

(19)



(11)

EP 2 831 299 B2

(12)

NEW EUROPEAN PATENT SPECIFICATION

After opposition procedure

(45) Date of publication and mention of the opposition decision:
29.04.2020 Bulletin 2020/18

(51) Int Cl.:
C21D 1/20 (2006.01) **C21D 8/02** (2006.01)
C22C 38/00 (2006.01) **C22C 38/12** (2006.01)
C21D 9/46 (2006.01) **C22C 38/02** (2006.01)
C22C 38/04 (2006.01) **C22C 38/06** (2006.01)

(45) Mention of the grant of the patent:
13.09.2017 Bulletin 2017/37

(86) International application number:
PCT/EP2013/056957

(21) Application number: **13717208.6**

(87) International publication number:
WO 2013/144377 (03.10.2013 Gazette 2013/40)

(22) Date of filing: **02.04.2013**

(54) **HIGH STRENGTH COLD ROLLED STEEL SHEET AND METHOD OF PRODUCING SUCH STEEL SHEET**

HOCHFESTES KALTGEWALZTES STAHLBLECH UND VERFAHREN ZUR HERSTELLUNG EINES SOLCHEN STAHLBLECHS

TÔLE D'ACIER LAMINÉE À FROID À HAUTE RÉSISTANCE ET PROCÉDÉ DE PRODUCTION D'UNE TÔLE D'ACIER DE CE TYPE

(84) Designated Contracting States:
AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR

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(43) Date of publication of application:
04.02.2015 Bulletin 2015/06

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- **ASEEL AL-HAMDANY ET AL: "Estimation of the Volume Percent of Normal and Nanostructured Bainite in Bainitic Steels", MATERIALS TODAY: PROCEEDINGS, vol. 2, 1 January 2015 (2015-01-01), pages S373-S382, XP055303956, ISSN: 2214-7853, DOI: 10.1016/j.matpr.2015.05.052**

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Description

TECHNICAL FIELD

5 **[0001]** The present invention relates to high strength cold rolled steel sheet suitable for applications in automobiles, construction materials and the like, specifically high strength steel sheet excellent in formability. In particular, the invention relates to a cold rolled steel sheet having a tensile strength of at least 980 MPa.

BACKGROUND ART

10 **[0002]** For a great variety of applications increased strength levels are a pre-requisite for light weight constructions in particular in the automotive industry, since car body mass reduction results in reduced fuel consumption.

[0003] Automotive body parts are often stamped out of sheet steels, forming complex structural members of thin sheet. However, such part cannot be produced from conventional high strength steels because of a too low formability for complex structural parts. For this reason multi phase Transformation Induced Plasticity aided steels (TRIP steels) have gained considerable interest in the last years.

15 **[0004]** TRIP steels possess a multi-phase microstructure, which includes a meta-stable retained austenite phase, which is capable of producing the TRIP effect. When the steel is deformed, the austenite transforms into martensite, which results in remarkable work hardening. This hardening effect, acts to resist necking in the material and postpone failure in sheet forming operations. The microstructure of a TRIP steel can greatly alter its mechanical properties. The most important aspects of the TRIP steel microstructure are the volume percentage, size and morphology of the retained austenite phase, as these properties directly affect the austenite to martensite transformation when the steel is deformed. There are several ways in which to chemically stabilize austenite at room temperature. In low alloy TRIP steels the austenite is stabilized through its carbon content and the small size of the austenite grains. The carbon content necessary to stabilize austenite is approximately 1 wt. %. However, high carbon content in steel cannot be used in many applications because of impaired weldability.

20 **[0005]** Specific processing routs are therefore required to concentrate the carbon into the austenite in order to stabilize it at room temperature. A common TRIP steel chemistry also contains small additions of other elements to help in stabilizing the austenite as well as to aid in the creation of microstructures which partition carbon into the austenite. The most common additions are 1.5 wt. % of both Si and Mn. In order to inhibit the austenite to decompose during the bainite transformation it is generally considered necessary that the silicon content should be at least 1 wt. %. The silicon content of the steel is important as silicon is insoluble in cementite. US 2009/0238713 discloses such a TRIP steel. However, high silicon content can be responsible for a poor surface quality of hot rolled steel and a poor coatability of cold rolled steel. Accordingly, partial or complete replacement of silicon by other elements has been investigated and promising results have been reported for Al-based alloy design. However, a disadvantage with the use of aluminium is the rise of the transformation temperature (A_{c3}) which makes full austenitizing in conventional industrial annealing lines very difficult or impossible.

25 **[0006]** Depending on the matrix phase the following main types of TRIP steels are cited:

40 TPF TRIP steel with matrix of polygonal ferrite

TPF steels, as already mentioned before-hand, contain the matrix from relatively soft polygonal ferrite with inclusions from bainite and retained austenite. Retained austenite transforms to martensite upon deformation, resulting in a desirable TRIP effect, which allows the steel to achieve an excellent combination of strength and drawability. Their stretch flangeability is however lower compared to TBF, TMF and TAM steels with more homogeneous microstructure and stronger matrix.

45 TBF TRIP steel with matrix of bainitic ferrite

TBF steels have been known for long and attracted a lot of interest because the bainitic ferrite matrix allows an excellent stretch flangeability. Moreover, similarly to TPF steels, the TRIP effect, ensured by the strain-induced transformation of metastable retained austenite islands into martensite, remarkably improves their drawability.

50 TMF TRIP steel with matrix of martensitic ferrite

TMF steels also contain small islands of metastable retained austenite embedded into strong martensitic matrix, which enables these steels to achieve even better stretch flangeability compared to TBF steels. Although these steels also exhibit the TRIP effect, their drawability is lower compared to TBF steels.

TAM TRIP steel with matrix of annealed martensite

55 TAM steels contain the matrix from needle-like ferrite obtained by re-annealing of fresh martensite. A pronounced TRIP effect is again enabled by the transformation of metastable retained austenite inclusions into martensite upon straining. Despite their promising combination of strength, drawability and stretch flangeability, these steels have not gained a remarkable industrial interest due to their complicated and expensive double-heat cycle.

[0007] The formability of TRIP steels is mainly affected by the transformation characteristics of the retained austenite phase, which is in turn affected by the austenite chemistry, its morphology and other factors. In ISIJ International Vol. 50(2010), No. 1, p. 162 -168 aspects influencing on the formability of TBF steels having a tensile strength of at least 980 MPa are discussed. However, the cold rolled materials examined in this document were annealed at 950 °C and the austempered at 300-500 °C for 200 s in salt bath. Accordingly, due to the high annealing temperature these materials are not suited for the production in a conventional industrial annealing line.

DISCLOSURE OF THE INVENTION

[0008] The present invention is directed to a high strength cold rolled steel sheet having a tensile strength of at least 980 MPa and having an excellent formability and a method of producing the same on an industrial scale. In particular, the invention relates to a cold rolled TBF steel sheet having properties adapted for the production in a conventional industrial annealing -line. Accordingly, the steel shall not only possess good formability properties but at the same time be optimized with respect to A_{c3} - temperature, M_s - temperature, austempering time and temperature and other factors such as sticky scale influencing the surface quality of the hot rolled steel sheet and the processability of the steel sheet in the industrial annealing line.

DETAILED DESCRIPTION

[0009] The invention is described in the claims.

[0010] The cold rolled high strength TBF steel sheet has a steel composition consisting of the following elements (in wt. %):

C	0.15 - 0.18
Mn	2.2 - 2.4
Si	0.7 - 0.9
Cr	0.1 - 0.9
Si + 0.8 Al +Cr	0.5 - 1.8
Al	0.2 - 0.6
Nb	< 0.1
Mo	< 0.3
Ti	< 0.2
V	< 0.2
Cu	< 0.5
Ni	< 0.5
S	≤ 0.01
P	≤ 0.02
N	≤ 0.02
B	< 0.005
Ca	< 0.005
Mg	< 0.005
REM	< 0.005

balance Fe apart from impurities.

[0011] The limitation of the elements is explained below.

[0012] The limitation of the elements C, Mn, Si, Al and Cr is essential to the invention for the reasons set out below:

C:

[0013] C is an element which stabilizes austenite and is important for obtaining sufficient carbon within the retained austenite phase. C is also important for obtaining the desired strength level. Generally, an increase of the tensile strength in the order of 100 MPa per 0.1 %C can be expected. When C is lower than 0.1 % then it is difficult to attain a tensile strength of 980 MPa. If C exceeds 0.3 % then weldability is impaired. For this reasons, the preferred range is 0.15 - 0.18 %, depending on the desired strength level.

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Mn:

5 **[0014]** Manganese is a solid solution strengthening element, which stabilises the austenite by lowering the Ms temperature and prevents ferrite and pearlite to be formed during cooling. In addition, Mn lowers the Ac3 temperature. At a content of less than 2% it might be difficult to obtain a tensile strength of 980 MPa and the austenitizing temperature might be too high for conventional industrial annealing lines. However, if the amount of Mn is higher than 3 % problems with segregation may occur and the workability may be deteriorated. The preferred range is therefore 2.2 - 2.4%.

10 Si:

[0015] Si acts as a solid solution strengthening element and is important for securing the strength of the thin steel sheet. Si is insoluble in cementite and will therefore act to greatly delay the formation of carbides during the bainite transformation as time must be given to Si to diffuse away from the bainite grain boundaries before cementite can form. The preferred range is therefore 0.7 - 0.9 %.

15 Cr:

20 **[0016]** Cr is effective in increasing the strength of the steel sheet. Cr is an element that forms ferrite and retards the formation of pearlite and bainite. The Ac3 temperature and the Ms temperature are only slightly lowered with increasing Cr content. However, due to the retardation of the bainite transformation longer holding times are required such that the processing on a conventional industrial annealing line is made difficult or impossible, when using normal line speeds. For this reason the amount of Cr is preferably limited to 0.6 %. The preferred range is 0.1-0.35

25 Si + 0.8 Al + Cr

[0017] Si, Al and Cr when added in combination have a synergistic and completely unforeseen effect, resulting in an increased amount of residual austenite, which, in turn, results in an improved ductility. For these reasons the amount of Si + 0.8 Al + Cr is limited to the range 1.4 - 1.8 %.

30 Al:

35 **[0018]** Al promotes ferrite formation and is also commonly used as a deoxidizer. Al, like Si, is not soluble in the cementite and therefore diffuses away from the bainite grain boundaries before cementite can form. The Ms temperature is increased with increasing Al content. A further drawback of Al is that it results in a drastic increase in the Ac3 temperature such that the austenitizing temperature might be too high for conventional industrial annealing lines. The contents of Al refers to acid soluble Al.

[0019] In addition to C, Mn, Si, Al and Cr the steel may optionally contain one or more of the following elements in order to adjust the microstructure, influence on transformation kinetics and/or to fine tune one or more of the mechanical properties of the steel sheet.

40 Nb: < 0.1

45 **[0020]** Nb is commonly used in low alloyed steels for improving strength and toughness because of its remarkable influence on the grain size development. Nb increases the strength elongation balance by refining the matrix microstructure and the retained austenite phase due to precipitation of NbC. At contents above 0.1 % the effect is saturated.

[0021] Preferred ranges are therefore 0.02-0.08 %, 0.02 - 0.04 % and 0.02 - 0.03 %.

Mo: < 0.3

50 **[0022]** Mo can be added in order to improve the strength of the steel sheet. Addition of Mo together with Nb results in precipitation of fine NbMoC which results in a further improvement in the combination of strength and ductility.

Ti: < 0.2; V: < 0.2

55 **[0023]** These elements are effective for precipitation hardening. Ti may be added in preferred amounts of $\leq 0.01 - 0.1$ %, 0.02 - 0.08 % or 0.02 - 0.05 %. V may be added in preferred amounts of 0.01 - 0.1 % or 0.02 - 0.08 %.

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Cu: < 0.5; Ni: < 0.5

[0024] These elements are solid solution strengthening elements and may have a positive effect on the corrosion resistance. They may be added in amounts of 0.05 - 0.5 % or 0.1 - 0.3 % if needed.

S: ≤ 0.01 ; P: ≤ 0.02 ; N: ≤ 0.02

[0025] These elements are not desired in this type of steel and should therefore be limited.

S preferably ≤ 0.003

P preferably ≤ 0.01

N preferably ≤ 0.003

B: < 0.005

[0026] B suppresses the formation of ferrite and improves the weldability of the steel sheet. For having a noticeable effect at least 0.0002 % should be added. However, excessive amounts of B deteriorate the workability. Preferred ranges are < 0.004 %, 0.0005- 0.003 % and 0.0008 -0.0017 %.

Ca: < 0.005; Mg: < 0.005; REM: < 0.005

[0027] These elements may be added in order to control the morphology of the inclusions in the steel and thereby improve the hole expansibility and the stretch flangeability of the steel sheet. Preferred ranges are 0.0005 -0.005 % and 0.001-0.003 %.

Si > Al

[0028] The high strength cold rolled steel sheet according to the invention has a silicon aluminium based design, i.e. the cementite precipitation during the bainitic transformation is accomplished by Si and Al. Although the amount of Si is reduced is preferably that it is larger than the amount of Al, preferably Si > 1.1 Al, more preferably Si > 1.3 Al or even Si > 2 Al.

Si > Cr

[0029] In the steel sheet of the present invention it is preferred to control the amount of Si to be larger than the amount of Cr and to restrict the amount of Cr in order to retard the bainite transformation too much. For this reason it is preferred to keep Si > Cr, preferably Si > 1.5 Cr, more preferably Si > 2 Cr, most preferably Si > 3 Cr.

[0030] The cold rolled high strength TBF steel sheet has a multiphase microstructure comprising (in vol. %)

retained austenite	5 - 20
bainite + bainitic ferrite + tempered martensite	≥ 80
polygonal ferrite	≤ 10

[0031] The amount of retained austenite is 5-20%, preferably from 5 - 16 %, most preferably from 5 - 10 %. Because of the TRIP effect retained austenite is a prerequisite when high elongation is necessary. High amount of residual austenite decreases the stretch flangeability. In these steel sheet the polygonal ferrite is replaced by bainitic ferrite (BF) and the microstructure generally contains more than 50 % BF. The matrix consists of BF laths strengthened by a high dislocation density and between the laths the retained austenite is contained.

[0032] MA (martensite/austenite) constituent represents the individual islands in the microstructure consisting of retained austenite and/or martensite. These two microstructural compounds are difficult to be distinguished by common etching technique for advanced high strength steels (AHSS) - Le Pera etching and also by investigations with scanning electron microscopy (SEM). Le Pera etching, which is very common to the person skilled in the art can be found in "F.S. LePera, Improved etching technique for the determination of percent martensite in high-strength dual-phase steels Metallography, Volume 12, Issue 3, September 1979, Pages 263-268". Furthermore, for properties such as hole expansion the amount and size of MA constituent plays an important role. Therefore, in an industrial practice the fraction and size of MA constituent are often used by AHSS for the correlations in terms of their mechanical properties and formability.

[0033] The size of the martensite-austenite (MA) shall be max 5 μm , preferably 3 μm . Minor amounts of martensite may be present in the structure. The amount of MA shall be max 20 %, preferably max 16 %, most preferably below 10 %.

[0034] The cold rolled high strength TBF steel sheet preferably has the following mechanical properties

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tensile strength (R _m)	≥ 980 - 1200	MPa
total elongation (A ₈₀)	≥ 11	%
hole expanding ratio (λ)	≥ 45	%, preferably ≥ 50 %.

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[0035] The R_m and A₈₀ values were derived according to the European norm EN 10002 Part 1, wherein the samples were taken in the longitudinal direction of the strip. The hole expanding ratio (λ) was determined by the hole expanding test according to ISO/WD 16630. In this test a conical punch having an apex of 60 ° is forced into a 10 mm diameter punched hole made in a steel sheet having the size of 100 x 100 mm². The test is stopped as soon as the first crack is determined and the hole diameter is measured in two directions orthogonal to each other. The arithmetic mean value is used for the calculation.

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[0036] The hole expanding ratio (λ) in % is calculated as follows:

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$$\lambda = (Dh - Do) / Do \times 100$$

wherein Do is the diameter of the hole at the beginning (10 mm) and Dh is the diameter of the hole after the test.

[0037] The formability properties of the steel sheet were further assessed by the parameters: strength-elongation balance (R_m x A₈₀) and stretch-flangeability (R_m x λ).

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[0038] An elongation type steel sheet has a high strength-elongation balance and a high hole expansibility type steel sheet has a high stretch flangeability.

[0039] The steel sheet of the present invention fulfils at least one of the following conditions:

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$$R_m \times A_{80} \geq 13\,000 \quad \text{MPa}\%$$

$$R_m \times \lambda \geq 50\,000 \quad \text{MPa}\%$$

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[0040] The mechanical properties of the steel sheet of the present invention can be largely adjusted by the alloying composition and the microstructure.

[0041] A comparative chemical composition may comprise 0.19 C, 2.6 Mn, 0.82 Si, 0.3-0.7 Al, 0.10 Mo, rest Fe apart from impurities.

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[0042] The steel sheets of the present invention can be produced using a conventional CA-line. The processing comprises the steps of:

- a) providing a cold rolled steel strip having a composition as set out above,
- b) annealing the cold rolled steel strip at an annealing temperature, T_{an}, above the A_{c3} temperature in order to fully austenitize the steel, followed by
- c) cooling the cold rolled steel strip from the annealing temperature, T_{an}, to a cooling stop temperature of rapid cooling, T_{RC}, at a cooling rate sufficient to avoid the ferrite formation, the cooling rate being 20 - 100 °C/s, while:

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- for a high hole expansion type steel sheet the cooling stop temperature, T_{RC}, being lower than the martensite start temperature, T_{MS}, T_{MS} being between 300 and 400 °C, preferably between 340 and 370 °C,
- for a high elongation type steel sheet the cooling stop temperature, T_{RC}, being between 360 and 460 °C, preferably between 380 and 420 °C, followed by

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- d) austempering the cold rolled steel strip at an overageing/austempering temperature, T_{OA}, that is between 360 and 460 °C, preferably between 380 and 420 °C, and

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- e) cooling the cold rolled steel strip to ambient temperature.

[0043] The process shall preferably further comprise the steps of:

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in step b) the annealing being performed at an annealing temperature, T_{an}, that is between 910 and 930 °C, during an annealing holding time, t_{an}, which is between 150-200 s, preferably 180 s,

in step c) the cooling being performed according to a cooling pattern having two separate cooling rates; a first cooling

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rate, CR1, of 80 - 100 °C/s, preferably of 85 - 95 °C/s, preferably about 90 °C/s to a temperature which is between 530 to 570 °C, preferably 550 °C, and a second cooling rate, CR2, of 35 - 45 °C, preferably about 40 °C/s to the stop temperature of rapid cooling, T_{RC} , and

5 in step d) the austempering being performed at an overageing/austempering holding time, t_{0A} , which is between 150 and 600 s, preferably 180 and 540 s.

[0044] Preferably, no external heating is applied to the steel strip between step c) and d).

[0045] The reasons for regulating the heat treatment conditions are set out below:

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Annealing temperature, T_{an} , > A_{c3} temperature:

[0046] By fully austenitizing the steel the amount of polygonal ferrite in the steel sheet can be controlled. If the annealing temperature, T_{an} , is below the temperature at which the steel is fully austenitic, A_{c3} , there is a risk that the amount of polygonal ferrite in the steel sheet will exceed 10%. Too much polygonal ferrite gives larger size of the MA constituent.

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Cooling stop temperature of rapid cooling, T_{RC} :

[0047] By controlling the cooling stop temperature of rapid cooling, T_{RC} , the size of MA constituent in the steel sheet can be controlled. If the cooling stop temperature of rapid cooling, T_{RC} , exceeds the martensite start temperature, T_{MS} , the size of MA constituent becomes larger which lowers the $R_m \times \lambda$ product under the value necessary for a high hole expansion type steel sheet. In the case of a high elongation type steel sheet the cooling stop temperature, T_{RC} might be above the martensite start temperature, T_{MS} .

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25 Austempering temperature, T_{0A} :

[0048] By controlling the austempering temperature, T_{0A} , to a temperature between 360 and 460 °C, preferably between 380 and 420 °C, the size of MA constituent and the amount of retained austenite, RA, can be controlled. A lower austempering temperature, T_{0A} , will lower the amount of RA. A higher austempering temperature, T_{0A} , will lower the amount of RA and increase the size of MA constituent. In both cases, this will lower the uniform elongation, A_g , and total elongation, A_{80} , of the steel sheet.

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First and second cooling rates, CR1, CR2:

[0049] By controlling the first cooling rate, CR1, of 80 - 100 °C/s, preferably of 85 - 95 °C/s, preferably about 90 °C/s to a temperature which is between 530 to 570 °C, preferably 550 °C, and a second cooling rate, CR2, of 35 - 45 °C preferably about 40 °C/s to the stop temperature of rapid cooling, T_{RC} , the amount of polygonal ferrite can be controlled. Lowering the cooling rates will increase the amount of polygonal ferrite to more than 10%.

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[0050] In one embodiment of the invention the steel sheet is a high elongation type steel having strength-elongation balance $R_m \times A_{80} \geq 13\ 000$ MPa%, preferably $\geq 15\ 000$ MPa.

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[0051] In another embodiment of the invention the steel sheet is a high hole expansibility type steel having stretch-flangeability $R_m \times \lambda \geq 50\ 000$ MPa%, preferably $\geq 55\ 000$ MPa.

EXAMPLES

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[0052] A number of test alloys A-M were manufactured having chemical compositions according to table I. Steel sheets were manufactured and subjected to heat treatment in a conventional CA-line according to the parameters specified in Table II. The microstructure of the steel sheets were examined along with a number of mechanical properties and the result is presented in Table II

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[0053] A completely different behaviour is found for the inventive steel sheets. Partly based on these results the claimed TBF steel sheet having a Si-Al based alloy design, optionally with additions of Cr having a high stretch flangeability and an improved processability for the production in a continuous annealing line was developed.

Quantitative measurement of microstructures

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[0054] Amount of retained austenite was measured by X ray analysis at a 1/4 position of the sheet thickness. A photograph of a microstructure taken by the SEM was subjected to image analysis to measure each of a volume-% of a MA, volume-% of matrix phase (bainitic ferrite + bainite + tempered martensite), volume-% of retained austenite and

volume-% of polygonal ferrite.

Bainitic ferrite + bainite + tempered martensite:

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[0055] A crystal grain in which a white point (or white line composed of a linear array of continuously connected white point) was observed in the image analysis of the SEM photograph.

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MA (martensite/austenite):

[0056] A crystal grain in which no white point (or no white line) was observed in the image analysis of the SEM photograph.

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Table I

Steel type No.	C	Si	Mn	P	S	sol-Al	Cr	Mo	Nb	sol-Ti	B	N	Si+Cr	Si+Cr+0.8Al	Ms point	Ac3*	comparative steel
A	0.192	0.82	2.55	0.008	0.0022	0.70	0.101					0.0040	0.83	1.39	386	902	comparative steel
B	0.187	0.83	2.56	0.007	0.0020	0.70	0.01		0.030			0.0029	0.84	1.40	388	904	comparative steel
C	0.196	0.82	2.58	0.008	0.0020	0.69	0.01	0.10				0.0033	0.83	1.38	381	904	comparative steel
D	0.192	0.82	2.58	0.008	0.0023	0.69	0.01	0.10	0.030			0.0032	0.83	1.38	383	903	comparative steel
E	0.205	0.78	2.57	0.008	0.0022	0.70	0.31			0.050		0.0033	1.09	1.65	374	903	comparative steel
F	0.175	0.81	2.28	0.008	0.0024	0.290						0.0045	0.81	1.04	403	870	comparative steel
G	0.172	0.79	2.27	0.009	0.0026	0.588						0.0043	0.79	1.26	405	903	comparative steel
H	0.171	0.79	2.25	0.008	0.0026	0.291					0.0005	0.0045	0.79	1.02	406	870	comparative steel
I	0.177	0.79	2.24	0.008	0.0027	0.590					0.0006	0.0048	0.79	1.26	403	902	comparative steel
J	0.195	0.56	2.26	0.0065	0.0025	0.85	0.038	0.005	0.002	0.005	0.0003	0.0025	0.598	1.28	393	951	comparative steel
K	0.198	0.62	1.74	0.008	0.0024	0.6	0.013	0.004	0.002	0.005	0.0004	0.0028	0.633	1.11	409	884	comparative steel
L	0.168	0.81	2.49	0.007	0.0025	0.57	0.01	0.10	0.002	0.006	0.0003	0.0042	0.82	1.28	397	910	comparative steel

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(continued)

Chemical composition in wt. %																	
Steel type No.	C	Si	Mn	P	S	sol-Al	Cr	Mo	Nb	sol-Ti	B	N	Si+Cr	Si+Cr+0.8Al	Ms point	Ac3*	
M	0.130	0.4	2.41	0.013	0.002	0.045						0.004	0.4	0.44	420	830	comparative steel
Ms = 561-474C%-33Mn-17Cr-21Mo Ac3 : Measured by dilatometer																	

Table II

CA Parameters, mechanical properties and microstructure

Examp No.	Steel type No.	Annealing temp. T _{an} °C	Annealing time. t _{an} s	Cooling rate. CR1 °C/s	Cooling rate. CR2 °C/s	Stop temp. of rapid cooling T _{rc} °C	Over- ageing temp. T _{oa} °C	Over- ageing time t _{oa} s	Thick- ness mm	Rp0.2 MPa	Rm MPa	A80 %	λ %	Rm #A80 MPa	Rm MPa	Retained Austenite vol%	Polygonal Ferrite vol%	Bainitic Ferrite + Bainite + Tempered Martensite vol%	Marten- site Austenite constituent size μm	Marten- site Austenite constituent vol%	comparative steel
1	A	910	180	90	41	340	420	540	1.44	1017	1140	13.7	54	15559	61153	7.5	0	96	2.6	4.5	comparative steel
2	A	930	180	90	42	340	420	540	1.43	1017	1140	13.7	54	15559	61153	7	0	95	1.9	4.7	comparative steel
3	A	910	180	90	41	340	460	540	1.43	906	1119	14.2	47	15888	52253	7.9	0	92	4.7	8.0	comparative steel
4	A	910	180	90	41	340	440	540	1.42	981	1131	15.3	46	17249	52031	8.6	0	91	4.0	9.0	comparative steel
5	D	930	180	90	40	370	380	540	1.47	876	1091	14.4	52	15716	56753	6.9	0	89	2.7	11.0	comparative steel
6	E	930	180	91	39	380	380	540	1.45	870	1114	13.8	50	15369	55685	7.1	0	90	2.8	10.0	comparative steel
7	F	910	180	90	39	360	400	540	1.42	1041	1133	11.8	60	13370	68436	5.1	0	94	2.1	6.0	comparative steel
8	G	910	180	90	39	370	400	180	1.43	912	1071	13.8	49	14785	52925	6.7	0	95	3.6	5.1	comparative steel
9	H	910	180	90	41	340	400	180	1.42	988	1149	11.5	57	13208	64951	5.2	0	96	1.4	4.0	comparative steel
10	H	910	180	90	39	360	400	540	1.42	977	1147	12.2	48	13938	55407	5.4	0	94	1.7	6.0	comparative steel
11	I	910	180	90	39	360	400	540	1.42	974	1150	12.8	53	14719	60830	6.3	0	92	1.5	8.0	comparative steel
12	L	930	180	90	40	380	400	540	1.43	873	1121	12.4	46	13900	51566	5.2	0	92	4.2	7.6	comparative steel
13	A	930	180	90	36	420	420	540	1.43	728	982	19.1	34	18762	33251	9.2	6	82	8.3	12.0	comparative steel
14	B	930	180	90	32	480	380	540	1.44	699	911	21.4	40	19493	36664	10.1	20	66	7.9	14.0	comparative steel
15	D	930	180	90	32	480	380	540	1.45	753	956	21	38	20085	36345	11.9	24	63	9.0	13.0	comparative steel
16	D	910	180	90	51	200	200	180	1.46	1036	1479	5.8	23	8581	33953	2	0	88	8.0	12.0	comparative steel
17	F	910	180	90	42	280	320	180	1.41	968	1312	8.2	62	10755	81385	2	0	85	12.0	15.0	comparative steel
18	J	930	180	90	39	360	400	540	1.42	731	904	19.8	35	17899	31640	8	12	78	4.5	10	comparative steel
19	K	910	180	90	40	360	400	540	1.43	698	859	23.2	25	19929	21475	10.2	20	69	5.2	11	comparative steel
20	L	850	180	90	40	340	380	540	1.45	691	958	23.6	30	22609	28740	9	35	52	5.4	13	comparative steel
21	M	850	180	90	36	350	300	540	1.41	769	1153	9.4	29	10838	33437	<1	8	81	8.0	11.0	comparative steel
22	M	880	180	90	38	350	420	540	1.41	701	1045	10	49	10450	51205	<1	0	89	4.9	11.0	comparative steel

CR1: Ann.temp → 550°C

CR2: 550°C → Stop.temp

INDUSTRIAL APPLICABILITY

[0057] The present invention can be widely applied to high strength steel sheets having excellent formability for vehicles such as automobiles.

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Claims

1. A high strength cold rolled steel sheet having

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a) a composition consisting of the following elements (in wt. %):

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C	0.15 - 0.18
Mn	2.2 - 2.4
Si	0.7 - 0.9
Cr	0.1 - 0.9
Al	0.2 - 0.6
Si + 0.8 Al + Cr	1.4-1.8
Nb	< 0.1
Mo	< 0.3
Ti	< 0.2
V	< 0.2
Cu	< 0.5
Ni	< 0.5
S	≤ 0.01
P	≤ 0.02
N	≤ 0.02
B	< 0.005
Ca	< 0.005
Mg	< 0.005
REM	< 0.005

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balance Fe apart from impurities,

b) a multiphase microstructure comprising (in vol. %)

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retained austenite	5-20
bainite + bainitic ferrite + tempered martensite	≥ 80
polygonal ferrite	≤ 10

c) the following mechanical properties

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a tensile strength (R_m)	980 - 1200 MPa
an elongation (A_{80})	≥ 11 %
a hole expanding ratio (λ)	≥ 45 %

50

and fulfilling at least one of the following conditions

$R_m \times A_{80}$	≥ 13 000 MPa%
$R_m \times \lambda$	≥ 50 000 MPa%

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2. A high strength cold rolled steel sheet according to any of the preceding claims fulfilling at least one of:

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		Nb	0.02 - 0.08
5		Mo	0.05 - 0.3
		Ti	0.02 - 0.08
		V	0.02 - 0.1
		Cu	0.05 - 0.4
		Ni	0.05 - 0.4
10		B	0.0005 - 0.003
		Ca	0.0005 - 0.005
		Mg	0.0005 - 0.005
		REM	0.0005 - 0.005

15 **3.** A high strength cold rolled steel sheet according to any of the preceding claims fulfilling at least one of:

		S	≤ 0.01 preferably ≤ 0.003
20		P	≤ 0.02 preferably ≤ 0.01
		N	≤ 0.02 preferably ≤ 0.003
		Ti	> 3.4N

25 **4.** A high strength cold rolled steel sheet according to any of the preceding claims wherein the maximum size of the martensite-austenite constituent (MA) is ≤ 5 μm, preferably ≤ 3 μm.

5. A high strength cold rolled steel sheet according to any of the preceding claims wherein the multiphase microstructure comprising (in vol. %)

		5 - 16, preferably below 10 %
30	retained austenite	
	bainite + bainite ferrite + tempered martensite	≥ 80
	polygonal ferrite	≤ 10
35	martensite-austenite constituent (MA)	≤ 20 %, preferably
		≤ 16 %, most preferably below 10 %

6. A high strength cold rolled steel sheet according to any of the preceding claims wherein the steel comprises

		Nb	0.02- 0.03
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7. A high strength cold rolled steel sheet any of the preceding claims wherein the ratio (Mn+Cr)/(Si+Al) ≥ 1.6.

45 **8.** A high strength cold rolled steel sheet according to any of the preceding claims wherein the amount of Si is on the order of the amount of Al or larger than the amount of Al, preferably Si > 1.1 Al, more preferably Si > 1.3 Al or even Si > 2 Al.

50 **9.** A high strength cold rolled steel sheet according to any of the preceding claims which is not provided with a hot dip galvanizing layer.

10. A method of producing a high strength cold rolled steel sheet according to any of the preceding claims comprising the steps of:

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- a) providing a cold rolled steel strip having a composition as set out in any of the preceding claims,
 - b) annealing the cold rolled steel strip at a temperature above the A_{c3} temperature in order to fully austenitize the steel, followed by

c) cooling the cold rolled steel strip from the annealing temperature, T_{an} , to a cooling stop temperature of rapid cooling, T_{RC} , that is between 360 and 460 °C, preferably between 380 and 420 °C, at cooling rate sufficient to avoid the ferrite formation, the cooling rate being 20 -100 °C/s, followed by
 d) austempering the cold rolled steel strip at an overageing/austempering temperature, T_{OA} , that is between 360 and 460 °C, preferably 380 and 420 °C, and
 e) cooling the cold rolled steel strip to ambient temperature,
 wherein the steel sheet is a high elongation type steel sheet having strength-elongation balance $R_m \times A_{80} \geq 13$ 000 MPa%, preferably ≥ 15 000 MPa%.

11. A method of producing a high strength cold rolled steel sheet according to any of claims 1-9 comprising the steps of:

a) providing a cold rolled steel strip having a composition as set out in any of the preceding claims,
 b) annealing the cold rolled steel strip at a temperature above the A_{c3} temperature in to fully austenitizing the steel, followed by
 c) cooling the cold rolled steel strip from the annealing temperature, T_{an} , to a cooling stop temperature of rapid cooling $T_{RC} < T_{MS}$, T_{MS} being between 300 and 400 °C, preferably between 340 and 370 °C, at cooling rate sufficient to avoid the formation ferrite, the cooling rate being 20 -100 °C/s, followed by
 d) austempering the cold rolled steel strip at an overageing/austempering temperature, T_{OA} that is between 360 and 460 °C, preferably between 380 and 420 °C, preferably $T_{OA} > T_{RC}$, and
 e) cooling the cold rolled steel strip to ambient temperature,
 wherein the steel sheet is a high hole expansibility type steel sheet having stretch-flangeability $R_m \times \lambda \geq 50$ 000 MPa% preferably ≥ 55 000 MPa.

12. A method of producing a high strength cold rolled steel sheet according to claim 10 and 11 wherein:

in step b) the annealing being performed at an annealing temperature, T_{an} , that is between 910 and 930 °C, during an annealing holding time, t_{an} , which is between 150 and 200 s, preferably 180 s,
 in step c) the cooling being performed according to a cooling pattern having two separate cooling rates; a first cooling rate, CR1, of 80 - 100 °C/s, preferably of 85 - 95 °C/s, preferably about 90 °C/s to a temperature which is between 530 to 570 °C, preferably 550 °C, and a second cooling rate, CR2, of 35 - 45 °C, preferably about 40 °C/s to the stop temperature of rapid cooling, T_{RC} , and
 in step d) the austempering of the steel being performed at a time interval of 150-600 s, preferably 180 - 540 s.

13. A method of producing a high strength cold rolled steel sheet according to claims 10 and 11 wherein no external heating being applied to the steel sheet between step c) and d).

Patentansprüche

1. Hochfestes kaltgewalztes Stahlblech, mit

a) einer Zusammensetzung bestehend aus den folgenden Elementen (in Gew.-%):

C	0.15 - 0.18
Mn	2.2 - 2.4
Si	0.7 - 0.9
Cr	0.1 - 0.9
Al	0.2 - 0.6
Si + 0.8 Al + Cr	1.4 - 1.8
Nb	< 0.1
Mo	< 0.3
Ti	< 0.2
V	< 0.2
Cu	< 0.5
Ni	< 0.5
S	≤ 0.01

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(fortgesetzt)

5	P	≤ 0.02
	N	≤ 0.02
	B	< 0.005
	Ca	< 0.005
	Mg	< 0.005
	REM	< 0.005

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der Rest Fe, bis auf Unreinheiten
b) mehrphasige Mikrostruktur, umfassend (in Vol.-%)

15	Rest austenit	5 - 20
	Bainit + bainitischer Ferrit + temperierter Martensit	≥ 80
	polygoner Ferrit	≤ 10

c) mindestens eine der folgenden mechanischen Eigenschaften

20	Zugfestigkeit (R_m)	980 - 1200 MPa
	Dehnung (A_{80})	≥ 11 %
	Lochaufweitungsrate (λ)	≥ 45 %,

25
und mindestens eine der folgenden Bedingungen erfüllt

30	$R_m \times A_{80}$	≥ 13000 MPa%
	$R_m \times \lambda$	≥ 50000 MPa%.

2. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, das zumindest eines der folgenden erfüllt:

35	Nb	0.02 - 0.08
	Mo	0.05-0.3
	Ti	0.02 - 0.08
	V	0.02-0.1
40	Cu	0.05 - 0.4
	Ni	0.05 - 0.4
	B	0.0005-0.003
	Ca	0.0005-0.005
45	Mg	0.0005-0.005
	REM	0.0005-0.005

3. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, das mindestens eines der folgenden erfüllt:

50	S	≤ 0,01	vorzugsweise	≤ 0,003
	P	≤ 0,02	vorzugsweise	≤ 0,01
	N	≤ 0,02	vorzugsweise	≤ 0,003
55	Ti	> 3,4 N		

4. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, wobei die maximale Größe der

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Martensit-Austenit-Konstituent (MA) $\leq 5 \mu\text{m}$ ist, vorzugsweise $\leq 3 \mu\text{m}$.

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5. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, wobei die mehrphasige Mikrostruktur umfasst (in Vol.-%)

Restaustenit	5 - 16, vorzugsweise unter 10%
Bainit + bainitischer Ferrit + temperierter Martensit	≥ 80
polygonaler Ferrit	≤ 10
Martensit-Austenit-Konstituent (MA)	$\leq 20\%$, vorzugsweise $\leq 16\%$, am meisten bevorzugt unter 10%

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6. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, wobei der Stahl umfasst:

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Nb 0,02 - 0,03

- 20
7. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, wobei das Verhältnis $(\text{Mn} + \text{Cr}) / (\text{Si} + \text{Al}) \geq 1,6$ ist.

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8. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, wobei die Menge von Si in der Größenordnung der Menge von Al oder größer als die Menge von Al ist, vorzugsweise $\text{Si} > 1,1 \text{ Al}$, noch bevorzugter $\text{Si} > 1,3 \text{ Al}$, oder sogar $\text{Si} > 2 \text{ Al}$.

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9. Hochfestes kaltgewalztes Stahlblech nach einem der vorhergehenden Ansprüche, das nicht mit einer feuerverzinkten Schicht versehen ist.

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10. Verfahren zum Herstellen eines hochfesten kaltgewalzten Stahlblechs nach einem der vorhergehenden Ansprüche, umfassend die Schritte:

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a) Bereitstellen eines kaltgewalzten Stahlstreifens mit einer Zusammensetzung wie in einem der vorhergehenden Ansprüche angegeben
b) Glühen des kaltgewalzten Stahlstreifens bei einer Temperatur oberhalb der A_{c3} -Temperatur, um den Stahl vollständig zu austenitisieren, gefolgt von
c) Abkühlen des kaltgewalzten Stahlstreifens von der Glühtemperatur, T_{an} , auf eine Kühlstoptemperatur einer Schnellabkühlung, T_{RC} , die zwischen 360 und 460°C liegt, bevorzugt zwischen 380 und 420°C , bei einer Kühlrate, die ausreichend ist, um Ferritbildung zu verhindern, wobei die Kühlrate 20 - 100°C/s beträgt, gefolgt von
d) Austempem des kaltgewalzten Stahlstreifens bei einer Überalterungs-/Austempertemperatur, T_{OA} , die zwischen 360 und 460°C liegt, vorzugsweise zwischen 380 und 420°C , und
e) Abkühlen des kaltgewalzten Stahlstreifens auf Raumtemperatur, wobei der Stahl ein hochdehnfähiger Stahl mit einer Festigkeits-Dehn-Balance von $R_m \times A_{80} \geq 13000 \text{ MPa}\%$, bevorzugt $\geq 15000 \text{ MPa}\%$ ist.

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11. Verfahren zum Herstellen eines hochfesten kaltgewalzten Stahlblechs nach einem der Ansprüche 1 bis 9, umfassend die Schritte:

- 50
a) Bereitstellen eines kaltgewalzten Stahlstreifens mit einer Zusammensetzung wie in einem der vorhergehenden Ansprüche angegeben,
b) Glühen des kaltgewalzten Stahlstreifens bei einer Temperatur oberhalb der A_{c3} -Temperatur, um den Stahl vollständig zu austenitisieren, gefolgt von
c) Abkühlen des kaltgewalzten Stahlstreifens von der Glühtemperatur, T_{an} , auf eine Kühlstoptemperatur einer Schnellabkühlung, $T_{RC} < T_{MS}$, wobei T_{MS} zwischen 300 und 400°C liegt, bevorzugt zwischen 340 und 370°C , bei einer Kühlrate, die ausreichend ist, um Ferritbildung zu verhindern, wobei die Kühlrate 20 - 100°C/s beträgt, gefolgt von
d) Austempem des kaltgewalzten Stahlstreifens bei einer Überalterungs-/Austempertemperatur, T_{OA} , die zwischen 360 und 460°C liegt, vorzugsweise zwischen 380 und 420°C , bevorzugt $T_{OA} > T_{RC}$, und
e) Abkühlen des kaltgewalzten Stahlstreifens auf Raumtemperatur,

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wobei das Stahlblech ein Stahlblech mit hoher Lochaufweitung mit einer Streckbarkeit von $R_m \times \lambda \geq 50000 \text{ MPa}\%$, bevorzugt $\geq 55000 \text{ MPa}\%$ ist.

12. Verfahren zum Herstellen eines hochfesten kaltgewalzten Stahlblechs gemäß Anspruch 10 und 11, wobei

5 in Schritt b) das Glühen bei einer Glüh­temperatur, T_{an} , durchgeführt wird, die zwischen 910 und 930°C liegt, während einer Glüh­haltezeit, t_{an} , die zwischen 150 und 200s liegt, vorzugsweise 180 s, in Schritt c) das Abkühlen gemäß einem Abkühl­muster durchgeführt wird, das zwei separate Kühl­raten aufweist; eine erste Kühl­rate, CR1, von 80-100°C/s, vorzugsweise von 85 - 95°C/s, bevorzugt um 90°C/s, auf eine Temperatur, die zwischen 530 bis 570°C liegt, bevorzugt 550°C, und eine zweite Kühl­rate, CR2, von 35-45°C, bevorzugt um 40°C/s, auf die Stoptemperatur der Schnellabkühlung, T_{RC} , und in Schritt d) das Austemp­ern des Stahls in einem Zeitintervall von 150-600s durchgeführt wird, bevorzugt 180-540s.

15 13. Verfahren zum Herstellen eines hochfesten kaltgewalzten Stahlblechs gemäß den Ansprüchen 10 und 11, wobei zwischen den Schritten c) und d) keine Erhitzung von außen auf das Stahlblech angewandt wird.

Revendications

20 1. Une tôle d'acier laminée à froid à haute résistance ayant,

a) une composition constituée des éléments suivants (en % en poids) :

25	C	0.15 - 0.18
	Mn	2.2 - 2.4
	Si	0.7 - 0.9
	Cr	0.1 - 0.9
30	Al	0.2 - 0.6
	Si + 0.8 Al + Cr	1.4 - 1.8
	Nb	< 0.1
	Mo	< 0.3
	Ti	< 0.2
35	V	< 0.2
	Cu	< 0.5
	Ni	< 0.5
	S	≤ 0.01
40	P	≤ 0.02
	N	≤ 0.02
	B	< 0,005
	Ca	< 0,005
	Mg	< 0,005
45	REM	< 0,005

complément en Fe à l'exception des impuretés,

b) une microstructure multiphase comprenant (en % du vol.)

50	austénite résiduelle	5 - 20
	bainite + ferrite bainitique + martensite trempée	≥ 80
	ferrite polygonale	≤ 10

55 c) au moins une des propriétés mécaniques suivantes

une résistance à la traction (R_m) 980 - 1200 MPa

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(suite)

un allongement (A_{80}) $\geq 11 \%$
un taux d'expansion de trous (λ) $\geq 45 \%$,

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et remplissant au moins une des conditions suivantes

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$R_m \times A_{80} \geq 13\,000 \text{ MPa}\%$
 $R_m \times \lambda \geq 50\,000 \text{ MPa}\%$

2. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, répondant à au moins un parmi ce qui suit :

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Nb	0,02 - 0,08
Mo	0,05 - 0,3
Ti	0,02 - 0,08
V	0,02 - 0,1
Cu	0,05 - 0,4
Ni	0,05 - 0,4
B	0,0005 - 0,003
Ca	0,0005 - 0,005
Mg	0,0005 - 0,005
REM	0,0005 - 0,005

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3. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, répondant à au moins un parmi ce qui suit :

30

S	$\leq 0,01$	de préférence $\leq 0,003$
P	$\leq 0,02$	de préférence $\leq 0,01$
N	$\leq 0,02$	de préférence $\leq 0,003$
Ti	$> 3,4N$	

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4. Tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, dans laquelle la taille maximale du constituant martensite-austénite (MA) est $\leq 5 \mu\text{m}$, de préférence $\leq 3 \mu\text{m}$.

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5. Tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, dans laquelle la microstructure multiphase comprend (en% du vol.)

45

austénite résiduelle	5 - 16, de préférence inférieure à 10%
bainite + bainite ferrite + martensite trempée	≥ 80
ferrite polygonale	≤ 10
constituant martensite-austénite (MA)	$\leq 20\%$, de préférence $\leq 16\%$, de manière la plus préférée, inférieur à 10%

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6. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, dans laquelle l'acier comprend Nb 0,02 à 0,03

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7. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, dans laquelle le rapport $(\text{Mn} + \text{Cr}) / (\text{Si} + \text{Al}) \geq 1,6$.

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8. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, dans laquelle la quantité de Si est de l'ordre de la quantité d'Al, ou supérieure à la quantité d'Al, de préférence $Si > 1,1 Al$, plus préférablement $Si > 1,3 Al$ ou même $Si > 2 Al$.
9. Une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, qui n'est pas pourvue d'une couche de galvanisation à chaud.
10. Un procédé de production d'une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications précédentes, comprenant les étapes consistant à :
- fournir une bande d'acier laminée à froid ayant une composition telle que définie dans l'une quelconque des revendications précédentes,
 - réaliser un recuit de la bande d'acier laminée à froid à une température supérieure à la température A_{C3} afin d'austénitiser complètement l'acier, suivie du fait de
 - refroidir la bande d'acier laminée à froid depuis la température de recuit, T_{an} , jusqu'à une température d'arrêt de refroidissement du refroidissement rapide, T_{RC} , qui est comprise entre 360 et 460°C, de préférence entre 380 et 420°C, à une vitesse de refroidissement suffisante pour éviter la formation de ferrite, la vitesse de refroidissement étant de 20 à 100°C / s, suivie du fait
 - d'opérer une trempe bainitique de la bande d'acier laminée à froid à une température de dépassement / de trempe bainitique, T_{OA} , comprise entre 360 et 460°C, de préférence 380 et 420°C, et
 - refroidir la bande d'acier laminée à froid à la température ambiante, la tôle d'acier étant une tôle d'acier de type à allongement élevé ayant un solde de résistance à l'allongement $R_m \times A_{80} \geq 13\ 000\ MPa\%$, de préférence $\geq 15\ 000\ MPa\%$.
11. Un procédé de production d'une tôle d'acier laminée à froid à haute résistance selon l'une quelconque des revendications 1 à 9, comprenant les étapes consistant à :
- fournir une bande d'acier laminée à froid ayant une composition telle que définie dans l'une quelconque des revendications précédentes,
 - opérer un recuit de la bande d'acier laminée à froid à une température supérieure à la température A_{C3} afin d'austénitiser complètement l'acier, suivie du fait de
 - refroidir la bande d'acier laminée à froid depuis la température de recuit, T_{an} , jusqu'à une température d'arrêt de refroidissement du refroidissement rapide $T_{RC} < T_{MS}$, T_{MS} étant comprise entre 300 et 400°C, de préférence entre 340 et 370°C, à une vitesse de refroidissement suffisante pour éviter la formation de ferrite, la vitesse de refroidissement étant de 20 à 100°C/s, suivie du fait
 - d'opérer une trempe bainitique de la bande d'acier laminée à froid à une température de dépassement / de trempe bainitique, T_{OA} , qui est comprise entre 360 et 460°C, de préférence entre 380 et 420°C, de préférence $T_{OA} > T_{RC}$, et
 - refroidir la bande d'acier laminée à froid à la température ambiante, la tôle d'acier étant une tôle d'acier de type à haute capacité de dilatation de trous ayant une résistance à l'étirement $R_m \times \lambda \geq 50\ 000\ MPa\%$, de préférence $\geq 55\ 000\ MPa$.
12. Un procédé de production d'une tôle d'acier laminée à froid à haute résistance selon les revendications 10 et 11, dans lequel :
- à l'étape b), le recuit est effectué à une température de recuit, T_{an} , qui est entre 910 et 930°C, pendant un temps de maintien de recuit, t_{an} , qui est compris entre 150 et 200 s, de préférence 180 s,
 - à l'étape c), le refroidissement est effectué selon un schéma de refroidissement ayant deux vitesses de refroidissement séparées ; une première vitesse de refroidissement, CR1, de 80 à 100°C/s, de préférence de 85 à 95°C/s, de préférence d'environ 90°C/s jusqu'à une température comprise entre 530 et 570°C, de préférence de 550°C, et une deuxième vitesse de refroidissement, CR2, de 35 à 45°C, de préférence d'environ 40°C/s jusqu'à la température d'arrêt du refroidissement rapide, T_{RC} , et
 - à l'étape d) la trempe bainitique de l'acier est effectuée sur un intervalle de temps de 150 à 600 s, de préférence de 180 à 540 s.
13. Un procédé de production d'une tôle d'acier laminée à froid à haute résistance selon les revendications 10 et 11, dans lequel aucun chauffage externe n'est appliqué sur la tôle d'acier entre les étapes c) et d).

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- US 20090238713 A [0005]

Non-patent literature cited in the description

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