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(54) **TILT ADAPTER FOR DIPLEXED ANTENNA WITH SEMI-INDEPENDENT TILT**

NEIGUNGSADAPTER FÜR EINE DIPLEX-ANTENNE MIT HALB-UNABHÄNGIGER NEIGUNG

ADAPTATEUR D'INCLINAISON POUR ANTENNE DIPLEXÉE AVEC INCLINAISON
SEMI-INDÉPENDANTE

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EP 3 125 366 B1

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Description**BACKGROUND**

5 **[0001]** Various aspects of the present disclosure relate to base station antennas, and, more particularly, to mechanical devices for controlling semi-independent tilt of diplexed antennas.

[0002] Cellular mobile operators are using more spectrum bands, and increasingly more spectrum within each band, to accommodate increased subscriber traffic, and for the deployment of new radio access technologies. Consequently, there is great demand for diplexed antennas that cover multiple closely-spaced bands (e.g., 790-862 MHz and 880-960 MHz). Based on network coverage requirements, operators often need to adjust the vertical radiation pattern of the antennas, i.e., the pattern's cross-section in the vertical plane. When required, alteration of the vertical angle of the antenna's main beam, also known as the "tilt", is used to adjust the coverage area of the antenna. Adjusting the beam angle of tilt may be implemented both mechanically and electrically. Mechanical tilt may be provided by angling the diplexed antenna physically downward, whereas electrical tilt may be provided by controlling phases of radiating signals of each radiating element so the main beam is moved downward. Mechanical and electrical tilt may be adjusted either individually, or in combination, utilizing remote control capabilities.

[0003] Network performance may be optimized if the tilt (e.g., electrical tilt) associated with each frequency band supported by an antenna is completely independently controlled. However, this independence may require a large number of diplexers and other components, adding significant cost and complexity to the creation of a diplexed antenna.

10 **[0004]** Accordingly, it would be advantageous to have a low complexity, cost-effective diplexed antenna able to produce high quality radiation patterns for each of the supported frequency bands and mechanical means for remotely controlling the same. Patent Document US 7 173 572 B1 is considered to be the closest prior art and relates to a dual band, dual pole, variable downtilt, 90 degree azimuth beamwidth antenna. The antenna includes dipole elements forming both a PCS band and a cellular band antenna. The PCS band antenna has two sections disposed each side of the cellular band antenna, the elements of each being positioned 90° with respect to the other. A microstrip feed network formed upon a common PC board feeds the respective dipole elements, and has serpentine portions with a corresponding dielectric member slideable thereover to establish the phase of the associated dipole antennas and achieve a linear downtilt of the respective antenna array. A slide rod adjustment assembly provides unitary movement of the dielectric members between two different slide rods. These dielectric members are secured with adhesive to the respective slide rods to achieve good dielectric control and no use of hardware. The radiating dipole elements are capacitively coupled to each microstrip, and are also capacitively associated reflector element. One arm of the reflector element is offset at least 45 degrees with respect to the other arm to improve cross polarization.

SUMMARY OF THE DISCLOSURE

35 **[0005]** According to the invention, the problem is solved by the subject-matter outlined in the independent claim. Advantageous further developments of the invention are set forth in the dependent claims.

[0006] Various aspects of the present disclosure are directed to a tilt adapter configured to facilitate a desired tilt of a first radio frequency (RF) band and a second RF band of an antenna. The antenna supports two or more frequency bands, in which the vertical tilt of each of the supported frequency bands is separately controlled by a coarse level of phase shifting, but commonly controlled by a fine level of phase shifting.

40 **[0007]** In one aspect, the tilt adapter may comprise a first rod coupled to at least one first coarse phase shifter, a second rod coupled to at least one second coarse phase shifter; a cross linkage member operatively engaged to both the first and second rods; a first rack coupled to the cross linkage member; and a second rack coupled to the first rack, at least one first fine phase shifter, and at least one second fine phase shifter. Lateral movement of the first rod or the second rod causes lateral movement of the second rack.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

50 **[0008]** The following detailed description will be better understood when read in conjunction with the appended drawings. For the purpose of illustrating the invention, there are shown in the drawings embodiments which are presently preferred. It should be understood, however, that the invention is not limited to the precise arrangements and instrumentalities shown.

[0009] In the drawings:

55 FIG. 1 is a schematic diagram of one example of a diplexed antenna with a simple design;

FIG. 2 is a schematic diagram of another example of a diplexed antenna with a more complex design;

FIG. 3 is a schematic diagram of a further example of a diplexed antenna, according to an aspect of the present disclosure;

FIG. 4 is a schematic diagram of a diplexed antenna using wiper arc and sliding dielectric phase shifters, according to an aspect of the present disclosure;

FIG. 5A is a schematic diagram of an example of a diplexed antenna having a length of 1.0 meters, with the first and second frequency bands having the same desired downtilt of 4° according to an aspect of the present disclosure;

FIG. 5B is a schematic diagram of an example of a diplexed antenna having a length of 1.0 meters, with the first and second frequency bands having the same desired downtilt of 8° , according to an aspect of the present disclosure;

FIG. 5C is a schematic diagram of an example of a diplexed antenna having a length of 1.0 meters, with the first frequency band having a desired downtilt of 4° and the second frequency band having a desired downtilt of 8° , according to an aspect of the present disclosure;

FIG. 6 is a perspective view of a portion of a backside of the diplexed antenna of FIGS. 5A-5C, according to an aspect of the present disclosure;

FIG. 7 is an enlarged perspective view of a tilt adapter, according to an aspect of the present disclosure;

FIG. 8 is a perspective view of a portion of the frontside of the diplexed antenna of FIG. 6, according to an aspect of the present disclosure; and

FIG. 9 is an enlarged view of a fine phase shifter according to an aspect of the present disclosure.

DETAILED DESCRIPTION OF VARIOUS EMBODIMENTS

[0010] Certain terminology is used in the following description for convenience only and is not limiting. The words "lower," "bottom," "upper" and "top" designate directions in the drawings to which reference is made. Unless specifically set forth herein, the terms "a," "an" and "the" are not limited to one element, but instead should be read as meaning "at least one." The terminology includes the words noted above, derivatives thereof and words of similar import. It should also be understood that the terms "about," "approximately," "generally," "substantially" and like terms, used herein when referring to a dimension or characteristic of a component of the invention, indicate that the described dimension/characteristic is not a strict boundary or parameter and does not exclude minor variations therefrom that are functionally similar. At a minimum, such references that include a numerical parameter would include variations that, using mathematical and industrial principles accepted in the art (e.g., rounding, measurement or other systematic errors, manufacturing tolerances, etc.), would not vary the least significant digit.

[0011] FIG. 1 is a schematic diagram of an example of a diplexed antenna 100. As shown, the diplexed antenna 100 includes first and second first level phase shifters 101, 103 coupled to inputs of respective diplexers 105, 107. Each output of the respective diplexers 105, 107 may be coupled to sub-arrays of radiating elements 109, 111 resulting in a fixed tilt within the sub-arrays of the radiating elements 109, 111. Employing a small number of diplexers, the diplexed antenna 100 exhibits simplicity and may be relatively inexpensive to implement. Unfortunately, the quality of radiation patterns produced by the diplexed antenna 100 may suffer due to some of the phase offsets being fixed.

[0012] Higher quality patterns may be realized when the electrical tilt of each frequency band is completely independently controlled, for example, as shown in a configuration of a four-radiating element diplexed antenna 200 illustrated in FIG. 2. As shown, each radiating element 201, 203, 205, 207 is coupled to a respective diplexer 209, 211, 213, 215, each of which is, in turn, coupled to outputs of each of phase shifters 217, 219. The number of diplexers may double when employing dual polarization functionality. Such diplexed antennas may increase in complexity and cost with greater lengths. For example, diplexed antennas having respective lengths of 1.4, 2.0, and 2.7 meters may require 10, 16, and 20 diplexers respectively, to produce high quality radiation patterns for each of the supported frequency bands.

[0013] As evident from the descriptions in connection with FIGS. 1 and 2, for better performance, it may be desirable for diplexed antennas to have an individually controllable tilt for each supported band. While completely individual controllable tilt may be desirable, there may be a significant correlation between (or among) the respective vertical tilt range of each supported band of the diplexed antenna, at least partly due to a frequency band tilt range's dependence on a mount height of the antenna supporting the frequency bands. More specifically, the higher above ground the antenna is mounted, the greater the tilt that may be required for acceptable operation.

[0014] Aspects of the present disclosure may take advantage of the above discussed tilt correlation by being directed

to a diplexed antenna for processing two or more frequency bands, where the vertical tilt of each of the supported frequency bands may be independently controlled by a coarse level of phase shifting, but commonly controlled by a fine level of phase shifting. As such, aspects of the present disclosure may achieve elevation patterns of a quality similar to that of the diplexed antenna 200 of FIG. 2 above, but at a low cost, light weight, and simplicity similar to that of the diplexed antenna 100 of FIG. 1 above.

[0015] Referring now to FIG. 3, according to an aspect of the present disclosure, a diplexed antenna 300 may include first and second coarse phase shifters 301, 303, first and second diplexers 305, 307, first and second fine phase shifters 309, 311, and radiating elements 313, 315. As discussed herein, each of the radiating elements may refer to single radiating elements or a sub-array of multiple radiating elements. The first coarse phase shifter 301 may be set to a tilt value α , which may provide a first contribution on a first tilt associated with a first frequency band, while the second coarse phase shifter 311 may be set to a tilt value β , which may provide a second contribution on a second tilt associated with a second frequency band. For example, the first coarse phase shifter 301 may be configured to receive an RF signal of the first frequency band (e.g., 790-862 MHz), and divide the RF signal into varied phase signals based on the set tilt value α . For example, one of the varied phase signals may have a first phase, and another of the varied phase signals may have a second phase different from the first phase. The second coarse phase shifter 311 may be configured to receive an RF signal of the second frequency band (e.g., 880-962 MHz), and divide the RF signal into varied phase signals in a similar fashion to that of the first coarse phase shifter 301.

[0016] The diplexers 305, 307 may be configured to diplex the varied phase signals output from the coarse phase shifters 301, 311. For example, the diplexer 305 may be configured to receive one or more varied phase signals output from the first coarse phase shifter 301, as well as one or more varied phase signals output from the second coarse phase shifter 303. Outputs from each of the diplexers 305, 307 may direct communication signals according to the first and second frequency bands.

[0017] An output from each of the first and second diplexers 305, 307 may be coupled to inputs of first and second fine phase shifters 309, 311 respectively. The first and second fine phase shifters 309, 311 may be configured to provide phase shifting among the radiating elements 313, 315. The first and second fine phase shifters 309, 311 may allow for operation on all of the supported frequency bands of the diplexed antenna with equal effect. More specifically, the first and second fine phase shifters 309, 311 may be configured to provide a phase shift based on the average of the set tilt values α° and β° of the supported frequency bands, or $(\alpha^\circ + \beta^\circ)/2$. To aid in the suppression of sidelobes of produced radiation patterns, each of the coarse and fine phase shifters may include a power divider (such as, for example, a Wilkinson power divider, not shown) to effect a tapered amplitude distribution (e.g., a linear phase progression) across the radiating elements 313, 315.

[0018] Referring now to FIG. 4, the first and second coarse phase shifters 401, 403 of a diplexed antenna 400, for example, may take the form of wiper-arc phase shifters, such as described in U.S. Pat. No. 7,463,190. Wiper-arc phase shifters may be preferred for coarse phase shifting due at least in part to their ability to generate a large phase shift in a small amount of area. The first and second fine phase shifters 409, 411 may take the form of sliding dielectric phase shifters or wiper arc phase shifters, as known in the art, to effect a tilt value of $(\alpha^\circ + \beta^\circ)/2$, as discussed above. Sliding dielectric phase shifters may be preferred, due at least in part, to their ease of allowance of differing power levels across respective outputs, which may be conducive to implementing a taper across an aperture of the diplexed antenna. Similar to the diplexed antenna 400, according to aspects of the present disclosure, to aid in the suppression of sidelobes of produced radiation patterns, each of the coarse and fine phase shifters may include a power divider (such as, for example, a Wilkinson power divider, not shown) to effect a tapered amplitude distribution across sub-arrays of radiating elements 413, 415.

[0019] Aspects of the present disclosure may be directed to various antenna lengths, which may incorporate the use of additional components (e.g., diplexers and phase shifters with additional outputs). For example, FIGS. 5A-5C are examples of diplexed antennas 500. As shown, the diplexed antenna 500 may comprise first and second coarse phase shifters 501, 503, first and second diplexers 505, 507, first and second fine phase shifters 509, 511, and radiating elements 502, 504, 506, 508.

[0020] The first coarse phase shifter 501 may be set to tilt value α , which may provide a first contribution on a first tilt associated with a first frequency band, while the second coarse phase shifter 503 may be set to tilt value β , which may provide a second contribution on a second tilt associated with a second frequency band. For example, the first coarse phase shifter 501 may be configured to receive an RF signal of the first frequency band and divide the RF signal into varied phase signals based on the set tilt value α . For example, one of the variable phase signals may have a first phase, and another of the variable phase signals may have a second phase different from the first phase. The second coarse phase shifter 503 may be configured to receive an RF signal of the second frequency band, and may divide the RF signal into varied phase signals in a similar fashion to that of the first coarse phase shifter 501.

[0021] The diplexers 505, 507 may be configured to diplex the varied phase shifted signals output from the coarse phase shifters 501, 503. For example, the diplexer 505 may be configured to receive one or more varied phase signals output from the first coarse phase shifter 501, as well as one or more varied phase signals output from the second coarse

phase shifter 503.

[0022] Outputs from each of the diplexers 505, 507 may direct communication signals responsive to the first and second frequency bands. An output of each of the first and second diplexers 505, 507 may be coupled to inputs of first and second fine phase shifters 509, 511 respectively. The first and second fine phase shifters 509, 511 may be configured to provide phase shifting among radiating elements 502, 504, 506, 508. The first and second fine phase shifters 509, 511 may allow for operation on all of the supported frequency bands of the diplexed antenna with equal effect. More specifically, the first and second fine phase shifters 509, 511 may be configured to provide a phase shift based on a combination of the set tilt values α and β of the respective coarse phase shifters 501, 503. This combination, may, for example, include an average of the set tilt values α° and β° of the supported frequency bands, or $(\alpha+\beta)/2$. To aid in the suppression of sidelobes of produced radiation patterns, each of the coarse phase shifters 501, 503 and fine phase shifters 509, 511 may include a power divider (such as, for example, a Wilkinson power divider, not shown) to effect a tapered amplitude distribution across the radiating elements 502, 504, 506, 508.

[0023] According to aspects of the present disclosure, a tilt value θ may be related to a phase shift generated by each of the phase shifters. For example, phase shift $= \sin(\theta) * S * k$, where S = a distance between radiating elements in degrees (wavelength $= 360^\circ$), and k = distance between phase shifter outputs measured in element spacings. For small values of downtilt, $\sin(\theta) * S \approx \sin(1) * S \approx 0.0175 * \theta * S$.

[0024] In the configurations illustrated in FIGS. 5A-5C, each coarse phase shifter 501, 503 may include outputs that are two element spacings apart (i.e., $k=2$). For example, according to the diplexed antenna 500 in FIGS. 5A-5C, each coarse phase shifter 501, 503 may shift every 2 radiating elements. Each fine phase shifter 509, 511 may include outputs that are one element spacing apart (i.e., $k=1$). For example, according to the diplexed antenna 500 in FIGS. 5A-5C, each fine phase shifter 509, 511 may shift every radiating element. The distance between radiating elements, S , may typically be between 250° - 300° . However, S may be other values outside this range in keeping with the invention. With a value of S in the range of 250° - 300° , $\sin(1) * S \approx 5^\circ$. It should be noted that each of the coarse phase shifters 501, 503 may include outputs that may be fewer or greater than two element spacings apart in keeping with the disclosure. Further, it should be noted that each of the fine phase shifters 509, 511 may include outputs that are greater than one element spacing apart in keeping with the disclosure.

[0025] Referring to FIG. 5A, when the set tilt value for each frequency band is equal (e.g., $\alpha=\beta=4^\circ$), the diplexed antenna may exhibit accuracy similar to that of each of the supported bands having completely independent tilt. Therefore, using the above equation, the phase shift generated by the first coarse phase shifter $501 = \alpha * \sin(1) * S * k = 4 * 5 * 2 = 40^\circ$. Therefore, the first coarse phase shifter 501 may generate a pair of varied phase signals varied by 40° in phase. This variation in phase shift may be realized by having one of the outputs of the first coarse phase shifter 501 having a phase of -20° and the other having a phase of $+20^\circ$. However, it should be noted that other phase shifts may be employed in keeping with the disclosure.

[0026] With $\alpha=\beta=4^\circ$, the first and second fine phase shifters 509, 511 may be configured to generate a phase shift based on a combination of the set tilt values of the supported bands of the diplexed antenna. For example, the first and second fine phase shifters 509, 511 may be configured to generate a phase shift based on an average of the set tilt values $\alpha=\beta=4^\circ$, which in this case, would be 4° . As such, according to the above equation, the phase shift generated by each of the first and second fine phase shifters 509, 511 may be 20° , which may result in a phase progression across the outputs of each of first and second fine phase shifter outputs 509, 511, of 10° and $+10^\circ$. Table 1 below provides a list of phase shifts applied to each radiating element 502, 504, 506, 508 as attributed to each phase shifter, and the total phase shift applied to each radiating element 502, 504, 506, 508, with such a configuration.

Table 1

$\alpha=\beta=4^\circ$				
Radiating Element#	502	504	506	508
Coarse phase shifters 501, 503	-20°	-20°	$+20^\circ$	$+20^\circ$
Fine phase shifters 505, 507	-10°	$+10^\circ$	-10°	$+10^\circ$
Total phase shift	-30°	-10°	$+10^\circ$	$+30^\circ$

[0027] Alternatively, as shown in FIG. 5B, if $\alpha=\beta=8^\circ$, the phase shift generated by the first and second coarse phase shifters 501,

$503 = \alpha * \sin(1) * S * k = 8 * 5 * 2 = 80^\circ$. Therefore, each of the first and second coarse phase shifters 501, 503 may generate a phase shift of 80° . For example, the output signals of the first and second coarse phase shifters 501, 503 may have a phase -40° and $+40^\circ$ respectively. However, it should be noted that other phase shifts may be employed in keeping with the disclosure. The first and second fine phase shifters 509, 511 may be configured to generate a phase shift based on

EP 3 125 366 B1

the average of the set tilt values α and β , which would, in this case, be 8° . As such, according to the above equation, the phase shift generated by each of the first and second fine phase shifters 509, 511 may be 40° , which may be realized with one of the output signals having a phase of -20° and the other of the output signals having a phase of $+20^\circ$. Table 2 below lists phase shifts applied to each radiating element 502, 504, 506, 508 as attributed to each phase shifter, and the total phase shift applied to each radiating element 502, 504, 506, 508:

Table 2

$\alpha=\beta=8^\circ$				
Radiating Element#	502	504	506	508
Coarse phase shifters 501, 503	-40°	-40°	$+40^\circ$	$+40^\circ$
Fine phase shifters 505, 507	-20°	$+20^\circ$	-20°	$+20^\circ$
Total phase shift	-60°	-20°	$+20^\circ$	$+60^\circ$

[0028] As shown in FIG. 5C, according to aspects of the present disclosure, when the desired tilts for the supported bands differ, performance may only slightly degrade, but may still be acceptable. For example, with the set tilts $\alpha=4^\circ$ and $\beta=8^\circ$, the fine phase shifters 509, 511 for both supported frequency bands may be configured to generate a phase shift based on the average set tilt values, which in this case would be $(\alpha+\beta)/2=6^\circ$. Therefore, according to the above equation, the phase shift generated by each of the first and second fine phase shifters 509, 511 would be $6 \times 5 = 30^\circ$, which may result in a phase shift of 30° , which may be realized with a linear phase progression across the outputs of the first and second fine phase shifters 509, 511 of -15° and $+15^\circ$. Table 3 below lists phase shifts applied to each radiating element 502, 504, 506, 508 as attributed to each phase shifter, and the total phase shift applied to each radiating element 502, 504, 506, 508, for this first band with tilt values $\alpha=4^\circ$ and $\beta=8^\circ$.

Table 3

Phase for band 1: $\alpha=4^\circ$, $\beta=8^\circ$				
Radiating Element#	502	504	506	508
Coarse phase shifters 501, 503	-20°	-20°	$+20^\circ$	$+20^\circ$
Fine phase shifters 505, 507	-15°	$+15^\circ$	-15°	$+15^\circ$
Total phase shift	-35°	-5°	$+5^\circ$	$+35^\circ$

[0029] Table 4 below lists phase shifts applied to each radiating element 502, 504, 506, 508 as attributed to each phase shifter, and the total phase shift applied to each radiating element 502, 504, 506, 508, for the second frequency band with tilt values $\alpha=4^\circ$ and $\beta=8^\circ$.

Table 4

Phase for band 2: $\alpha=4^\circ$, $\beta=8^\circ$				
Radiating Element#	502	504	506	508
Coarse phase shifters 501, 503	-40°	-40°	$+40^\circ$	$+40^\circ$
Fine phase shifters 505, 507	-15°	$+15^\circ$	-15°	$+15^\circ$
Total phase shift	-55°	-25°	$+25^\circ$	$+55^\circ$

[0030] Through analysis of the above data, the total phase shifts of the radiating elements 502, 504, 506, 508 of the dual band implementations of the diplexed antenna listed in Tables 3 and 4 may be relatively close to the ideal (e.g., effectively completely independent tilt implementations, as reflected in Tables 1 and 2) phase shifts of the radiating elements 502, 504, 506, 508. Consequently, aspects of the present disclosure may be able to achieve elevation patterns of a quality similar to that of more complex diplexed antenna.

[0031] FIG. 6 is a perspective view of a portion of a backside of the diplexed antenna 500. Each of the first and second coarse phase shifters 501, 503 may include two wiper arc phase shifters 501a, 501b, 503a, 503b, respectively. For example, the first phase shifter 501 may include one wiper arc phase shifter 501a configured to adjust a phase shift for $+45^\circ$ polarization, and another wiper arc phase shifter 501b configured to adjust a phase shift for -45° polarization of

the first frequency band. Similarly, the second coarse phase shifter 503 may include one wiper arc phase shifter 503a configured to adjust a phase shift for +45° polarization and another wiper arc phase shifter 503b configured to adjust a phase shift for -45° polarization of the second frequency band.

[0032] The first and second coarse phase shifters 501, 503 may be connected to respective first and second frequency band inputs 601, 603, and a tilt adapter 605 via respective connecting members 607, 609. More specifically, the connecting member 607 may be connected to the first frequency band input 601, the first phase shifter 501, and a first rod 611 of the tilt adapter 605. Similarly, the connecting member 609 may be connected to the second frequency band input 603, the second phase shifter 503, and a second rod 613 of the tilt adapter 605.

[0033] FIG. 7 is an enlarged perspective view of the tilt adapter 605 which may be configured to effect the desired tilt of the first and second frequency bands of operation of the diplexed antenna 500. The tilt adapter 605 may include a chassis 615 defining a cavity within an interior thereof. Two opposing side walls 616 of the chassis 615 may include a plurality of respective openings 617 with which portions of a first level rack 619, the first level rod 611, and the second level rod 613 may be slidably engaged.

[0034] A cross linkage member 621 may be pivotably connected to the first level rack 619, the first level rod 611, and the second level rod 613, at a position between the two opposing side walls 616. The cross linkage member 621 may include slots 623, 625 positioned at opposing ends of the cross linkage member 621. Respective pins 627, 629 may be affixed to, and may extend from, the first and second level rods 611, 613. The respective slots 623, 625 may allow for movement of the respective pins 627, 629 within the respective slots 623, 625.

[0035] Consequently, lateral movement of the first level rod 611 may cause movement of the pin 627 within the slot 623 as well as effect rotational movement of the cross linkage member 621 about the pin 629 affixed to the second level rod 613. The rotational movement of the cross linkage member 621 may cause a center 639 of the cross linkage member 621 to move in the same lateral direction as the first level rod 611. The lateral movement of the center 639 of the cross linkage member 621 may, in turn, cause the first level rack 619 to move a distance in the same lateral direction as the first level rod 611. As discussed herein throughout, lateral movement may refer to linear movement along an axis Y-Y.

[0036] Similarly, lateral movement of the second level rod 613 may cause movement of the pin 629 within the slot 625 as well as effect rotational movement of the cross linkage member 621 about the pin 627 affixed to the first level rod 611. The rotational movement of the cross linkage member 621 may cause the center 639 of the cross linkage member 621 to move in the same lateral direction as the second level rod 613. The lateral movement of the center 639 of the cross linkage member 621 may, in turn, cause the first level rack 619 to move in the same lateral direction as the second level rod 613.

[0037] The first level rack 619 may be configured to move at a predetermined fraction of the distance traveled by either of the first and second level rods 611, 613. To effect the average of the set tilt values α , β , of the supported first and second frequency bands, the predetermined fraction may be $\frac{1}{2}$. Stated differently, the first level rack 619 may be configured to move a lateral distance of $\frac{1}{2}$ the distance moved by either of the first and second level rods 611, 613.

[0038] The first level rack 619 may be in toothed engagement with a first pinion gear 631 which may, in turn, be connected to a second pinion gear 633 via a shaft 635. The second pinion gear 633 may be in toothed engagement with a second level rack 637. As such, the above discussed lateral movement of the first level rack 619 may cause lateral movement of the second level rack 637. The lateral movement of the second level rack 637 may be in accordance with a gear ratio of the first level rack 619 to the second level rack 637.

[0039] More specifically, as the first level rack 619 moves laterally, the first pinion gear 631 may rotate, which, in turn, may cause rotation of the shaft 635, which may drive rotation of the second pinion gear 633. Further, rotation of the second pinion gear 633 may cause lateral movement of the second level rack 637, positioned on the frontside of the diplexed antenna 500 (e.g., opposite the backside) and coupled to the fine phase shifters 509, 511.

[0040] The various components of the tilt adapter 605 may be constructed of aluminum, or any material suitable to withstand the normal operating conditions of the diplexed antenna 500 without deviating from the inventive concept, such as other metals or polymeric materials.

[0041] FIG. 8 is a perspective view of the frontside (e.g. opposite the backside) of the diplexed antenna 500 with a radome removed. The diplexed antenna 500 may include radiating elements 502, 504, 506, 508 which may be first and/or second band radiating elements mounted to one of the feed boards 702. Fine phase shifters 509, 511 may be integrated into one of the feed boards 702. The second level rack 637 may be connected to an elongated bar 704, which may couple each of the fine phase shifters 509, 511 to a wiper connecting bar 706, opposing ends of which may be connected to respective wiper arms 708 (as shown in FIG. 9) of the fine phase shifters 509, 511 (an example of one of the phase shifters 509 or 511 of which is shown in FIG. 9). As such, lateral movement of the second level rack 637 may cause lateral movement of the elongated bar 704. Such lateral movement of the elongated bar 704 may cause movement of one or more of the wiper connecting bars 706 resulting in movement of respective wiper arms 708 causing the fine level phase shift to effect the desired level of tilt.

[0042] In operation, in accordance with the input of the desired tilt value α , the connecting member 607 may move laterally, causing the first coarse phase shifter 501 to provide a first contribution on a first tilt associated with the first

frequency band. In accordance with the input of the desired tilt value β the connecting member 609 may move laterally, causing the second coarse phase shifter 503 to provide a second contribution on a second tilt associated with a second frequency band.

[0043] Lateral movement of the connecting members 607, 609 may cause movement of the respective first and second level rods 611, 613. Movement of the first and/or second level rods 611, 613 may cause movement of the first level rack 619, which, via the first pinion gear 631, shaft 635, and second pinion gear 633, may cause lateral movement of the second level rack 637. Lateral movement of the second level rack 637 may cause the first and second fine phase shifters 509, 511 to provide a phase shift based on a combination of the set tilt values α and β of the respective coarse phase shifters 501, 503.

[0044] It should be noted that the different antenna types may include a different number of radiating elements, which may result in different radiating element spacings and phase shifter arc radii. As such, the coarse phase shifters and fine phase shifters may be affected differently by such variations. For example, antennas of longer lengths may include a greater number of radiating elements, which may increase the distance between some phase shifter outputs measured in element spacings, while antennas of shorter lengths may include fewer radiating elements, which may result in a reduction of the distance between some phase shifter outputs. As discussed above, a phase shift value of a phase shifter may be proportional to the distance between each of the outputs of the phase shifter. For example, the coarse phase shifters' shift values may depend on the total number of radiating elements in the diplexed antenna, and, as such, the coarse phase shift values may be increased or decreased based on a length of the diplexed antenna. The phase shift values output from the fine phase shifters, however, may not be similarly affected. For example, to account for a greater number of radiating elements, diplexed antenna may employ additional feedboards including additional fine phase shifters to drive the same. As such, the distance between the outputs of each of the fine phase shifters may not change, or may not change in the same fashion as the outputs of the coarse phase shifters.

[0045] Because the coarse phase shifters and fine phase shifters are affected differently by the diplexed antenna types in which they are implemented, one or more components of the tilt adapter to which they are coupled may also need to be modified. To effect a proper coarse and fine phase shifting for different antenna types, the gear ratio may be adjusted to produce the desired movement of the second level rack 637 relative to the first level rack 619. For example, the diameter of the first pinion gear 631 and/or the second pinion gear 633 may be increased or decreased to account for different antenna types, such as other antenna types and arrangements discussed in U.S. patent application Ser. No. 14/812,339. For example, a diameter of the first pinion gear 631 may be increased, which, in turn, may increase the number of teeth along the circumference of the first pinion gear 631. This modification may result in an increased gear ratio. Alternatively, a diameter of the first pinion gear 631 may be decreased, which, in turn, may decrease the number of teeth along the circumference of the first pinion gear 631. This modification may result in a decreased gear ratio.

[0046] As used herein, "input", "output", and some other terms or phrases refer to the transmit signal path. However, because the structures described herein may be passive components, the networks and components also perform reciprocal operations in the receive signal path. Therefore, the use of "input", "output", and some other terms is for clarity only, and is not meant to imply that the diplexed antennas do not operate concurrently in both receive and transmit directions.

[0047] Various aspects of the present disclosure have now been discussed in detail; however, the invention should not be understood as being limited to these specific aspects. It should also be appreciated that various modifications, adaptations, and alternative embodiments thereof may be made within the scope of the present invention.

Claims

1. An antenna, comprising:

a first coarse phase shifter (301, 501) configured to receive a radio frequency (RF) signal of a first frequency band;
 a second coarse phase shifter (303, 503) configured to receive a RF signal of a second frequency band;
 first and second diplexers (305, 307) each configured to combine a varied phase signal output by the first coarse phase shifter (301, 501) with a varied phase signal output by the second coarse phase shifter (303, 503);
 a first fine phase shifter (309, 509) comprising an input coupled to an output of the first diplexer;
 a second fine phase shifter (311, 509) comprising an input coupled to an output of the second diplexer;
 a plurality of radiating elements (313, 315, 502, 506) comprising at least one first radiating element coupled to a respective output of the first fine phase shifter (309, 509) and at least one second radiating element coupled to a respective output of the second fine phase shifter (311, 509); and
 a tilt adapter (605), which is coupled to the both the first and second coarse phase shifters (301, 501, 303, 503) as well as the first and second fine phase shifters (309, 509, 311, 509), and which is configured to adjust the first fine phase shifter (309, 509) based on adjustments made to the first and second coarse phase shifters

(301, 501, 303, 503) and further configured to adjust the second fine phase shifter (311, 509) based on adjustments made to the first and second coarse phase shifters (301, 501, 303, 503), wherein the first and second coarse phase shifters (301, 501, 303, 503) are independently adjustable.

- 5 **2.** The antenna of claim 1, wherein the tilt adapter (605) comprises a cross linkage member (621) that moves in response to movement of a first member (611) and in response to movement of a second member (613).
- 10 **3.** The antenna of claim 2, wherein a first adjustable element (708) of the first fine phase shifter (309, 509) and a second adjustable element (708) of the second fine phase shifter (311, 509) are operatively coupled to the cross linkage member (621) so that movement of the cross linkage member (621) is configured to move the first and second adjustable elements (708).
- 15 **4.** The antenna of claim 3, wherein the cross linkage member (621) is coupled to the first and second adjustable elements (708) via a first rack (619) that is connected to the cross linkage member (621) and that is configured to move in response to movement of the cross linkage member (621), a first gear (631) that engages the first rack (619), a second gear (633) that moves in response to movement of the first gear (631), and a second rack (637) that engages the second gear (633).
- 20 **5.** The antenna of claim 4, wherein a gear ratio between the first and second gears is selected to produce a desired amount of movement of the second rack (631) relative to the first rack (637).
- 25 **6.** The antenna of any of claims 2-5, wherein the cross linkage member (621) is configured to rotate in response to movement of the first member (611) and is configured to rotate in response to movement of the second member (613).
- 30 **7.** The antenna of claim 6, wherein rotational movement of the cross linkage member (621) is configured to result in lateral movement of a first moveable member (619) that is connected to the cross linkage member (621).
- 35 **8.** The antenna of any of claims 1-7, wherein a phase shift applied by the first coarse phase shifter (301, 501) exceeds a phase shift applied by the first fine phase shifter (309, 509), and wherein a phase shift applied by the second coarse phase shifter (303, 503) exceeds a phase shift applied by the second fine phase shifter (311, 509).
- 40 **9.** The antenna of any of claims 1-8, wherein the first coarse phase shifter (301, 501) applies first phase shifts to signals output therefrom and the second coarse phase shifter (303, 503) applies second phase shifts to signals output therefrom, the first phase shifts being different from the second phase shifts, and wherein the first fine phase shifter (309, 509) applies third phase shifts to signals output therefrom and the second fine phase shifter (303, 503) applies fourth phase shifts to signals output therefrom, the third phase shifts being the same as the fourth phase shifts.
- 45 **10.** The antenna of any of claims 2-9, wherein the first member comprises a first rod (611) having a first pin (627) and the second member (613) comprises a second rod (613) having a second pin (629), and wherein the cross linkage member (621) includes a first slot (623) that receives the first pin (627) and a second slot (625) that receives the second pin.
- 50 **11.** The antenna of claim 1, the tilt adapter (605) comprising:
a first member (611) coupled to the first coarse phase shifter (301, 501);
a second member (613) coupled to the second coarse phase shifter (303, 503);
a cross linkage member (621) operatively engaged to both the first and second members (611, 613);
a first moveable member (619) coupled to the cross linkage member (621) and configured to move in response to movement of the cross linkage member (621);
a second moveable member (637) coupled to the first fine phase shifter (309, 509), wherein lateral movement of the first member (611) or the second member (613) is configured to cause movement of the second moveable member (637).
- 55 **12.** The antenna of claim 11, wherein the first moveable member (619) moves a distance that is a predetermined fraction of a distance moved by the first or second members (611, 613).
- 60 **13.** The antenna of claim 1, the tilt adapter comprising:

a first rod (611) coupled to the first coarse phase shifter (301, 501);
a second rod (613) coupled to the second coarse phase shifter (303, 503);
a cross linkage member (621) operatively engaged to both the first and
second rods (611, 613);
a first rack (619) coupled to the cross linkage member (621);
a second rack (637) coupled to the first rack (619), the first fine phase shifter (309, 509), and the second fine
phase shifter (311, 509), wherein lateral movement of the first rod or the second rod (611, 613) causes lateral
movement of the second rack (637).

Patentansprüche

1. Antenne, aufweisend:

einen ersten Grobphasenschieber (301, 501), der zum Empfangen eines Hochfrequenz(HF)-Signals eines
ersten Frequenzbandes konfiguriert ist;
einen zweiten Grobphasenschieber (303, 503), der zum Empfangen eines Hochfrequenz(HF)-Signals eines
zweiten Frequenzbandes konfiguriert ist;
erste und zweite Diplexer (305, 307), die jeweils konfiguriert sind, um ein variiertes Phasensignal, das von dem
ersten Grobphasenschieber (301, 501) ausgegeben wird, mit einem variierten Phasensignal, das von dem
zweiten Grobphasenschieber (303, 503) ausgegeben wird, zu kombinieren;
einen ersten Feinphasenschieber (309, 509) mit einem Eingang, der mit einem Ausgang des ersten Diplexers
gekoppelt ist;
einen zweiten Feinphasenschieber (311, 509) mit einem Eingang, der mit einem Ausgang des zweiten Diplexers
gekoppelt ist;
eine Vielzahl abstrahlender Elemente (313, 315, 502, 506), umfassend mindestens ein abstrahlendes Element,
das mit einem entsprechenden Ausgang des ersten Feinphasenschiebers (309, 509) gekoppelt ist, und min-
destens ein zweites abstrahlendes Element, das mit einem entsprechenden Ausgang des zweiten Feinpha-
senschiebers (311, 509) gekoppelt ist; und
einen Neigungsadapter (605), der sowohl mit dem ersten und zweiten Grobphasenschieber (301, 501, 303,
503) als auch mit dem ersten und zweiten Feinphasenschieber (309, 509, 311, 509) gekoppelt ist, und der dazu
ausgebildet ist, den ersten Feinphasenschieber (309, 509) basierend auf den an den ersten und zweiten Grob-
phasenschiebern (301, 501, 303, 503) vorgenommenen Korrekturen anzupassen, und ferner dazu ausgebildet
ist, den zweiten Feinphasenschieber (311, 509) basierend auf den an den ersten und zweiten Grobphasen-
schiebern (301, 501, 303, 503) vorgenommenen Korrekturen anzupassen,
wobei der erste und der zweite Grobphasenschieber (301, 501, 303, 503) unabhängig voneinander einstellbar ist.

2. Antenne nach Anspruch 1, wobei der Neigungsadapter (605) ein Querverbindungselement (621), das sich als
Reaktion auf die Bewegung eines ersten Elements (611) und als Reaktion auf die Bewegung eines zweiten Elements
(613) bewegt, umfasst.

3. Antenne nach Anspruch 2, wobei ein erstes einstellbares Element (708) des ersten Feinphasenschiebers (309,
509) und ein zweites einstellbares Element (708) des zweiten Feinphasenschiebers (311, 509) funktionsfähig mit
dem Querverbindungselement (621) gekoppelt ist, so dass eine Bewegung des Querverbindungselements (621)
zum Bewegen des ersten und zweiten einstellbaren Elements (708) ausgelegt ist.

4. Antenne nach Anspruch 3, wobei das Querverbindungselement (621) mit den ersten und zweiten einstellbaren
Elementen (708) über eine erste Zahnstange (619), die mit dem Querverbindungselement (621) verbunden ist,
gekoppelt ist, und dazu ausgebildet ist, um als Reaktion auf die Bewegung des Querverbindungselements (621)
ein erstes Zahnrad (631) zu bewegen, das in die erste Zahnstange (619) eingreift, und über eine zweite Zahnstange
(637), die in das zweite Zahnrad (633) eingreift.

5. Antenne nach Anspruch 4, wobei ein Übersetzungsverhältnis zwischen dem ersten und dem zweiten Zahnrad
ausgewählt wird, um eine gewünschte Bewegungsgröße der zweiten Zahnstange (631) relativ zur ersten Zahnstange
(637) zu erzeugen.

6. Antenne nach einem der Ansprüche 2-5, wobei das Querverbindungselement (621) dazu ausgebildet ist, sich als
Reaktion auf die Bewegung des ersten Elements (611) zu drehen und dazu ausgebildet ist, sich als Reaktion auf

die Bewegung des zweiten Elements (613) zu drehen.

7. Antenne nach Anspruch 6, wobei die Drehbewegung des Querverbindungselements (621) dazu ausgebildet ist, eine seitliche Bewegung eines ersten beweglichen Elements (619) zu bewirken, das mit dem Querverbindungselement (621) verbunden ist.

8. Antenne nach einem der Ansprüche 1-7, wobei eine durch den ersten Grobphasenschieber (301, 501) beaufschlagte Phasenverschiebung größer ist als eine durch den ersten Feinphasenschieber (309, 509) beaufschlagte Phasenverschiebung, und wobei eine durch den zweiten Grobphasenschieber (303, 503) beaufschlagte Phasenverschiebung größer ist als eine durch den zweiten Feinphasenschieber (311, 509) beaufschlagte Phasenverschiebung.

9. Antenne nach einem der Ansprüche 1-8, wobei der erste Grobphasenschieber (301, 501) erste Phasenverschiebungen auf die von ihm ausgegebenen Signale beaufschlagt und der zweite Grobphasenschieber (303, 503) zweite Phasenverschiebungen auf die von ihm ausgegebenen Signale beaufschlagt, wobei sich die ersten Phasenverschiebungen von den zweiten Phasenverschiebungen unterscheiden, und wobei der erste Feinphasenschieber (309, 509) dritte Phasenverschiebungen auf die von ihm ausgegebenen Signale beaufschlagt und der zweite Feinphasenschieber (303, 503) vierte Phasenverschiebungen auf die von ihm ausgegebenen Signale beaufschlagt, wobei die dritten Phasenverschiebungen die gleichen wie die vierten Phasenverschiebungen sind.

10. Antenne nach einem der Ansprüche 2-9, wobei das erste Element eine erste Stange (611) mit einem ersten Stift (627) und das zweite Element (613) eine zweite Stange (613) mit einem zweiten Stift (629) umfasst, und wobei das Querverbindungselement (621) einen ersten Schlitz (623), der den ersten Stift (627) aufnimmt, und einen zweiten Schlitz (625) umfasst, der den zweiten Stift aufnimmt.

11. Antenne nach Anspruch 1, wobei der Neigungsadapter (605) aufweist:

ein erstes Element (611), das mit dem ersten Grobphasenschieber (301, 501) gekoppelt ist;
ein zweites Element (613), das mit dem zweiten Grobphasenschieber (303, 503) gekoppelt ist;
ein Querverbindungselement (621), das funktionsfähig mit dem ersten und zweiten Element (611, 613) verbunden ist;
ein erstes bewegliches Element (619), das mit dem Querverbindungselement (621) gekoppelt und dazu ausgebildet ist, sich als Reaktion auf die Bewegung des Querverbindungselements (621) zu bewegen;
ein zweites bewegliches Element (637), das mit dem ersten Feinphasenschieber (309, 509) gekoppelt ist, wobei eine Seitwärtsbewegung des ersten Elements (611) oder des zweiten Elements (613) derart ausgelegt ist, dass eine Bewegung des zweiten beweglichen Elements (637) bewirkt wird.

12. Antenne nach Anspruch 11, wobei das erste bewegliche Element (619) eine Strecke zurücklegt, die ein vorbestimmter Bruchteil einer Strecke ist, die vom ersten oder zweiten Elementen (611, 613) zurückgelegt wird.

13. Antenne nach Anspruch 1, wobei der Neigungswinkel aufweist:

eine erste Stange (611), die mit dem ersten Grobphasenschieber (301, 501) gekoppelt ist;
eine zweite Stange (613), die mit dem zweiten Grobphasenschieber (303, 503) gekoppelt ist;
ein Querverbindungselement (621), das operativ mit der ersten als auch mit der zweiten Stange (611, 613) verbunden ist;
eine erste Zahnstange (619), die mit dem Querverbindungselement (621) gekoppelt ist;
eine zweite Zahnstange (637), die mit der ersten Zahnstange (619), dem ersten Feinphasenschieber (309, 509), und dem zweiten Feinphasenschieber (311, 509) verbunden ist, wobei eine seitliche Bewegung der ersten oder der zweiten Stange (611, 613) eine Seitwärtsbewegung der zweiten Zahnstange (637) bewirkt.

Revendications

1. Antenne, comprenant :

un premier déphaseur grossier (301, 501) configuré pour recevoir un signal radiofréquence (RF) d'une première bande de fréquences ;
un deuxième déphaseur grossier (303, 503) configuré pour recevoir un signal RF d'une deuxième bande de

fréquences ;

des premier et deuxième diplexeurs (305, 307) configurés chacun pour combiner un signal à phase variée délivré par le premier déphaseur grossier (301, 501) avec un signal à phase variée délivré par le deuxième déphaseur grossier (303, 503) ;

un premier déphaseur fin (309, 509) comprenant une entrée couplée à une sortie du premier diplexeur ;

un deuxième déphaseur fin (311, 509) comprenant une entrée couplée à une sortie du deuxième diplexeur ;

une pluralité d'éléments rayonnants (313, 315, 502, 506) comprenant au moins un premier élément rayonnant couplé à une sortie respective du premier déphaseur fin (309, 509) et au moins un deuxième élément rayonnant couplé à une sortie respective du deuxième déphaseur fin (311, 509) ; et

un adaptateur d'inclinaison (605) qui est couplé aux premier et deuxième déphaseurs grossiers (301, 501, 303, 503) ainsi qu'aux premier et

deuxième déphaseurs fins (309, 509, 311, 509) et qui est configuré pour régler le premier déphaseur fin (309, 509) sur la base de réglages effectués sur les premier et deuxième déphaseurs grossiers (301, 501, 303, 503) et configuré en outre pour régler le deuxième déphaseur fin (311, 509) sur la base de réglages effectués sur

les premier et deuxième déphaseurs grossiers (301, 501, 303, 503),

dans laquelle les premier et deuxième déphaseurs grossiers (301, 501, 303, 503) sont réglables indépendamment.

2. Antenne selon la revendication 1, dans laquelle l'adaptateur d'inclinaison (605) comprend un élément de liaison transversale (621) qui se déplace en réponse à un mouvement d'un premier élément (611) et en réponse à un mouvement d'un deuxième élément (613).

3. Antenne selon la revendication 2, dans laquelle un premier élément réglable (708) du premier déphaseur fin (309, 509) et un deuxième élément réglable (708) du deuxième déphaseur fin (311, 509) sont couplés fonctionnellement à l'élément de liaison transversale (621) de sorte que le mouvement de l'élément de liaison transversale (621) est configuré pour déplacer les premier et deuxième éléments réglables (708).

4. Antenne selon la revendication 3, dans laquelle l'élément de liaison transversale (621) est couplé aux premier et deuxième éléments réglables (708) par l'intermédiaire d'une première crémaillère (619) qui est reliée à l'élément de liaison transversale (621) et qui est configurée pour se déplacer en réponse à un mouvement de l'élément de liaison transversale (621), d'une première roue dentée (631) qui vient en prise avec la première crémaillère (619), d'une deuxième roue dentée (633) qui se déplace en réponse à un mouvement de la première roue dentée (631) et d'une deuxième crémaillère (637) qui vient en prise avec la deuxième roue dentée (633).

5. Antenne selon la revendication 4, dans laquelle un rapport de démultiplication entre les première et deuxième roues dentées est sélectionné pour produire une quantité souhaitée de mouvement de la deuxième crémaillère (637) par rapport à la première crémaillère (619).

6. Antenne selon l'une quelconque des revendications 2 à 5, dans laquelle l'élément de liaison transversale (621) est configuré pour tourner en réponse à un mouvement du premier élément (611) et est configuré pour tourner en réponse à un mouvement du deuxième élément (613).

7. Antenne selon la revendication 6, dans laquelle un mouvement de rotation de l'élément de liaison transversale (621) est configuré pour provoquer un mouvement latéral d'un premier élément mobile (619) qui est relié à l'élément de liaison transversale (621).

8. Antenne selon l'une quelconque des revendications 1 à 7, dans laquelle un déphasage appliqué par le premier déphaseur grossier (301, 501) dépasse un déphasage appliqué par le premier déphaseur fin (309, 509) et dans laquelle un déphasage appliqué par le deuxième déphaseur grossier (303, 503) dépasse un déphasage appliqué par le deuxième déphaseur fin (311, 509).

9. Antenne selon l'une quelconque des revendications 1 à 8, dans laquelle le premier déphaseur grossier (301, 501) applique des premiers déphasages à ses signaux de sortie et le deuxième déphaseur grossier (303, 503) applique des deuxième déphasages à ses signaux de sortie, les premiers déphasages étant différents des deuxième déphasages, et dans laquelle le premier déphaseur fin (309, 509) applique des troisième déphasages à ses signaux de sortie et le deuxième déphaseur fin (303, 503) applique des quatrième déphasages à ses signaux de sortie, les troisième déphasages étant les mêmes que les quatrième déphasages.

10. Antenne selon l'une quelconque des revendications 2 à 9, dans laquelle le premier élément comprend une première barre (611) ayant une première broche (627) et le deuxième élément (613) comprend une deuxième barre (613) ayant une deuxième broche (629), et dans laquelle l'élément de liaison transversale (621) inclut une première fente (623) qui reçoit la première broche (627) et une deuxième fente (625) qui reçoit la deuxième broche.

11. Antenne selon la revendication 1, dans laquelle l'adaptateur d'inclinaison (605) comprend :

un premier élément (611) couplé au premier déphaseur grossier (301, 501) ;
un deuxième élément (613) couplé au deuxième déphaseur grossier (303, 503) ;
un élément de liaison transversale (621) en prise fonctionnelle avec les premier et deuxième éléments (611, 613) ;
un premier élément mobile (619) couplé à l'élément de liaison transversale (621) et configuré pour se déplacer en réponse à un mouvement de l'élément de liaison transversale (621) ;
un deuxième élément mobile (637) couplé au premier déphaseur fin (309, 509), un mouvement latéral du premier élément (611) ou du deuxième élément (613) étant configuré pour provoquer un mouvement du deuxième élément mobile (637).

12. Antenne selon la revendication 11, dans laquelle le premier élément mobile (619) parcourt une distance qui est une fraction prédéterminée d'une distance parcourue par les premier ou deuxième éléments (611, 613).

13. Antenne selon la revendication 1, dans laquelle l'adaptateur d'inclinaison comprend :

une première barre (611) couplée au premier déphaseur grossier (301, 501) ;
une deuxième barre (613) couplée au deuxième déphaseur grossier (303, 503) ;
un élément de liaison transversale (621) en prise fonctionnelle avec les première et deuxième barres (611, 613) ;
une première crémaillère (619) couplée à l'élément de liaison transversale (621) ;
une deuxième crémaillère (637) couplée à la première crémaillère (619), au premier déphaseur fin (309, 509) et au deuxième déphaseur fin (311, 509), un mouvement latéral de la première barre ou de la deuxième barre (611, 613) provoquant un mouvement latéral de la deuxième crémaillère (637).

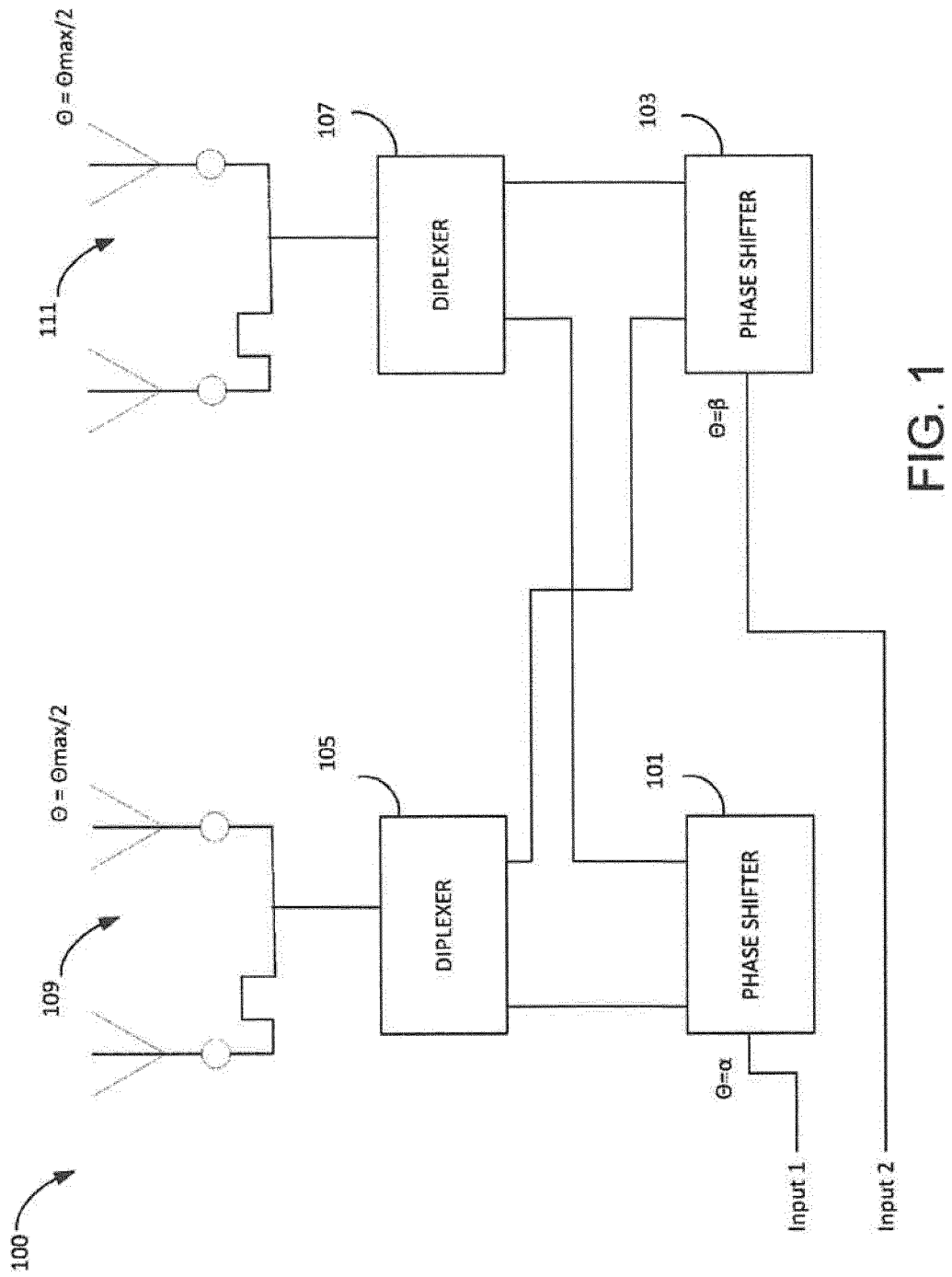


FIG. 1

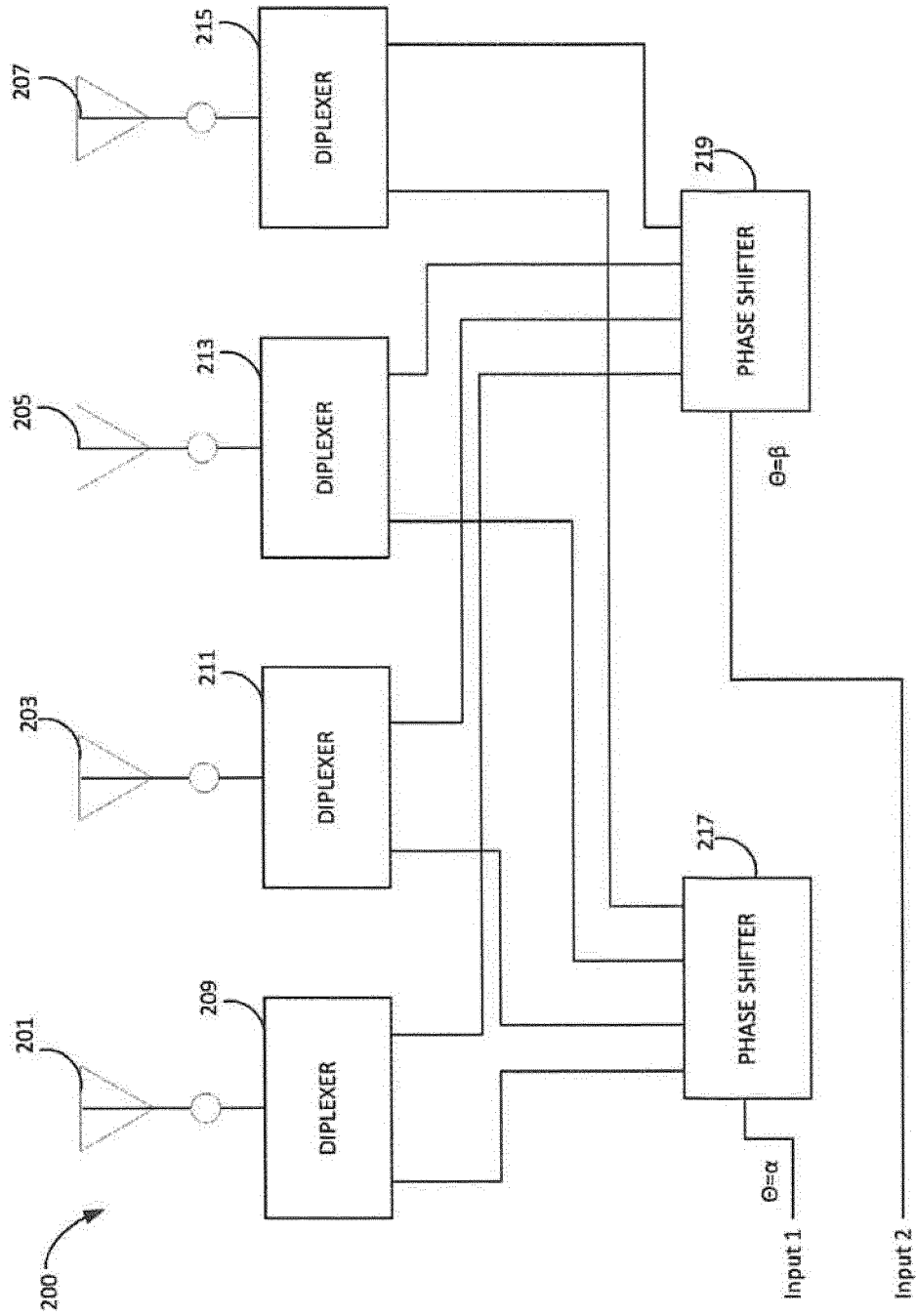


FIG. 2

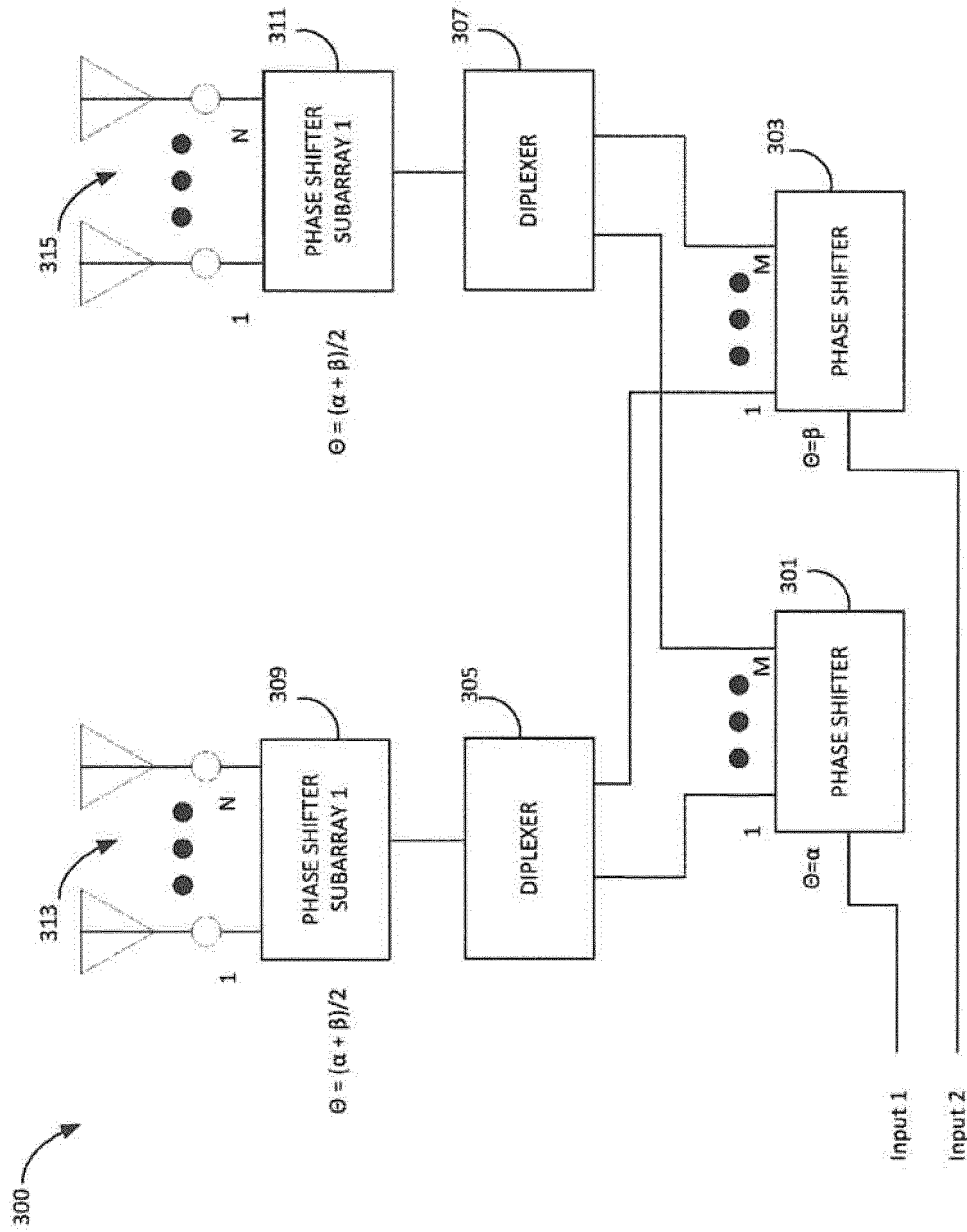


FIG. 3

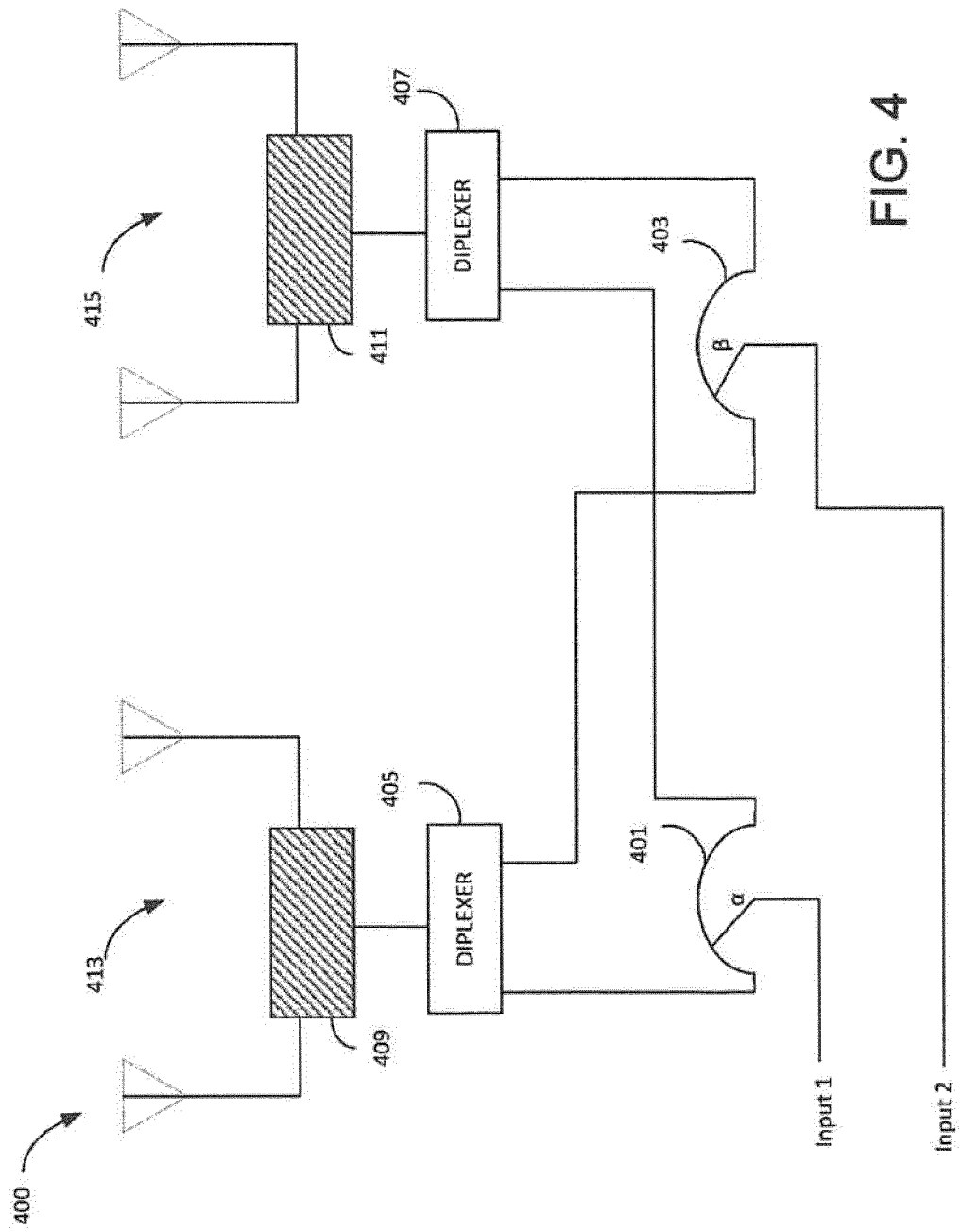


FIG. 4

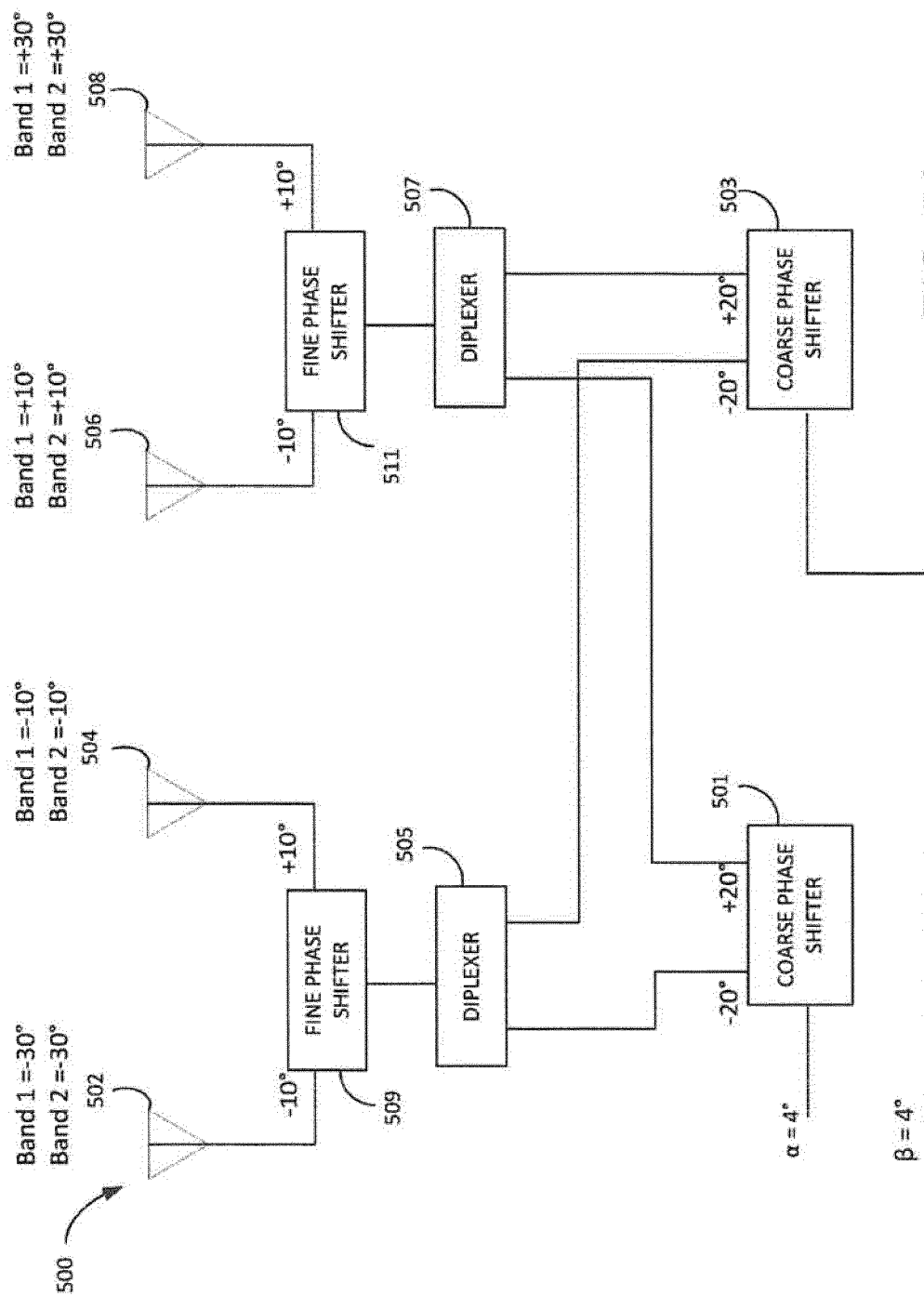


FIG. 5A

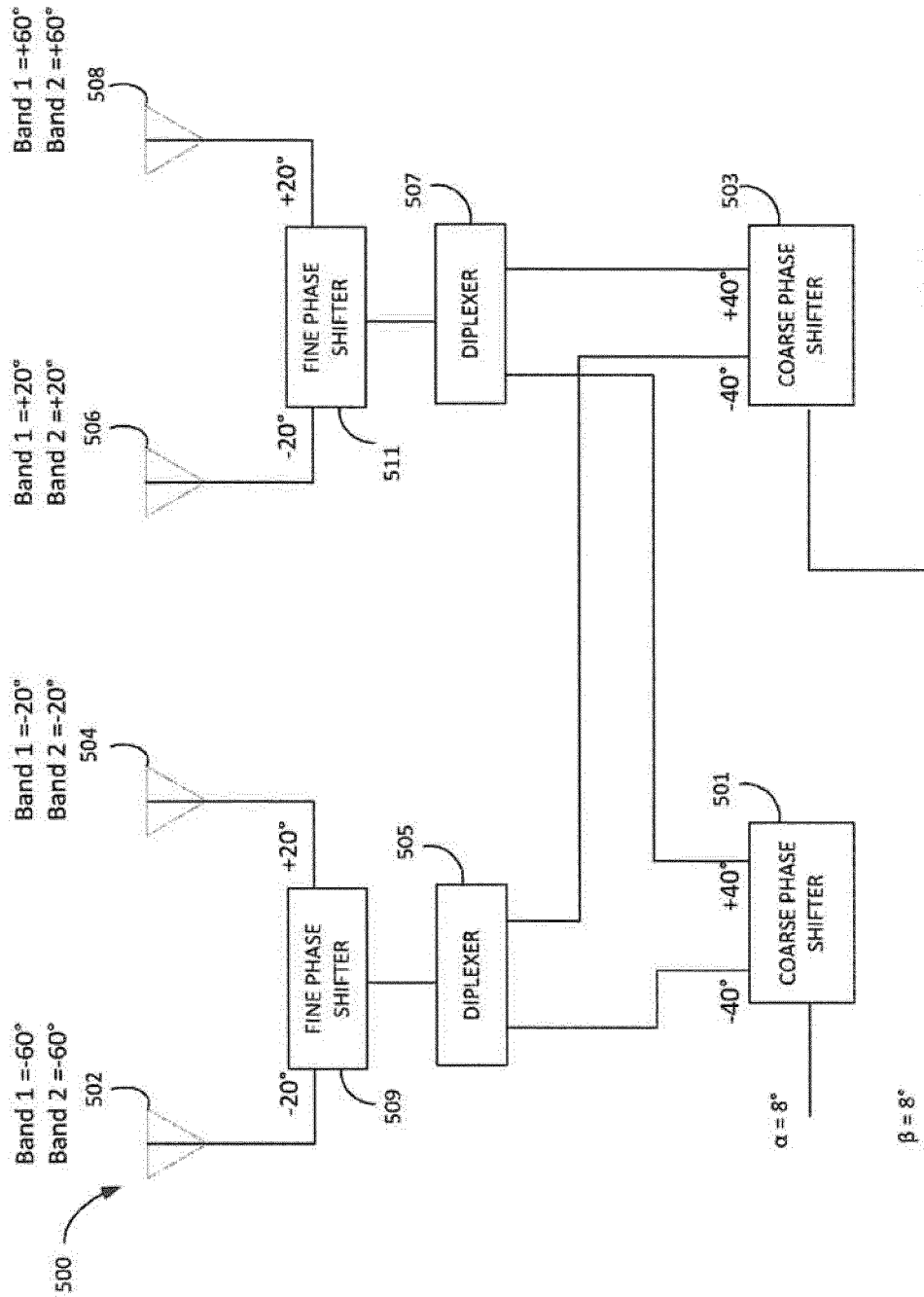


FIG. 5B

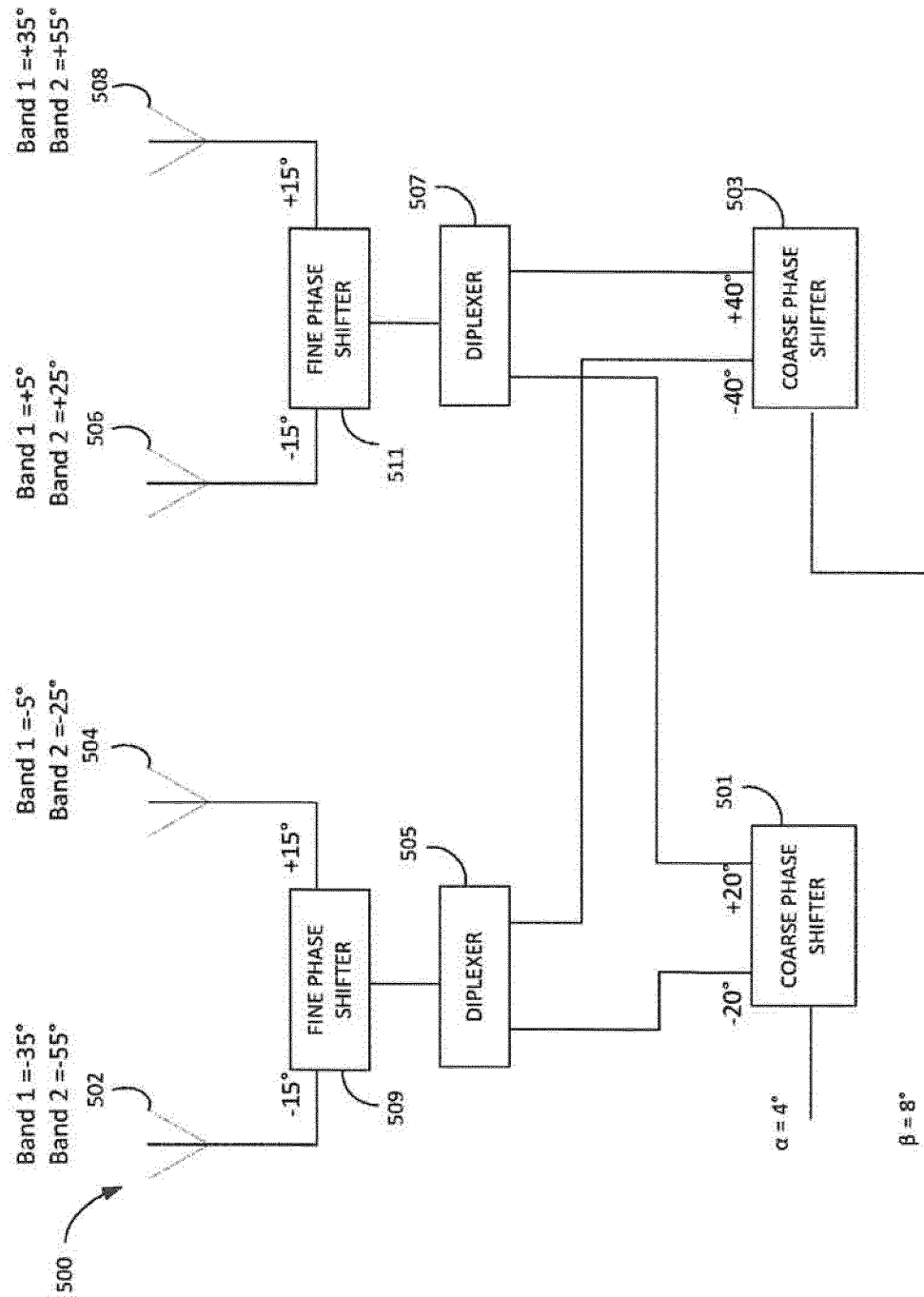
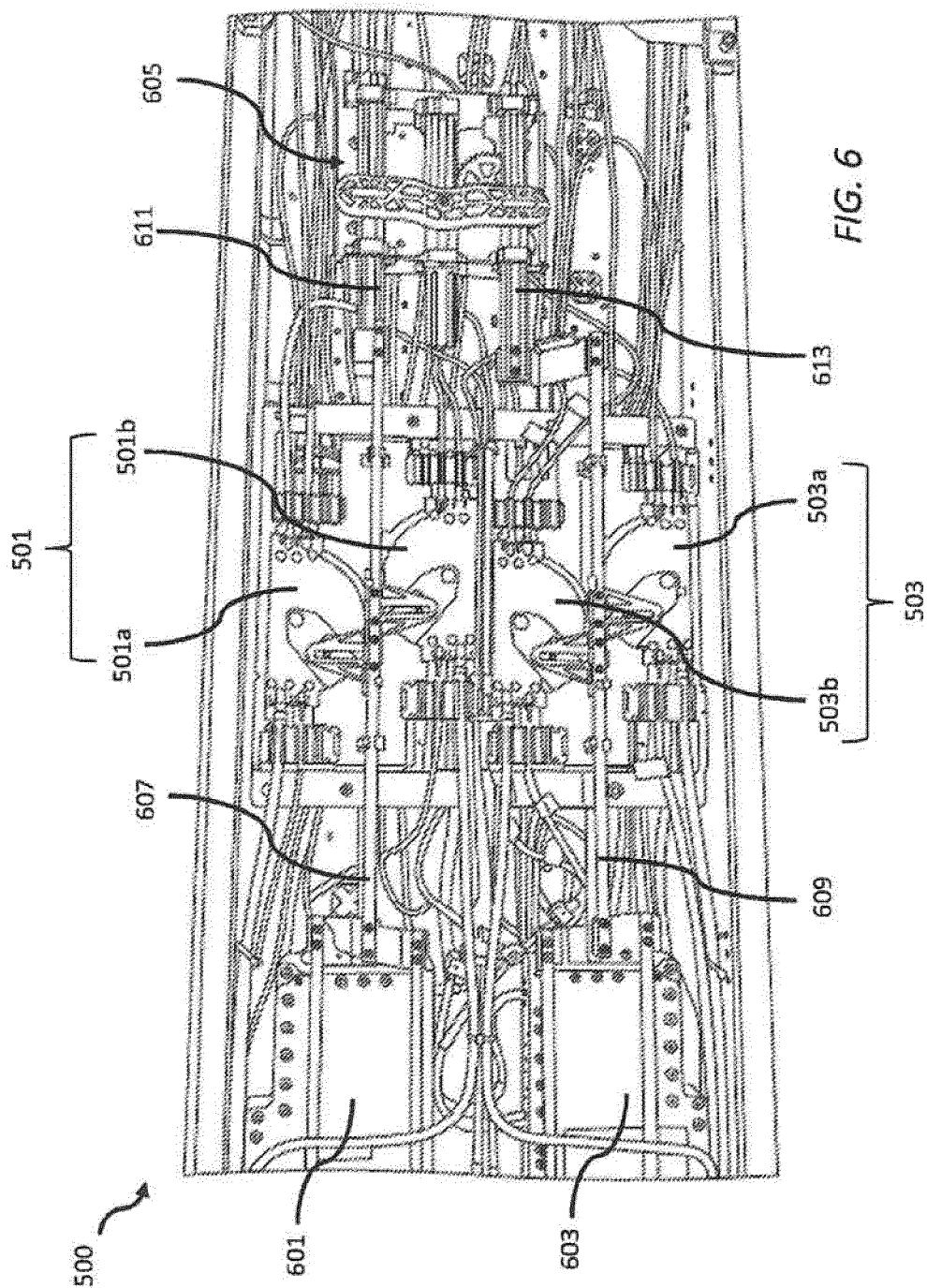


FIG. 5C



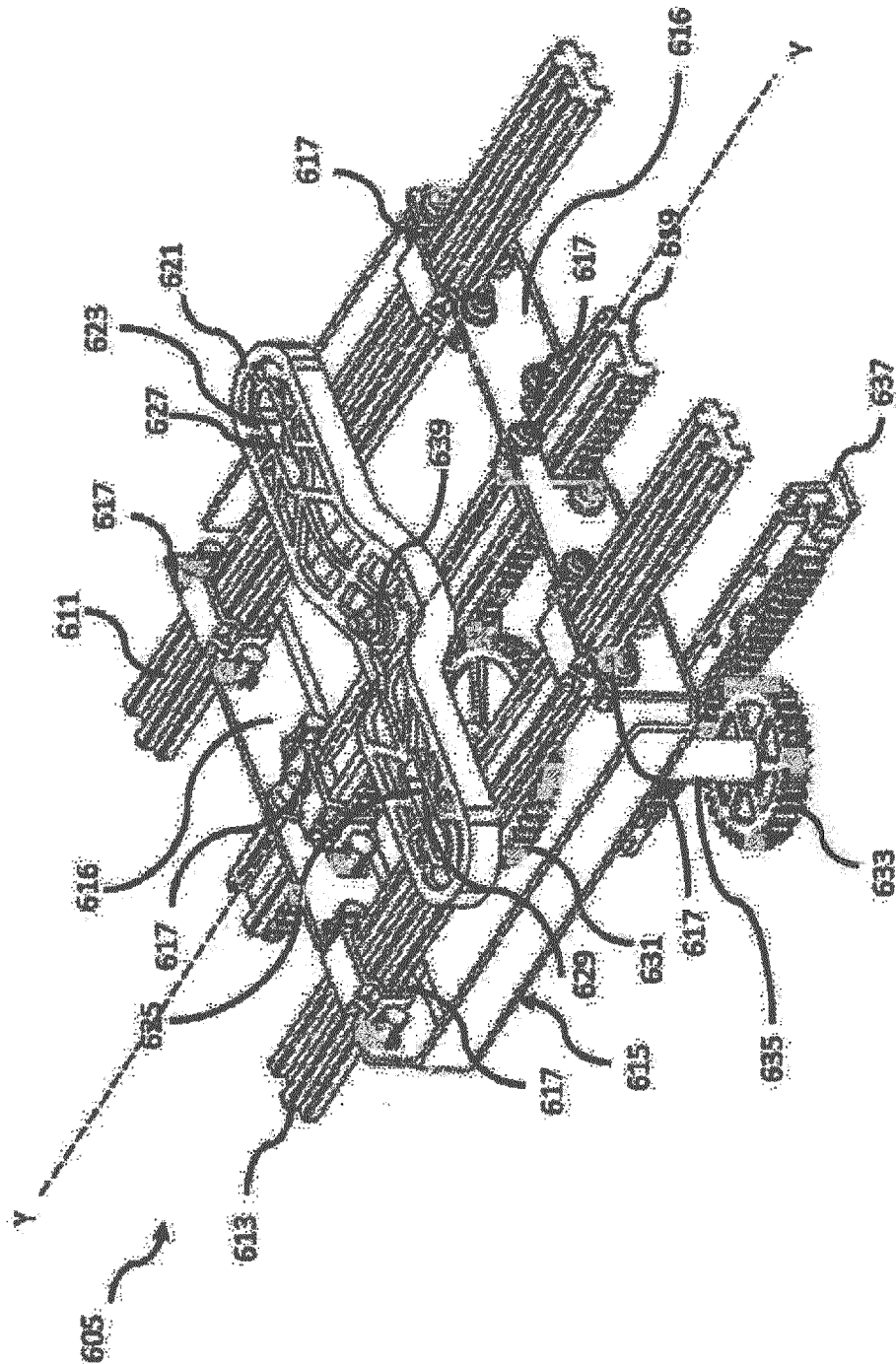


FIG. 7

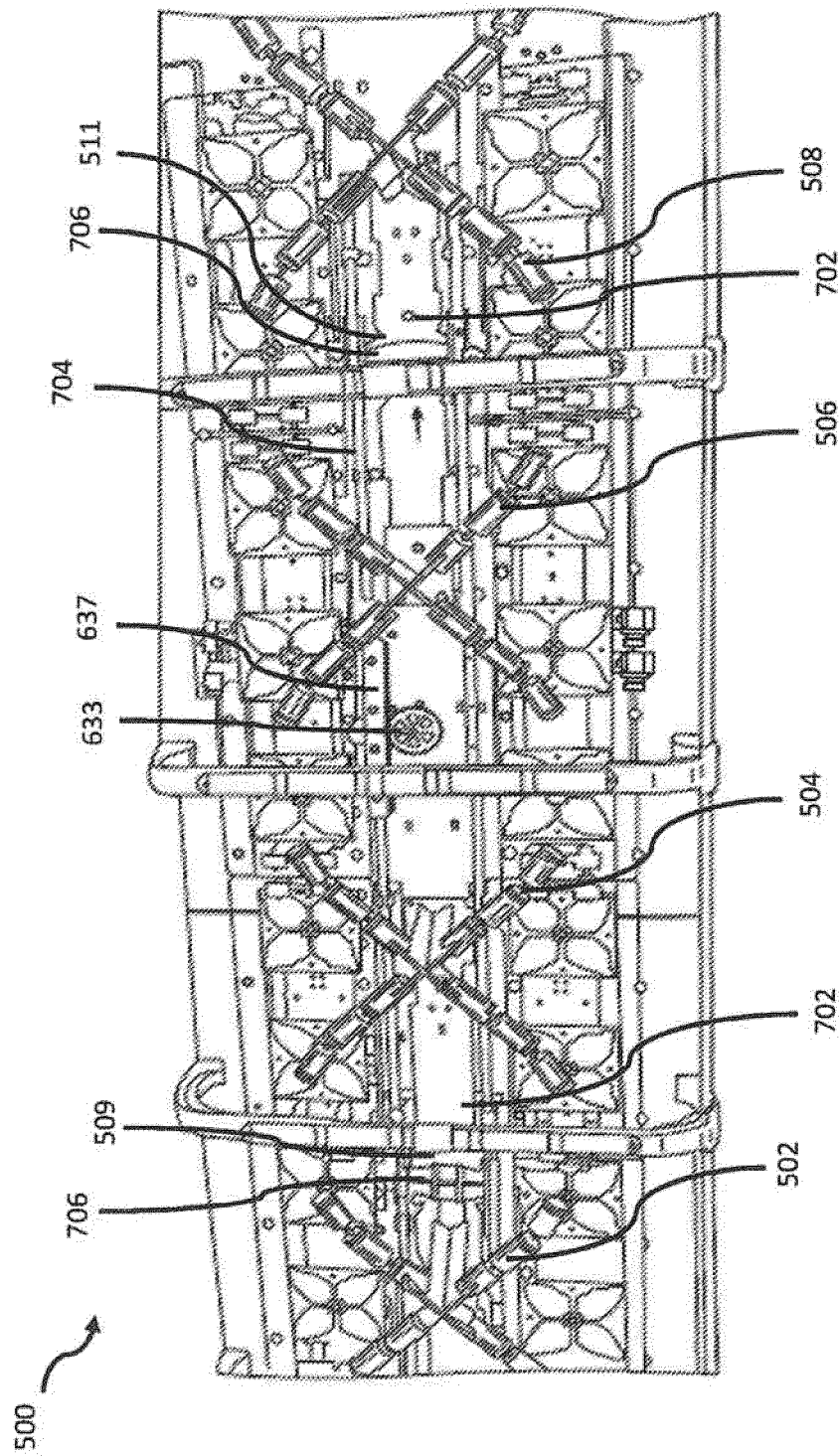


FIG. 8

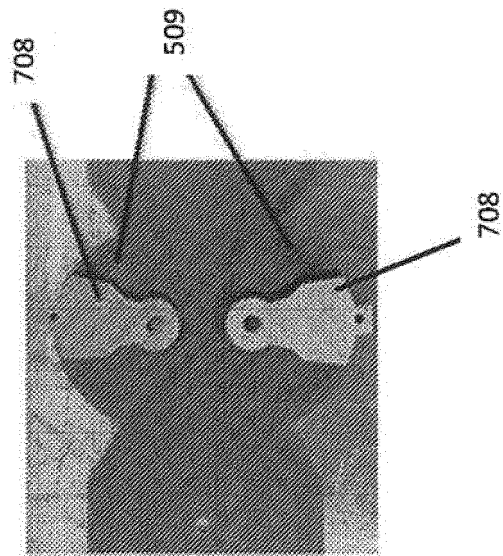


FIG. 9

REFERENCES CITED IN THE DESCRIPTION

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