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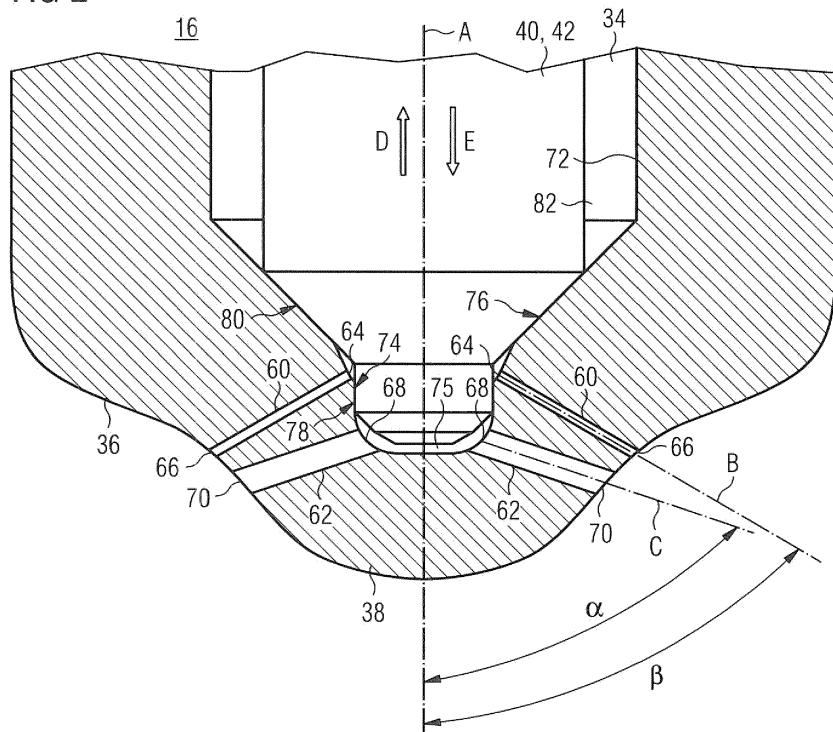
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(54) FUEL INJECTOR FOR A DUAL FUEL ENGINE

(57) A fuel injector (16) for a common rail fuel system (12) is disclosed. The fuel injector (16) comprises a nozzle body (36) extending along a central longitudinal axis (A), and including a central bore (34) having a first cylindrical sealing face (74). The fuel injector (16) further comprises at least one first injection hole (60) extending from a first inlet (64) being spaced apart from the first cylindri-

cal sealing face (74). The fuel injector (16) further comprises at least one second injection hole (62) extending from a second inlet (68) being spaced apart from the first cylindrical sealing face (74). The fuel injector (16) is particularly suitable for use in a dual fuel internal combustion engine.

FIG 2



Description**Technical Field**

[0001] The present disclosure generally relates to fuel injection systems and methods for operating the same. Particularly, the present disclosure relates to a fuel injector, a dual fuel internal combustion engine, and a method for operating the fuel injector.

Background

[0002] Dual fuel engines are capable of running on gaseous fuel or liquid fuel or a combination of both, thereby allowing to fulfil increased emission standards. Typically, dual fuel engines are operable at least in a liquid fuel mode (LFM) and a gaseous fuel mode (GFM). Herein, a dual fuel engine running on liquid fuel (for example diesel fuel, light fuel oil (LFO), heavy fuel oil (HFO), liquid bio fuel (LBF), or crude oil (CRO)) is referred to as running in the liquid fuel mode (LFM). A dual fuel engine running on gaseous fuel (for example natural gas or biogas) is referred to as running in the gaseous fuel mode (GFM). Exemplary fields of applying dual fuel engines include the global marine industry and power generation systems.

[0003] Dual fuel types of internal combustion engines are usually based on diesel engines. The cycle of an exemplary four stroke diesel engine comprises an intake stroke, a compression stroke, a power stroke, and an exhaust stroke.

[0004] In LFM, dual fuel engines may operate like diesel engines. The dual fuel engine combusts liquid fuel by compressing a mixture of air and fuel (compression stroke) to a point where the liquid fuel is injected and ignited by the heating which accompanies the compression.

[0005] In GFM, the gaseous fuel-air mixture does not self-ignite when it is compressed during the compression stroke. Different types of dual fuel engines were developed to overcome this problem.

[0006] In some types of dual fuel engines, the ignition source may be provided by a spark plug similar to those used in spark ignited engines to trigger the power stroke.

[0007] In other types of dual fuel engines, the ignition source is provided by injecting a small amount of igniting liquid fuel (for example diesel fuel) with a fuel injector into the compressed mixture of air and gaseous fuel at the end of the compression stroke and/or the beginning of the power stroke. Typically, in GFM, an individual ignition fuel injector separate from a liquid fuel injector used for LFM provides the small amount of liquid ignition fuel. Within the compressed mixture of air and gaseous fuel, the small amount of liquid fuel ignites, which in turn ignites the mixture of air and gaseous fuel for the combustion process during the power stroke.

[0008] For example, a fuel injector for a diesel engine is disclosed in US 6,725,838 of Caterpillar Inc. The fuel

injector is capable of injecting fuel for a homogeneous charge compression ignition injection event, which is a conventional injection event. The fuel injector also has a mixed mode that includes a homogeneous charge compression ignition injection and a conventional injection in a single compression stroke for the engine.

[0009] The present disclosure is directed, at least in part, to improving or overcoming one or more aspects of prior systems.

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Summary of the Disclosure

[0010] In one aspect, a fuel injector for a common rail fuel system is disclosed. The fuel injector comprises a nozzle body extending along a central longitudinal axis, and including a central bore having a first cylindrical sealing face circumferentially extending about the central longitudinal axis. The fuel injector further comprises at least one first injection hole extending from a first inlet in the central bore. The first inlet is spaced apart from the first cylindrical sealing face in a first direction along the central longitudinal axis. The fuel injector further comprises at least one second injection hole extending from a second inlet in the central bore. The second inlet is spaced apart from the first cylindrical sealing face in a second direction along the central longitudinal axis opposite the first direction. The fuel injector further comprises a needle member slidably arranged in the central bore between a first position and a second position, the needle member including a second cylindrical sealing face circumferentially extending about the central longitudinal axis and being configured to sealingly contact the first cylindrical sealing face in the first position, and to be spaced apart from the first cylindrical sealing face in the first direction in the second position.

[0011] In another aspect, a dual fuel internal combustion engine is disclosed. The dual fuel internal combustion engine is configured to operate in a liquid fuel mode and in a gaseous fuel mode. A liquid fuel is used in the gaseous fuel mode for igniting a mixture of air and gaseous fuel. The dual fuel internal combustion engine comprises at least one fuel injector as exemplary disclosed herein.

[0012] In yet another aspect, a method for operating the fuel injector as exemplary disclosed herein is provided. The method comprises operating the fuel injector in a first operation mode by moving the needle member between the first position and an intermediate position situated between the first position and the second position such that a fuel is injected through the at least one first injection hole only. The method further comprises operating the fuel injector in a second operation mode by moving the needle member between the first position and the second position such that the fuel is injected through the at least one first injection hole and the at least one second injection hole.

[0013] Other features and aspects of this disclosure will be apparent from the following description and the

accompanying drawings.

Brief Description of the Drawings

[0014] The accompanying drawings, which are incorporated herein and constitute a part of the specification, illustrate exemplary embodiments of the disclosure and, together with the description, serve to explain the principles of the disclosure. In the drawings:

Fig. 1 shows a schematic drawing of a portion of a dual fuel internal combustion engine, particularly a portion of a fuel system of the dual fuel internal combustion engine, according to the present disclosure.

Fig. 2 shows a cut view through a nozzle portion of a fuel injector in a closed position, according to the present disclosure.

Fig. 3 shows a cut view through the nozzle portion of the fuel injector in an intermediate, partially opened position, according to the present disclosure.

Fig. 4 shows a cut view through the nozzle portion of the fuel injector in a (fully) opened position, according to the present disclosure.

Fig. 5A shows a first graph indicating a fuel flow rate over time through the fuel injector according to the present disclosure, and Fig. 5B shows a second graph indicating a lift of a needle member of the fuel injector over time according to the present disclosure. Fig. 5A and Fig. 5B correspond to each other with respect to the time axes.

Detailed Description

[0015] The following is a detailed description of exemplary embodiments of the present disclosure. The exemplary embodiments described therein and illustrated in the drawings are intended to teach the principles of the present disclosure, enabling those of ordinary skill in the art to implement and use the present disclosure in many different environments and for many different applications. Therefore, the exemplary embodiments are not intended to be, and should not be considered as, a limiting description of the scope of patent protection. Rather, the scope of patent protection shall be defined by the appended claims.

[0016] The present disclosure is based in part on the realization that although an amount of liquid fuel required in LFM may be considerably larger than an amount of liquid fuel required in GFM, for example by a factor within a range between 50 and 200, it may be possible to use a specifically configured liquid fuel injector for both LFM and GFM. In other words, an additional ignition fuel injector for GFM can be omitted.

[0017] According to the present disclosure, the liquid fuel injector is usable for both LFM and GFM due to a particular configuration of a nozzle portion and a needle member of the fuel injector. Particularly, the fuel injector

is configured to provide a small amount of liquid fuel in GFM via at least one first injection hole. The fuel injector is further configured to provide a large amount of liquid fuel in LFM via the at least one first injection hole and at least one second injection hole. That behaviour of the fuel injector is enabled by a specific configuration of a needle tip of the fuel injector's needle member cooperating with a specific configuration of a tip section of the fuel injector's central bore.

[0018] The present disclosure is further based in part on the realization that the fuel injector, which is operable for both LFM and GFM in a dual fuel internal combustion engine, may be also suitable for use in other internal combustion engines where different injection patterns for different operation modes are desired.

[0019] Still further, the present disclosure is based in part on the realization that the fuel injector is particularly suitable for use in large internal combustion engines, more particularly large internal dual fuel internal combustion engines, having a power output of more than 150 kW per cylinder. In those large dual fuel engines, an absolute difference between a large amount of liquid fuel required in LFM, and a small amount of liquid fuel required in GFM may be considerably large. As a result, it is typically not possible to use a conventional fuel injector for both LFM and GFM by controlling the fuel injector to inject liquid fuel for a very short duration in GFM to achieve the required small amount, and to inject liquid fuel for a longer duration in LFM to achieve the required large amount. Instead, those large dual fuel engines conventionally require two separate fuel injectors, one for LFM and the other one for GFM.

[0020] Referring to Fig. 1, a portion of a dual fuel internal combustion engine 10 is depicted. Particularly, a portion of a fuel system 12 of the dual fuel internal combustion engine 10 is shown.

[0021] The dual fuel internal combustion engine 10 may include features not shown, such as air systems, cooling systems, peripheries, drivetrain components, etc. Furthermore, the engine 10 may be of any size, with any number of cylinders, and in any configuration (e.g., "V," in-line, radial, etc.). The engine 10 may be used to power any machine or other device, including locomotive applications, on-highway trucks or vehicles, off-highway trucks or machines, earth moving equipment, generators, aerospace applications, marine applications, offshore applications, pumps, stationary equipment, or other engine powered applications.

[0022] In the shown embodiment, the dual fuel engine 10 is a large internal combustion engine having a power output of at least 150 kW per cylinder. The dual fuel engine 10 is capable to run in a liquid fuel mode (LFM), and in a gaseous fuel mode (GFM). In GFM, a liquid fuel, for example diesel fuel, is used as ignition fuel. However, as noted above, it is also contemplated that the engine 10 may be any other type of engine (diesel fuel, gas fuel, etc.), and in any other size, where a fuel injector with different injection patterns for different operation modes

is desired.

[0023] The fuel system 12 comprises a common rail 14, and a plurality of fuel injectors 16 (only one of which is shown in Fig. 1), one for each cylinder of the dual fuel internal combustion engine 10. The fuel injector 16 is accommodated in a cylinder head 18 of the dual fuel internal combustion engine 10.

[0024] The common rail 14 of a common rail system not shown in further detail runs at the outside of the cylinder head 18, although it may also be arranged to run either inside the cylinder head 18 or above the cylinder head 18. The common rail 14 is fluidly connected to the fuel injector 16 via a connection line 20 to provide high pressure fuel (for example diesel fuel, LFO, HFO, LBF, CRO) to the fuel injector 16. For example, the connection line 20 at least partially runs inside the cylinder head 18 and/or near a top of the cylinder head 18.

[0025] The fuel injector 16 comprises an accumulator 22, a flow limiter 24, an injection unit 26, and a control valve 28.

[0026] The accumulator 22 is fluidly connected to the common rail 14 via the connection line 20. The accumulator 22 receives high pressure fuel from the common rail 14. In the shown embodiment, the accumulator 22 is housed in the fuel injector 16, however, in other embodiments, the accumulator 22 may be fluidly connected upstream of the fuel injector 16. The accumulator 22 may be an elongated pressure vessel arranged in a back portion of the fuel injector 16, for example extending along a longitudinal axis of the fuel injector 16.

[0027] The flow limiter 24 is fluidly connected downstream of the accumulator 22. Specifically, the flow limiter 24 is arranged in a fuel supply line 30 extending between the high pressure fuel accumulator 22 and the injection unit 26 of the fuel injector 16. The flow limiter 24 operates to ensure that fuel is injected into the cylinder only when such is desired. For example, the flow limiter 24 may detect changes in flow pressure and may adjust the fuel flow in case of abnormal pressure drop conditions. In one example, the flow limiter 24 blocks supply of liquid fuel from the accumulator 22 to the injection unit 26 if the injection unit 26 is leaking.

[0028] The injection unit 26 comprises a fuel injector body 32 with a central bore or fuel space 34. The central bore 34 accommodates several elements of the injection unit 26 as described below. The fuel injector body 32 further includes a nozzle body 36 of a nozzle tip 38. The nozzle body 36 is arranged at a (front) end of the fuel injector body 32. The nozzle tip 38 faces a combustion chamber of the engine cylinder of the dual fuel engine 10. The nozzle tip 38 is provided with a plurality of fuel injection holes for injecting liquid fuel into the combustion chamber as described in more detail with reference to Figs. 2 to 4 later on.

[0029] The injection unit 26 further comprises a needle member 40 arranged centrally in the central bore 34. The needle member 40 is slidably arranged in the central bore 34. A front or first end portion 42 of the needle member

40 is configured to block or allow a fluid flow from the central bore 34 into the fuel injection holes depending on a position of the needle member 40 (the needle member first end portion 42).

[0030] In some embodiments, the needle member is a one-piece needle member. In other embodiments, the needle member 40 is formed by an outer needle member surrounding an inner needle member, wherein the outer needle member and the inner needle member may be 10 slidable relative to each other.

[0031] Furthermore, in some embodiments, the needle member 40, specifically the needle member first end portion 42, is formed as a solid body. Stated differently, the needle member 40 or the needle member first end portion 15 42 does not include any inner fuel channels.

[0032] A second end portion 46 of the needle member 40, which is positioned opposite to the first end portion 42, is slidably arranged within a collar or bushing 44. The collar 44 and the end portion 46 together define a, for 20 example cylindrical, pressure chamber 48 disposed within the central bore 34. The pressure chamber 48 is fluidly connected to the accumulator 22 via the fuel line 30, and a valve orifice plate 50 of the injection unit 26. Normally, a fuel pressure within the pressure chamber 48 is equal 25 to the full fuel pressure. The fuel pressure of the pressure chamber 48 acts on the rear end portion 46 of the needle member 40, and urges the needle member 40 in a direction to the nozzle tip 38. Thereby, the needle member 40 is pushed against a needle member seat, and fuel is inhibited from flowing through the injection holes for injection into the combustion chamber.

[0033] A spring 52 is arranged below the collar 44 between a shoulder of the needle member 40 and a front end of the collar 44 to bias the collar 44 against the valve orifice plate 50. The central bore 34 is fluidly connected 35 with the accumulator 22 via the fuel line 30 and the flow limiter 24 such that the full fuel pressure acts on all faces of the needle member 40. The needle member 40 is configured such that the fuel pressure in the central bore 34 40 surrounding the needle member 40 tends to lift the needle member 40 upwards away from the nozzle tip 38. However, the force originating from the full fuel pressure acting 45 onto the end of the needle member in the chamber 48 keeps the needle member 40 closed irrespective of the opposite force created by the fuel pressure acting on the needle member 40 in the central bore 34.

[0034] The operation of the injection unit 26 (the fuel injector 16) is controlled by the control valve 28. The control valve 28 opens, for example by means of a solenoid, 50 when a fuel injection event is desired. The control valve 28 is communicatively connected to a control unit 54 schematically indicated by a box in Fig. 1. The control unit 54 may activate the control valve 28 to open a flow connection from the chamber 48 via the valve orifice plate 50 and a fuel line 56 to a low pressure fuel reservoir 58. Said flow connection reduces the pressure in the chamber 48 such that the fuel pressure in the central bore 34 55 acting onto the needle member 40 lifts the needle mem-

ber 40 to start an injection event. To end an injection event, the control unit 54 allows the control valve 28 to return to its rest position (closed position). For example, a solenoid current supplied to a solenoid of the control valve 28 may be cut off. Then, the control valve 28 blocks the flow from the chamber 48 to the low pressure fuel reservoir 58. As a result, the flow connection from the accumulator 22 to the low pressure fuel reservoir 58 via the chamber 48 and the valve orifice plate 50 is cut off. The chamber 48 is pressurized again, and the needle member 40 is urged in its seated position again to block a fuel flow to the injection holes provided in the nozzle tip 38.

[0035] Referring to Fig. 2, a front section of the injection unit 26 of the fuel injector 16 is depicted.

[0036] As can be seen, the nozzle body 36 extends along a central longitudinal axis A and includes the central bore 34. A plurality of first injection holes 60 (two of which are shown in Fig. 2) and a plurality of second injection holes 62 (two of which are shown in Fig. 2) extend through the nozzle tip 38 of the nozzle body 36. Specifically, the first injection holes 60 extend between first inlets 64 and first outlets 66 along first injection hole axes B. Similarly, the second injection holes 62 extend between second inlets 68 and second outlets 70 along second injection hole axes C. The first and second inlets 64 and 68 open into a front end section of the central bore 34. More specifically, the first inlets 64 are spaced apart from the second inlets 68 in a first direction D of the central longitudinal axis A (a direction from the nozzle tip 38 to the rear end 46 of the needle member 40 (see Fig. 1)). The first and second outlets 66 and 70 open into the combustion chamber of the respective cylinder, in other words, to an exterior of the fuel injector 16. In some embodiment, the first outlets 66 may open into the second injection holes 62.

[0037] As one skilled in the art will appreciate, a number of the first injection holes 60 and a number of the second injection holes 62 may depend on various factors, for example flow cross-sectional area, fuel pressure, and engine configuration. For example, the number of the first injection holes 60 may be within a range between 1 and 10, and/or the number of the second injection holes 62 may be within a range between 1 and 10.

[0038] In some embodiments, a plurality of first injection holes 60 may be provided. The first inlets 64 may be arranged in a distributed manner in a plurality of bands. The bands extend circumferentially about the central longitudinal axis A and are spaced apart from each other in the first direction D (do not entirely overlap each other). For example, one inlet of the first inlets 64 may be arranged in a first band, whereas another inlet of the first inlets 64 may be arranged in a second band spaced apart from the first band in the first direction D.

[0039] Similarly, in some embodiments, a plurality of second injection holes 62 may be provided. The second inlets 68 may be arranged in a distributed manner in a plurality of bands. The bands extend circumferentially

about the central longitudinal axis A and are spaced apart from each other in the first direction D (do not entirely overlap each other). For example, one inlet of the second inlets 68 may be arranged in a third band, whereas another inlet of the second inlets 68 may be arranged in a fourth band spaced apart from the third band in the first direction D.

[0040] As is described in more detail later on with reference to Figs. 2 to 5, the first injection holes 60 are used for injecting the ignition fuel in GFM. On the other hand, in LFM, the first and second injection holes 60 and 62 are used for injecting fuel.

[0041] As can be seen from the schematic drawing of Fig. 2, the first injection holes 60 have a smaller flow cross-sectional area than the second injection holes 62, because considerably less liquid fuel is required in GFM. More generally, the first injection holes 60 together define a total flow cross-sectional area being smaller than a total flow cross-sectional area defined by all second injection holes 62. For example, the total flow cross-sectional area of the second injection holes 62 may be greater than the total flow cross-sectional area of the first injection holes 60 by a factor within a range between about 5 and about 100, particularly 5 to 10, more particularly by a factor of about 7.5.

[0042] Further, each first injection hole axis B and the central longitudinal axis A confine a first acute angle α (also referred to as injection angle of the first injection holes 60). Similarly, each second injection hole axis C and the central longitudinal axis A confine a second acute angle β (injection angle of the second injection holes 62).

[0043] In some embodiments, for example as shown in Fig. 2, the first acute angle α of the first injection holes 60 is smaller than the second acute angle β of the second injection holes 62. The reason is that the first injection holes 60 are provided for injecting the ignition fuel into the combustion chamber in GFM, which is typically performed before a respective piston reaches the top dead center, for example, about 10° to 20° before the top dead center. In contrast, the fuel injection in LFM is mainly performed by the second injection holes 62, which typically starts when the piston is already closer to the top dead center compared to GFM. Accordingly, at the start of the liquid fuel injection, the combustion chamber may have greater volume in GFM than in LFM. Therefore, the injection angle α defined by the first injection holes 60 can be made smaller than the injection angle β defined by the second injection holes 62 while ensuring that the injected fuel is not directly injected onto a heated top face of the piston which is generally undesirable as one skilled in the art will appreciate. For example, the injection angle α may be within a range from 0° to 90°, particularly between 25° and 80°, and/or the injection angle β may be within a range from 0° to 90°, particularly between 45° and 85°.

[0044] In some embodiments, the injection angles α may differ between different first injection holes 60. In other words, the injection angles α may be not equal for

all first injection holes 60. Additionally or alternatively, the injection angles β may differ between different second injection holes 62. Stated differently, the injection angles β may be not equal for all second injection holes 62.

[0045] Furthermore, in the embodiment depicted in Fig. 2, the two shown first injection holes 60 and the two shown second injection holes 62 are positioned at equal positions with respect to a circumferential direction about the central longitudinal axis A. In other words, the first injection hole axes B and the second injection hole axes C and the central longitudinal axis A lie in the same plane (the paper plane of Fig. 2). However, in some embodiments, the first injection holes 60 (the first injection hole axes B) and the second injection holes 62 (the second injection hole axes C) may be arranged spaced apart from each other in the circumferential direction about the central longitudinal axis A. Stated differently, the first injection hole axis B and the second injection hole axis C and the central longitudinal axis A may not share a common plane. Those embodiments may provide an improved rigidity of the needle first end portion 42. Additionally, those embodiments allow to provide the first outlets 66 closer to the second outlets 70 in the second direction E of the central longitudinal axis A. Still further, those embodiments also allow to provide the first outlets 66 spaced apart from the second outlets 70 in the first direction D of the central longitudinal axis such that the first injection angle α would be greater than the second injection angle β , which might be desirable in some embodiments.

[0046] The central bore 34 includes an inner circumferential face 72 extending circumferentially about the central longitudinal axis A. The inner circumferential face 72 comprises a first cylindrical sealing face 74, and a first conical sealing face 76. The cylindrical sealing face 74 extends along the central longitudinal axis A as a cylinder jacket. Further, the cylindrical sealing face 74 is formed as a circumferential face of a blind hole section 75 of the central bore 34. The blind hole section 75 constitutes an end portion of the central bore 34 in a region of the needle tip 38. For example, the cylindrical sealing face 74 may have a circular cross-section. The first conical sealing face 76 extends along the central longitudinal axis A, and tapers in the second direction E of the central longitudinal axis A opposite the first direction D (the second direction E is a direction from the rear end 46 of the needle member 40 (see Fig. 1) to the nozzle tip 38).

[0047] In the shown embodiment, the first conical sealing face 76 is arranged spaced apart from the first inlets 64 of the first injection holes 60 in the first direction D. Additionally or alternatively, for example, at least one of the first inlets 64 may open into the first conical sealing face 76.

[0048] The first cylindrical sealing face 74 is arranged between the first inlets 64 and the second inlets 68 with respect to a direction of the central longitudinal axis A. Specifically, the first inlets 64 are spaced apart from the first cylindrical sealing face 74 in the first direction D of

the central longitudinal axis A, and the second inlets 68 are spaced apart from the first cylindrical sealing face 74 in the second direction E of the central longitudinal axis A. Stated differently, the first inlets 64 are displaced from the first cylindrical sealing face 74 in the first direction D, and the second inlets 68 are displaced from the first cylindrical sealing face 74 in the second direction E.

[0049] Similarly, the needle member 40 includes a second cylindrical sealing face 78 and a second conical sealing face 80. In the shown embodiment, the second cylindrical sealing face 78 is positioned adjacent to the second conical sealing face 80.

[0050] The first cylindrical sealing face 74 and the second cylindrical sealing face 78 are configured to mate with each other for providing a sealing engagement between both faces 74 and 78 when the needle member 40 is in a closed position as shown in Fig. 2, and in an intermediate position as shown in Fig. 3. For obtaining the desired sealing effect while allowing a smooth sliding

movement between both faces 74, 78 until both faces 74, 78 eventually lose contact (disengage), for example, as shown in Fig. 4, a distance between both faces measured in a radial direction of the central longitudinal axis (in a plane perpendicular to the central longitudinal axis A) may be smaller than about 10 μm , particularly smaller than about 5 μm , more particularly about 3 μm , or even smaller. In some embodiments, the clearance may be as small as manufacturing and assembly tolerances allow.

[0051] Similarly, the first conical sealing face 76 and the second conical sealing face 80 are configured to mate with each other such that the second conical sealing face 76 sealingly contacts the first conical sealing face when the needle member 40 is in the closed position as shown in Fig. 2. The first conical sealing face 76 serves as a seating face for the needle member 40.

[0052] In some embodiments, the at least one second injection hole 62 may include an inlet that is arranged in a cylindrical face extending from the first cylindrical sealing face 74 in the second direction E. Said cylindrical face 40 may have the same diameter or circumference as the first cylindrical sealing face 74.

[0053] Referring to Figs. 1 to 5, the operation of the fuel injector 16 is explained in the following. As noted above, the operation and actuation of the fuel injector 16 is controlled by the control unit 54.

[0054] The fuel injector 16 is in a closed position (first position) as shown in Fig. 2 when no fuel injection into the combustion chamber is desired. In the closed position, the conical sealing face 80 of the needle member 40 sealingly contacts the conical sealing face 76 of the nozzle body 36. As a result, liquid fuel present in an annular fuel supply passage 82 of the central bore 34 cannot flow to the first injection holes 60 and second injection holes 62. The fuel supply passage 82 is positioned adjacent to the first conical sealing face 76 in the first direction D.

[0055] In case a liquid fuel injection through the first injection holes 60 only is desired (for example in GFM),

the needle member 40 is caused to move in the first direction D as shown in Fig. 3 without reaching the fully opened position as shown in Fig. 4. In other words, the needle member 40 continuously travels from the fully closed position as shown in Fig. 2 in the direction D as shown in Fig. 3, but ends travel in the first direction D before reaching the fully opened position as shown in Fig. 4 to return to the fully closed position as shown in Fig. 2. In an intermediate position (third position) as shown in Fig. 3, the conical sealing face 80 of the needle member 40 and the conical sealing face 76 of the nozzle body 36 are spaced apart from each other in the first and second directions D and E. Thus, liquid fuel can flow from the fuel supply passage 82 to the first injection holes 60, and through the first injection holes 60 into the combustion chamber. It is noted that, as shown in Fig. 3, the first cylindrical sealing face 74 of the nozzle body 36 and the second cylindrical sealing face 78 of the needle member 40 still sealingly contact each other in the intermediate position such that the liquid fuel is blocked from flowing to the second inlets 68 of the second injection holes 62.

[0056] In case a liquid fuel injection through the first injection holes 60 and the second injection holes 62 is desired (for example in LFM), the needle member 40 is caused to move into the fully opened position (second position) as shown in Fig. 4. Here, the fuel supply passage 82 is fluidly connected to both the first injection holes 60 and the second injection holes 62, because neither the sealing faces 76 and 80 are in sealing contact with each other nor the sealing faces 74 and 78 are in sealing contact with each other.

[0057] As used herein, the term "blocked" refers to a situation, in which a fuel flow is substantially blocked, including a small leakage due to, for example, manufacturing and assembling tolerances.

[0058] The operation of the fuel injector 16 is also shown in Figs. 5A and 5B. Fig. 5A shows a first graph indicating a fuel flow injected by the fuel injector 16 (axis of ordinate) over time (axis of abscissa). Fig. 5B shows a second graph indicating a lift of the needle member 40 of the fuel injector 16 (axis of ordinate) over time (axis of abscissa) according to the present disclosure. The time axes of both Fig. 5A and Fig. 5B correspond to each other.

[0059] Figs. 5A and 5B particularly show a fuel flow rate injected by the fuel injector 16 (Fig. 5A) and a lifting motion of the needle member 40 (Fig. 5B) obtained in a full lift operation of the fuel injector 16. In other words, in Figs. 5A and 5B, operation of the fuel injector 16 during LFM is shown, in which the needle member 40 is caused to slide between the first end position as shown in Fig. 2 and the second end position as shown in Fig. 4.

[0060] The valve is actuated at a time x1. The needle member 40 starts to lift from the closed position as shown in Fig 2. The conical sealing faces 76 and 80 are no longer in sealing engagement, and the conical sealing face 80 of the needle member 40 moves away from the conical sealing face 76 of the nozzle body 36 in the first direction D. A liquid fuel from the fuel supply passage 82 of the

central bore 34 flows along the sealing faces 76, 80, reaches the first injection holes 60, and is injected via the first injection holes 60 into the combustion chamber. The liquid fuel flow rate increases until a time x2. From this time, the fuel flow rate is limited by the flow cross-sectional area of the first injection holes 60. The time x2 may be reached at a lift of the needle member 40 of, for example, 10 % of a total lift of the needle member 40.

[0061] The needle member 40 then continues to move away from the first conical sealing face 76 of the nozzle body 36, and the fuel injector 16 continues to inject liquid fuel at a constant flow rate until a time x3. Thereby, the needle member 40 also passes an intermediate position as shown in Fig. 3.

[0062] In case the engine 10 is operated in GFM, actuation of the fuel injector 16 is stopped at or before the time x3. For example, solenoid current supplied to the solenoid of the control valve 28 is stopped. The needle member 40 then stops travelling away from the first conical sealing face 76, reverses its moving direction to move in the second direction E, and moves back to its closed position as indicated by dashed lines in Figs. 5A and 5B. As a result, the flow rate reduces until zero when the sealing faces 76 and 80 reach the sealing engagement again. The fuel injector 16 is now ready for the next actuation cycle. It should be noted, that during GFM (more generally, a first operation mode of the fuel injector 16 and the engine 10), the fuel injector 16 is controlled such that the needle member 40 moves only a part of its full possible lift during one actuation cycle. It was found that needle member lifts within a range between about 15% and about 70%, particularly between about 20% and about 55%, more particularly about 25%, are suitable. However, other partial lifts below 100% of the full possible lift of the needle member 40 are also contemplated.

[0063] In case the engine 10 is operated in LFM (shown as solid lines in Figs. 5A and 5B), actuation of the fuel injector 16 is not stopped at or before the time x3. Instead, the control valve 28 continues to cause the needle member 40 two move in the first direction D. As a result, the first and second cylindrical sealing faces 74 and 78 are no longer in sealing engagement from the time x3 on. Thus, fuel from the fuel supply passage 82 is allowed to flow to the second injection holes 62, too. Specifically, liquid fuel from the fuel supply passage 82 of the central bore 34 flows along the sealing faces 76, 80, reaches the first inlets 64 of the first injection holes 60, flows along the sealing faces 74, 78, reaches the second inlets 68 of the second injection holes 62, and is injected via the first and second injection holes 60, 62 into the combustion chamber. The liquid fuel flow rate increases until a time x5 shortly after a time x4, at which the needle member 40 reached its second position (see Fig. 4). The fuel injector is de-energized at a time x6, at which the needle member 40 is caused to move back from the second position (shown in Fig. 4) in the second direction E. As a result, the flow rate starts to decrease at a time x7 until the fuel flow is eventually stopped about a time x8, at

which the needle member 40 reached its closed position (first position) as shown in Fig. 2. Upon reaching the closed position, the fuel injector 16 is ready for the next actuation cycle.

[0064] Again, it should be noted that during LFM (more generally, a second operation mode of the fuel injector 16 and the engine 10), the fuel injector 16 is controlled such that the needle member 40 is caused to move the full possible lift during one actuation cycle. 5

[0065] The fuel injector 16 may be controlled such that a fuel injection amount in GFM (the first operation mode) may be within a range between 0.25% and 2%, particularly between 0.5% and 1.5%, of a rated full load fuel injection amount in LFM (the second operation mode) during one actuation cycle. 10

[0066] In some embodiments, the first operation mode may be used for pre-injections of a multiple injection strategy including a plurality of injection pulses. 15

Industrial Applicability

[0067] The fuel injector 16 as disclosed herein is applicable in internal combustion engines where different injection patterns for different operation modes are desired. As described in detail herein, the fuel injector 16 is particularly suitable for use in a dual fuel internal combustion engine configured to operate in LFM and GFM. 25

[0068] Terms such as "about", "around", "approximately", or "substantially" as used herein when referring to a measurable value such as a parameter, an amount, a temporal duration, and the like, is meant to encompass variations of $\pm 10\%$ or less, preferably $\pm 5\%$ or less, more preferably $\pm 1\%$ or less, and still more preferably $\pm 0.1\%$ or less of and from the specified value, insofar as such variations are appropriate to perform in the disclosed invention. It is to be understood that the value to which the modifier "about" refers is itself also specifically, and preferably, disclosed. The recitation of numerical ranges by endpoints includes all numbers and fractions subsumed within the respective ranges, as well as the recited endpoints. 35

[0069] Although the preferred embodiments of this invention have been described herein, improvements and modifications may be incorporated without departing from the scope of the following claims. 40

Claims

1. A fuel injector (16) for a common rail fuel system (12), comprising: 50

a nozzle body (36) extending along a central longitudinal axis (A), and including a central bore (34) having a first cylindrical sealing face (74) circumferentially extending about the central longitudinal axis (A); 55
at least one first injection hole (60) extending

from a first inlet (64) in the central bore (34), the first inlet (64) being spaced apart from the first cylindrical sealing face (74) in a first direction (D) along the central longitudinal axis (A), at least one second injection hole (62) extending from a second inlet (68) in the central bore (34), the second inlet (68) being spaced apart from the first cylindrical sealing face (74) in a second direction (E) along the central longitudinal axis (A) opposite the first direction (D); and a needle member (40) slidably arranged in the central bore (34) between a first position and a second position, the needle member (40) including a second cylindrical sealing face (78) circumferentially extending about the central longitudinal axis (A) and being configured to sealingly contact the first cylindrical sealing face (74) in the first position, and to be spaced apart from the first cylindrical sealing face (74) in the first direction (D) in the second position.

2. The fuel injector (16) of claim 1, wherein:

the needle member (40) is a one-piece needle member; and/or
the needle member (40) is formed as a solid body.

3. The fuel injector (16) of claim 1 or claim 2, wherein:

the central bore (34) further includes a first conical sealing face (76) circumferentially extending about the central longitudinal axis (A), the first conical sealing face (76) being spaced apart from the at least one first inlet (64) in the first direction (D); and

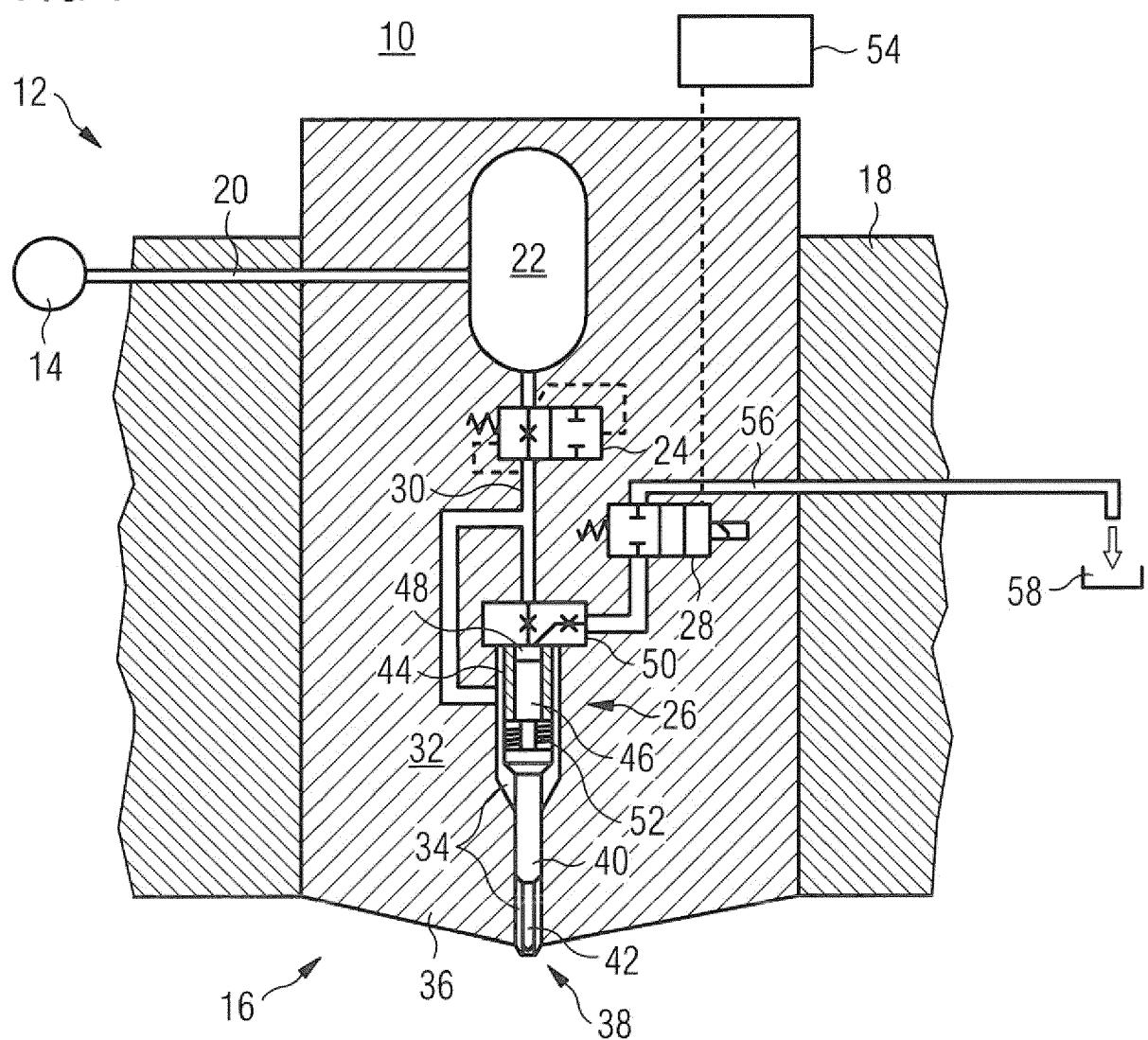
the needle member (40) further includes a second conical sealing face (80) circumferentially extending about the central longitudinal axis (A), the second conical sealing face (80) being configured to sealingly contact the first conical sealing face (76) in the first position, and to be spaced apart from the first conical sealing face (76) in the first direction (D) in the second position.

4. The fuel injector (16) of any one of the preceding claims, wherein the first injection hole (60) has a smaller flow cross-sectional area than the second injection hole (62).

5. The fuel injector (16) of any one of the preceding claims, wherein
the first injection holes (60) together define a first total flow cross-sectional area; and
the second injection holes (62) together define a second total flow cross-sectional area greater than the first total flow cross-sectional area.

6. The fuel injector (16) of claim 5, wherein the second total flow cross-sectional area is greater than the first total flow cross-sectional area by a factor within a range between about 5 and about 100.
7. The fuel injector (16) of any one of the preceding claims, wherein at least one first injection hole (60) extends along a respective first injection hole axis (B) intersecting the central longitudinal axis (A) to define a first acute angle (α) therebetween; at least one second injection hole (62) extends along a respective second injection hole axis (C) intersecting the central longitudinal axis (A) to define a second acute angle (β) therebetween, the second acute angle (β) being greater than the first acute angle (α). 10
8. The fuel injector (16) of any one of the preceding claims, wherein the at least one first injection hole (60) is arranged spaced apart from the at least one second injection hole (62) in a circumferential direction about the central longitudinal axis (A). 20
9. The fuel injector (16) of any one of the preceding claims, wherein a plurality of first injection holes (60) is provided, and the first inlets (64) of the first injection holes (60) are arranged in a distributed manner in a plurality of bands, which extend circumferentially about the central longitudinal axis (A) and are spaced apart from each other in the first direction (D). 25
10. The fuel injector (16) of any one of the preceding claims, wherein the central bore (34) includes a blind hole section (75) at one end thereof, and the first cylindrical sealing face (74) is formed as a circumferential face of the blind hole section (75). 35
11. The fuel injector (16) of any one of the preceding claims, wherein: 40
- in the first position, a fuel flow is blocked from flowing through the at least one first injection hole (60) and the at least one second injection hole (62); and/or
- in the second position, a fuel is allowed to flow through the at least one first injection hole (60) and the at least one second injection hole (62); and/or
- in a third position situated between the first position and the second position, the fuel is allowed to flow through the at least one first injection hole (60) and blocked from flowing through the at least one second injection hole (62). 45
12. A dual fuel internal combustion engine (10) operable in a liquid fuel mode and in a gaseous fuel mode, wherein a liquid fuel is used in the gaseous fuel mode for igniting a mixture of air and gaseous fuel, the dual 50
- fuel internal combustion engine (10) comprising at least one fuel injector (16) according to any one of the preceding claims.
5. 13. The dual fuel internal combustion engine (10) of claim 12, further comprising a control unit (54) controlling operation of the at least one fuel injector (16), wherein in the liquid fuel mode, the at least one fuel injector (16) is operated to move the needle member (40) between the first position and the second position such that the liquid fuel is injected through the at least one first injection hole (60) and the at least one second injection hole (62); and in the gaseous fuel mode, the at least one fuel injector (16) is operated to move the needle member (40) between the first position and an intermediate position only, the intermediate position being situated between the first position and the second position, such that the liquid fuel is injected through the at least one first injection hole (60) only. 15
14. The dual fuel internal combustion engine (10) of claim 13, wherein the intermediate position is defined by a lift of the needle member (40) within a range between 15% and 70%, particularly between 20% and 55% of a full lift defined between the first position and the second position. 20
- 30 15. A method for operating the fuel injector (16) of any one of claims 1 to 11, comprising:
- operating the fuel injector (16) in a first operation mode by moving the needle member (40) between the first position and an intermediate position situated between the first position and the second position such that a fuel is injected through the at least one first injection hole (60) only; and
- operating the fuel injector (16) in a second operation mode by moving the needle member (40) between the first position and the second position such that the fuel is injected through the at least one first injection hole (60) and the at least one second injection hole (62). 35

FIG 1



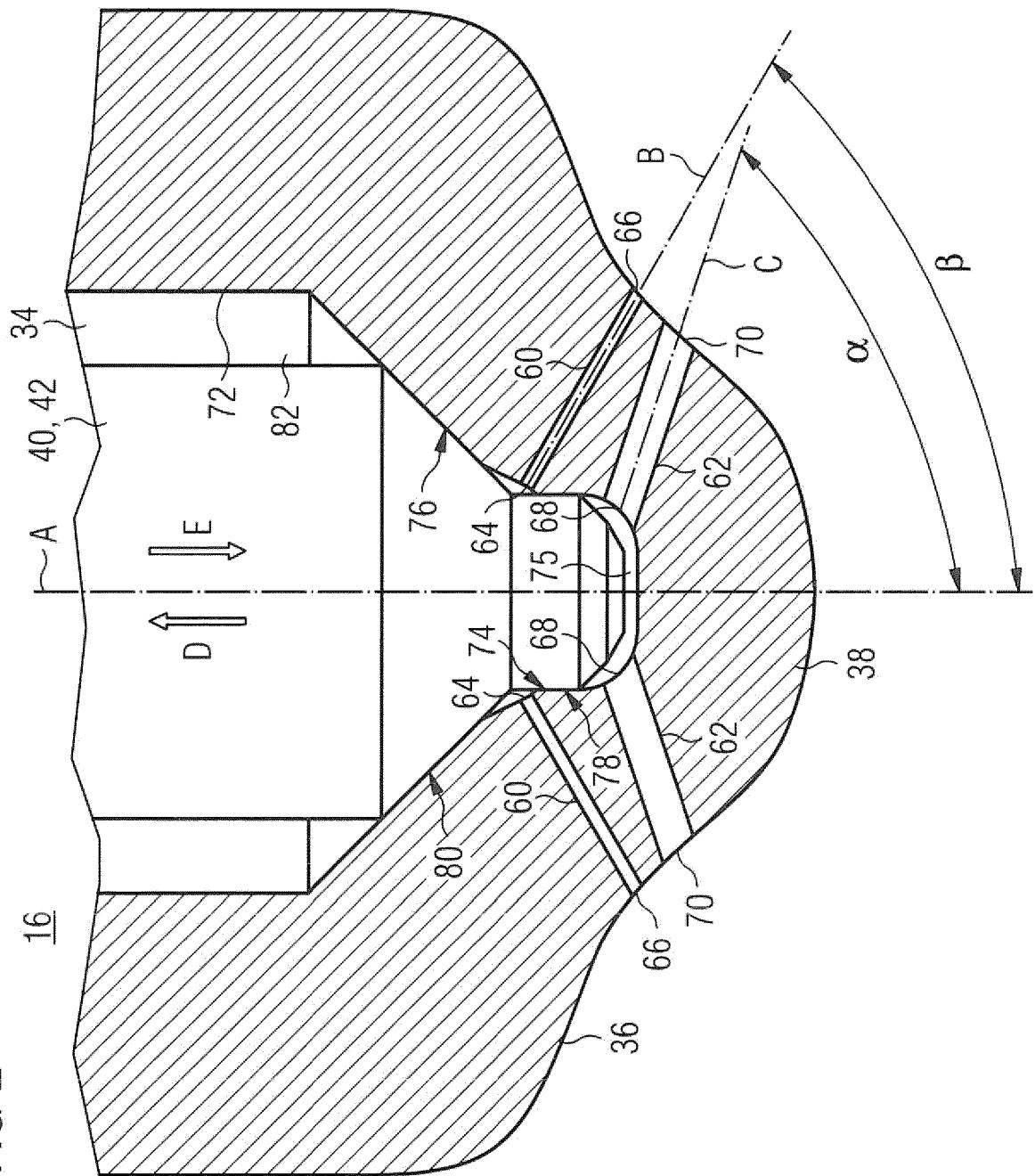


FIG 2

FIG 3

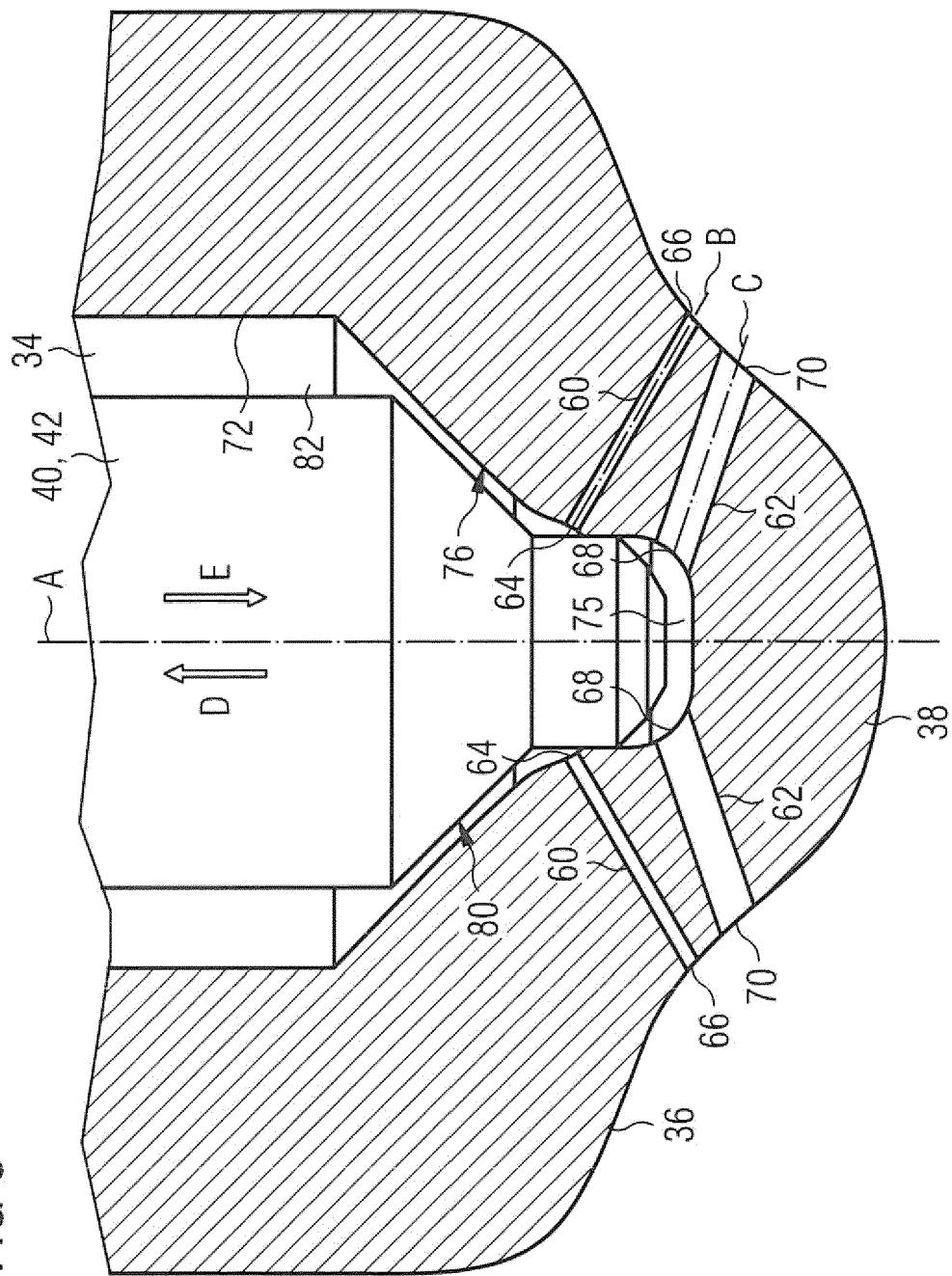


FIG 4

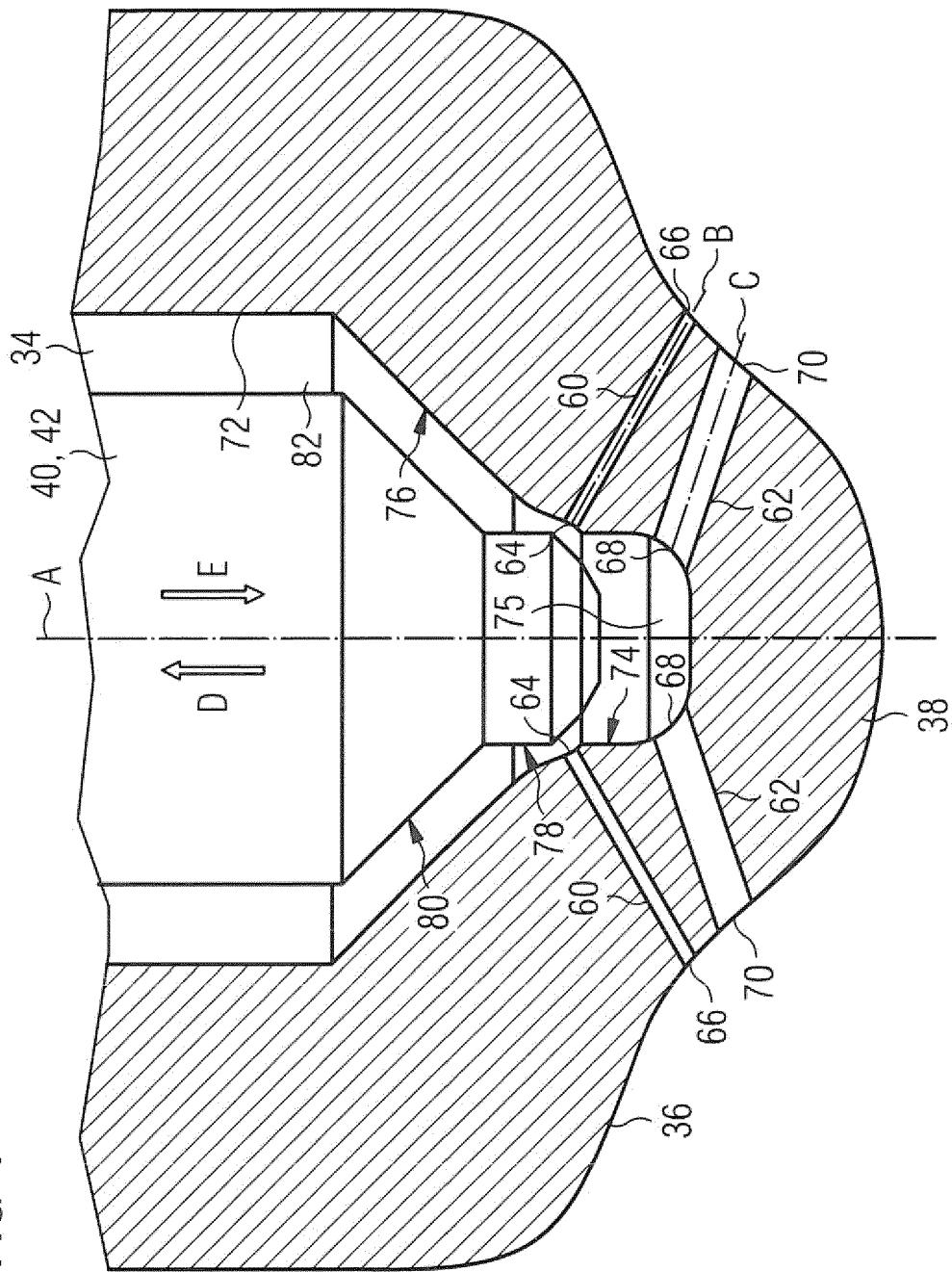


FIG 5A

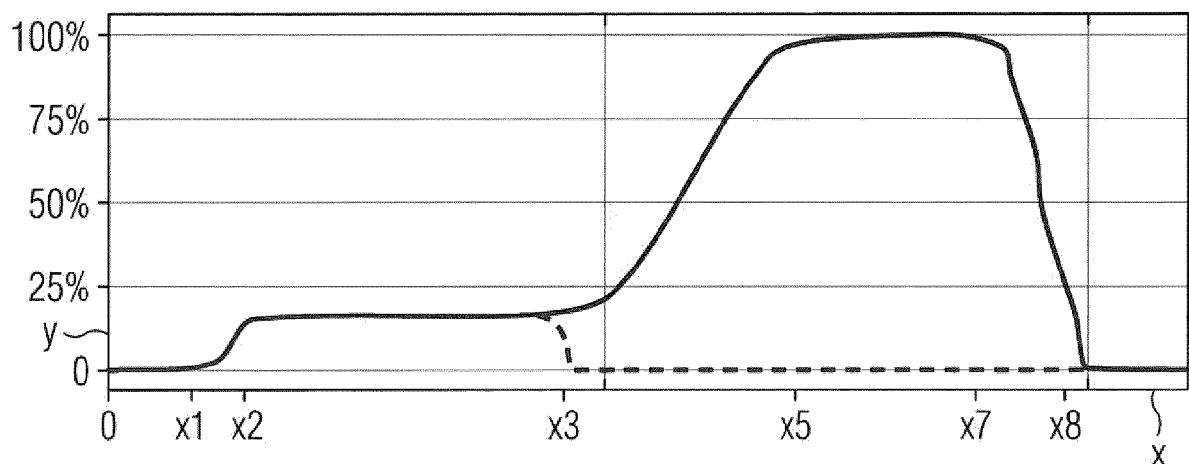
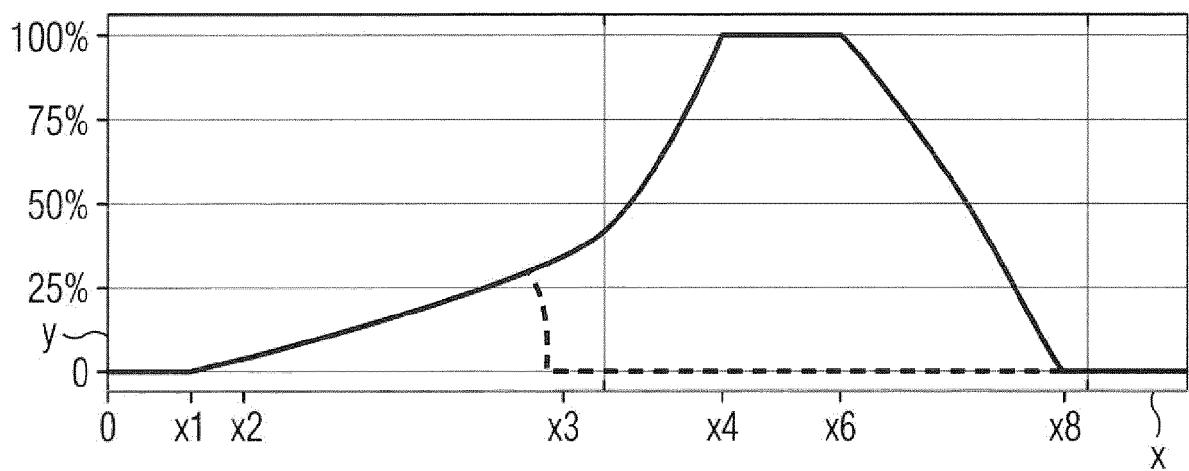


FIG 5B





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