the copolymer obtained,

in terms of solids content (SC) and average particle size (D), is given below:

$$D = 50 \text{ nm}$$

Example 6 (styrene-methyl acrylate copolymer

[0054] A 2 I reactor with stirrer and reflux condenser was charged with 739.5 g of deionized water and 420 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0055] Feed stream I:

193 g of styrene193 g of methyl methacrylate

[0056] Feed stream II:

2 g of ammonium peroxodisulfate 136 g of deionized water

[0057] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318.2 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μ m.

[0058] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$SC = 30.0 \%$$

$$D = 70 \text{ nm}$$

Example 7 (styrene-maleic anhydride as component B)

[0059] A 2 I reactor with stirrer and reflux condenser was charged with 400 g of deionized water and 750 g of 14 % strength solution of styrene-maleic anhydride copolymer, this initial charge then being heated to 85 °C

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with stirring under a nitrogen atmosphere. **[0060]** Feed stream I:

390 g of methyl methacrylate

[0061] Feed stream II:

2 g of ammonium peroxodisulfate 130 g of deionized water

[0062] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 318.2 g of deionized water. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μm .

[0063] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$D = 70 \text{ nm}$$

Example 8 (high colloid fraction)

[0064] A 2 I reactor with stirrer and reflux condenser was charged with 21.1 g of deionized water and 750 g of 25 % strength solution of styrene-acrylic acid copolymer, this initial charge then being heated to 85 °C with stirring under a nitrogen atmosphere.

[0065] Feed stream I:

390 g of methyl methacrylate

[0066] Feed stream II:

2 g of ammonium peroxodisulfate 130 g of deionized water

[0067] When an internal temperature of 85 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 3 h 30, with stirring and retention of the reaction temperature. The pumps were flushed with 80 g of deionized water. After the end of both feed streams, the mixture was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 $\mu m.$

[0068] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

Example 9 (styrene-acrylic acid copolymer with Tg of about 30 °C)

[0069] A 2 I reactor with stirrer and reflux condenser was charged with 433 g of deionized water, and 3 grams of lauryl sulfate (30 % strength solution), this initial charge then being heated to 80 $^{\circ}$ C with stirring under a nitrogen atmosphere.

[0070] Feed stream I:

5 g of ammonium peroxodisulfate 62 g of deionized water

[0071] Feed stream II:

400 g of styrene,
260 g of butyl acrylate,
10 g of methacrylic acid,
11 g of surfactant solution (lauryl sulfate, 30 %),
384 g of deionized water

[0072] When an internal temperature of 80 °C had been reached, feed stream I and feed stream II were metered continuously into the polymerization batch via two separate feeds, beginning simultaneously, over a period of 4 h, with stirring and retention of the reaction temperature. The pumps were flushed with 235 g of deionized water. After the end of both feed streams, the system was left to after react at the reaction temperature for a further 25 minutes. After that, the reaction mixture was cooled to room temperature and filtered on a filter having a mesh size of 160 μm .

[0073] The characterization of the copolymer obtained, in terms of solids content (SC) and average particle size (D), is given below:

$$D = 185 \, \text{nm}$$

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Tg = 30 °C

Claims

- 1. A method for inhibiting pitch deposition on pulping and papermaking equipment or machinery comprising adding to a pulp slurry containing pitch an effective amount of polymer dispersion comprising a component A and a component B, wherein component A being a homopolymer and/or copolymer of acrylic acid and/or its alkyl esters, or methacrylic acid and/or its alkyl esters, styrene and/or methylstyrene, vinyl acetate, itaconic acid, glycidyl methacrylate, 2-hydroxyalkyl (meth)acrylate, methacrylamide, N-hydroxyethyl(meth)acrylamide, dimethacrylate monomers, 1,3-butylene glycol dimethacrylate, ethylene glycol dimethacrylate, diethylene glycol dimethacrylate, propylene glycol dimethacrylate, dipropylene glycol dimethacrylate, 4-methyl-1,4-pentanediol dimethacrylate, divinylbenzene and/or trivinylbenzene, and component B being an aqueous solution of a styrene copolymer with acrylic acid, maleimide and/or maleic anhydride.
- The method as claimed in claim 1, wherein component A possesses a glass transition temperature > 90 °C.
- The method as claimed in at least one of the preceding claims, wherein component B possesses a molecular weight in the range from 3000 to 15 000 g/mol, preferably 3000 to 7000 g/mol.
- 4. The method as claimed in at least one of the preceding claims, wherein the aqueous polymer dispersion is applied in combination with calcium and or magnesium salts, often naturally occurring in the processing water, or component C, a cationic fixative, any of which promote the coagulation of the aqueous emulsion particles.
- 5. The method as claimed in claim 4, wherein component C is selected from the following group: polyethyleneimine (PEI), polydiallyldimethylammonium chloride (polyDADMAC), polyvinylamine (PVAm), polyaluminum chloride (PAC), zirconium salts, polyacrylamide (PAAM), polyamine and polyamideamine.
- 6. The method as claimed in at least one of the preceding claims, wherein the aqueous polymer dispersion further comprises a component D in the form of a surfactant.
- 7. The method as claimed in any of the preceding

claims, wherein the water fraction of the aqueous polymer dispersion is 93 % to 17.7 %, preferably 80 % to 45 % by weight.

- 8. An aqueous polymer dispersion for coagulating and detackifying pitch in the processing of wood pulp or during the papermaking procedure, comprising a component A selected from a homopolymer and/or copolymer of the following group: acrylic acid and/or its alkyl esters, or methacrylic acid and/or its alkyl esters, styrene and/or methylstyrene, vinyl acetate, itaconic acid, glycidyl methacrylate, 2-hydroxyalkyl (meth)acrylate, methacrylamide, N-hydroxyethyl (meth)acrylamide, dimethacrylate monomers, 1,3butylene glycol dimethacrylate, ethylene glycol dimethacrylate, diethylene glycol dimethacrylate, propylene glycol dimethacrylate, dipropylene glycol dimethacrylate, 4-methyl-1,4-pentanediol dimethacrylate, divinylbenzene and/or trivinylbenzene, and component B, which is an aqueous solution of a styrene copolymer with acrylic acid, maleimide and/or maleic anhydride.
- 9. The aqueous polymer dispersion as claimed in claim 8, wherein the dispersion is applied in combination with calcium and or magnesium salts, often naturally occurring in the processing water, or component C, a cationic fixative, selected from the following group: polyethyleneimine (PEI), polydiallyldimethylammonium chloride (polyDADMAC), polyvinylamine (PVAm), polyaluminum chloride (PAC), zirconium salts, polyacrylamide (PAAM), polyamine and polyamideamine.
- 10. The aqueous polymer dispersion as claimed in claim 8 and/or 9, wherein the dispersion comprises a further component D in the form of a surfactant.
- 11. The aqueous polymer dispersion as claimed in at least one of claims 8 to 10, which comprises 2 % to 50 %, preferably 5 % to 30 % of component A, 1 % to 30 %, preferably 3 % to 10 % of component B, 100 to 400 ppm calcium and/or magnesium carbonate (water hardness) 0 % to 2 % of component C, 0 % to 0.3 %, preferably 0 % to 0.2 % of component D, and 96 % to 17.7 %, preferably 90 % to 45 % of water (component E).
 - 12. The use of an aqueous polymer dispersion comprising a component A and a component B, component A being a homopolymer and/or copolymer of methyl methacrylate, acrylate and/or styrene and component B being an aqueous solution of styrene copolymer with acrylic acid, maleimide and/or maleic anhydride, for coagulating and detackifying pitch particles in the processing of pulp and paper.

13. The use as claimed in claim 12, the polymer dispersion is further combined with calcium and/or magnesium salts or the natural water hardness in the pulp and/or papermaking process water or component C, a cationic fixative.

14. The use as claimed in claim 12, whereby the amount of aqueous dispersion applied to the cellulosic pulp slurry is preferably 0.05 to 0.5 %, more preferably 0.1 to 0.2 %, based on the dry weight of the cellulose.



EUROPEAN SEARCH REPORT

Application Number EP 12 00 1801

	DOCUMENTS CONSID					
Category	Citation of document with ir of relevant passa	ndication, where appropriate, ages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)		
Х	KOHLER ACHIM [DE];	CLARIANT INT LTD [CH]; COWMAN JOHN [GB]; uary 2011 (2011-02-10)	1-14	INV. D21C9/08 D21H21/02		
A	WO 98/05819 A1 (ASH 12 February 1998 (1 * the whole documen	998-02-12)	1-14			
A	US 2006/048908 A1 (9 March 2006 (2006- * the whole documen		1-14			
A	US 6 150 452 A (LIN 21 November 2000 (2 * the whole documen		1-14			
A	US 2011/094695 A1 (ET AL) 28 April 201 * the whole documen		1-14			
A	US 2004/226676 A1 (AL) 18 November 200 * the whole documen		1-14	TECHNICAL FIELDS SEARCHED (IPC) D21C D21H		
A	WO 01/25535 A1 (HER 12 April 2001 (2001 * the whole documen	-04-12)	1-14			
	The present search report has I	Deen drawn up for all claims Date of completion of the search 2 August 2012	Kar	Examiner		
X : parti Y : parti docu	ATEGORY OF CITED DOCUMENTS ioularly relevant if taken alone cularly relevant if combined with anothent of the same category nological background	T : theory or principle E : earlier patent door after the filing date D : document cited in L : document oited for	ument, but publis the application rother reasons	shed on, or		

ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 12 00 1801

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

02-08-2012

	atent document d in search report		Publication date		Patent family member(s)		Publication date
WO	2011015297	A1	10-02-2011	EP US WO	2462278 2012186761 2011015297	A1	13-06-2012 26-07-2012 10-02-2011
WO	9805819	A1	12-02-1998	AU AU CA EP JP US WO	716411 4047197 2262953 0929717 2000515591 7052579 9805819	A A1 A1 A B1	24-02-2000 25-02-1998 12-02-1998 21-07-1999 21-11-2000 30-05-2006 12-02-1998
US	2006048908	A1	09-03-2006	CA EP US WO	2579510 1802806 2006048908 2006029404	A1 A1	16-03-2006 04-07-2007 09-03-2006 16-03-2006
US	6150452	A	21-11-2000	AU CA EP JP NO US US WO ZA	6563798 2293312 0986670 2002513450 995958 5936024 6150452 9855692 9801600	A1 A A A A A	21-12-1998 10-12-1998 22-03-2000 08-05-2002 04-02-2000 10-08-1999 21-11-2000 10-12-1998 31-08-1998
US	2011094695	A1	28-04-2011	ИОИ	IE		
US	2004226676	A1	18-11-2004	AT AU BR CA CN DE EP ES JP KR MX NZ PT RU US WO	352659 2004238948 PI0410301 2524205 1788119 602004004527 1623067 2280028 4584929 2007500290 20060011866 PA05012092 543245 1623067 2347865 2004226676 2004101882	A1 A A1 A T2 A1 T3 B2 A A A A E C2 A1	15-02-2007 25-11-2004 23-05-2006 25-11-2004 14-06-2006 22-11-2007 08-02-2006 01-09-2007 24-11-2010 11-01-2007 03-02-2006 08-02-2006 31-07-2008 30-03-2007 27-02-2009 18-11-2004 25-11-2004

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ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 12 00 1801

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

02-08-2012

	Patent document cited in search report		Publication date		Patent family member(s)		Publication date
				ZA	200508431	A	31-01-2007
	WO 0125535	A1	12-04-2001	AU WO	7723600 0125535	A A1	10-05-2001 12-04-2001
O FORM P0459							
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