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(54) **VARIABLE CAPACITY PISTON PUMP**

KOLBENPUMPE MIT VARIABLER KAPAZITÄT

POMPE À PISTON À CAPACITÉ VARIABLE

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(56) References cited:

EP-A2- 0 922 858

JP-A- H0 518 350

JP-A- H04 272 482

JP-A- 2005 201 175

JP-U- H 036 073

JP-U- S63 121 781

JP-U- S63 121 781

US-A- 3 489 094

US-A- 3 753 627

US-A1- 2006 123 984

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EP 3 171 022 B1

Description

Technical Field

[0001] The present invention relates to a variable capacity piston pump.

Background Art

[0002] As a variable capacity piston pump in the related art, for example, as described in Patent Literature 1 (Japanese Unexamined Patent Publication No. 2006-348911), a variable capacity piston pump which is used as a hydraulic pressure generation source of a hydraulic circuit and changes a discharge capacity by adjusting the inclination of a swashplate is known. The variable capacity piston pump described in Patent Literature 1 includes a control piston which presses the swashplate and a swashplate return spring which biases the swashplate from a side opposite to the control piston. As the control pressure of the control piston is changed, the magnitude of a pressing force exerted on the swashplate is changed. By controlling the magnitude of the pressing force, the inclination of the swashplate is adjusted. Specifically, when the pressing force of the control piston is decreased, the inclination of the swashplate is increased by the biasing force of the swashplate return spring. When the pressing force of the control piston is increased, the inclination of the swashplate is decreased. When the inclination is changed, the swashplate turns about a certain turning center.

[0003] JP S63 121781 U discloses a variable capacity piston pump in accordance with the preamble of claim 1. US 2006/123984 A1 discloses a longitudinally adjustable reversible axial piston machine.

Summary of Invention

Technical Problem

[0004] The inventors found that when the inclination of the swashplate is changed, the distance between the pressing force of the control piston and the turning center (that is, the length of a moment arm of the pressing force of the control piston about the turning center) is changed, resulting in deterioration in controllability over the inclination of the swashplate.

[0005] For example, when the control piston presses the swashplate to decrease the inclination of the swashplate, in a case where the length of the moment arm is shortened as the inclination of the swashplate is decreased, the moment of the pressing force of the control piston about the turning center is decreased, and it becomes difficult for the swashplate to rotate. In this case, the responsiveness of the inclination of the swashplate to the pressing force of the control piston deteriorates (for example, the response speed becomes slow), and inappropriate control over the inclination of the swash-

plate may be incurred.

[0006] In contrast, when the control piston presses the swashplate to decrease the inclination of the swashplate, in a case where the length of the moment arm is lengthened as the inclination of the swashplate is decreased, the moment of the pressing force of the control piston about the turning center is increased, and the swashplate more easily rotates. In this case, the response of the inclination of the swashplate to the pressing force of the control piston becomes excessively sensitive (for example, the response speed becomes excessively fast), and inappropriate control over the inclination of the swashplate may be incurred.

[0007] An object of various aspects of the present invention is to provide a variable capacity piston pump which achieves an improvement in controllability over the inclination of a swashplate.

Solution to Problem

[0008] This object is solved by a variable capacity piston pump in accordance with claim 1. According to an aspect of the present invention, there is provided a variable capacity piston pump performing suction and discharge of a hydraulic fluid by reciprocation of a piston in a cylinder block rotating integrally with a rotating shaft, the stroke of the reciprocation of the piston depending on an inclination of a swashplate, wherein the swashplate includes a sliding contact surface contacting slidably with one end portion of the piston via a shoe, the swashplate being disposed to enable to turn about a turning center to change the inclination that defines the stroke of the piston, the variable capacity piston pump comprising: a pressing portion disposed on one side with respect to the sliding contact surface of the swashplate, the pressing portion causing a pressing force to act along one direction by pressing a pressed portion of the swashplate to adjust the inclination of the swashplate between a maximum inclination and a minimum inclination, wherein a discharge capacity of the hydraulic fluid is maximized at the maximum inclination and the discharge capacity of the hydraulic fluid is minimized at the minimum inclination, and a swashplate return spring disposed on the other side with respect to the sliding contact surface of the swashplate, the swashplate return spring biasing the pressed portion of the swashplate toward the one side of the sliding contact surface, wherein the pressed portion is capable of taking a first action position and a second action position, wherein the first action position is a position at which the pressing force of the pressing portion acts when the inclination of the swashplate is the maximum inclination and the second action position is a position at which the pressing force of the pressing portion acts when the inclination of the swashplate is the minimum inclination, and wherein there is a positional relationship in which a vertical reference line passes between the first action position and the second action position, the vertical reference line being a straight line per-

pendicular to a parallel reference line and passing through the turning center of the swashplate, the parallel reference line being a straight line parallel to a direction in which the pressing force of the pressing portion acts and passing through the turning center of the swashplate.

[0009] In the variable capacity piston pump described above, there is a positional relationship in which the vertical reference line passes between the first action position which is the position at which the pressing force of the pressing portion acts on the pressed portion when the inclination of the swashplate is the maximum inclination and the second action position which is the position at which the pressing force of the pressing portion acts on the pressed portion when the inclination of the swashplate is the minimum inclination. When the position at which the pressing force of the pressing portion acts on the pressed portion is on the vertical reference line or near the vertical reference line, the length of a moment arm of the pressing force due to the pressing portion barely changes. In the variable capacity piston pump described above, since the first action position and the second action position are positioned with the vertical reference line interposed therebetween, the position at which the pressing force of the pressing portion acts on the pressed portion is on the vertical reference line or near the vertical reference line. Therefore, even when the inclination of the swashplate changes from the maximum inclination to the minimum inclination, the length of the moment arm of the pressing force barely changes. Accordingly, the amount of variation in the moment of the pressing force can be suppressed regardless of the inclination of the swashplate. As a result, controllability over the inclination of the swashplate can be improved.

[0010] According to the present invention, in the variable capacity piston pump, there is a positional relationship in which the vertical reference line passes through a midpoint between the first action position and the second action position. In this case, the length of the moment arm when the inclination of the swashplate is the maximum inclination and the length of the moment arm when the inclination of the swashplate is the minimum inclination can be equal to each other. Therefore, the amount of a change in the length of the moment arm of the pressing force while the inclination of the swashplate displaces from the maximum inclination to the minimum inclination can be minimized. Accordingly, the amount of variation of the moment of the pressing force due to the displacement of the inclination of the swashplate can be suppressed to the maximum degree.

As a result, controllability over the inclination of the swashplate can be further improved.

[0011] According to another aspect of the present invention, in the variable capacity piston pump, the pressing portion may be disposed in parallel to the rotating shaft. In this case, design of the variable capacity piston pump can be facilitated.

Advantageous Effects of Invention

[0012] According to the various aspects of the present invention, a variable capacity piston pump which achieves an improvement in controllability over the inclination of a swashplate is provided.

Brief Description of Drawings

[0013]

FIG. 1 is a schematic sectional view illustrating a variable capacity piston pump according to an embodiment of the present invention.

FIG. 2 is a perspective view of a swashplate illustrated in FIG. 1.

FIG. 3 is a side view of the swashplate illustrated in FIG. 1 viewed from a side of a sliding contact surface.

FIG. 4 is a side view of the swashplate illustrated in FIG. 1 viewed on a side opposite to the sliding contact surface.

FIG. 5 is a view schematically illustrating the positional relationship between the sliding contact surface of the swashplate and a turning center of the swashplate.

FIG. 6 is a schematic view illustrating variation in an action position of a pressing force of a piston portion.

FIG. 7 is a schematic view illustrating variation in the action position of the pressing force of the piston portion as a comparative example of the embodiment in addition to the case of FIG. 6.

FIG. 8 is a schematic view illustrating variation in the action position of the pressing force of the piston portion at a position different from that of FIG. 6.

FIG. 9 is a perspective view illustrating a swashplate according to a modification example.

FIG. 10 is a schematic sectional view illustrating main parts of a variable capacity piston pump according to a modification example.

Description of Embodiments

[0014] Hereinafter, an embodiment of the present invention will be described in detail with reference to the accompanying drawings. In the description, like elements which are the same or having the same function are denoted by like reference numerals, and overlapping description thereof will be omitted.

[0015] First, a variable capacity piston pump (hereinafter, "a pump") according to the embodiment will be described with reference to FIG. 1. A pump 1 includes a pump housing 10, a rotating shaft 20, and a cylinder block 14.

[0016] The pump housing 10 is configured by bonding a front housing 10a, a center housing 10b, and a rear housing 10c together, and has a crank chamber 12 therein.

[0017] Most of the rotating shaft 20 is accommodated

in the crank chamber 12 of the pump housing 10, and only one end portion thereof protrudes from the pump housing 10. The rotating shaft 20 is rotatably held in the crank chamber 12 by a bearing. The end portion of the rotating shaft 20 protruding from the pump housing 10 is connected to a power take-off (not illustrated) such that the entirety of the rotating shaft 20 is driven to rotate by an engine.

[0018] The cylinder block 14 is also accommodated in the crank chamber 12 of the pump housing 10. The cylinder block 14 is spline-fitted to the rotating shaft 20 so as to rotate integrally with the rotating shaft 20. In the cylinder block 14, a plurality of cylinder bores 14a, each including an opening on a side of the protruding end portion of the rotating shaft 20, are provided, and the plurality of cylinder bores 14a are disposed with intervals therebetween at a predetermined angle around the rotating shaft 20 in the cylinder block 14. In addition, in each of the plurality of cylinder bores 14a, a piston 16a having a head protruding toward the side of the protruding end portion of the rotating shaft 20 is accommodated.

[0019] A swashplate 30 is further accommodated in the crank chamber 12 of the pump housing 10. Hereinafter, the configuration of the swashplate 30 will be described with reference to FIGS. 2 to 4. FIG. 2 is a perspective view of the swashplate 30 illustrated in FIG. 1. FIG. 3 is a side view of the swashplate illustrated in FIG. 1 viewed from a side of a sliding contact surface. FIG. 4 is a side view of the swashplate illustrated in FIG. 1 viewed on a side opposite to the sliding contact surface.

[0020] As illustrated in FIGS. 2 to 4, the swashplate 30 includes a body portion 31, a pair of sliding portions 32, and a pressed portion 33.

[0021] The body portion 31 has a substantially plate shape, and the center portion thereof is provided with a through-hole 31a through which the above-described rotating shaft 20 is inserted. The pair of sliding portions 32 are provided at positions with the body portion 31 interposed therebetween to be integrated with the body portion 31.

[0022] The rear surface side of the body portion 31 and the sliding portions 32 become a flat surface 30a as illustrated in FIG. 3, and this surface is the sliding contact surface, which will be described later. On the other hand, the front surface side of the body portion 31 and the sliding portions 32 has a shape in which the sliding portions 32 protrude from the body portion 31 as illustrated in FIGS. 2 and 4. The section of the sliding portion 32 has a half-moon shape (D shape), and has a sliding surface 32a which is curved at a predetermined curvature so as to be convex toward the front surface side.

[0023] In addition, in the body portion 31, the pressed portion 33 which extends upward from the body portion 31 is provided. On the rear surface side in the pressed portion 33, an accommodation hole 33a is formed, and a cylindrical member 33b, which will be described later, is disposed in the accommodation hole 33a. In addition, the cylindrical member 33b may be disposed in a fixed

state so as not to be turned, or may be disposed so as to be turned. In addition, on the front surface side in the pressed portion 33, at a position biased by the tip end portion of a swashplate return spring 60, a protruding portion 33c and a planar portion 33d with which the tip end portion of the swashplate return spring 60 is engaged are formed.

[0024] Returning to FIG. 1, the position of the swashplate 30 is held by a swashplate receiving member 34 disposed on the front surface side thereof. The swashplate receiving member 34 has a support surface 34a having substantially the same curvature as that of the sliding surface 32a of the sliding portion 32 of the swashplate 30 described above. The swashplate 30 is disposed so as to cause the sliding surface 32a of the sliding portion 32 to come into contact with the support surface 34a of the swashplate receiving member 34 and is thus supported by the swashplate receiving member 34 to be oscillated along the curvature. More specifically, the swashplate 30 is capable of turning (regarded as tilting or regarded as rotating) about the center X of curvature of the support surface 34a of the swashplate receiving member 34 as the origin. The center X of curvature is also the center of curvature of the sliding surface 32a of the sliding portion 32 of the swashplate 30. In addition, the center X of curvature can be defined as a point at a constant distance (shortest distance) from the sliding contact surface 30a regardless of the turning position of the swashplate 30. In the following description, the center of curvature is referred to as a turning center X. In addition, in FIG. 1, the turning center X is denoted by a dot. However, in practice, the line of the turning center X extends in an inward direction (a direction perpendicular to the figure).

[0025] The swashplate 30 is disposed so as to turn about the turning center X and change the inclination that defines the stroke of the piston 16. For example, the inclination can be defined as an angle with respect to a straight line perpendicular to the axial line of the rotating shaft 20. In the embodiment, the inclination is defined as an angle of the sliding contact surface 30a with respect to the straight line perpendicular to the axial line of the rotating shaft 20.

[0026] The sliding contact surface 30a on the rear surface side of the swashplate 30 faces the cylinder block 14 side. The head (one end portion) of each piston 16 protruding from the cylinder block 14 comes into sliding contact with the sliding contact surface 30a via a shoe 36. The shoe 36 to which the head of the piston 16 attached is held in a disk-shaped retainer 35 having a hole into which the shoe 36 is inserted. When the cylinder block 14 is rotated along with the rotating shaft 20, each piston 16 rotates about the rotating shaft 20 while sliding on the sliding contact surface 30a via the shoe 36.

[0027] As the swashplate 30 is turned and inclined about the turning center X, the end portion of the head side (the left end portion in FIG. 1) of each piston 16 accommodated in the cylinder block 14 comes in pressing contact via the shoe 36, and the cylinder block 14

comes into pressing contact with a valve plate 40 fixed to the inner end wall surface of the rear housing 10c.

[0028] In addition, as the cylinder block 14 and the rotating shaft 20 rotate integrally with each other, the stroke of each piston 16 defined by the inclination of the swashplate 30 is reciprocated, and the cylinder bore 14a alternately communicates with a suction port 40a and a discharge port 40b forming an arc shape, which are provided to penetrate through the valve plate 40. Accordingly, hydraulic oil is suctioned into the cylinder bore 14a from the suction port 40a, and the hydraulic oil in the cylinder bore 14a is discharged from the discharge port 40b due to a pump action. In addition, a suction passage 10d and a discharge passage 10e are formed in the rear housing 10c to respectively communicate with the suction port 40a and the discharge port 40b.

[0029] The pump 1 is further provided with a control piston 50 provided on the rear surface side of the swashplate 30, that is, on the cylinder block 14 side. The control piston 50 is provided at a side portion of the center housing 10b of the pump housing 10, and includes a housing 52 that communicates with the crank chamber 12 and a piston portion 58 that reciprocates in the housing 52. The housing 52 has a substantially cylindrical shape extending in a direction inclined with respect to the rotating shaft 20 so as to cause the piston portion 58 to face the pressed portion 33 of the swashplate 30.

[0030] One opening of the openings of the housing 52 distant from the swashplate 30 is blocked by a screw 54. Accordingly, a piston accommodation chamber 56 is defined in the housing 52, and the piston portion 58 is accommodated in the piston accommodation chamber 56.

[0031] The piston portion 58 has a columnar external shape. The diameter of the piston portion 58 is designed such that there is no gap from the inner wall surface of the piston accommodation chamber 56 and the piston portion 58 slides in the piston accommodation chamber 56. The end surface of the piston portion 58 on the swashplate 30 is a planar shape and can move to a position that comes into contact with the cylindrical member 33b in the pressed portion 33 of the swashplate 30. As illustrated in FIG. 1, the end surface of the piston portion 58 on the swashplate 30 side, which is a pressing portion, comes into contact with the cylindrical member 33b of the pressed portion 33 of the swashplate 30 to always press the cylindrical member 33b with a predetermined pressing force.

[0032] A space between the piston portion 58 and the screw 54 in the piston accommodation chamber 56 functions as a control chamber 56a into which the hydraulic oil flows. The pressure in the control chamber 56a (hereinafter, referred to as control pressure) is changed due to the inflow of the hydraulic oil. The control piston 50 causes the piston portion 58 to slide due to a change in the control pressure and press the swashplate 30 from the cylinder block 14 side. Accordingly, the control piston 50 adjusts the inclination of the swashplate 30 between the maximum inclination, at which the discharge capacity

of the hydraulic oil is maximized, and the minimum inclination, at which the discharge capacity of the hydraulic oil is minimized.

[0033] The pump 1 further includes the swashplate return spring 60 which is a cylindrical spiral shape (coil spring) extending in one direction on the front surface side of the swashplate 30. That is, the swashplate return spring 60 is disposed on the side opposite to the control piston 50 with respect to the sliding contact surface 30a of the swashplate 30. Specifically, the base end portion of the swashplate return spring 60 is accommodated in a spring chamber 70 formed in the front housing 10a of the pump housing 10.

[0034] In the embodiment, the spring chamber 70 is formed in parallel to the rotating shaft 20, and the swashplate return spring 60 extends toward the swashplate 30 from the spring chamber 70. As a result, the swashplate return spring 60 is disposed so that the axial direction thereof is parallel to the rotating shaft 20. The tip end portion of the swashplate return spring 60 abuts the front surface of the pressed portion 33 of the swashplate 30 described above and is engaged with the protruding portion 33c and the planar portion 33d formed on the front surface. The swashplate return spring 60 is not fixed to the spring chamber 70 and the swashplate 30 and the position and posture thereof are held in a state of being interposed between the spring chamber 70 and the pressed portion 33.

[0035] In other words, regarding the seat surfaces (spring end surfaces) of the swashplate return spring 60, a seat surface 60a of the base end portion abuts the bottom wall of the spring chamber 70, and a seat surface 60b of the tip end portion abuts the pressed portion 33 of the swashplate 30. Accordingly, the swashplate return spring 60 is compressed such that the swashplate 30 is biased toward the cylinder block side with respect to the sliding contact surface 30a. In addition, the swashplate return spring 60 is a wire spring formed by processing a metallic wire rod such as SWP-B.

[0036] Next, with reference to Figs 5 to 7, an action position which is a position at which the pressing force of the piston portion 58 which is the pressing portion acts on the pressed portion 33 will be described in detail. Here, the position at which the pressing force of the piston portion 58 acts on the pressed portion 33 is, for example, a position at which the end surface of the piston portion 58 on the swashplate 30 side comes into contact with the cylindrical member 33b of the pressed portion 33 of the swashplate 30 and presses the cylindrical member 33b with a predetermined pressing force. Hereinafter, the position at which the end surface of the piston portion 58 on the swashplate 30 side comes into contact with the cylindrical member 33b of the pressed portion 33 of the swashplate 30 and presses the cylindrical member 33b with a predetermined pressing force is referred to as an action position of the pressing force of the piston portion 58.

[0037] First, references such as the turning center X,

the vertical reference line and the parallel reference line for the action position of the pressing force of the piston portion 58 will be described. FIG. 5 is a view schematically illustrating the positional relationship between the sliding contact surface 30a of the swashplate 30 and the turning center X of the swashplate 30. In addition, in FIG. 5, the turning center X is denoted by a dot. However, the line of the turning center X extends in an inward direction (a direction perpendicular to the figure).

[0038] As illustrated in FIG. 5, a distance d from the sliding contact surface 30a of the swashplate 30 to the turning center X at the maximum inclination indicated by "Max" and a distance d from the sliding contact surface 30a of the swashplate 30 to the turning center X at the minimum inclination indicated by "Min" are the same. That is, the distance of the turning center X from the sliding contact surface 30a is constant regardless of the inclination of the swashplate 30. In addition, in a section, an imaginary circle E that touches both the sliding contact surface 30a of the swashplate 30 at the maximum inclination and the sliding contact surface 30a of the swashplate 30 at the minimum inclination is drawn as a circle having the turning center X as its center. That is, the turning center X is the axial line of a column having, as its section, the imaginary circle E that touches the sliding contact surface 30a of the swashplate 30 regardless of the inclination of the swashplate 30.

[0039] The parallel reference line Y is a straight line which is parallel to a direction in which the pressing force of the piston portion 58 acts and passes through the turning center X. A straight line that is perpendicular to the parallel reference line Y and passes through the turning center X is defined as the vertical reference line Z.

[0040] FIG. 6 is a schematic view illustrating variation in the action position of the pressing force of the piston portion 58 of the control piston 50. In FIG. 6, the parallel reference line Y, the vertical reference line Z, and the turning center X shown in FIG. 5 are shown. In FIG. 6, furthermore, the pressing force of the piston portion 58 is indicated by a pressing force F, a line of action of the pressing force F when the inclination of the swashplate 30 is the maximum inclination is indicated by a line of action S1, and a line of action when the inclination of the swashplate 30 is the minimum inclination is indicated by a line of action S2. In addition, a direction in which the pressing force F acts is a direction parallel to the parallel reference line Y.

[0041] In FIG. 6, variation in the action position of the pressing force of the piston portion 58 in the pump 1 according to the embodiment is indicated by a double-headed arrow A. The double-headed arrow A represents that the action position of the pressing force F varies between a position of the pressing force F when the inclination of the swashplate 30 is the maximum inclination (hereinafter, referred to as a first action position) A1, and a position of the pressing force F when the inclination of the swashplate 30 is the minimum inclination (hereinafter, referred to as a second action position) A2. The an-

gular difference between the maximum inclination and the minimum inclination of the swashplate 30 is indicated by θ . As illustrated in FIG. 6, the action position of the pressing force F moves between the first action position A1 and the second action position A2 along an arc of the imaginary circle having the turning center X as its center. This is because the distance between the cylindrical member 33b on which the pressing force F acts and the turning center X is always constant regardless of the inclination.

[0042] As indicated by the double-headed arrow A of FIG. 6, in the pump 1 according to the embodiment, for example, when viewed in a direction perpendicular to a plane parallel to the parallel reference line Y and the vertical reference line Z (a direction perpendicular to the figure), the vertical reference line Z passes between the first action position A1 when the inclination of the swashplate 30 is the maximum inclination and the second action position A2 when the inclination of the swashplate 30 is the minimum inclination. That is, the vertical reference line Z is interposed between the first action position A1 when the inclination of the swashplate 30 is the maximum inclination and the second action position A2 when the inclination of the swashplate 30 is the minimum inclination.

[0043] In a case where the first action position A1, the second action position A2, and the vertical reference line Z have this positional relationship, as illustrated in FIG. 6, the action position of the pressing force F moves just beside the action position in the range of the double-headed arrow A, and there is substantially no displacement in upward and downward directions (that is, directions of the vertical reference line Z) of FIG. 6. Therefore, even when the inclination of the swashplate 30 moves from the maximum inclination to the minimum inclination and accordingly the action position of the pressing force F moves from the first action position A1 to the second action position A2, there is substantially no displacement in the directions of the vertical reference line Z (a change in the height position of each of the lines of action S1 and S2 with respect to the parallel reference line Y).

[0044] As described above, while the inclination of the swashplate 30 moves from the maximum inclination to the minimum inclination, the action position of the pressing force F barely displaces in the directions of the vertical reference line Z. Therefore, the distance between the pressing force F and the turning center X when the inclination of the swashplate 30 is the maximum inclination (that is, the length of a moment arm of the pressing force F about the turning center X) La_1 and the distance between the pressing force F and the turning center X when the inclination of the swashplate 30 is the minimum inclination La_2 barely change. That is, even when the inclination of the swashplate 30 moves from the maximum inclination to the minimum inclination, the length of the moment arm of the pressing force F about the turning center X barely changes. Therefore, the amount of variation in the moment of the pressing force F about the

turning center X due to a change in the inclination of the swashplate 30 can be suppressed.

[0045] FIG. 7 is a schematic view illustrating variation in the action position of the pressing force F of the piston portion 58 as a comparative example of the embodiment in addition to the case of FIG. 6. In FIG. 7, while the case where the vertical reference line Z passes between the first action position A1 and the second action position A2 is indicated by the double-headed arrow A as in FIG. 6, cases where the vertical reference line Z does not pass between a first action position and a second action position are indicated by double-headed arrows B and C. In addition, in any case of the double-headed arrows B and C, the difference θ between the maximum inclination and the minimum inclination is the same as the difference θ of the double-headed arrow A described above.

[0046] The double-headed arrow B indicates variation in the action position of the pressing force F in a case where both a first action position B1 and a second action position B2 are positioned on the swashplate return spring 60 side in relation to the vertical reference line Z. As illustrated in FIG. 7, when the inclination of the swashplate 30 changes from the maximum inclination to the minimum inclination and accordingly the action position of the pressing force F moves from the first action position B1 to the second action position B2, the action position of the pressing force F gradually moves in a downward direction and significantly displaces in the directions of the vertical reference line Z. Therefore, regarding the case of the double-headed arrow B, the length Lb_2 of the moment arm of the pressing force F when the inclination of the swashplate 30 is the minimum inclination becomes shorter than the length Lb_1 of the moment arm of the pressing force F when the inclination of the swashplate 30 is the maximum inclination.

[0047] As described above, when the length of the moment arm of the pressing force F is shortened as the inclination of the swashplate 30 is decreased, the moment of the pressing force F is decreased, and it is difficult for the swashplate 30 to rotate. Therefore, the responsiveness of the inclination of the swashplate 30 to the pressing force F of the piston portion 58 deteriorates (for example, the response speed becomes slow), and the inclination of the swashplate 30 is not appropriately controlled.

[0048] The double-headed arrow C indicates variation in the action position of the pressing force F in a case where both a first action position C1 and a second action position C2 are positioned on the control piston 50 side in relation to the vertical reference line Z. As illustrated in FIG. 7, when the inclination of the swashplate 30 changes from the maximum inclination to the minimum inclination and accordingly the action position of the pressing force F moves from the first action position C1 to the second action position C2, the action position of the pressing force F gradually moves in an upward direction and significantly displaces in the directions of the vertical reference line Z. Therefore, regarding the case

of the double-headed arrow C, the length Lc_2 of the moment arm of the pressing force F when the inclination of the swashplate 30 is the minimum inclination becomes longer than the length Lc_1 of the moment arm of the pressing force F when the inclination of the swashplate 30 is the maximum inclination.

[0049] As described above, when the length of the moment arm of the pressing force F is lengthened as the inclination of the swashplate 30 is decreased, the moment of the pressing force F is increased, and the swashplate 30 more easily rotate. Therefore, the response of the inclination of the swashplate 30 to the pressing force F of the piston portion 58 becomes excessively sensitive (for example, the response speed becomes excessively fast), and the inclination of the swashplate 30 is also not appropriately controlled.

[0050] As described above, in the pump 1 according to the embodiment, since the first action position A1 and the second action position A2 are positioned with the vertical reference line Z interposed therebetween, the position at which the pressing force F of the piston portion 58 of the control piston 50 acts on the cylindrical member 33b of the pressed portion 33 is on the vertical reference line Z or near the vertical reference line Z. Therefore, even when the inclination of the swashplate 30 displaces from the maximum inclination to the minimum inclination, the length of the moment arm of the pressing force F barely changes, and the amount of variation in the moment of the pressing force F due to the displacement of the inclination of the swashplate 30 can be suppressed. As a result, controllability over the inclination of the swashplate 30 can be improved.

[0051] In addition, the positional relationship in which the vertical reference line Z passes between the first action position A1 and the second action position A2, that is, the positional relationship in which the vertical reference line Z is interposed between the first action position A1 and the second action position A2 includes a positional relationship in which the vertical reference line Z overlaps the first action position A1 or the second action position A2.

[0052] In addition, as indicated by the double-headed arrow A of FIG. 8, the positional relationship between the first action position A1, the second action position A2, and the vertical reference line Z may be an embodiment in which the vertical reference line Z passes through a midpoint P which is the point that bisects a straight line that connects the first action position A1 and the second action position A2. In this case, the vertical reference line is coincident with the perpendicular bisector of the straight line that connects the first action position A1 and the second action position A2.

[0053] At this time, the length La_1 of the moment arm when the inclination of the swashplate 30 is the maximum inclination and the length La_2 of the moment arm when the inclination of the swashplate 30 is the minimum inclination can be equal to each other. That is, the length of the moment arm does not excessively increases in any

of cases where the inclination of the swashplate 30 is the maximum inclination or the minimum inclination. Therefore, the amount of variation of the moment due to the displacement of the inclination of the swashplate 30 can be minimized.

[0054] Accordingly, controllability over the inclination of the swashplate 30 can be further improved.

[0055] The swashplate 30 is not limited to that in the embodiment. For example, instead of the swashplate 30, a swashplate 130 having a shape illustrated in FIG. 9 may be employed.

[0056] The swashplate 130 includes a pair of rotating shaft portions 132 instead of the pair of sliding portions 32 of the swashplate 30. The above-described swashplate 30 has a form that oscillates about the turning center X by cooperation between the sliding portions 32 and the swashplate receiving member 34. However, the swashplate 130 can oscillate about the turning center X since the pair of rotating shaft portions 132 having a columnar shape extending along the turning center X are rotatably held in the crank chamber 12. The swashplate 130 also includes a disk-shaped body portion 131 having the same function as that of the body portion 31 of the swashplate 30 described above. The body portion 131 includes a sliding contact surface 130a, which is the same as the sliding contact surface 30a, on the rear surface side thereof and further includes a pressed portion 133 which is the same as the pressed portion 33 at the upper portion thereof. The swashplate 130 illustrated in FIG. 8 has functions which are the same as or equivalent to those of the swashplate 30 described above. Moreover, since the swashplate 130 includes the pair of rotating shaft portions 132, the swashplate receiving member 34 described above becomes unnecessary, and simplification of the configuration of the pump 1 can be achieved.

[0057] In addition, FIG. 10 is a schematic sectional view illustrating main parts of a variable capacity piston pump according to a modification example. In FIG. 10, the vicinity of the control piston 50 in the variable capacity piston pump according to the modification example is enlarged to be illustrated.

[0058] As illustrated in FIG. 10, in the variable capacity piston pump according to the modification example, the piston portion 58 of the control piston 50 is disposed in parallel to the rotating shaft 20. The pump 1 is generally designed on the basis of the axial line of the rotating shaft 20. Therefore, when the piston portion 58 of the control piston 50 is disposed in parallel to the rotating shaft 20, design of the control piston 50 or the pump housing 10 (particularly the center housing 10b in which the control piston 50 is provided) is facilitated.

[0059] In addition, in the case where the control piston 50 is disposed obliquely with respect to the rotating shaft 20 as in the above-described embodiment, the dimensions (diameter dimension) of the center housing 10b are greater than those of the front housing 10a or the rear housing 10c. In the case where the piston portion 58 of the control piston 50 is disposed in parallel to the rotating

shaft 20, an increase in the dimensions is suppressed. As a result, miniaturization of the variable capacity piston pump can be realized.

5 Reference Signs List

[0060]

1	variable capacity piston pump
10 14	cylinder block
16	piston
20	rotating shaft
30, 130	swashplate
30a	sliding contact surface
15 33, 133	pressed portion
58	piston portion (pressing portion)
60	swashplate return spring
X	turning center
Y	parallel reference line
20 Z	vertical reference line
A1	first action position
A2	second action position

25 Claims

1. A variable capacity piston pump (1) performing suction and discharge of a hydraulic fluid by reciprocation of a piston (16) in a cylinder block (14) rotating integrally with a rotating shaft (20), the stroke of the reciprocation of the piston (16) depending on an inclination of a swashplate (30),

wherein the swashplate (30) includes a sliding contact surface (30a) contacting slidably with one end portion of the piston (16) via a shoe (36), the swashplate (30) being disposed to enable to turn about a turning center (X) to change the inclination that defines the stroke of the piston (16),
the variable capacity piston pump (1) comprising:

a pressing portion (58) disposed on one side with respect to the sliding contact surface (30a) of the swashplate (30), the pressing portion (58) causing a pressing force (F) to act along one direction by pressing a pressed portion (33, 133) of the swashplate (30) to adjust the inclination of the swashplate (30) between a maximum inclination (Max) and a minimum inclination (Min), wherein a discharge capacity of the hydraulic fluid is maximized at the maximum inclination (Max) and the discharge capacity of the hydraulic fluid is minimized at the minimum inclination (Min), and
a swashplate return spring (60) disposed on

the other side with respect to the sliding contact surface (30a) of the swashplate (30), the swashplate return spring (60) biasing the pressed portion (33, 133) of the swashplate (30) toward the one side of the sliding contact surface (30a),
 wherein the pressed portion (33, 133) is capable of taking a first action position (A1) and a second action position (A2), wherein the first action position (A1) is a position at which the pressing force (F) of the pressing portion (58) acts when the inclination of the swashplate (30) is the maximum inclination (Max) and the second action position (A2) is a position at which the pressing force (F) of the pressing portion (58) acts when the inclination of the swashplate (30) is the minimum inclination (Min), and
 wherein there is a positional relationship in which a vertical reference line (Z) passes between the first action position (A1) and the second action position (A2), the vertical reference line (Z) being a straight line perpendicular to a parallel reference line (Y) and passing through the turning center (X) of the swashplate (30), the parallel reference line (Y) being a straight line parallel to a direction in which the pressing force (F) of the pressing portion (58) acts and passing through the turning center (X) of the swashplate (30);
characterized in that there is a positional relationship in which the vertical reference line (Z) passes through a midpoint (P) between the first action position (A1) and the second action position (A2).

2. The variable capacity piston pump according to claim 1,
 wherein the pressing portion (58) is disposed in parallel to the rotating shaft (20).

Patentansprüche

1. Eine Kolbenpumpe (1) mit variabler Kapazität, die ein Ansaugen und ein Ausstoßen einer Hydraulikflüssigkeit durch eine Hin- und Herbewegung eines Kolbens (16) in einem Zylinderblock (14) durchführt, der sich integral mit einer Drehwelle (20) dreht, wobei der Hub der Hin- und Herbewegung des Kolbens (16) von einer Neigung einer Taumelscheibe (30) abhängt,
 wobei die Taumelscheibe (30) eine Gleitkontaktfläche (30a) aufweist, die gleitend mit einem Endabschnitt des Kolbens (16) über einen Schuh (36) in Kontakt steht, wobei die Taumelscheibe (30) so angeordnet ist, dass sie sich um ein Drehzentrum

(X) drehen kann, um die Neigung zu ändern, die den Hub des Kolbens (16) definiert,
 wobei die Kolbenpumpe (1) mit variabler Kapazität umfasst:

einen Druckabschnitt (58), der auf einer Seite in Bezug auf die Gleitkontaktfläche (30a) der Taumelscheibe (30) angeordnet ist, wobei der Druckabschnitt (58) bewirkt, dass eine Druckkraft (F) entlang einer Richtung wirkt, indem er auf einen gedrückten Abschnitt (33, 133) der Taumelscheibe (30) drückt, um die Neigung der Taumelscheibe (30) zwischen einer maximalen Neigung (Max) und einer minimalen Neigung (Min) einzustellen, wobei eine Ausstoßkapazität der Hydraulikflüssigkeit bei der maximalen Neigung (Max) maximiert wird und die Ausstoßkapazität der Hydraulikflüssigkeit bei der minimalen Neigung (Min) minimiert wird, und
 eine Taumelscheibenrückholfeder (60), die auf der anderen Seite in Bezug auf die Gleitkontaktfläche (30a) der Taumelscheibe (30) angeordnet ist, wobei die Taumelscheibenrückholfeder (60) den gedrückten Abschnitt (33, 133) der Taumelscheibe (30) in Richtung der einen Seite der Gleitkontaktfläche (30a) vorspannt,
 wobei der gedrückte Abschnitt (33, 133) in der Lage ist, eine erste Wirkposition (A1) und eine zweite Wirkposition (A2) einzunehmen, wobei die erste Wirkposition (A1) eine Position ist, in der die Druckkraft (F) des Druckabschnitts (58) wirkt, wenn die Neigung der Taumelscheibe (30) die maximale Neigung (Max) ist, und die zweite Wirkposition (A2) eine Position ist, in der die Druckkraft (F) des Druckabschnitts (58) wirkt, wenn die Neigung der Taumelscheibe (30) die minimale Neigung (Min) ist, und
 wobei es eine Positionsbeziehung gibt, in der eine vertikale Referenzlinie (Z) zwischen der ersten Wirkposition (A1) und der zweiten Wirkposition (A2) verläuft, wobei die vertikale Referenzlinie (Z) eine gerade Linie ist, die senkrecht zu einer parallelen Referenzlinie (Y) ist und durch den Drehmittelpunkt (X) der Taumelscheibe (30) verläuft, wobei die parallele Referenzlinie (Y) eine gerade Linie ist, die parallel zu einer Richtung ist, in der die Druckkraft (F) des Druckabschnitts (58) wirkt, und durch den Drehmittelpunkt (X) der Taumelscheibe (30) verläuft;
dadurch gekennzeichnet, dass es eine Positionsbeziehung gibt, in der die vertikale Bezugslinie (Z) durch einen Mittelpunkt (P) zwischen der ersten Wirkposition (A1) und der zweiten Wirkposition (A2) verläuft.

2. Die Kolbenpumpe mit variabler Kapazität nach Anspruch 1,
 wobei der Druckabschnitt (58) parallel zur Drehwelle

(20) angeordnet ist.

Revendications

1. Pompe à piston à capacité variable (1) réalisant l'aspiration et la décharge d'un fluide hydraulique par le mouvement de va-et-vient d'un piston (16) dans un bloc-cylindres (14) tournant de manière solidaire avec un arbre de rotation (20), la course du mouvement de va-et-vient du piston (16) dépendant d'une inclinaison d'un plateau oscillant (30), dans laquelle le plateau oscillant (30) comprend une surface de contact coulissante (30a) en contact de manière coulissante avec une partie d'extrémité du piston (16) via un patin (36), le plateau oscillant (30) étant disposé pour permettre de tourner autour d'un centre de rotation (X) afin de modifier l'inclinaison qui définit la course du piston (16), la pompe à piston à capacité variable (1) comprenant :

une partie de pression (58) disposée d'un côté par rapport à la surface de contact coulissante (30a) du plateau oscillant (30), la partie de pression (58) amenant une force de pression (F) à agir le long d'une direction en comprimant une partie comprimée (33, 133) du plateau oscillant (30) pour ajuster l'inclinaison du plateau oscillant (30) entre une inclinaison maximum (Max) et une inclinaison minimum (Min), dans laquelle une capacité de décharge du fluide hydraulique est maximisée à l'inclinaison maximum (Max) et la capacité de décharge du fluide hydraulique est minimisée à l'inclinaison minimum (Min), et

un ressort de rappel de plateau oscillant (60) disposé de l'autre côté par rapport à la surface de contact coulissante (30a) du plateau oscillant (30), le ressort de rappel de plateau oscillant (60) sollicitant la partie comprimée (33, 133) du plateau oscillant (30) vers le premier côté de la surface de contact coulissante (30a), dans laquelle la partie comprimée (33, 133) peut prendre une première position d'action (A1) et une seconde position d'action (A2), dans laquelle la première position d'action (A1) est une position dans laquelle la force de pression (F) de la partie de pression (58) agit lorsque l'inclinaison du plateau oscillant (30) est l'inclinaison maximum (Max) et la seconde position d'action (A2) est une position dans laquelle la force de pression (F) de la partie de pression (58) agit lorsque l'inclinaison du plateau oscillant (30) est l'inclinaison minimum (Min), et

dans laquelle il y a une relation de position dans laquelle une ligne de référence verticale (Z) passe entre la première position d'action (A1) et la

seconde position d'action (A2), la ligne de référence verticale (Z) étant une ligne droite perpendiculaire à une ligne de référence parallèle (Y) et passant par le centre de rotation (X) du plateau oscillant (30), la ligne de référence parallèle (Y) étant une ligne droite parallèle à une direction dans laquelle la force de pression (F) de la partie de pression (58) agit et passant par le centre de rotation (X) du plateau oscillant (30) ; **caractérisée en ce qu'il y a une relation de position dans laquelle la ligne de référence verticale (Z) passe par un point médian (P) entre la première position d'action (A1) et la seconde position d'action (A2).**

2. Pompe à piston à capacité variable selon la revendication 1, dans laquelle la partie de pression (58) est disposée parallèlement à l'arbre de rotation (20).

Fig.1

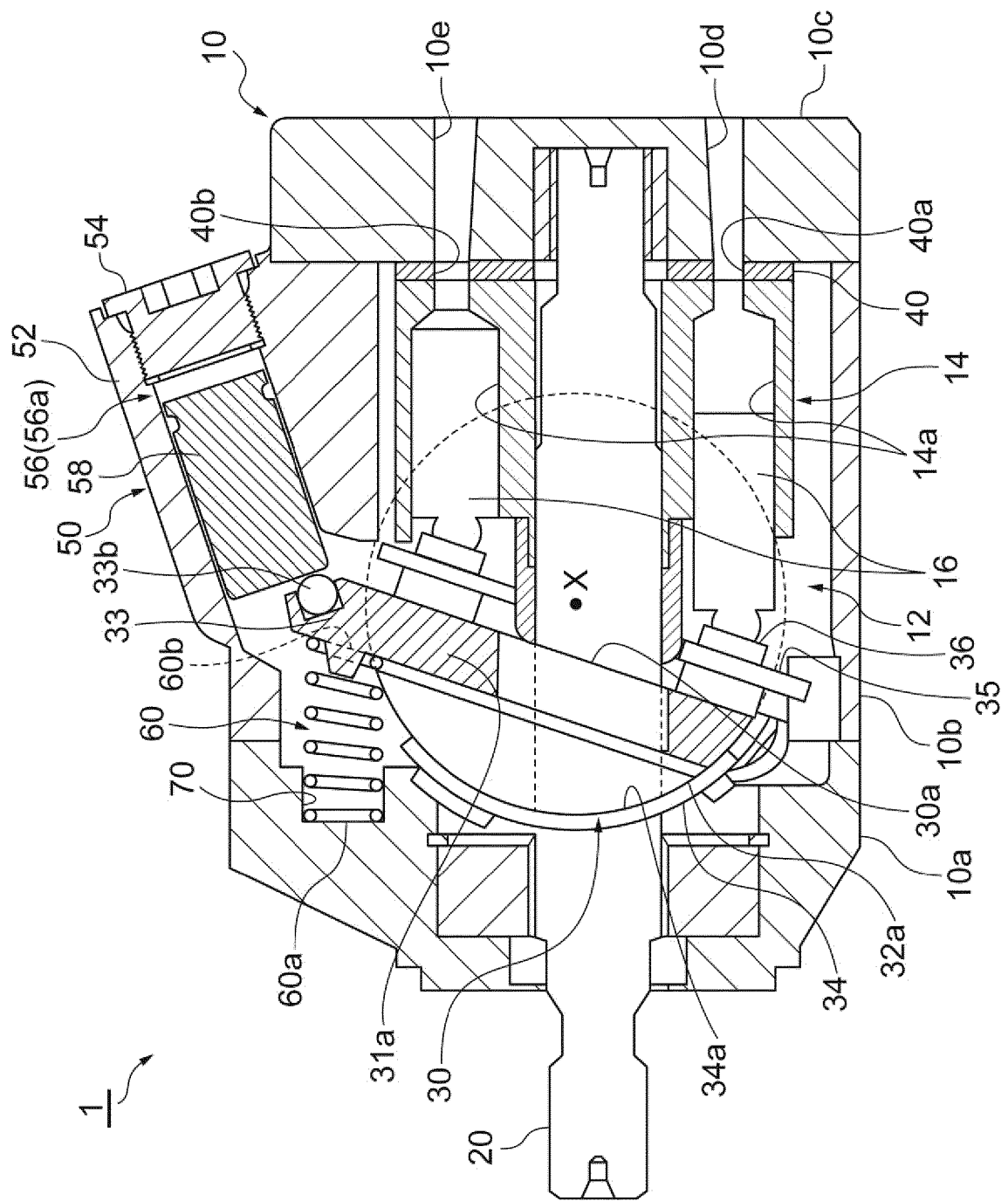


Fig.2

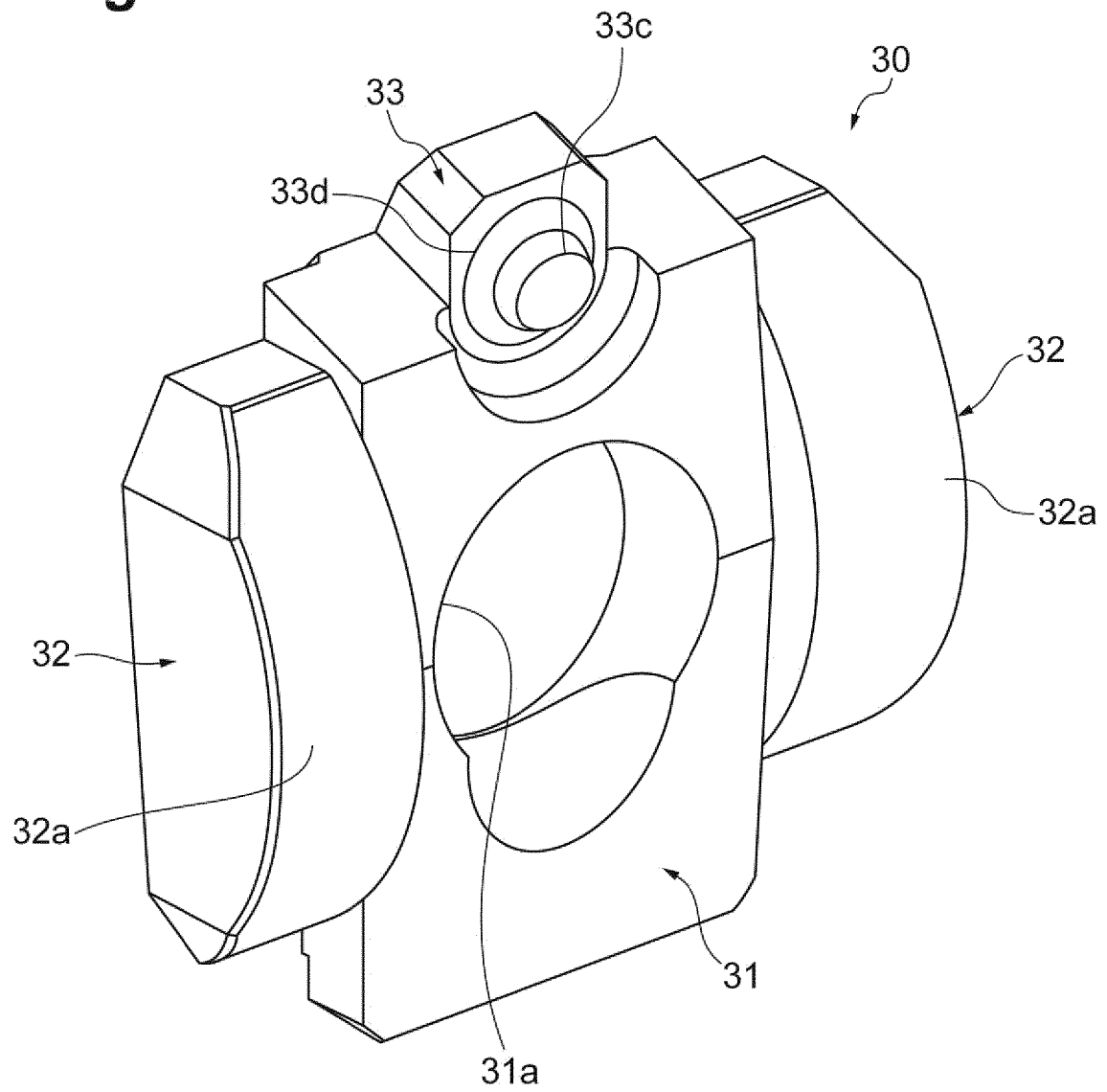


Fig.3

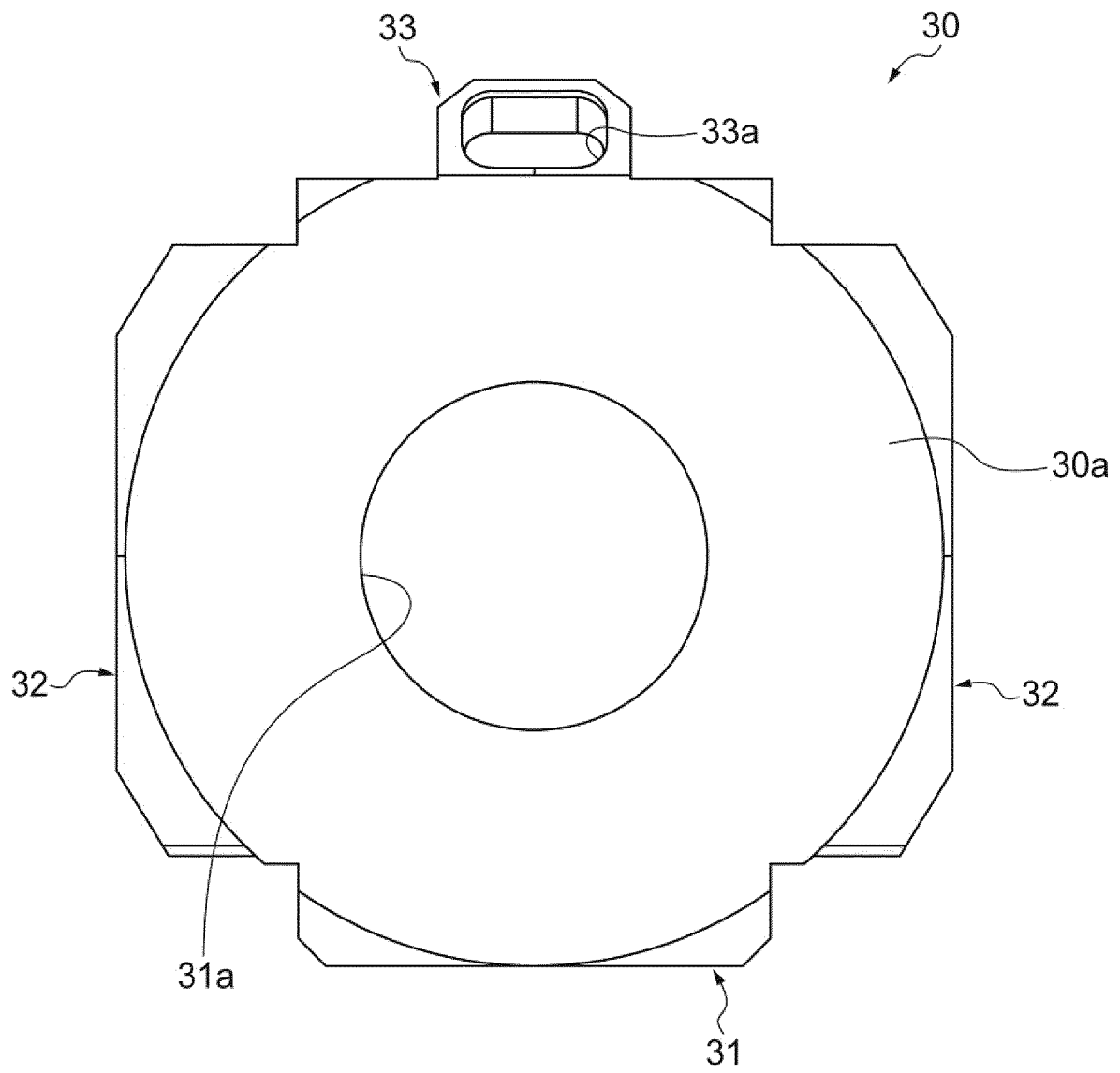


Fig.4

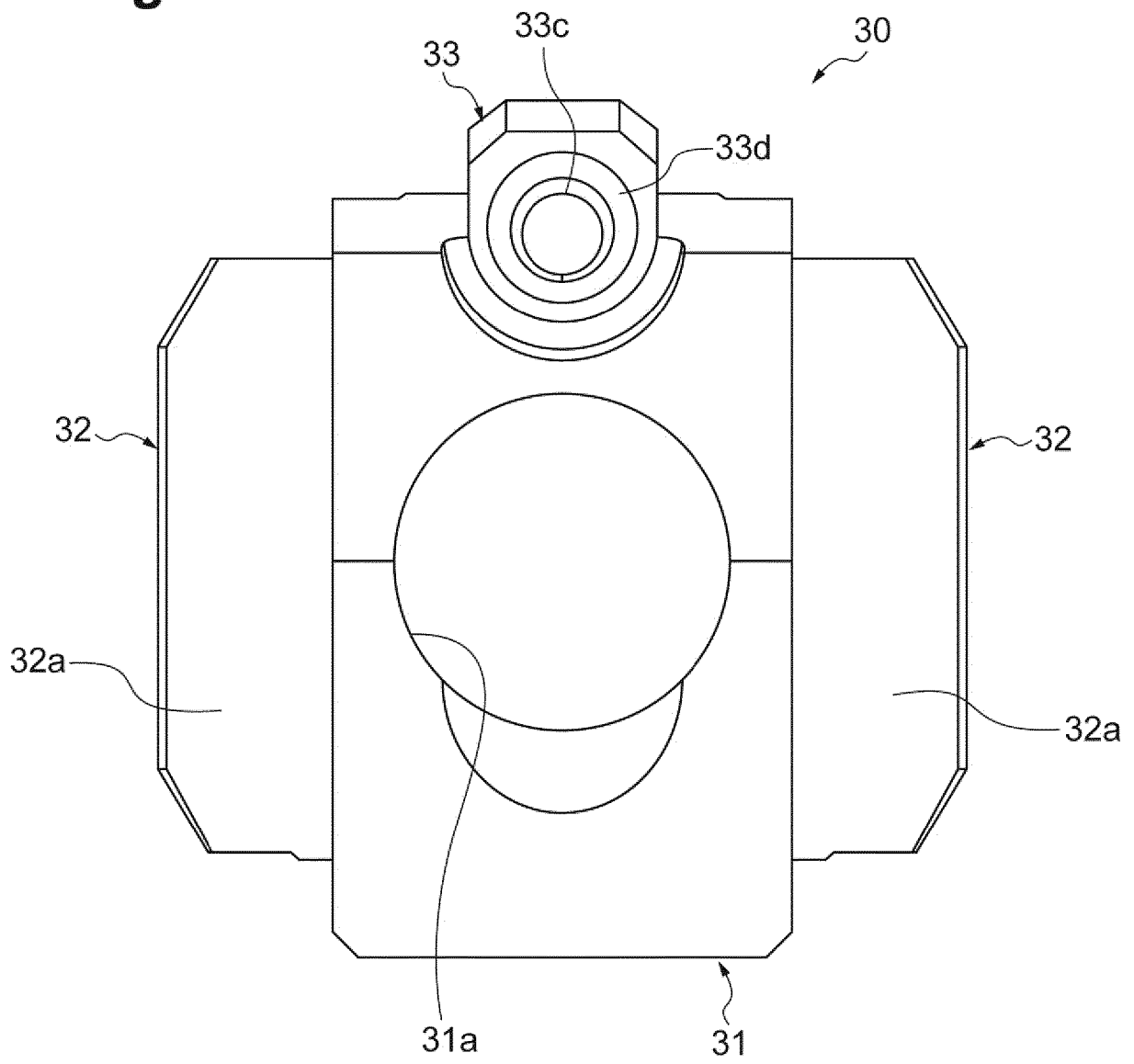


Fig.5

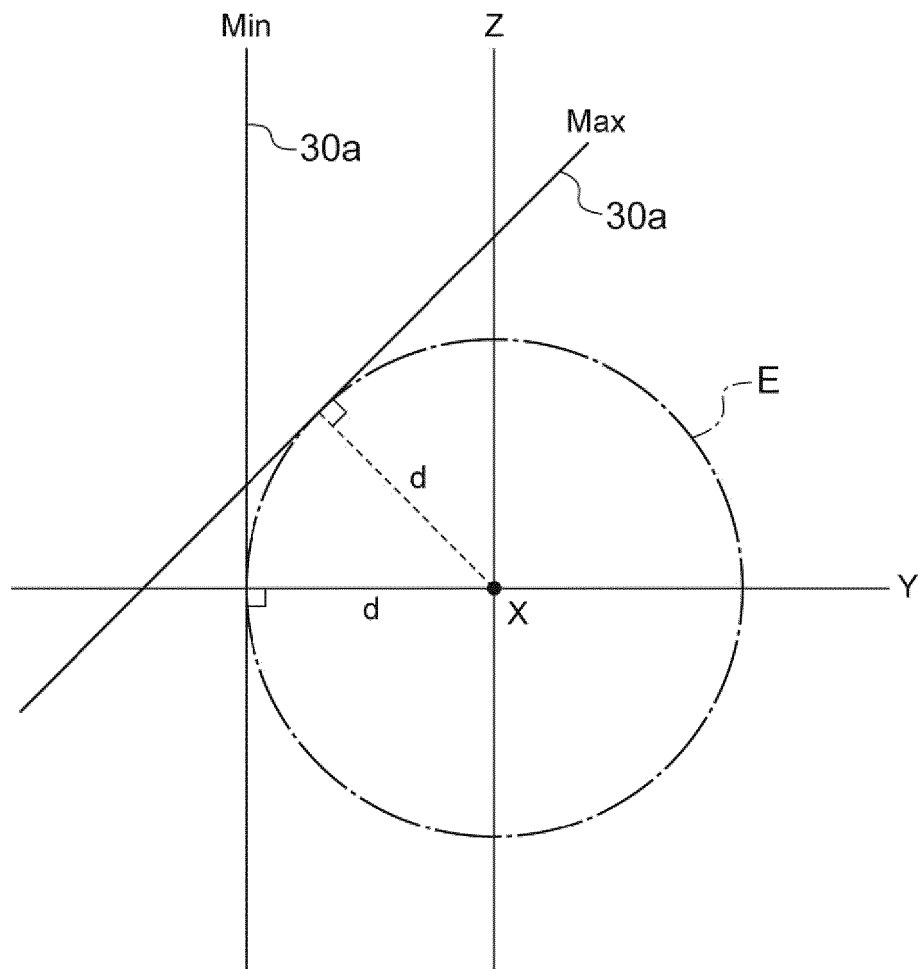


Fig.6

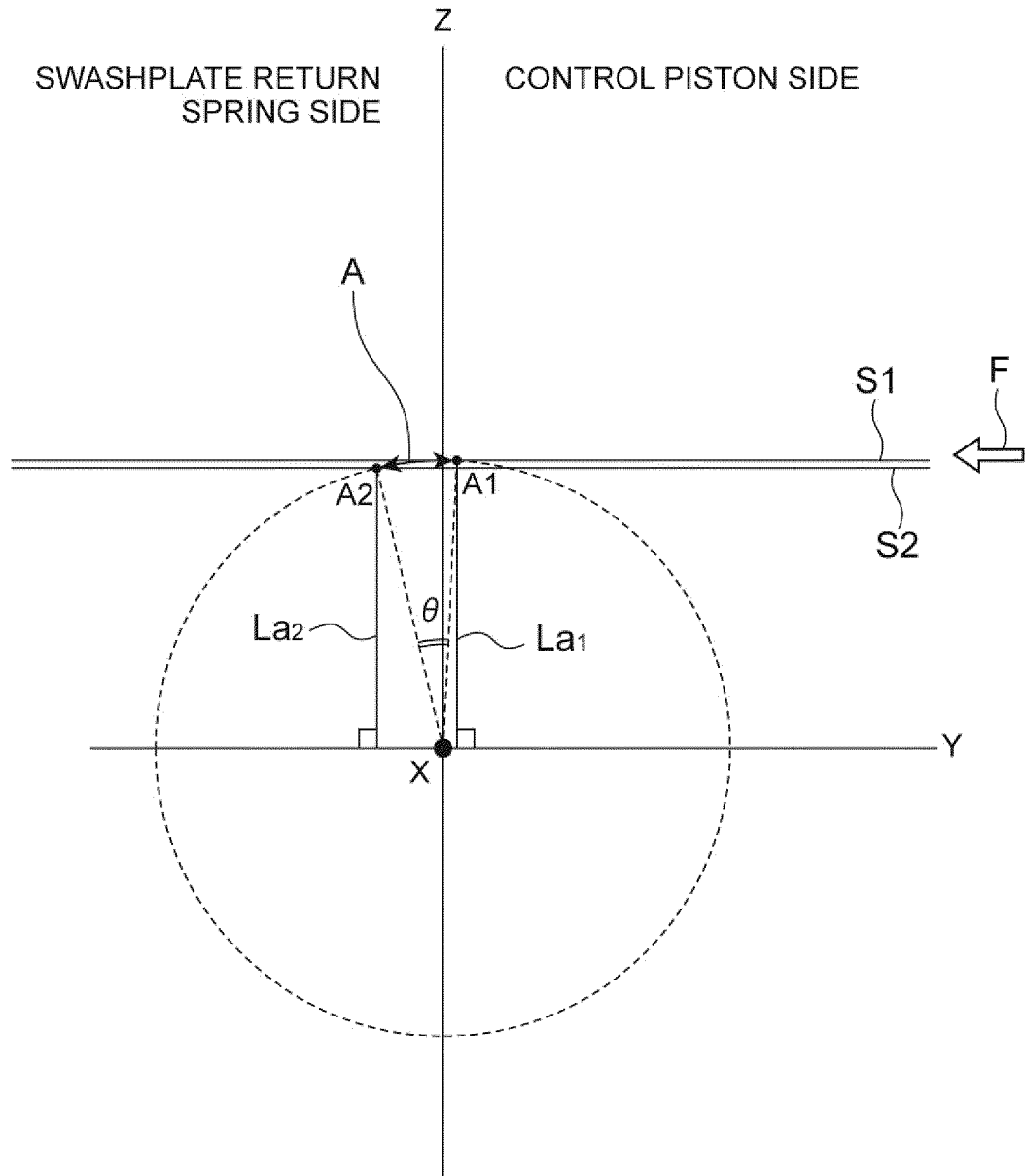


Fig.7

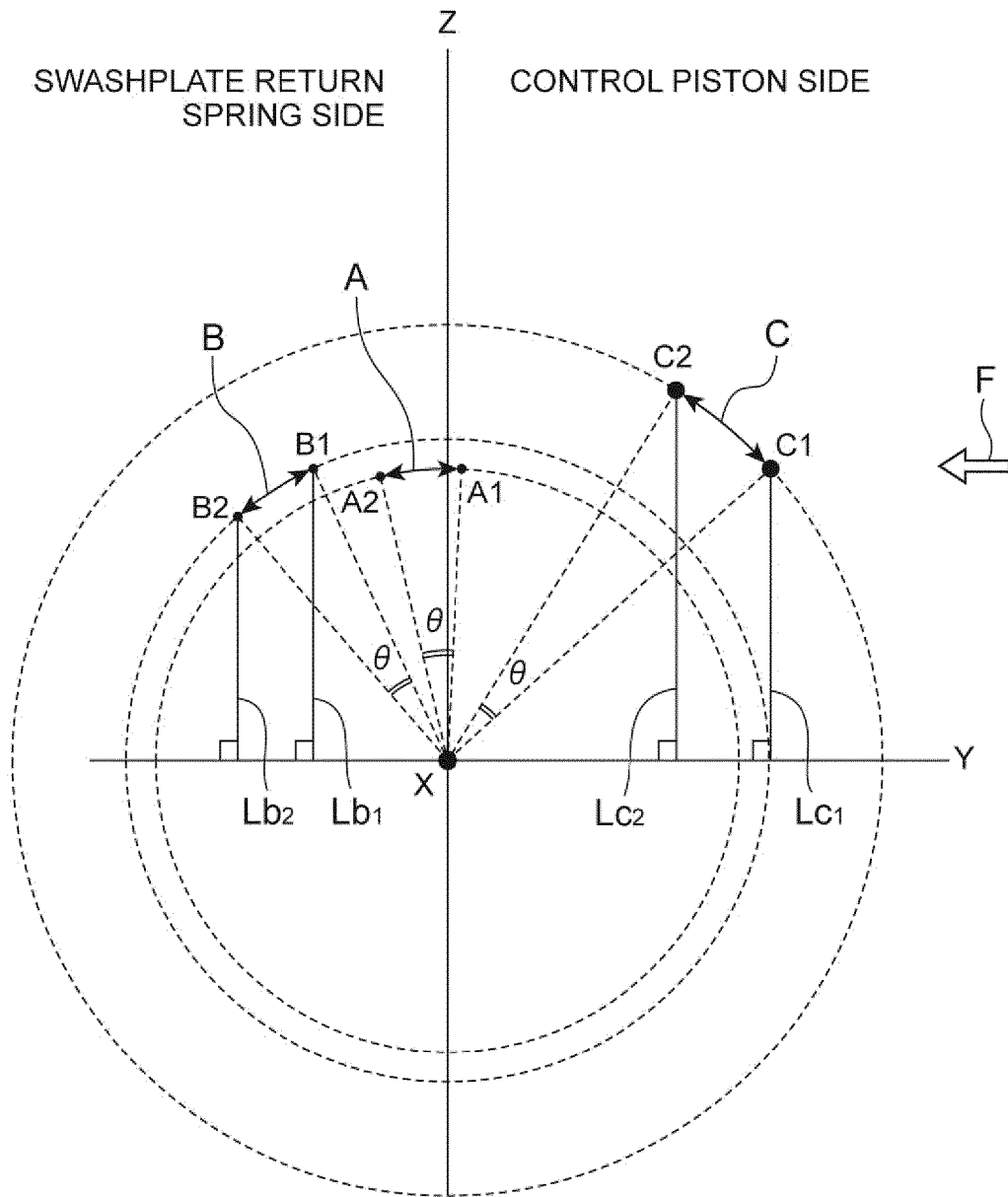


Fig.8

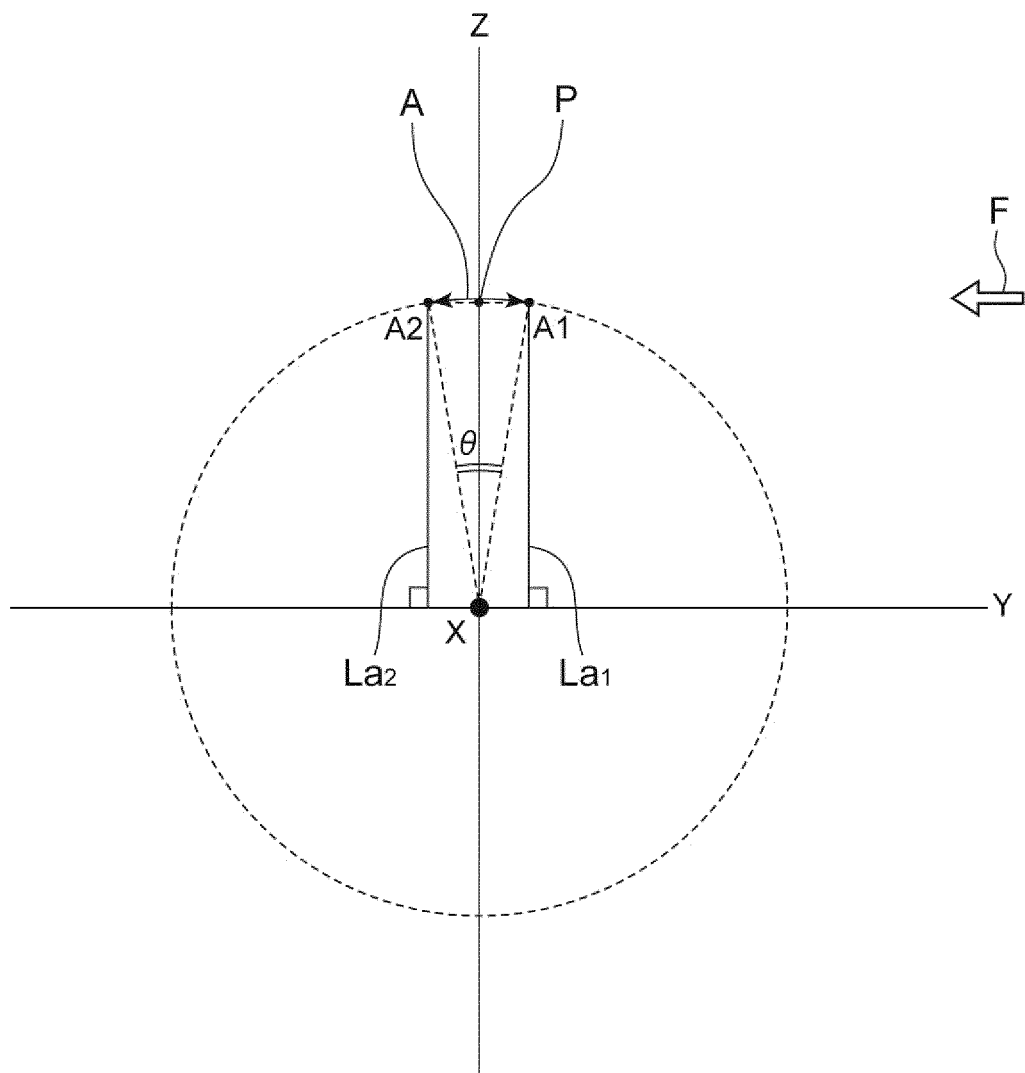


Fig.9

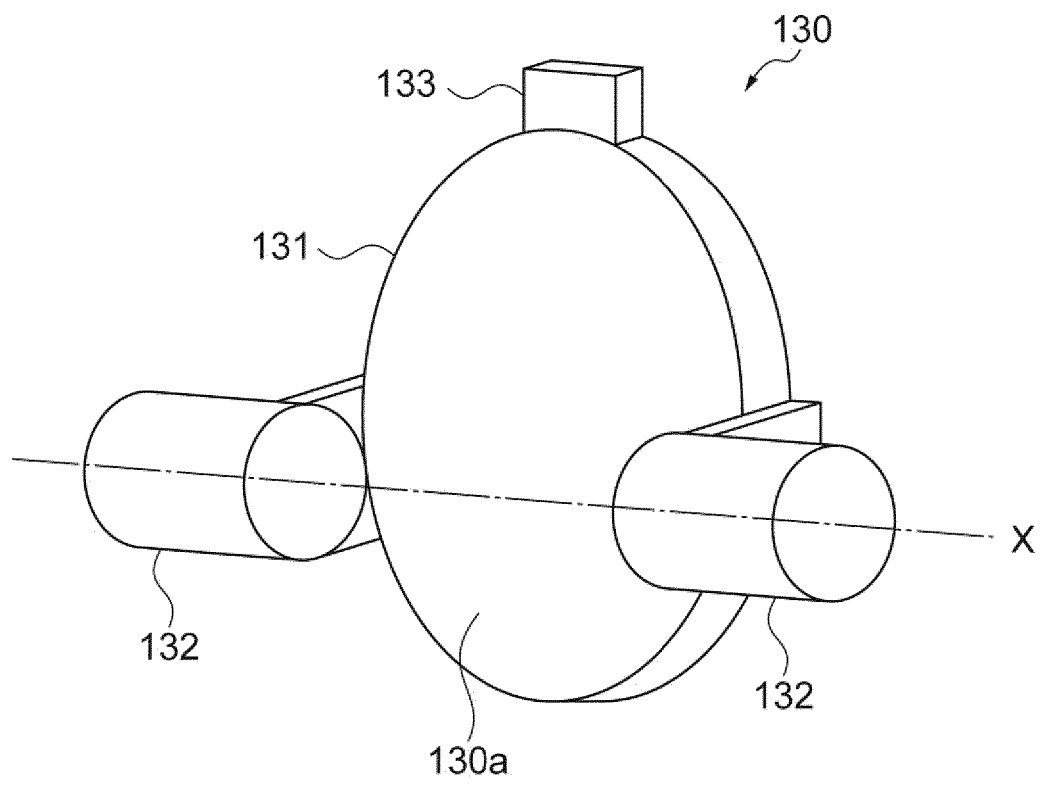
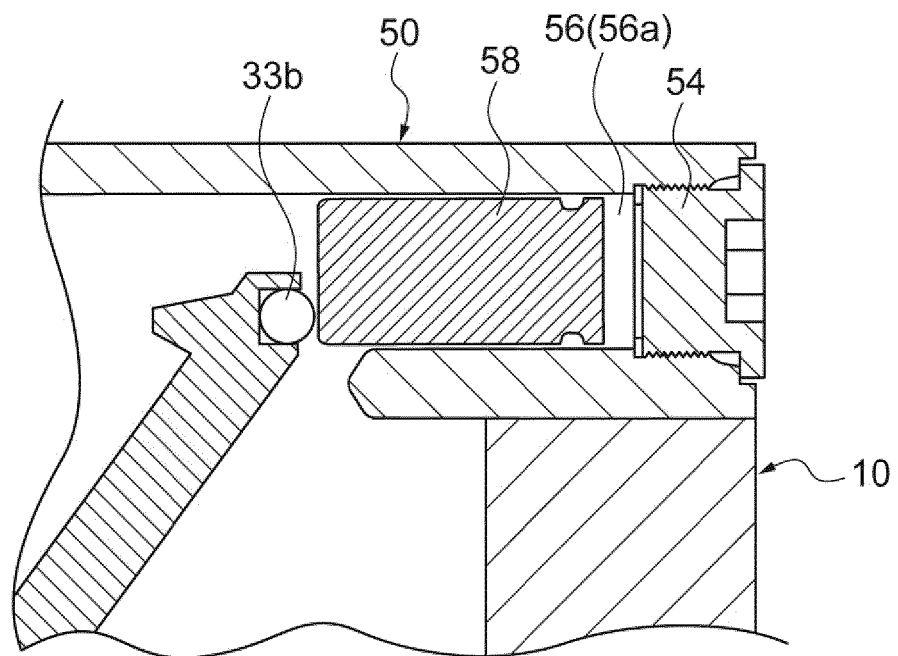


Fig.10



REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- JP 2006348911 A [0002]
- JP S63121781 U [0003]
- US 2006123984 A1 [0003]