EP 2 644 853 A1 (11)

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:

(51) Int CI.: F01K 25/10 (2006.01) 02.10.2013 Bulletin 2013/40 F01K 23/10 (2006.01)

F01K 27/02 (2006.01)

(21) Application number: 12162043.9

(22) Date of filing: 29.03.2012

(84) Designated Contracting States:

AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR

Designated Extension States:

BA ME

(71) Applicant: Alstom Technology Ltd 5400 Baden (CH)

(72) Inventors:

- Brack, Reinhard 65934 Frankfurt (DE)
- · Strohm, Kathrin 55278 Dexheim (DE)
- (54)Energy saving and heat recovery in carbon dioxide compression systems and a system for accomplishing the same
- A method and apparatus for capturing heat at a power plant is disclosed. The method includes absorbing the heat released from carbon dioxide gas from the power plant using a refrigerant (130); transferring the absorbed heat from the refrigerant (130) to a water condensate (115) obtained at the power plant to raise a temperature

of the water condensate (115); and supplying the heated water condensate (115) to the power plant to capture the heat released from the carbon dioxide. A power plant and using the methods disclosed herein captures heat from carbon dioxide exhaust and generates power using in part on the captured heat.

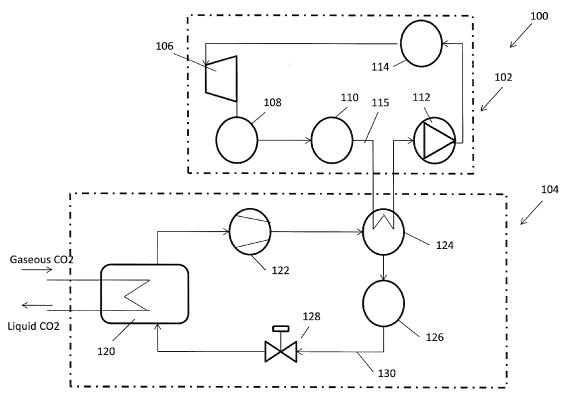


Figure 1

40

45

FIELD OF THE INVENTION

[0001] This disclosure is related to methods of recovering heat from power plant exhaust gases. In particular, this disclosure is related to methods of capturing heat from carbon dioxide gases exhausted from the power plant during sequestration procedures.

1

BACKGROUND OF THE INVENTION

[0002] The combustion of a fuel, such as coal, oil, peat, waste, biofuels, and the like, in a combustion plant such as a power plant, generates a hot process gas stream known as a flue gas stream. In general, the flue gas stream contains particulates and gaseous contaminants such as carbon dioxide (CO₂). The negative environmental effects of releasing carbon dioxide to the atmosphere have been recognized and have resulted in the development of processes for removing the carbon dioxide from flue gas streams and sequestering the removed carbon dioxide. In various sequestration processes, the carbon dioxide gas is compressed to form liquid carbon dioxide which can then be pumped underground. The heat released during carbon dioxide compression and condensation to liquid is generally absorbed by cooling water that is on hand for such purposes. During warm season, the preparation (i.e., cooling) of this water can be costly. In addition, the heat absorbed by this cooling water is typically wasted, leading to reduced power plant efficiency. Therefore, there is a desire to provide a method of capturing heat from the condensation of carbon dioxide for use at power plants.

SUMMARY

[0003] Disclosed herein is a method of capturing heat at a power plant that includes absorbing the heat released from carbon dioxide gas from the power plant using a refrigerant; transferring the absorbed heat from the refrigerant to a water condensate obtained at the power plant to raise a temperature of the water condensate; and supplying the heated water condensate to the power plant to capture the heat released from the carbon dioxide.

[0004] Disclosed herein too is an apparatus for recirculating heat in a power plant that includes a first heat transfer device configured to transfer heat from a carbon dioxide exhaust gas of the power plant to a refrigerant; and a second heat transfer device configured to transfer the heat from the refrigerant to a water condensate of the power plant, wherein the heated water condensate is provided to the power plant to recirculate the heat.

[0005] Disclosed herein too is a power plant system comprising an exhaust of the power plant system configured to release a carbon dioxide gas; a first heat exchanger configured to transfer heat from the carbon dioxide

gas to a refrigerant; the first heat exchanger being downstream of the power plant system; a second heat exchanger configured to transfer the heat from the refrigerant to a water condensate of the power plant system, where the second heat exchanger lies downstream of the first heat exchanger; and a steam turbine configured to generate power using the heated water condensate from the second heat exchanger, where the steam turbine lies down stream of the second heat exchanger.

[0006] Disclosed herein too is a method of operating a power plant, the method including obtaining a carbon dioxide gas from an exhaust of the power plant; transferring heat from the obtained carbon dioxide gas to a heat transfer medium; transferring the heat from the heat transfer medium to a water condensate obtained at the power plant; supplying the heated water condensate to the power plant; and generating steam from the heated water condensate to generate power at a steam turbine of the power plant.

BRIEF DESCRIPTION OF THE FIGURES

[0007] Figure 1 shows an exemplary system for capturing heat from carbon dioxide exhaust in an exemplary embodiment of the present disclosure.

[0008] Figure 2 shows an alternate embodiment for capturing heat from carbon dioxide using a heat exchanger in parallel with the system of Figure 1.

DETAILED DESCRIPTION

[0009] The present disclosure is directed to a method and apparatus for capturing and recirculating heat from a power plant. In one aspect, the present disclosure describes a method of heating a boiler feed water for a power plant using heat generated during a carbon dioxide sequestration process. In general, the heat is captured from carbon dioxide that is isolated from an exhaust stream of the power plant. The heat is released when the carbon dioxide is compressed and condensed from a gaseous phase to a liquid phase. The carbon dioxide is compressed at pressures that are less than a critical point of carbon dioxide. The "critical point" as disclosed herein refers to the pressure and temperature characteristics at which carbon dioxide is converted to supercritical carbon dioxide. A first heat exchanger and a second heat exchanger are used to capture the heat released from the carbon dioxide. The first heat exchanger transfers heat from condensation and/or compression of the carbon dioxide to a refrigerant or suitable heat transfer medium. In an exemplary embodiment, the refrigerant is methylamine. The second heat exchanger transfers the heat from the refrigerant to a water condensate collected from a steam turbine. The water condensate results from the condensation of steam that is used as a working gas at the steam turbine. The heat is transferred from the refrigerant to the water condensate to elevate the temper-

20

25

40

45

50

ature of the water condensate for use as boiler feed water. Supplying the boiler feed water to the power plant therefore recirculates the heat generated by sequestration back to the power plant. In another aspect, the present disclosure further describes a power plant and a method of operating a power plant.

[0010] Figure 1 shows an exemplary heat recovery system 100 suitable for use with a combustion-type power plant. The exemplary heat recovery system includes a steam turbine cycle 102 and a refrigeration cycle 104. The steam turbine cycle 102 comprises a feed water pump 112, a boiler 114, a steam turbine 106, a surface condenser 108 and a pump 110 in fluid communication with a second heat exchanger 124. While the feed water pump 112, the boiler 114, the steam turbine 106, the surface condenser 108, the pump 110 and the second heat exchanger 124 are part of the steam turbine recycle loop 102, it is to be noted that the feed water pump 112, the boiler 114, the steam turbine 106, the surface condenser 108 and the pump 110 lie downstream of the second heat exchanger 124 in succession. It is to be noted that since the steam turbine cycle 102 and the refrigeration cycle 104 are recycle loops, some components can be both upstream as well as downstream of a particular point in the loop.

[0011] The refrigeration cycle 104 comprises a first heat exchanger 120, a refrigerant compressor 122, the second heat exchanger 124, a condensate receiver 126, an expansion valve 128 all of which are in fluid communication with one another. The refrigerant compressor 122, the second heat exchanger 124, the condensate receiver 126, and the expansion valve 128 all lie downstream of the first heat exchanger 120 in succession. It is to be noted that the second heat exchanger 124 is a part of both the steam turbine cycle 102 and the refrigeration cycle 104.

[0012] The steam turbine cycle 102 generally circulates water in either a gaseous or liquid phase throughout the power plant to generate power. Water held at the boiler 114 is heated to produce steam which is then introduced at an inlet to the steam turbine 106. In accordance with one embodiment heating of water in the boiler 114 to produce steam may be achieved by combusting a fuel, such as coal, oil, peat, waste, biofuels etc., and transferring heat from a flue gas stream formed by such combustion to the water in the boiler 114. The flue gas stream generated from such combustion of a fuel comprises carbon dioxide. Hence, at least a portion of the heat transferred from the flue gas stream to the water in the boiler 114 is transferred to the water from carbon dioxide comprised in the flue gas stream. The steam passes through the steam turbine 106 as a working gas to generate electricity and/or power. The steam is generally cooled and expanded as it exits the steam turbine and therefore condenses to water, which is collected at the surface condenser 108. Pump 110 pumps the condensed water 115 to the second heat exchanger 124 of the refrigeration cycle 104. At the second heat exchanger

124, the water 115 absorbs heat from a refrigerant of the refrigeration cycle 104, as discussed in detail below. Boiler feed water pump 112 then pumps the heated water to the boiler 114, at which point the water is boiled to generate steam for power generation, thereby completing the steam turbine cycle 102.

[0013] The exemplary refrigeration cycle 104 includes the first heat exchanger 120 and the second heat exchanger 124. A refrigerant 130 or other medium suitable for heat conduction and/or heat transfer is circulated back and forth between the first heat exchanger 120 and the second heat exchanger 124 to complete the refrigeration cycle 104. The first heat exchanger 120 receives carbon dioxide (from a carbon dioxide emitter) and refrigerant 130 and is configured for carbon dioxide compression and condensation and for evaporation of the refrigerant. Heat that is released from the carbon dioxide due to compression and condensation is transferred to the refrigerant and causes the refrigerant to evaporate. The carbon dioxide condenses at a pressure that is less than the critical pressure of carbon dioxide. The second heat exchanger 124 receives refrigerant gas 130 and water 115 and allows for the refrigerant gas 130 to condense. Heat released from condensation of the refrigerant 130 at the second heat exchanger 124 is absorbed by the water 115 to heat the water 115.

[0014] In one embodiment, the carbon dioxide gas received at the first heat exchanger 120 is carbon dioxide gas emitted from the power plant. The carbon dioxide emission gas is generally separated from other emission gases, such as NOx and SOx gases, using various gas separation processes (not shown). The condensation of the separated carbon dioxide emission gas to a liquid carbon dioxide phase is performed for various reasons, one of which is to sequester the carbon dioxide to a selected location, such as underground. The separated carbon dioxide generally undergoes various cycles of compression and cooling in order to obtain carbon dioxide liquid. For at least the last cycle, the first heat exchanger 120 receives the carbon dioxide and absorbs heat of compression and condensation.

[0015] In various embodiments, the refrigerant compressor 122 is disposed along a circulation path of the refrigerant gas 130 from the first heat exchanger 120 to the second heat exchanger 124. The refrigerant compressor 122 raises the pressure and temperature of the refrigerant gas prior to the second heat exchanger 124. The refrigerant condensate receiver 126 and the expansion valve 128 are disposed along the circulation path of the refrigerant liquid 130 from the second heat exchanger 124 to the first heat exchanger 120. The refrigerant condensate receiver 126 collects condensed refrigerant 130 from the second heat exchanger 124. The expansion valve 128 delivers the condensed refrigerant 130 to the first heat exchanger 120 at a pressure and temperature suitable for heat absorption at the first heat exchanger 120.

[0016] Figure 1 is discussed below with respect to var-

20

25

40

45

ious exemplary temperatures and pressures which are provided for illustrative purposes only and which are not meant as a limitation of the present disclosure. In an exemplary embodiment, the refrigerant is methylamine. However, various other mediums, gases and liquids for heat transfer can be suitable in performing the heat capture described herein. In the exemplary embodiment, the gaseous carbon dioxide phase enters the first heat exchanger 120 at a temperature of about 110°C and a pressure of about 65 bars and exits the first heat exchanger 120 at a temperature of about 25°C and a pressure of about 65 bars (66.28 kilograms per square centimeter). Although a pressure of 65 bars is illustrative, it is noted that the carbon dioxide condenses to liquid at a pressure below a critical point of carbon dioxide, i.e., without entering a supercritical carbon dioxide phase. Meanwhile, liquid refrigerant 130 enters the first heat exchanger 120 at about 20°C and about 2.4 bars (2.44 kilograms per square centimeters) and evaporates to a gas having the same temperature and pressure. The heat released from the carbon dioxide is absorbed by the refrigerant, causing the refrigerant to evaporate from a liquid to a gas. In one aspect of the present disclosure, the pressure of the refrigerant at the first heat exchanger 120 is less than the pressure of the carbon dioxide at the first heat exchanger 120. Thus, any leakage or damage at the first heat exchanger 120 will cause contamination of the refrigerant rather than contamination of the carbon dioxide.

[0017] The refrigerant gas 130 is compressed at the refrigerant compressor 122 which elevates the temperature and pressure of the refrigerant gas prior to entering the second heat exchanger 124. In one embodiment, the refrigerant compressor 122 is a centrifugal compressor for refrigerants having a molecular weight in a range from about 25 to about 40 grams per mole. In an exemplary embodiment, the refrigerant compressor 122 raises the temperature of the refrigerant gas 130 to about 120°C and raises the pressure to about 16 bar (16.315 kilograms per square centimeters). The refrigerant gas 130 then condenses at the second heat exchanger 124 to a liquid having an exemplary temperature of about 80°C and an exemplary pressure of about 16 bars. Heat released from the refrigerant at the second heat exchanger 124 is absorbed by the water condensate 115 of the steam turbine cycle 102. In an exemplary embodiment, the water condensate 115 enters the second heat exchanger 124 at about 50°C and 20 bars (20.39 kilograms per square centimeters) and exits that second heat exchanger 124 at about 70°C and 20 bars. The pressure of the refrigerant 130 at the second heat exchanger 124 is selected to be less than the pressure of the water condensate 115 at the second heat exchanger 124. Therefore, any leakage or damage at the second heat exchanger 124 will cause contamination of the refrigerant 130 rather than of the water condensate 115.

[0018] Thus, in one embodiment, the heat released by compression and condensation of the carbon dioxide is captured and returned to the power plant using the re-

frigeration cycle 104 and steam turbine cycle 102 of Figure 1 as shown in Figure 1. In an alternate embodiment, additional heat capture methods can be used alongside the system of Figure 1, as discussed below.

[0019] Figure 2 shows an alternative system 200 for carbon dioxide condensation that is suitable for use with the present disclosure. Carbon dioxide gas pipeline 202 divides along two branches 204 and 206. Carbon dioxide that is sent along the branch 204 is cooled using cooling water. Carbon dioxide that is sent along branch 206 is cooled using the exemplary methods of the present disclosure (detailed above with respect to the Figure 1). The amount of carbon dioxide sent along branches 204 and 206 depends on which branch supplies cooling at the lowest temperature. When the temperature of the cooling water is relatively high, i.e., during warm weather, the refrigeration cycle 104 is started in order to ensure that the carbon dioxide remains in a subcritical range during condensation. Once the refrigeration system reaches a temperature inside heat exchanger 120 that is lower than the cooling water temperature, the ratio of carbon dioxide along branches 204 and 206 may be adjusted accordingly, thereby increasing an efficiency of the power plant. When the temperature of the cooling water is relatively low, i.e., during cold weather, then the ratio is adjusted to increase an amount of carbon dioxide sent along branch 204.

[0020] Operation of the power plant in this manner ensures that a carbon dioxide compressor pump system that is used for sequestration purposes can be operated in the subcritical region of carbon dioxide all year. The refrigeration system of the present disclosure can be run all year. For various reasons related to cost and efficiency, the present disclosure is used in warm weather rather than, or more often than, in cold weather.

[0021] Therefore, disclosed herein is a method of capturing heat at a power plant that includes absorbing the heat released from carbon dioxide gas from the power plant using a refrigerant; transferring the absorbed heat from the refrigerant to a water condensate obtained at the power plant to raise a temperature of the water condensate; and supplying the heated water condensate to the power plant to capture the heat released from the carbon dioxide. The heat is generally released from the carbon dioxide gas during either condensation of the carbon dioxide from a gas to a liquid or compression of the carbon dioxide gas or both. Carbon dioxide is condensed from gas to liquid at a pressure that is less than a critical pressure of carbon dioxide. The water condensate can be obtained from condensation of steam that moves through a steam turbine to generate power at the power plant. The heated water condensate is then supplied to the steam turbine for further power generation. In an exemplary embodiment, the refrigerant absorbs the heat released from the carbon dioxide at a first heat exchanger and transfers the heat to the water condensate at a second heat exchanger. A pressure of the refrigerant at the first heat exchanger is less than a pressure of the carbon

55

20

25

35

40

45

dioxide at the first heat exchanger, and a pressure of the refrigerant at the second heat exchanger is less than a pressure of the water condensate at the second heat exchanger. The heat released from the carbon dioxide can also be absorbed at a cooling water heat exchanger that is in parallel with the first heat exchanger. The ratio of heat absorbed by the refrigerant and by the cooling water can be determined by a relative temperature of the refrigerant and the cooling water. In various embodiments, the refrigerant is methylamine.

[0022] Disclosed herein too is an apparatus for recirculating heat in a power plant that includes a first heat transfer device configured to transfer heat from a carbon dioxide exhaust gas of the power plant to a refrigerant; and a second heat transfer device configured to transfer the heat from the refrigerant to a water condensate of the power plant, wherein the heated water condensate is provided to the power plant to recirculate the heat. The heat from the carbon dioxide exhaust gas is generated by at least one of: (i) condensation of the carbon dioxide gas to a liquid; and (ii) compression of the carbon dioxide gas. The carbon dioxide condenses from liquid to gas at the first heat exchanger at a pressure that is less than a critical pressure of carbon dioxide. A steam turbine provides the water condensate to the second heat transfer device from condensation of steam used as a working gas at the steam turbine. The pressure of the refrigerant at the first heat exchanger is selected to be less than the pressure of the carbon dioxide at the first heat exchanger, and the pressure of the refrigerant at the second heat exchanger is selected to be less than the pressure of the water condensate at the second heat exchanger. The refrigerant is methylamine. In one embodiment, a cooling water heat exchanger is configured to receive carbon dioxide gas in parallel with the first heat exchanger.

[0023] Disclosed herein too is a power plant system that includes an exhaust of the power plant system configured to release a carbon dioxide gas; a first heat exchanger configured to transfer heat from the carbon dioxide gas to a refrigerant; a second heat exchanger configured to transfer the heat from the refrigerant to a water condensate of the power plant system; and a steam turbine configured to generate power using the heated water condensate from the second heat exchanger. The first heat exchanger is configured to transfer heat obtained during a condensation of carbon dioxide form a gaseous phase to a liquid phase. A cooling water heat exchanger can be used to absorb heat from the carbon dioxide in parallel with the first heat exchanger.

[0024] Disclosed herein too is a method of operating a power plant, the method including obtaining a carbon dioxide gas from an exhaust of the power plant; transferring heat from the obtained carbon dioxide gas to a heat transfer medium; transferring the heat from the heat transfer medium to a water condensate obtained at the power plant; supplying the heated water condensate to the power plant; and generating steam from the heated water condensate to generate power at a steam turbine

of the power plant. In one embodiment, the heat transferred to the heat transfer medium is obtained during a condensation of carbon dioxide from a gaseous phase to a liquid phase. The carbon dioxide condenses at a pressure that is less than a critical pressure of carbon dioxide.

[0025] It will be understood that, although the terms "first," "second," "third" etc. may be used herein to describe various elements, components, regions, layers and/or sections, these elements, components, regions, layers and/or sections should not be limited by these terms. These terms are only used to distinguish one element, component, region, layer or section from another element, component, region, layer or section. Thus, "a first element," "component," "region," "layer" or "section" discussed below could be termed a second element, component, region, layer or section without departing from the teachings herein.

[0026] The terminology used herein is for the purpose of describing particular embodiments only and is not intended to be limiting. As used herein, the singular forms "a," "an" and "the" are intended to include the plural forms as well, unless the context clearly indicates otherwise. It will be further understood that the terms "comprises" and/or "comprising," or "includes" and/or "including" when used in this specification, specify the presence of stated features, regions, integers, steps, operations, elements, and/or components, but do not preclude the presence or addition of one or more other features, regions, integers, steps, operations, elements, components, and/or groups thereof.

[0027] Furthermore, relative terms, such as "lower" or "bottom" and "upper" or "top, " may be used herein to describe one element's relationship to other elements as illustrated in the Figures. It will be understood that relative terms are intended to encompass different orientations of the device in addition to the orientation depicted in the Figures. For example, if the device in one of the figures is turned over, elements described as being on the "lower" side of other elements would then be oriented on "upper" sides of the other elements. The exemplary term "lower, " can therefore, encompasses both an orientation of "lower" and "upper, " depending on the particular orientation of the figure. Similarly, if the device in one of the figures is turned over, elements described as "below" or "beneath" other elements would then be oriented "above" the other elements. The exemplary terms "below" or "beneath" can, therefore, encompass both an orientation of above and below.

[0028] Unless otherwise defined, all terms (including technical and scientific terms) used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this disclosure belongs. It will be further understood that terms, such as those defined in commonly used dictionaries, should be interpreted as having a meaning that is consistent with their meaning in the context of the relevant art and the present disclosure, and will not be interpreted in an idealized or overly

15

20

25

30

35

40

45

50

55

formal sense unless expressly so defined herein.

[0029] Exemplary embodiments are described herein with reference to cross section illustrations that are schematic illustrations of idealized embodiments. As such, variations from the shapes of the illustrations as a result. for example, of manufacturing techniques and/or tolerances, are to be expected. Thus, embodiments described herein should not be construed as limited to the particular shapes of regions as illustrated herein but are to include deviations in shapes that result, for example, from manufacturing. For example, a region illustrated or described as flat may, typically, have rough and/or nonlinear features. Moreover, sharp angles that are illustrated may be rounded. Thus, the regions illustrated in the figures are schematic in nature and their shapes are not intended to illustrate the precise shape of a region and are not intended to limit the scope of the present claims. [0030] The term and/or is used herein to mean both "and" as well as "or". For example, "A and/or B" is construed to mean A, B or A and B.

[0031] While this disclosure describes exemplary embodiments, it will be understood by those skilled in the art that various changes can be made and equivalents can be substituted for elements thereof without departing from the scope of the disclosed embodiments. In addition, many modifications can be made to adapt a particular situation or material to the teachings of this disclosure without departing from the essential scope thereof. Therefore, it is intended that this disclosure not be limited to the particular embodiment disclosed as the best mode contemplated for carrying out this disclosure.

Claims

- A method of capturing heat at a power plant, comprising:
 - absorbing the heat released from carbon dioxide gas from the power plant using a refrigerant (130);
 - transferring the absorbed heat from the refrigerant (130) to a water condensate (115) obtained at the power plant to raise a temperature of the water condensate (115); and
 - supplying the heated water condensate (115) to the power plant to capture the heat released from the carbon dioxide.
- 2. The method of claim 1, further comprising absorbing the heat that is released from the carbon dioxide gas during at least one of: (i) condensation of the carbon dioxide from a gas to a liquid; and (ii) compression of the carbon dioxide gas.
- 3. The method of claim 2, further comprising condensing the carbon dioxide from gas to liquid at a pressure that is less than a critical pressure of carbon dioxide.

- **4.** The method of any one of claims 1-3, wherein the water condensate (115) is obtained from condensation of steam that moves through a steam turbine (106) to generate power at the power plant.
- **5.** The method of claim 4, wherein the heated water condensate (115) is supplied to the steam turbine (106) for power generation.
- 6. The method of any one of claims 1-5, wherein the refrigerant (130) absorbs the heat released from the carbon dioxide at a first heat exchanger (120) and transfers the heat to the water condensate (115) at a second heat exchanger (124).
 - 7. The method of claim 6, wherein a pressure of the refrigerant (130) at the first heat exchanger (120) is less than a pressure of the carbon dioxide at the first heat exchanger (120) and a pressure of the refrigerant (130) at the second heat exchanger (124) is less than a pressure of the water condensate (115) at the second heat exchanger (124).
- **8.** The method of any one of claims 6-7, further comprising absorbing the heat released from the carbon dioxide at a cooling water heat exchanger in parallel with the first heat exchanger (120).
- 9. The method of claim 8, wherein a ratio of heat absorbed by the refrigerant (130) and absorbed by the cooling water is related to a relative temperature of the refrigerant (130) and the cooling water.
- **10.** The method of any one of claims 1-9, wherein the refrigerant (130) is methylamine.
- 11. A power plant system having an exhaust of the power plant system configured to release a carbon dioxide gas **characterized by**:
 - a first heat exchanger (120) configured to transfer heat from the carbon dioxide gas to a refrigerant (130); the first heat exchanger (120) being downstream of the power plant system;
 - a second heat exchanger (124) configured to transfer the heat from the refrigerant (130) to a water condensate (115) of the power plant system, where the second heat exchanger (124) lies downstream of the first heat exchanger (120); and
 - a steam turbine (106) configured to generate power using the heated water condensate (115) from the second heat exchanger (124), where the steam turbine (106) lies downstream of the second heat exchanger (124).
- **12.** The power plant system of claim 11, wherein the first heat exchanger (120) is configured to transfer heat

6

obtained during a condensation of carbon dioxide from a gaseous phase to a liquid phase.

- **13.** The power plant system of any one of claims 11-12, further comprising a cooling water heat exchanger configured to absorb heat from the carbon dioxide in parallel with the first heat exchanger (120).
- **14.** A method of operating a power plant, comprising:

obtaining a carbon dioxide gas from an exhaust of the power plant; transferring heat from the obtained carbon dioxide gas to a heat transfer medium (130); transferring the heat from the heat transfer medium (130) to a water condensate (115) obtained at the power plant; supplying the heated water condensate (115) to the power plant; and generating steam from the heated water condensate (115) to generate power at a steam tur-

15. The method of claim 14, further comprising transferring heat to the heat transfer medium (130) that is obtained during a condensation of carbon dioxide from a gaseous phase to a liquid phase.

bine (106) of the power plant.

16. The method of claim 15, wherein the carbon dioxide condenses from gas to liquid at a pressure that is less than a critical pressure of carbon dioxide.

35

40

45

50

55

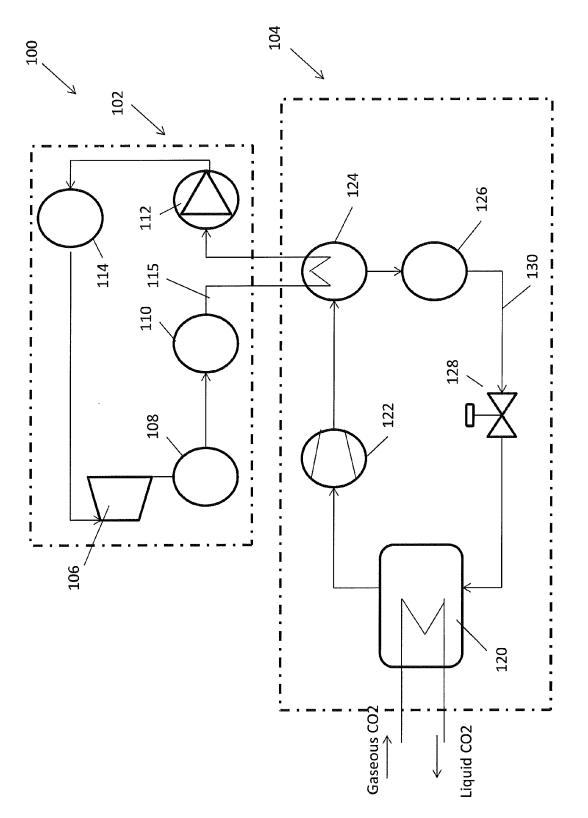
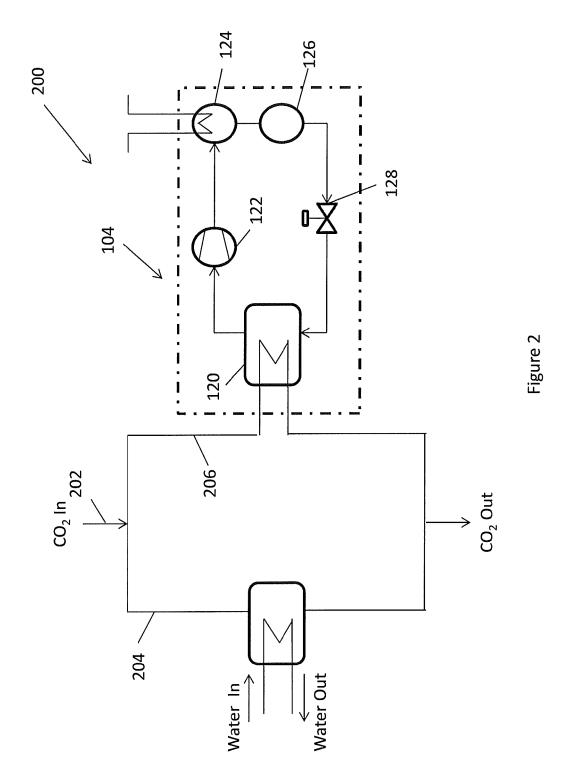


Figure 1





EUROPEAN SEARCH REPORT

Application Number EP 12 16 2043

	DOCUMENTS CONSID	ERED TO BE RELEVANT			
Category	Citation of document with in of relevant pass	ndication, where appropriate, ages		Relevant o claim	CLASSIFICATION OF THE APPLICATION (IPC)
Χ	GMBH [DE]) 13 Janua	1 (HITACHI POWER EUROF 1ry 2011 (2011-01-13) - [0070]; figure 1 *		9, -16	INV. F01K25/10 F01K27/02 F01K23/10
Α	AL) 3 November 2011	DROUVOT PAUL [FR] ET . (2011-11-03) - [0060]; figures 1-3		16	TOTALSY TO
Α	[US] ET AL) 26 May	HANDAGAMA NARESHKUMAR 2011 (2011-05-26) - [0076]; figure 2 *	B 1-	16	
					TECHNICAL FIELDS SEARCHED (IPC)
	The present search report has	been drawn up for all claims			
	Place of search	Date of completion of the search			Examiner
	Munich	23 August 2012	23 August 2012 Röl		
X : part Y : part docu A : tech O : non	ATEGORY OF CITED DOCUMENTS icularly relevant if taken alone icularly relevant if combined with anot iment of the same category nological background written disclosure rinediate document	L : document cite	documer date d in the	nt, but public application er reasons	shed on, or

ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 12 16 2043

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

23-08-2012

US 2011265477 A1 03-11-2011 CN 102287244 A 21-12-20 EP 2383522 A1 02-11-201 US 201120128 A1 26-05-2011 AU 2010322317 A1 21-06-20 US 2011120128 A1 26-05-2011 AU 2010322317 A1 21-06-20 CA 2781266 A1 26-05-20	Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2011120128 A1 26-05-2011 AU 2010322317 A1 21-06-20 CA 2781266 A1 26-05-20	DE 102009032537 A	13-01-2011	DE 102009032537 A1 EP 2452051 A2	13-01-20 13-01-20 16-05-20 13-01-20
CA 2781266 A1 26-05-20	US 2011265477 AI	03-11-2011	EP 2383522 A1 JP 2011231765 A	21-12-20 02-11-20 17-11-20 03-11-20
	US 2011120128 AT	26-05-2011	CA 2781266 A1 US 2011120128 A1	21-06-20 26-05-20 26-05-20 26-05-20

FORM P0459

© For more details about this annex : see Official Journal of the European Patent Office, No. 12/82