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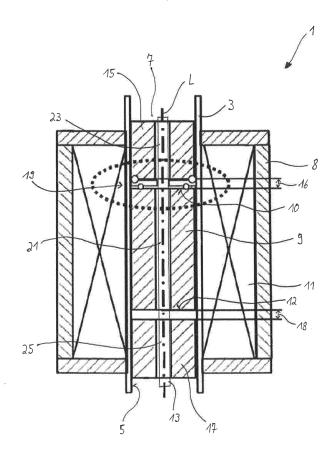
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(54) Fluid injection valve for a combustion engine and method for operating the same

(57) A fluid injection valve (1) for a combustion engine is specified. It has a pole piece (9), a first armature (15) which faces a first axial end (10) of the pole piece (9) and a second armature (17) which faces a second axial end (12) of the pole piece (9) with respect to a longitudinal axis (L). The first and second armatures (15,

17) are axially displaceable towards the pole piece (9) by means of a magnetic force induced by a coil (11) to generate a first mechanical force (F1) and a second mechanical force (F2), respectively, to axially move a valve needle (13). A method for operation of the fluid injection valve (1) is also disclosed.

FIG 1



EP 3 009 656 A1

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[0001] The invention relates to a fluid injection valve for a combustion engine and to a method for operating the same.

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[0002] Injection valves, also called injectors, are in widespread use, in particular for combustion engines where they may be arranged in order to dose a fluid into an intake manifold of the combustion engine or directly into a combustion chamber of a cylinder of the combustion engine.

[0003] In general, an injector has tough performance requirements to enable injection of accurate quantities of fluid and to fulfill pollution restrictions during operation of the injector and a corresponding combustion engine. Two main requirements are the ability to open fast at high pressures, for example higher than 200 bar in case of gasoline injectors, and to enable fast closing times, for example less than 500 microseconds in order to have a low flow and low actuation time.

[0004] Such requirements also concern hydraulic valves like solenoid actuated valves, for example. Regarding a solenoid injector, the mentioned requirements can be fulfilled using high magnetic forces to enable fast opening of a valve needle of the injector. Generally, the magnetic force is generated by a coil which induces a movement of an armature which impacts on the valve needle and hence causes a movement of the valve needle. To allow for a fast opening process of the valve needle high magnetic forces are needed to overcome high hydraulic pressures of a fluid inside the injector, for example. One object of the invention is to create a fluid injection valve for a combustion engine which enables a reliable and secure functioning with particular high energy efficiency.

[0005] The object is achieved by a fluid injection valve and a method having the features of the independent claims. Advantageous embodiments of the invention are given in the dependent claims.

[0006] According to a first aspect of the invention a fluid injection valve for a combustion engine is specified. It comprises a valve body, a pole piece, a coil, a valve needle, a first armature and a second armature. The fluid injection valve is in particular a fuel injector of the combustion engine.

[0007] The valve body has a longitudinal axis and comprises a wall - in particular a circumferential side wall - which forms a recess that enables a streaming fluid to pass through the fluid injection valve during operation. The pole piece has a first axial end and a second axial end on opposite sides of the pole piece along the longitudinal axis. The pole piece is positionally fix relative to the valve body.

[0008] The first armature faces the first axial end and the second armature faces the second axial end of the pole piece with respect to the longitudinal axis. The first armature and the second armature are arranged axially movably in the recess and are axially displaceable to-

wards the pole piece by a magnetic force induced by the coil to generate a first mechanical force and a second mechanical force, respectively, to axially move the valve needle along the longitudinal axis. Specifically, axial displacement of the first armature in a first axial direction towards the pole piece effects the first mechanical force and axial displacement of the second armature in a second axial direction towards the pole piece effects the second mechanical force.

[0009] In a preferred embodiment, the fluid injection valve comprises a leverage mechanism which is arranged between the pole piece and the first armature with respect to the longitudinal axis to transfer a mechanical force from the first armature to the valve needle for generating the first mechanical force acting on the valve needle during the operation of the fluid injection valve. The leverage mechanism has in particular a mechanical advantage so that the first mechanical force is larger than said mechanical force which is exerted on the leverage mechanism by the first armature.

[0010] Such a configuration of the fluid injection valve describes a simple and reliable possibility to increase a mechanical force acting on the valve needle during an operation of the fluid injection valve or an injector comprising the fluid injection valve. In this context, the magnetic force generated by one single magnetic circuit of the fluid injection valve is efficiently transferred into mechanical force acting on the valve needle due to coaction of the first and the second armature and, in particular, the leverage mechanism.

[0011] The described fluid injection valve has a reliable and secure function in particular when a high magnetic force is required from one single magnetic circuit. Due to the leverage mechanism there is no need for a second solenoid or a second magnetic circuit and a difficult design of the injector, for example. Hence, product cost can be reduced and the fluid injection valve enables a competitive arrangement of an injector which is simple in design and which exhibits an improved axial movement of the valve needle compared to an injector which comprises one armature and no leverage mechanism.

[0012] According to one embodiment of the first aspect, the leverage mechanism commutates the mechanical force generated by the first armature and the second armature. In other words, the leverage mechanism interacts mechanically with the first armature and with the valve needle so that the first mechanical force on the valve needle which is generated by axial displacement of the first armature towards the pole piece in the first axial direction and the second mechanical force on the valve needle which is generated by axial displacement of the second armature towards the pole piece in the second axial direction, opposite to the first axial direction, are both directed in the same one of the first and second axial directions, i.e. the first and second mechanical forces are either both directed in the first axial direction or in the second axial direction.

[0013] According to a further embodiment of the first

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aspect, the pole piece and at least one of the first armature and the second armature comprise penetrating openings respectively through which the valve needle extends.

[0014] This embodiment of the invention describes one possible configuration of the fluid injection valve and enables a symmetrical arrangement of the mentioned components along the longitudinal axis, for example. Hence, the pole piece, the first armature, the second armature and the valve needle are rotation-symmetrically constructed which is advantageous for manufacturing reasons and which realizes a simple arrangement of the fluid injection valve.

[0015] According to a further embodiment of the first aspect, the first armature generates the first force when the valve needle is in first axial positions and the second armature generates the second force when the needle is in second axial positions. In one development, the first positions are axially offset relative to the second positions. According to another development, the first positions and the second positions axially overlap at least partially. In another development, the first positions are a subregion of the second positions or vice versa.

[0016] This embodiment of the invention indicates that there the valve needle is axially displaceable between different regions in which only the first armature acts on the valve needle, only the second armature acts on the valve needle or both armatures act on the valve needle. The regions depend on the configuration of the corresponding armatures and on a possible lift which is realized by a predetermined distance of the respective armature to the pole piece for example. Hence, different movement characteristics for different needle positions of the valve needle along the longitudinal axis can be realized, for example.

[0017] Where the first and second positions overlap, the valve needle may experience a particularly large mechanical force acting on it. For example, it is advantageous that the first positions and the second positions overlap at the beginning of an opening transient to enable a fast opening of the fluid injection valve even against high fluid pressures. Accordingly, only one armature may drive further movement of the valve needle at the end of the opening transient which prevents an overshoot of the valve needle or at least reduces an impact of the valve needle to the valve body, for example. Hence, using such a configuration of the fluid injection valve enables a fast opening of the injector and a reduced movement of the valve needle at an end of the opening transient.

[0018] According to a further embodiment of the first aspect the valve needle comprises an edge - in particular a step - that interacts with the leverage mechanism during the operation of the fluid injection valve. In particular, the leverage mechanism is operable to engage in a form-fit connection with the edge. The form-fit engagement is in particular releasable to disengage the first armature from the valve needle, so that only the second armature coupled to to the valve needle in at least some of the second

positions.

[0019] This configuration of the fluid injection valve describes one possible arrangement of the valve needle which interacts with the leverage mechanism. In this context, the edge of the valve needle is formed in the area of the leverage mechanism between the first armature and the pole piece with respect to the longitudinal axis. Hence, the edge realizes a simple embodiment of a contact point where the leverage mechanism impacts on the valve needle.

[0020] According to a further embodiment of the first aspect the leverage mechanism comprises a first lever and a second lever. The first lever and the second lever are preferably positioned vis-à-vis with respect to the longitudinal axis in the recess.

[0021] This enables in a simple and reliable way an arrangement of the leverage mechanism and hence a commutation of the mechanical force generated by the movement of the first and second armature and induced by the magnetic force due to the coil.

[0022] For example, the first armature is coupled to the leverage mechanism and the two separate levers which are basically ashlar-formed. Furthermore, there is a contact region between the first armature and the first and second lever as well as between the edge of the valve needle and the first and second lever, for example. The contact regions are axially displaceable relative to the pole piece and the valve body while a fulcrum of each lever is preferably positionally fix relative to the pole piece and the valve body. This simple construction of the fluid injection valve realizes a simple force reversal of the mechanical force effected by the movement of the first armature and, thus, - in coaction with the movement of the second armature - an enhanced movement of the valve needle.

[0023] According to a second aspect of the invention a method for operation of an fluid injection valve in accordance with one of the preceding embodiments of the first aspect comprises a step of providing a fluid injection valve in accordance with one of the preceding embodiments and acting of a first force on the valve needle generated by the first armature within a first time period. The method further comprises acting of a second force on the valve needle generated by the second armature within a second time period wherein the first time period and the second time period at least partially temporarily overlap with each other. The first and second time periods may correspond to the above described first and second positions of the valve needle, respectively.

[0024] This aspect of the invention indicates a possible enhanced movement of the valve needle as a process of time analogously to the above mentioned spatial overlap of the first and second positions. For instances, the first force represents the mechanical force effected by the first armature and the leverage mechanism on the valve needle and the second force represents the mechanical force on the valve needle effected by the second armature. An overlap of the first and the second time

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periods enables a fast opening of the fluid injection valve while a non-overlapping portion, for example of the second time period, may reduce impact of the valve needle to the valve body. Therefore, the first time period within the first armature generates the first force acting on the valve needle is temporally shorter than the second time period. But both time periods start from a beginning of an opening transient of the injector. Later on, only the second armature acts on the valve needle due to the temporally longer second time period and the second force generated there within.

[0025] Exemplary embodiments of the invention are explained in the following with the aid of schematic drawings and reference numbers. Identical reference numbers designate elements or components with identical functions. The figures show:

Figure 1 an exemplary embodiment of a fluid injection valve for a combustion engine;

Figure 2 an exemplary embodiment of a leverage mechanism;

Figure 3 a further exemplary embodiment of a leverage mechanism; and

Figure 4 a flow chart for an exemplary embodiment of a method for operation of a fluid injection valve.

[0026] Figure 1 shows an exemplary embodiment of a fluid injection valve 1 which comprises a valve body 3, a pole piece 9, a coil 11, a valve needle 13, a first armature 15, a second armature 17 and a leverage mechanism 19. The valve body 3 has a longitudinal axis L and comprises a circumferential side wall 5 which forms a recess 7 that enables a streaming fluid to pass through the fluid injection valve 1 during an operation. The pole piece 9 is fixed to the wall 5 of the valve body 3 inside the recess 7. [0027] The first armature 15, the pole piece 9 and the second armature 17 are axially subsequently arranged along the longitudinal axis L inside the recess 7 of the valve body 3. Furthermore, the first armature 15 and the second armature 17 are arranged axially movably in the recess 7 along the longitudinal axis L relative to the pole piece 9. They are displaceable towards the pole piece 9 by a magnetic force induced by the coil 11 so that the first armature 15 moves in a first axial direction D1 towards the pole piece 9 and the second armature 17 moves in a second axial direction D2 towards the pole piece 9, opposite to the first axial direction D1 (cf. Fig. 2). In this embodiment the coil 11 surrounds the valve body 3 and the components inside the recess 7.

[0028] The first armature 15 comprises a penetrating opening 23, the pole piece 9 comprises a penetrating opening 21 and the second armature 17 comprises a penetrating opening 25 in which the valve needle 13 is arranged to prevent a fluid flow in a closed position or

otherwise to enable it. The first armature 15 faces a first axial end 10 of the pole piece 9 whereas the second armature 17 faces a second axial end 12 of the pole piece 9. Hence, the first armature 15 and the second armature 17 are arranged on opposite sides of the pole piece 9 along the longitudinal axis L.

[0029] Furthermore, the fluid injection valve 1 comprises the leverage mechanism 19 which is arranged between the first armature 15 and the pole piece 9 with respect to the longitudinal axis L. The leverage mechanism 19 is configured to reverse a direction of a mechanical force generated by the first armature 15. In other embodiments of the fluid injection valve 1 the leverage mechanism 19 may be arranged between the second armature 17 and the pole piece 9 with respect to the longitudinal axis L to reverse a direction of a mechanical force generated by the second armature 17.

[0030] During an operation of the fluid injection valve 1, the coil 11 is energized and the first armature 15 and the second armature 17 are attracted by the pole piece 9 by means of the magnetic force induced by the coil 11. Hence, the armatures 15, 17 move in opposite directions towards each other as described above. They are configured to generate a first mechanical force F1 and a second mechanical force F2, respectively. The first and second forces F1, F2 act on the valve needle 13 to axially move the valve needle 13 along the longitudinal axis L. Because of the leverage mechanism 19 a direction of the mechanical force which is effected by the first armature 15 is inverted by means of the leverage mechanism 19 to generate the first mechanical force F1. Therefore, the mechanical force which is effected by the first armature 15 on the leverage mechanism 19 and the first mechanical force F1 on the valve needle 13 are directed in opposite axial directions. Therefore, both the first armature 15 and the second armature 17 generate a mechanical force - the first and second forces F1, F2 - on the valve needle 13 in the same axial direction. In this context, the second force F2 on the valve needle 13 is directly transferred to the valve needle 13 by the second armature 17, i.e. without directional change.

[0031] Figure 2 schematically illustrates the functioning of the fluid injection valve 1 and shows the first armature 15, the second armature 17, the leverage mechanism 19 and the valve needle 13. Regarding this example, the pole piece 9 and the penetrating openings 23, 25 of the first armature 15 and the second armature 17 are omitted to simplify the explanation of the working principle of the fluid injection valve 1.

[0032] The leverage mechanism 19 comprises a first lever 31 and a second lever 32. Due to this simple arrangement using two separate levers 31, 32 a commutation of the force direction generated by movement of the first armature 15 can easily been realized. In this figure 2, straight arrows indicate the first and second axial directions D1 and D2 in which the appropriate components move for generating the first and second mechanical forces F1 and F2.

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[0033] When the coil 11 is energized, a respective movement of the first armature 15 and the second armature 17 is induced in direction of the pole piece 9, in particular due to the described arrangement relative to one another along the longitudinal axis L. The first armature 15 moves in the first axial direction D1 and the second armature 17 moves in the second direction D2 which is the opposite direction of the first direction D1. The leverage mechanism 19 comprises at least four contact regions, two to the first armature 15 and two to the pole piece 9 which is not illustrated in this figure 2 but only roughly indicated by the horizontal line directly below the leverage mechnism. The contact regions of the leverage mechanism 19 with the pole piece 9 - in particular with the first axial end 10 of the pole piece 9 - represent fulcrums of the first and second levers 31, 32, respectively. Due to the movement of the first armature 15 and its contact regions - one corresponding to each lever 31, 32 - the respective lever 31 and 31 are tilted with respect to the longitudinal axis L. Specifically, they may be rotated around the contact regions of the first and second lever 31, 32 to the pole piece 9 which act like fulcrums.

[0034] The first and the second lever 31, 32 further contact an edge 33 of the valve needle 13 - in particular on a side of the respective lever 31, 32 opposite of the respective contact region with the first armature 15 with respect to the fulcrum - and hence generate the first force F1 on the valve needle 13 which is directed in the second axial direction D2 to promote a movement of the valve needle 13 in the second axial direction due D2 to the induced tilt by the movement of the first armature 15 in the first axial direction D1. The second armature 17 for example directly contacts a further edge or a nose of the valve needle 13 and hence generates a movement of the valve needle 13 in the same direction as the one of the second armature 17 namely the second direction.

[0035] In this context, the contact regions between the two levers 31, 32 and the first armature 15 and the pole piece 9 can be punctual realized but also line- or area-shaped in dependence of the leverage mechanism needed for application.

[0036] Such a configuration of the fluid injection valve 1 describes a simple and reliable possibility to increase a mechanical force acting on the valve needle 13 during an operation of the fluid injection valve 1. In this context, the magnetic force generated by one single magnetic circuit of the fluid injection valve 1 comprising at least one valve body 3, one pole piece 9, one coil 11 and two armatures 15, 17 is efficiently transferred into mechanical force acting on the valve needle 13 due to coaction of the first and the second armature 15, 17 and the leverage mechanism 19. The leverage mechanism 19 commutates the movements of the first and the second armature 15, 17 which originally move towards each other because of its arrangement on opposite sides of the pole piece 9 along the longitudinal axis L.

[0037] The described fluid injection valve 1 enables a reliable and secure function in particular when high mag-

netic force is required from one magnetic circuit. Due to the leverage mechanism 19, there is no need for a second solenoid or a second magnetic circuit and a difficult design of the injector, for example. Hence, product cost can be reduced and the fluid injection valve 1 enables a competitive arrangement of an injector which is simple in design and which exhibits an improved axial movement of the valve needle 13 compared to an injector which comprises one armature and no leverage mechanism 19.

[0038] In figure 3 a further exemplary embodiment of the leverage mechanism 19 is illustrated in a perspective view. The first lever 31 and the second lever 32 are formed as two separate substantially ashlar-formed components which act on the edge 33 of the valve needle 13. The valve needle 13 is symmetrically arranged along the longitudinal axis L - i.e. in particular a needle axis of the valve needle 13 being coaxial to the longitudinal axis L - and the pole piece 9 comprises a recess 14 in which the first lever 31 and the second lever 32 are arranged. Concerning this exemplary embodiment, the first armature 15 comprises a disc like shape whereas the pole piece 9 substantially comprises a cylindrical shape with the above mentioned recess 14.

[0039] In this embodiment, the edge 33 of the valve needle 13 overlaps with the fulcrums of the levers 31, 32 in top view along the longitudinal axis, while the contact regions of the levers 31, 32 with the first armature 15 are positioned in an outer radial end region of each lever 31, 32. In this way, a large mechanical advantage is achieved so that the first mechanical force F1 on the valve needle 13 is particularly large. At the same time, a comparatively large axial displacement of the first armature 15 is translated into a much smaller axial displacement of the valve needle 13 at the end of which the levers 31, 32 may disengage from the form-fit connection with the edge 33 and the valve needle is further displaced in the second axial direction D2 by means of direct mechanical interaction with the second armature 17 (not shown in Fig. 3). Such a configuration is particularly advantageous for displacing the valve needle 13 away from a closing position, where it is in sealing contact with a valve seat of the fluid injection valve 1, against high fluid pressures. In this case, a large force is needed at the beginning of the opening transient to overcome the hydraulic force of the fluid pressure. Once there is a small gap between the valve needle 13 and the valve seat, the hydraulic force decreases and only a smaller force is needed to displace the valve needle 13 further away from the valve seat.

[0040] Figure 4 illustrates a simple exemplary flow-chart of a method for operation of the fluid injection valve 1 or a corresponding injector.

[0041] In a first step S1 the fluid injection valve 1 and the injector starts its operation by means of starting of an injection event, for example.

[0042] In a second step S2 an opening transient of the fluid injection valve 1 is initiated wherein a generated first force F1 and second force F2 act on the valve needle 13 within a first time period T1 and a second time period T2,

respectively. For example, the second time period T2 is longer than the first time period T1 while both time periods preferably start simultaneously and hence the second force F2 acts for a longer time on the valve needle than the first force F1.

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[0043] In this context, the first force F1 and the second force F2 are generated by the movements of the first armature 15 and the second armature 17, respectively, which movements are induced by energizing the coil 11 and generating a magnetic force attracting the armatures 15, 17 towards the pole piece 9. For instance, the first force F1 represents the mechanical force effected by the first armature 15 via the leverage mechanism 19 and the second force F2 represents the mechanical force given by the second armature 17. Therefore, due to the leverage mechanism 19 described above, the magnetically induced movements of the armatures 15 and 17 are translated into forces which are directed in the same axial direction so that the absolute values of the first and second forces F1, F2 add up to move and/or accelerate the valve needle 13 along the longitudinal axis L.

[0044] Hence, an overlap of the first time period T1 and the second time period T2 of the respective armature 15, 17 enables a fast opening of the fluid injection valve 1 and the corresponding injector and reduces an impact of the valve needle 13 to the valve body 3, for example.

[0045] In a third step S3, only the second time period T2 is still active - i.e. for example only the second armature 17 is still moving towards the pole piece 9 while the first armature 15 may already be in form-fit connection with the pole piece 9 or a separate stopper - and hence only the second force F2 generated by the second armature 17 is still acting on the valve needle 13. For this reason, the resulting movement of the valve needle 13 is induced only by the second armature 17 for example to achieve the complete opening position of the valve needle 13 and the fluid injection valve 1. Such a method for operating the fluid injection valve 1 prevents an impact or at least makes a contribution to reduce an impact of the valve needle 13 and/or the second armature 17 on adjacent components of the injector like the valve body 3, for instances.

[0046] Step S4 represents an ending of the method for operating the fluid injection valve 1 and may correspond to deactivation of the coil 11 for closing the fluid injection valve 1 to end the injection event, for example.

[0047] The method for operation of the fluid injection valve 1 describes two differently driven movements of the valve needle 13 which at least partially overlap in time. This allows for an enhanced movement of the valve needle 13 which is advantageous to rapidly move the valve needle 13 from its closed position even against high pressures of the fluid inside the injector, for example. This further allows for an axially movement of the valve needle 13 for different needle lift along the longitudinal axis L, for example, and enables a reliable and secure functioning of a fuel injector for a combustion engine with an improved energy efficiency because there is one coil

11 energized which generates two movements of two separate armatures 15 and 17 respectively.

[0048] Using the described fluid injection valve 1 and/or method for operation it is also possible to operate two valves simultaneously and differently. Hence, the movement of the first armature 15 may act on another valve than the movement of the second armature 17. This advantageously allows for different movements of two valves concerning an absolute value of needle lift, for example, and enables an injection of different quantities of fluid amongst others.

[0049] Further, it is possible that the two armatures 15 and 17 exhibit different magnetic gaps 16, 18 to the pole piece 9 and each armature 15, 17 can be submitted to a different spring load.

[0050] If there is no leverage mechanism 19 it is also possible to operate two valves in opposite directions by using two armatures 15, 17 and one pole piece 9 and one coil 11. This concerns one inward and one outward opening valve, for example.

Claims

- Fluid injection valve (1) for a combustion engine comprising
 - a valve body (3) having a longitudinal axis (L) and comprising a wall (5) which forms a recess (7) that enables a streaming fluid pass the fluid injection valve (1) during operation,
 - a pole piece (9),
 - a coil (11),
 - a valve needle (13),
 - a first armature (15), and
 - a second armature (17),

wherein

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- the pole piece (9) has a first axial end (10) and a second axial end (12) on opposite sides of the pole piece (9) with respect to the longitudinal axis (L),
- the first armature (15) faces the first axial end (10) and the second armature (17) faces the second axial end (12) of the pole piece (9) with respect to the longitudinal axis (L),
- the first armature (15) and the second armature (17) are arranged axially movable in the recess (7) and are axially displaceable towards the pole piece (9) by means of a magnetic force induced by the coil (11) to generate a first mechanical force (F1) and a second mechanical force (F2), respectively, to axially move the valve needle (13) during operation
- 2. Fluid injection valve (1) in accordance with claim 1, wherein the fluid injection valve (1) further comprises

a leverage mechanism (19) which is arranged between the pole piece (9) and the first armature (15) with respect to the longitudinal axis (L) to transfer a mechanical force from the first armature (15) to the valve needle (13) for generating the first mechanical force (F1).

- 3. Fluid injection valve (1) in accordance with claim 2, wherein the leverage mechanism (19) commutates the mechanical force generated by the first armature (15) and the second armature (17) so that the first mechanical force (F1) on the valve needle (13) generated by axial displacement of the first armature (15) towards the pole piece (9) in a first axial direction (D1) and the second mechanical force (F2) on the valve needle (13) generated by axial displacement of the second armature (17) towards the pole piece (9) in a second axial direction (D2), opposite to the first axial direction (D1), are both directed in the same one of the first and second axial directions (D1, D2).
- 4. Fluid injection valve (1) in accordance with one of claims 2 or 3, wherein the valve needle (13) comprises an edge (33) that interacts with the leverage mechanism (19) during the operation of the fluid injection valve (1).
- **5.** Fluid injection valve (1) in accordance with one of the preceding claims, wherein the leverage mechanism (19) comprises a first lever (31) and a second lever (32).
- 6. Fluid injection valve (1) in accordance with one of the preceding claims, wherein the first armature (15) generates the first mechanical force (F1) when the valve needle (13) is in first axial positions and the second armature (17) generates the second mechanical force (F2) when the valve needle (13) is in second axial positions.
- 7. Fluid injection valve (1) in accordance with claim 6, wherein the first positions and the second positions axially overlap at least partially.
- 8. Fluid injection valve (1) in accordance with one of the preceding claims, wherein the pole piece (9), and at least one of the first armature (15) and the second armature (17) comprise penetrating openings (21, 23, 25) respectively, through which the valve needle (13) extends.
- Method for operation of a fluid injection valve (1) in accordance with one of the proceeding claims, comprising
 - providing an fluid injection valve (1) in accordance with one of the preceding claims,
 - acting of a first force (F1) on the valve needle

(13) generated by the first armature (15) within a first time period (T1), and

- acting of a second force (F2) on the valve needle (13) generated by the second armature (17) within a second time period (T2) wherein the first time period (T1) and the second time period (T2) at least partially temporally interfere with each other.

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FIG 1

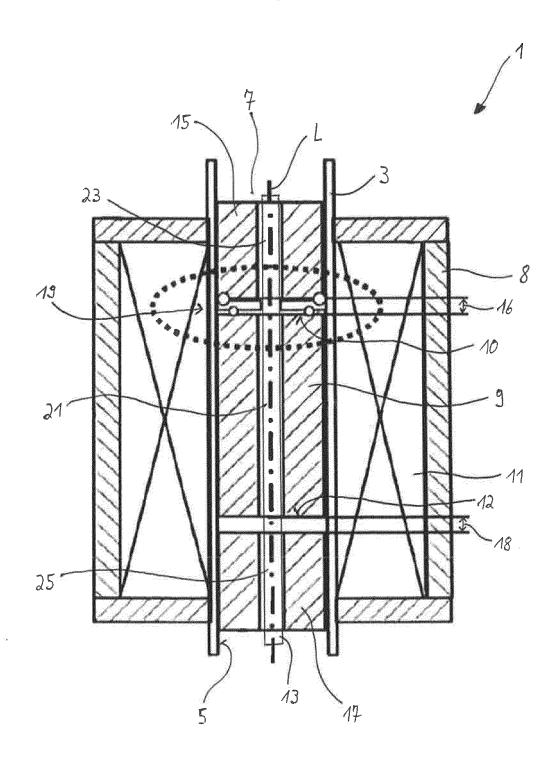


FIG 2

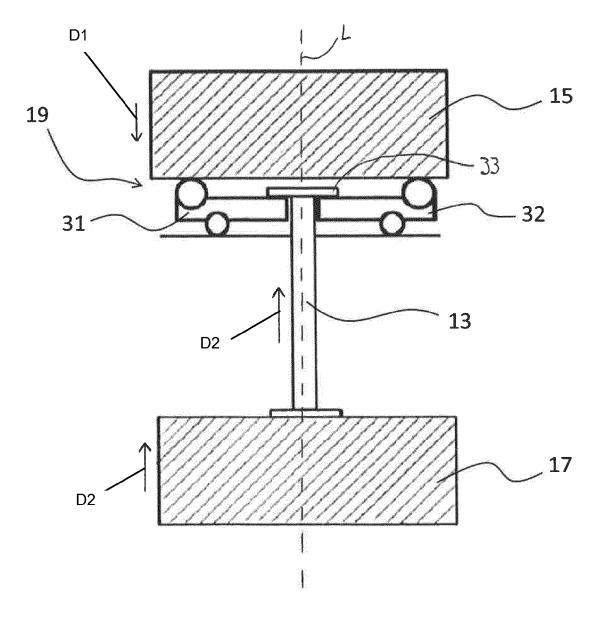


FIG 3

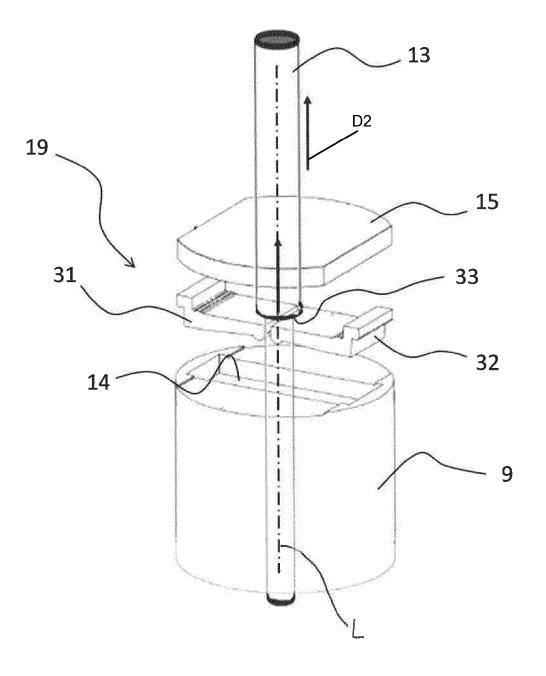
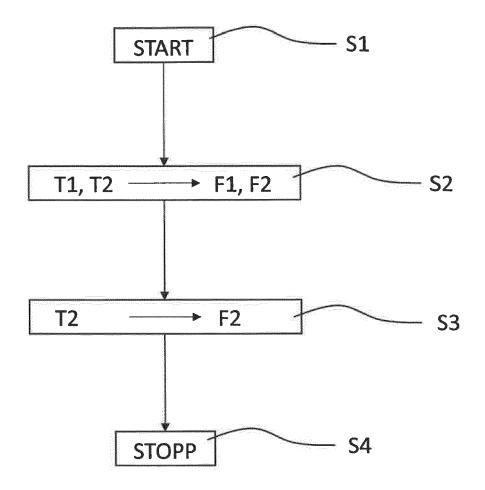


FIG 4





EUROPEAN SEARCH REPORT

Application Number EP 14 18 9025

CLASSIFICATION OF THE APPLICATION (IPC)

TECHNICAL FIELDS SEARCHED (IPC)

F₀2M H01F

Examiner

INV. F02M51/06

F02M63/00

H01F7/16

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DOCUMENTS CONSIDERED TO BE RELEVANT Citation of document with indication, where appropriate, Relevant Category of relevant passages 10 EP 0 404 357 A2 (GEN MOTORS CORP [US]) 27 December 1990 (1990-12-27) * column 3, line 7 - column 4, line 48; 1.6-8 Α 9 figures 4-6 * DE 10 2011 076956 A1 (BOSCH GMBH ROBERT [DE]) 6 December 2012 (2012-12-06) * paragraphs [0011], [0023]; figure * Α 2,4,5 15 EP 0 188 673 A2 (WABCO WESTINGHOUSE FAHRZEUG [DE]) 30 July 1986 (1986-07-30) Χ 1 20 * abstract; figures * DE 10 2012 218763 A1 (CONTINENTAL 2,4,5 Α AUTOMOTIVE GMBH [DE]) 17 April 2014 (2014-04-17) * paragraph [0026]; figures * 25 EP 2 236 807 A1 (CONTINENTAL AUTOMOTIVE Α 1,9 GMBH [DE]) 6 October 2010 (2010-10-06) * abstract; figures * 30 35 40 45 The present search report has been drawn up for all claims 1 Place of search Date of completion of the search 50 Munich 25 March 2015 Godrie, Pierre T: theory or principle underlying the invention
E: earlier patent document, but published on, or after the filing date
D: document cited in the application CATEGORY OF CITED DOCUMENTS 1503 03.82 X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category

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A : technological background
O : non-written disclosure
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EP 3 009 656 A1

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EP 14 18 9025

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25-03-2015

10	Patent document cited in search report	Publication date	Patent family member(s)	Publication date
15	EP 0404357 A2	27-12-1990	AU 618901 B2 AU 5680690 A DE 69005919 D1 DE 69005919 T2 EP 0404357 A2 JP H0343662 A JP H06103015 B2	09-01-1992 03-01-1991 24-02-1994 05-05-1994 27-12-1990 25-02-1991 14-12-1994
20	DE 102011076956 A1	06-12-2012	NONE	
25	EP 0188673 A2	30-07-1986	DE 3501708 A1 EP 0188673 A2 JP S61171978 A US 4655255 A	24-07-1986 30-07-1986 02-08-1986 07-04-1987
20	DE 102012218763 A1	17-04-2014	NONE	
30	EP 2236807 A1	06-10-2010	EP 2236807 A1 KR 20100106244 A US 2010264229 A1	06-10-2010 01-10-2010 21-10-2010
35				
40				
45				
50				
55	FORM P0459			

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82