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(54) **CONTROL DEVICE, CONTROL METHOD, AND INDUCTION COOKER**

(57) The present invention provides a control device (1) for an induction cooker (2, 20), the control device (1) comprising a driving circuit (4, 26) configured to controllably drive an induction coil (6) of the induction cooker (2, 20), a controller (7, 27) coupled to the driving circuit (4, 26) and configured to control the driving circuit (4, 26) with a control signal (8, 28) to drive the induction coil (6) with a power signal (5) of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value, and a

first measurement device (9, 29) configured to measure a feedback signal (10, 30, 56) at the induction coil (6) and provide the measured feedback signal (10, 30, 56) to the controller (7, 27). The controller (7, 27) is configured to adapt the first threshold value (40, 41) and the second threshold value (42, 43) based on the feedback signal (10, 30, 56), which is measured in a predetermined time period (50) after application of the power signal (5). The present invention further provides a respective method and an induction cooker.

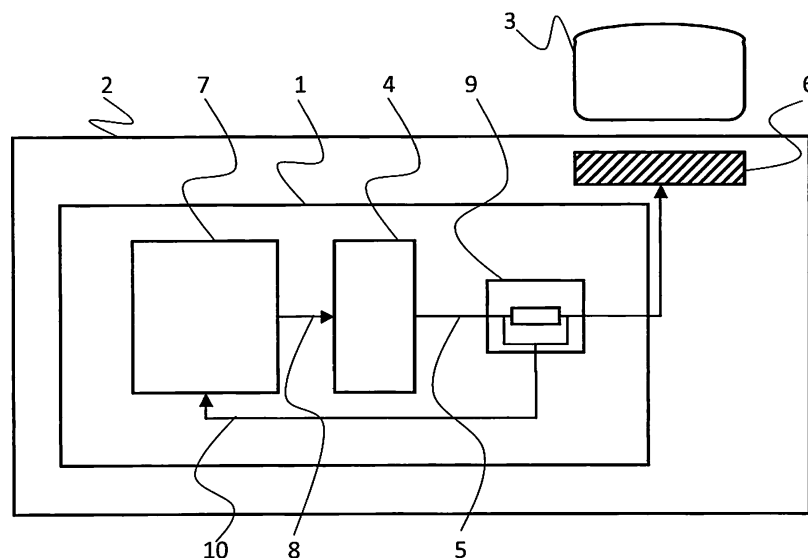


Fig. 1

Description

TECHNICAL FIELD

5 **[0001]** The invention relates to a control device and a control method for an induction cooker. Further, the present invention refers to a respective induction cooker.

BACKGROUND

10 **[0002]** Although applicable to any system that uses energy transfer via induction to heat an element, the present invention will be mainly described in combination with induction cookers.

[0003] Induction cookers are usually used to heat cooking vessels by magnetic induction. Usually a high frequency power signal is provided to an induction coil. This generates a magnetic field around the induction coil, which is magnetically coupled to a conductive cooking vessel, such as a pan, placed over the induction coil. The magnetic field then
15 generates eddy currents in the cooking vessel, causing the cooking vessel to heat.

[0004] In particular, the output power of the induction coil is a function of the power signal input, the coil inductance, the resistance of the cooking vessel, and the resonance frequency of the system. In known induction cookers, the induction coil is usually driven with a power signal at the resonance frequency of the system. The closer the system is driven to its resonance frequency, the more power can be delivered to the system. However, it is difficult to accurately
20 measure the resonance frequency.

[0005] Accordingly, there is a need for an improved power control in induction cookers.

SUMMARY

25 **[0006]** The present invention provides a control device with the features of claim 1, a control method with the features of claim 8, and an induction cooker with the features of claim 15.

[0007] Accordingly a control device for an induction cooker comprises a driving circuit configured to controllably drive an induction coil of the induction cooker, a controller coupled to the driving circuit and configured to control the driving circuit with a control signal to drive the induction coil with a power signal of a configurable operating frequency, which
30 is higher than a first initial threshold value and lower than a second initial threshold value, and a first measurement device configured to measure a feedback signal, e.g. a current signal or a voltage signal, at the induction coil and provide the measured feedback signal to the controller. The controller is configured to adapt the first threshold value and the second threshold value based on the feedback signal, which is measured in a predetermined time period after application of the power signal.

35 **[0008]** Further, a control method for controlling an induction cooker comprises the steps of controllably driving an induction coil of the induction cooker with a power signal of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value, measuring a feedback signal, e.g. a current signal or a voltage signal or a power signal, at the induction coil, and adapting the first threshold value and the second threshold value based on the feedback signal, which is measured in a predetermined time period after application of the
40 power signal.

[0009] Finally, an induction cooker comprises an induction coil, and a control device according to the present invention.

[0010] Induction cookers usually use a fixed operating frequency range for the power signal, which drives the induction coils. The fixed operating frequency range usually starts at the resonance frequency of the induction coil and ends at a safety limit frequency. The maximum power is transferred to the cooking vessel at the resonance frequency of the system of induction coil and cooking vessel. Increasing the frequency will lower the transferred energy. However, at increased
45 frequencies, the impedance of the induction coil will fall and the current through the induction coil will raise. Therefore, a maximum frequency is defined, which is not surpassed.

[0011] Further, the effect a cooking vessel has on the input impedance and the resonance frequency of the induction coil can be taken into account when selecting the fixed frequency range. The operating frequency range can e.g. be
50 selected for a virtual idealized or standardized cooking vessel, which represents an average of the existing cooking vessels. Objects, which are placed over the induction coil to cook, like e.g. pans or pots, will be referred to as cooking vessels throughout this description.

[0012] The present invention is based on the knowledge that the ideal operating frequency range of the power signal depends on not only the position of a cooking vessel in relation to the induction coil, i.e. the presence or absence and the coverage ratio, but also on the material, which the cooking vessel is made of.
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[0013] However, if the ideal operating frequency range is determined by the material, which the cooking vessel is made of, one single fixed operating frequency range cannot provide the best performance with all cooking vessels.

[0014] The present invention uses this knowledge and provides an adaptive operating frequency range, i.e. variable

first and second threshold values. The operating frequency range can therefore be adapted to different cooking vessels, i.e. different materials used in cooking vessels.

[0015] The initial first and second threshold values can be predetermined and e.g. be selected to be suitable for the majority of cooking vessels. The initial first and second threshold values can therefore also be selected based on the above-mentioned virtual idealized or standardized cooking vessel, which represents an average of the existing cooking vessels.

[0016] In order to adapt the first and second threshold values the present invention does not rely e.g. on a measurement of the resonance frequency, but analyses the feedback signal in a predetermined time period after the power signal is applied. This can also be seen as analyzing a step response of the induction coil to the application of the power signal. The predetermined time period can e.g. be defined as a time period, which is long enough to accommodate the relevant section of the feedback signal for any possible cooking vessel. The predetermined time period can e.g. be experimentally determined, by measuring the step response of the induction coil with a plurality of different cooking vessels and measuring the settling time. The settling time is the time the feedback signal takes to come to a constant value or nearly constant value, i.e. within a predetermined signal range. The feedback signal can e.g. be in the form of a measured current through the induction coil. In the present patent application, the term induction coil can also refer to the resonant unit comprising the induction coil and a respective capacitor in parallel to the induction coil.

[0017] Analyzing the step response of the induction coil when the power signal is applied reveals detailed information about the resonant circuit of induction coil and cooking vessel, i.e. about the cooking vessel's properties and influences on the induction coil.

[0018] Further embodiments of the present invention are subject of the further subclaims and of the following description, referring to the drawings.

[0019] In one embodiment, the controller can be configured to control the driving circuit to drive the induction coil with a power signal of a predetermined operating frequency. Further, the controller can be configured to determine the presence of a cooking vessel if the feedback signal is equal to or exceeds a third threshold value, wherein the controller is configured to adapt the first threshold value and the second threshold value after it determined the presence of a cooking vessel. The third threshold value can be empirically or experimentally predetermined as a value, which is reached only if a cooking vessel is at least partially in reach of the induction coil. The term "in reach" in this case means that electrical energy is at least partially transferred between the induction coil and the cooking vessel.

[0020] Different induction coils with different sizes, i.e. with different nominal power levels, can be used in induction cookers. The feedback signal depends on the power level of the respective coil. If e.g. the induction coils work efficiently with a nominal power of 1600 Watt. The target can e.g. be to drive the coil when the bottom of the cooking vessel covers 50% of the induction coil. This means that the induction cooker starts heating the cooking vessel only if the bottom of the cooking vessel covers 50% of the induction coil or more. This means that the third threshold value would represent 50% of the nominal power of the induction coil, in the above example about 800 Watt ($1600 \cdot 50\%$).

[0021] Detecting the presence of the cooking vessel allows determining the point in time at which the first and second threshold values should be determined. I.e. the step response of the induction coil will only be determined if a cooking vessel is present over the induction coil.

[0022] In one embodiment, the controller can be configured to compare the measured feedback signal in the predetermined time period after application of the power signal to a predetermined expected or target feedback signal. Further, the controller can be configured to determine the first threshold value and the second threshold value based on a rise time of the measured feedback signal, and/or an overshoot value of the measured feedback signal, and/or a settling time of the measured feedback signal, and/or a steady state error of the measured feedback signal. The expected or target feedback signal can be provided in the form of a constant value. The expected target feedback signal represents the nominal power of the induction coil, e.g. 1600 Watt.

[0023] The rise time refers to the time the measured feedback signal takes to rise to its maximum value after the power signal is applied. The overshoot value refers to the difference between the expected or target feedback signal and the maximum value of the feedback signal. The settling time refers to the time the measured feedback signal takes to reach a constant value after the power signal is applied. Finally, the steady state error refers to the difference between the constant value of the measured feedback signal and the expected or target feedback signal.

[0024] In one embodiment, the controller can be configured to calculate the first threshold value based on the division of the initial first threshold value multiplied by the steady state error and multiplied by a first constant and the sum of a second constant multiplied by the rise time and multiplied by the overshoot value and a third constant multiplied by the settling time.

[0025] The corresponding formula would be:

$$C = (A \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling_time}))$$

[0026] Wherein A is the initial first threshold value and C is the newly calculated first threshold value, which is used in further operation of the induction coil.

[0027] In one embodiment, the controller can be configured to calculate the second threshold value based on the division of the initial second threshold value multiplied by the steady state error and multiplied by a first constant and the sum of a second constant multiplied by the rise time and multiplied by the overshoot value and a third constant multiplied by the settling time.

[0028] The corresponding formula would be:

$$D = (B \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling_time}))$$

[0029] Wherein B is the initial second threshold value D is the newly calculated second threshold value, which is used in further operation of the induction coil.

[0030] In one embodiment, the constants K1 - K3 can be experimentally defined. The respective mathematical formulas would be:

$$T0 = A \times (T1 / T2)$$

(where A can be replaced by B for the second threshold value)

$$T1 = (K1 \times \text{steady_state_error})$$

$$T2 = ((K2 \times (\text{over_shoot}/\text{rise_time})) + (K3 \times \text{settling_time}))$$

$$T2 = T3 + T4$$

$$T3 = (K2 \times (\text{over_shoot}/\text{rise_time}));$$

$$T4 = (K3 \times \text{settling_time})$$

[0031] Without the present invention, T0 should be "1" to keep the operation range constant. Therefore, T1 + T2 = 1.

[0032] It is further assumed that T1 and T2 should be "1", T3 and T4 should be "0.5".

[0033] Consequently:

$$K1 = X/\text{steady_state_error}$$

$$K2 = \text{rise_time} \times Y / 2 \times \text{over_shoot}$$

$$K3 = Y / 2 * \text{settling_time}$$

[0034] For a stable system, the steady_state_error should be %5 or lower of the target feedback signal. If for example the target feedback signal represents 1600 Watt or a corresponding current value then a worst-case steady_state_error should be 80 Watt or the corresponding current value.

[0035] Consequently K1 would be:

$$K1 = X/80 = 0.0125 * X$$

[0036] It is further assumed that the standard rise time is about 100ms, nevertheless other rise times are possible depending on the exact dimensions of the induction coil and the driving circuit. Further, the system may have an over-voltage protection. This protection is activated if the feedback signal is %25 higher than target feedback signal, i.e. 25% higher than the nominal power of the induction coil. If e.g. the target feedback signal represents 1600 Watt the protection limit is 1600 Watt + 25% = 2000Watt. The over voltage should therefore be 2000Watt - 1600Watt = 400Watt at the maximum.

$$K2 = (0.1s * Z * Y) / 2 * 400 = Y * Z / 8000 = 0.000125 * Y * Z$$

[0037] Also, a rise time of 100ms can be assumed and it can further be assumed that the system has an over power protection. This protection is activated if the feedback signal is 25% higher than the target feedback signal. If e.g. the target feedback signal is 1600 Watt the protection limit is 1600 Watt + 25% = 2000 Watt. Then the over shoot should be 2000 Watt -1600 Watt = 400 Watt.

$$K2 = (0.1s * Z * Y) / 2 * 400 = Y * Z / 8000 = 0.000125 * Y * Z$$

[0038] Either way, if the system comprises an overvoltage protection or an overpower protection, the result for K2 is the same.

[0039] A final assumption can be that the settling time is 1s* W. Then

$$K3 = Y / (2 * W) = Y / (2 * W)$$

[0040] Consequently, K1, K2 and K3 can be defined as:

$$K1 = 0.0125 * X$$

$$K2 = 0.000125 * Y * Z$$

$$K3 = Y / (2 * W) \quad \text{for } X+Y = 1;$$

[0041] X, Y,Z and W are parameters which depend on the size of the induction coil, glass types over the coil, the mechanical structure of induction cooker etc. These values can e.g. be experimentally determined after the hardware design and the mechanical design of the induction cooker is complete. The values of X,Y,Z and W can e.g. be varied until the required system performance is achieved.

[0042] Exemplary values can e.g. be

$$K1 = 1/80 = 0.0125$$

$$K2 = (0.5 * 0.1s) / 400 = 1/8000 = 0.000125$$

$$K3 = 0.5/1 = 0.5$$

[0043] The above assumptions and examples refer to an induction coil with 1600 Watt nominal power and can further be varied depending on the coil power, glass types over the coil, the mechanical structure of cooker and the like.

[0044] In one embodiment, the control device can comprise a control algorithm, which can be configured to drive the induction coil based on the adapted first threshold and second threshold, wherein the controller is configured to stop operation of the induction coil if the measured feedback signal drops below a fourth threshold value while driving the induction coil. The fourth threshold value is a lower limit for the measured feedback signal, which, as the third threshold value, can be empirically or experimentally predetermined as a value, which is reached only if a cooking vessel is at least partially in reach of the induction coil. In contrast to the third threshold value, the fourth threshold value is used when the induction coil is operated with other than the first and second threshold values.

[0045] The fourth threshold value can e.g. be the same as the third threshold value.

BRIEF DESCRIPTION OF THE DRAWINGS

[0046] For a more complete understanding of the present invention and advantages thereof, reference is now made to the following description taken in conjunction with the accompanying drawings. The invention is explained in more detail below using exemplary embodiments, which are specified in the schematic figures of the drawings, in which:

Fig. 1 shows a block diagram of an embodiment of a control device according to the present invention in an embodiment of an induction cooker according to the present invention;

Fig. 2 shows a block diagram of another embodiment of induction cooker according to the present invention;

Fig. 3 shows a diagram with embodiments of first and second threshold values for different cooking vessels;

Fig. 4 shows a diagram with an embodiment of a measured feedback signal;

Fig. 5 shows a flow diagram of an embodiment of a method according to the present invention; and

Fig. 6 shows a flow diagram of another embodiment of a method according to the present invention.

[0047] In the figures like reference signs denote like elements unless stated otherwise.

DETAILED DESCRIPTION OF THE DRAWINGS

[0048] In Fig. 1 a control device 1 is installed in an induction cooker 2, which is used to heat a cooking vessel 3. The control device 1 comprises a driving circuit 4, which provides a power signal 5 to an induction coil 6 of the induction cooker 2. It is understood, that the induction coil 6 is only shown schematically and can comprise further elements, like e.g. parallel capacitors.

[0049] Electrical power must be transferred from the induction coil 6 to the cooking vessel 3 to heat up the cooking vessel 3. Therefore, the driving circuit 4 is controlled by controller 7 via control signal 8 to operate the power signal 5 at a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value. This implies that the power signal 5 is a changing signal with a changing amplitude. The such driven induction coil 6 will therefore generate a magnetic field, which in turn will induce eddy currents in the cooking vessel 3. Because of the electrical resistance of the material of the cooking vessel 3, the eddy currents will heat up the cooking vessel 3.

[0050] The controller 7 is further coupled to a measurement device 9, which will measure the current through the induction coil 6, i.e. the current transported in the power signal 5, and provide a respective feedback signal 10. Based on the feedback signal 10, the controller 7 determines the electrical power, which is provided to the induction coil 6, and with the control signal 8 controls the frequency of the power signal 5.

[0051] The first threshold value for the frequency can e.g. be the resonance frequency of the induction coil 6 and the cooking vessel 3, i.e. the resonance frequency of the coupled system consisting of induction coil 6 and the cooking

vessel 3. The second threshold value can e.g. be a maximum allowed frequency for the respective system. When the frequency is higher than the resonance frequency of the system, the impedance of the system will fall, therefore the current will rise. The second threshold value will therefore limit the maximum current through system of the induction coil 6 and the cooking vessel 3.

[0052] The initial first and second threshold values can e.g. be determined based on a virtual idealized or standardized cooking vessel 3, which represents an average of the existing cooking vessels 3.

[0053] Nevertheless, a wide variety of cooking vessels 3 exist. The resonance frequency of the system of induction coil 6 and cooking vessel 3 also depends on the material and the geometry of the cooking vessel 3. The initial first and second threshold values will therefore not be valid for all types of cooking vessel 3. This will lead to a reduced performance or efficiency of the induction cooker 2.

[0054] Therefore, the controller 7 will analyze the feedback signal 10 in the start phase of the induction coil 6, i.e. the step response of the feedback signal 10 during a predetermined time period (see Fig. 4). Based on this step response the controller 7 will adapt the first and second threshold values accordingly.

[0055] The details of how the controller 7 adapts the first and the second threshold values will be explained in conjunction with Fig. 4.

[0056] It is understood, that prior to adapting the first and second threshold values and driving the induction coil 6 to heat a cooking vessel 3, the controller 7 can perform a vessel detection. During the vessel detection, the controller 7 will identify if a cooking vessel 3 is present over the induction coil 6. The controller 7 can e.g. control the driving circuit 4 to drive the induction coil 6 with a power signal 5 of a predetermined operating frequency. The controller 7 then determines the presence of a cooking vessel 3 if the feedback signal 10 is equal to or exceeds a third threshold value.

[0057] Further, after adapting the first and second threshold values and driving the induction coil 6 to heat up the cooking vessel 3, the controller 7 can also continuously verify if the cooking vessel 3 is still present. If the cooking vessel 3 is not present any more, the controller 7 will stop the driving circuit 4 and therefore shut down the induction cooker 2.

[0058] Fig. 2 shows another possible schematic arrangement for an induction cooker 20.

[0059] A rectifier 22 can e.g. be connected to the mains power and provides a rectified electrical power. The rectified electrical power is provided to a parallel circuit of a coil 23 and capacitor 24. These two elements, coil 23 and capacitor 24, form the induction coil of the induction cooker 20 and heat up a cooking vessel 25.

[0060] The driving circuit is provided in the form of a transistor 26, which can be controlled via the control signal 28 by the controller 27. The controller 27 therefore provides a control signal 28 with the frequency, which is required to drive the coil 23. A shunt resistor 29 provides the feedback signal 30 to the controller via an amplifier 31.

[0061] The diagram of Fig. 3 shows the output power of the driving circuit 4 with respect to the frequency of the power signal 5 at different frequencies for two different cooking vessels 46, 47. The first threshold values 40, 41 represent the resonance frequency of the induction coil 6 with the respective cooking vessel 46, 47. The second threshold values 42, 43 represent the frequency, at which the maximum allowed electrical power of the driving circuit 4, 26 is reached with the induction coil 6 with the respective cooking vessel 46, 47.

[0062] It can be seen, that for cooking vessel 46 the first threshold 40 value is at first frequency and the second threshold value 42 at a second frequency. However, the first threshold value 41 for the cooking vessel 47 is at a frequency even higher than the second threshold value 42. That means that the frequency ranges of the cooking vessels 46 and 47 do not even overlap.

[0063] It is understood from Fig. 3 that it is necessary to adapt the initial frequency range for driving the induction coil 6 accordingly for different cooking vessels 3.

[0064] Fig. 4 shows a step response of the feedback signal 56 after initially driving e.g. the induction coil 6 or the coil 23, respectively.

[0065] It can be seen that the feedback signal 56 does not linearly rise until it reaches the target or expected feedback signal 51. Instead, the feedback signal 56 overshoots the expected feedback signal 51 by an overshoot value 53 after a certain rise time 52. The rise time 52 in Fig. 4 is only exemplarily measured after the feedback signal 56 reaches 10% of the maximum or overshoot value 53 until the feedback signal 56 reaches 90% of the maximum or overshoot value 53. It is understood that the rise time can be defined differently in other embodiments.

[0066] In the diagram, the settling time 54 of the feedback signal 56 is further shown. The settling time 54 refers to the time, which the feedback signal 56 takes to settle into a predetermined corridor or interval. Finally, in the diagram, the difference between the final value of the feedback signal 56 and the expected feedback signal 51 is shown as steady state error 55.

[0067] The controller 7, 27 will calculate the new first threshold value 40, 41 based on the division of the initial first threshold value multiplied by the steady state error 55 and multiplied by a first constant K1 and the sum of a second constant K2 multiplied by the rise time 52 and multiplied by the overshoot value 53 and a third constant K3 multiplied by the settling time 54.

[0068] The corresponding formula would be:

$$C = (A \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling time}))$$

[0069] Wherein C is the newly calculated first threshold value 40, 41, which is used in further operation of the induction coil 6.

[0070] Further, the controller 7, 27 will calculate the second threshold value 42, 43 based on the division of the initial second threshold value multiplied by the steady state error 55 and multiplied by the first constant K1 and the sum of the second constant K2 multiplied by the rise time 52 and multiplied by the overshoot value 53 and the third constant K3 multiplied by the settling time 54.

[0071] The corresponding formula would be:

$$D = (B \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling time}))$$

[0072] Wherein D is the newly calculated second threshold value 42, 43, which is used in further operation of the induction coil 6.

[0073] The constants K1 - K3 can be defined as already indicated above. Exact values can e.g. be K1 = 0.0125, K2 = 0.000125, and K3 = 0.5.

[0074] Fig. 5 shows a flow diagram of a method for controlling an induction cooker 2, 20. The method comprises in step S1 controllably driving an induction coil 6 of the induction cooker 2, 20 with a power signal 5 of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value. In step S2 a feedback signal 10, 30, 56 is measured at the induction coil 6. Finally, in step S3 the first threshold value 40, 41 and the second threshold value 42, 43 are adapted based on the feedback signal 10, 30, 56, which is measured in a predetermined time period 50 after application of the power signal 5.

[0075] The step of adapting S3 can e.g. comprise comparing the measured feedback signal 10, 30, 56 in the predetermined time period 50 after application of the power signal 5 to a predetermined expected feedback signal 51, i.e. the step response.

[0076] The first threshold value 40, 41 and the second threshold value 42, 43 can then be determined based on a rise time 52 of the measured feedback signal 10, 30, 56, and/or an overshoot value 53 of the measured feedback signal 10, 30, 56, and/or a settling time 54 of the measured feedback signal 10, 30, 56, and/or a steady state error 55 of the measured feedback signal 10, 30, 56.

[0077] The first threshold value 40, 41 can e.g. be calculated based on the division of the initial first threshold value 40, 41 multiplied by the steady state error 55 and multiplied by a first constant K1 and the sum of a second constant K2 multiplied by the rise time 52 and multiplied by the overshoot value 53 and a third constant K3 multiplied by the settling time 54.

[0078] The second threshold value 42, 43 can be calculated based on the division of the initial second threshold value 42, 43 multiplied by the steady state error 55 and multiplied by a first constant K1 and the sum of a second constant K2 multiplied by the rise time 52 and multiplied by the overshoot value 53 and a third constant K3 multiplied by the settling time 54.

[0079] The corresponding formula for the first threshold value 40, 41 would be:

$$C = (A \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling time}))$$

[0080] Wherein C is the newly calculated first threshold value 40, 41, which is used in further operation of the induction coil 6.

[0081] The corresponding formula for the second threshold value 42, 43 would be:

$$D = (B \times K1 \times \text{steady_state_error}) / ((K2 \times \text{rise_time} \times \text{over_shoot}) + (K3 \times \text{settling time}))$$

[0082] Wherein D is the newly calculated second threshold value 42, 43, which is used in further operation of the induction coil 6.

[0083] Fig. 6 shows a flow diagram of another method for controlling an induction cooker 2, 20.

[0084] Prior to driving S1, measuring S2, and adapting S3, the method in Fig. 6 comprises steps S4 and S5, which serve to detect if a cooking vessel 3, 25, 46, 47 is present over the induction coil 6.

[0085] Step S4 comprises driving the induction coil 6 with a power signal 5 of a predetermined operating frequency. The presence of a cooking vessel 3, 25, 46, 47 is then determined in step S5 if the feedback signal 10, 30, 56 is equal to or exceeds a third threshold value. Decision D1 branches to the steps S1 - S3 only after the presence of a cooking vessel 3, 25, 46, 47 is determined in step S5. Otherwise, decision D1 branches back to step S4.

[0086] If a cooking vessel 3, 25, 46, 47 is detected, the steps S1 - S3 as described above are performed. Following step S3, the step S6 comprises driving S6 the induction coil 6 based on the adapted first threshold value 40, 41 and second threshold value 42, 43.

[0087] While the induction coil 6 is driven based on the adapted first threshold value 40, 41 and second threshold value 42, 43, it is further supervised if the cooking vessel 3, 25, 46, 47 is still present over the induction coil 6. Decision D2 returns to step S6 if the cooking vessel 3, 25, 46, 47 is present. Otherwise, decision D2 branches to step S7, where operation of the induction coil 6 is stopped.

[0088] For detecting if the cooking vessel 3, 25, 46, 47 is still present, it can be verified, if the measured feedback signal 10, 30, 56 drops below the fourth threshold value while driving the induction coil 6.

[0089] Although specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that a variety of alternate and/or equivalent implementations exist. It should be appreciated that the exemplary embodiment or exemplary embodiments are only examples, and are not intended to limit the scope, applicability, or configuration in any way. Rather, the foregoing summary and detailed description will provide those skilled in the art with a convenient road map for implementing at least one exemplary embodiment, it being understood that various changes may be made in the function and arrangement of elements described in an exemplary embodiment without departing from the scope as set forth in the appended claims and their legal equivalents. Generally, this application is intended to cover any adaptations or variations of the specific embodiments discussed herein.

[0090] The present invention provides a control device (1) for an induction cooker (2, 20), the control device (1) comprising a driving circuit (4, 26) configured to controllably drive an induction coil (6) of the induction cooker (2, 20), a controller (7, 27) coupled to the driving circuit (4, 26) and configured to control the driving circuit (4, 26) with a control signal (8, 28) to drive the induction coil (6) with a power signal (5) of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value, and a first measurement device (9, 29) configured to measure a feedback signal (10, 30, 56) at the induction coil (6) and provide the measured feedback signal (10, 30, 56) to the controller (7, 27). The controller (7, 27) is configured to adapt the first threshold value (40, 41) and the second threshold value (42, 43) based on the feedback signal (10, 30, 56), which is measured in a predetermined time period (50) after application of the power signal (5). The present invention further provides a respective method and an induction cooker.

List of reference signs

[0091]

1	control device
2, 20	induction cooker
3, 25, 46, 47	cooking vessel
4, 26	driving circuit
5	power signal
6	induction coil
7, 27	controller
8, 28	control signal
9, 29	measurement device
10, 30, 56	feedback signal

22	rectifier
23	coil
24	capacitor
31	amplifier
32	ground

40, 41 first threshold value
 42, 43 second threshold value
 44, 45 human hearing limit

5 50 predetermined time period
 51 expected feedback signal
 52 rise time
 53 overshoot value
 54 settling time
 10 55 steady state error

S1 - S7 method steps

15 Claims

1. Control device (1) for an induction cooker (2, 20), the control device (1) comprising:

20 a driving circuit (4, 26) configured to controllably drive an induction coil (6) of the induction cooker (2, 20) with a power signal (5),
 a controller (7, 27) coupled to the driving circuit (4, 26) and configured to control the driving circuit (4, 26) with a control signal (8, 28) to drive the induction coil (6) with the power signal (5) of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value, and
 25 a first measurement device (9, 29) configured to measure a feedback signal (10, 30, 56) at the induction coil (6) and provide the measured feedback signal (10, 30, 56) to the controller (7, 27),

wherein the controller (7, 27) is configured to adapt the first threshold value (40, 41) and the second threshold value (42, 43) based on the feedback signal (10, 30, 56), which is measured in a predetermined time period (50) after application of the power signal (5).

30 2. Control device (1) according to claim 1, wherein the controller (7, 27) is configured to control the driving circuit (4, 26) to drive the induction coil (6) with a power signal (5) of a predetermined operating frequency and to determine the presence of a cooking vessel (3, 25, 46, 47) if the feedback signal (10, 30, 56) is equal to or exceeds a third threshold value, wherein the controller (7, 27) is configured to adapt the first threshold value (40, 41) and the second threshold value (42, 43) after it determined the presence of a cooking vessel (3, 25, 46, 47).

3. Control device (1) according to any one of the preceding claims, wherein the controller (7, 27) is configured to compare the measured feedback signal (10, 30, 56) in the predetermined time period (50) after application of the power signal (5) to a predetermined expected feedback signal (51) and determine the first threshold value (40, 41) and the second threshold value (42, 43) based on a rise time (52) of the measured feedback signal (10, 30, 56), and/or an overshoot value (53) of the measured feedback signal (10, 30, 56), and/or a settling time (54) of the measured feedback signal (10, 30, 56), and/or a steady state error (55) of the measured feedback signal (10, 30, 56).

4. Control device (1) according to claim 3, wherein the controller (7, 27) is configured to calculate the first threshold value (40, 41) based on the division of the initial first threshold value (40, 41) multiplied by the steady state error (55) and multiplied by a first constant and the sum of a second constant multiplied by the rise time (52) and multiplied by the overshoot value (53) and a third constant multiplied by the settling time (54).

5. Control device (1) according to any one of claims 3 and 4, wherein the controller (7, 27) is configured to calculate the second threshold value (42, 43) based on the division of the initial second threshold value (42, 43) multiplied by the steady state error (55) and multiplied by a first constant and the sum of a second constant multiplied by the rise time (52) and multiplied by the overshoot value (53) and a third constant multiplied by the settling time (54).

6. Control device (1) according to claims 4 and 5, wherein the first constant is defined as 0.0125, and wherein the second constant is defined as 0.000125, and wherein the third constant is defined as 0.5.

7. Control device (1) according to any one of the preceding claims, wherein the control device (1) comprises a control algorithm, which is configured drive the induction coil (6) based on the adapted first threshold value (40, 41) and

second threshold value (42, 43), wherein the controller (7, 27) is configured to stop operation of the induction coil (6) if the measured feedback signal (10, 30, 56) drops below a fourth threshold value while driving the induction coil (6).

8. Control method for controlling an induction cooker (2, 20), the control method comprising the steps of:

controllably (S1) driving an induction coil (6) of the induction cooker (2, 20) with a power signal (5) of a configurable operating frequency, which is higher than a first initial threshold value and lower than a second initial threshold value,

measuring (S2) a feedback signal (10, 30, 56) at the induction coil (6), and

adapting (S3) the first threshold value (40, 41) and the second threshold value (42, 43) based on the feedback signal (10, 30, 56), which is measured in a predetermined time period (50) after application of the power signal (5).

9. Control method according to claim 8, further comprising driving (S4) the induction coil (6) with a power signal (5) of a predetermined operating frequency, and determining (S5) the presence of a cooking vessel (3, 25, 46, 47) if the feedback signal (10, 30, 56) is equal to or exceeds a third threshold value, and adapting (S3) the first threshold value (40, 41) and the second threshold value (42, 43) after the presence of a cooking vessel (3, 25, 46, 47) is determined.

10. Control method according to any one of the preceding claims 8 and 9, wherein adapting (S3) comprises comparing the measured feedback signal (10, 30, 56) in the predetermined time period (50) after application of the power signal (5) to a predetermined expected feedback signal (51), and determining the first threshold value (40, 41) and the second threshold value (42, 43) based on a rise time (52) of the measured feedback signal (10, 30, 56), and/or an overshoot value (53) of the measured feedback signal (10, 30, 56), and/or a settling time (54) of the measured feedback signal (10, 30, 56), and/or a steady state error (55) of the measured feedback signal (10, 30, 56).

11. Control method according to claim 10, wherein adapting (S3) further comprises calculating the first threshold value (40, 41) based on the division of the initial first threshold value (40, 41) multiplied by the steady state error (55) and multiplied by a first constant and the sum of a second constant multiplied by the rise time (52) and multiplied by the overshoot value (53) and a third constant multiplied by the settling time (54).

12. Control method according to any one of claims 10 and 11, wherein adapting (S3) further comprises calculating the second threshold value (42, 43) based on the division of the initial second threshold value (42, 43) multiplied by the steady state error (55) and multiplied by a first constant and the sum of a second constant multiplied by the rise time (52) and multiplied by the overshoot value (53) and a third constant multiplied by the settling time (54).

13. Control method according to any one of claims 11 and 12, wherein the first constant is defined as 0.0125, and wherein the second constant is defined as 0.000125, and wherein the third constant is defined as 0.5.

14. Control method according to any one of the preceding claims 8 to 13, further comprising driving (S6) the induction coil (6) based on the adapted first threshold (40, 41) value and second threshold value (42, 43), wherein operation of the induction coil (6) is stopped (S7) if the measured feedback signal (10, 30, 56) drops below a fourth threshold value while driving the induction coil (6).

15. Induction cooker (2, 20), comprising an induction coil (6), and a control device (1) according to any one of claims 1 - 7.

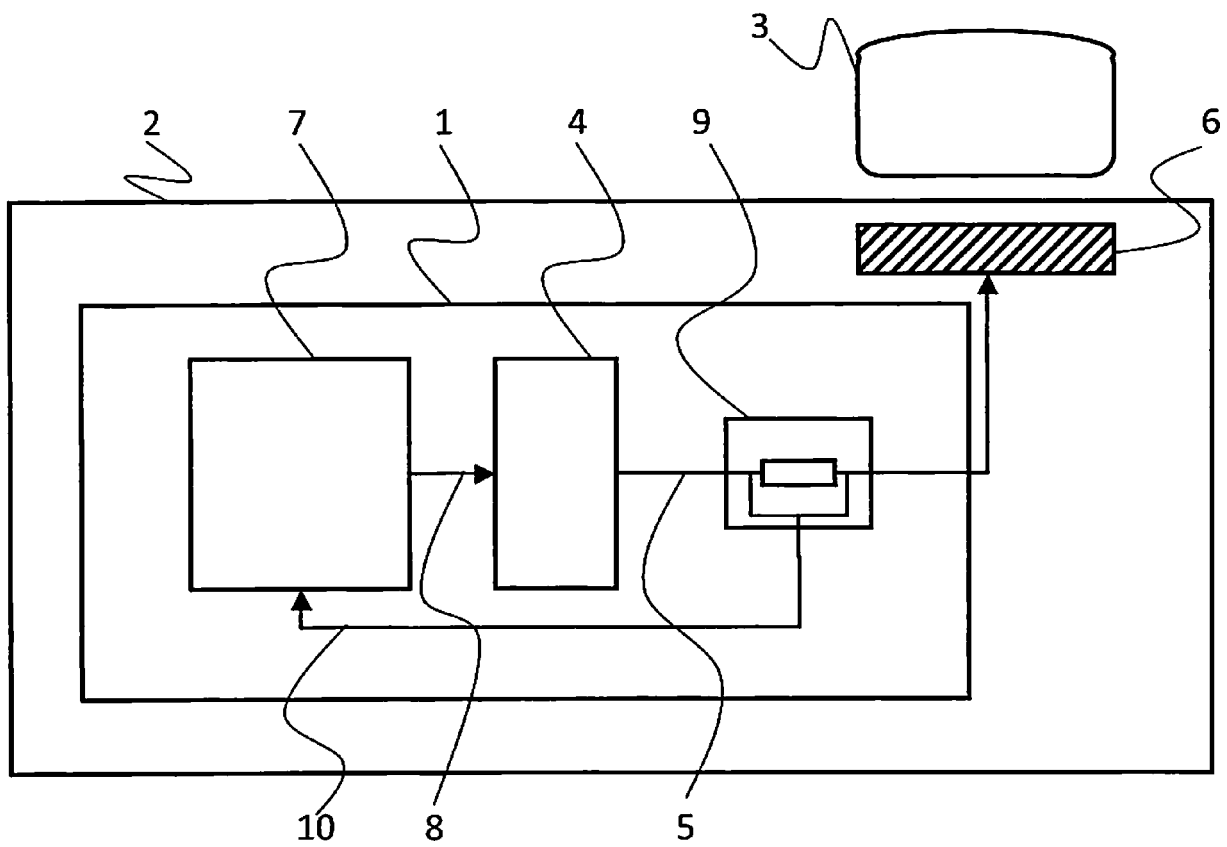


Fig. 1

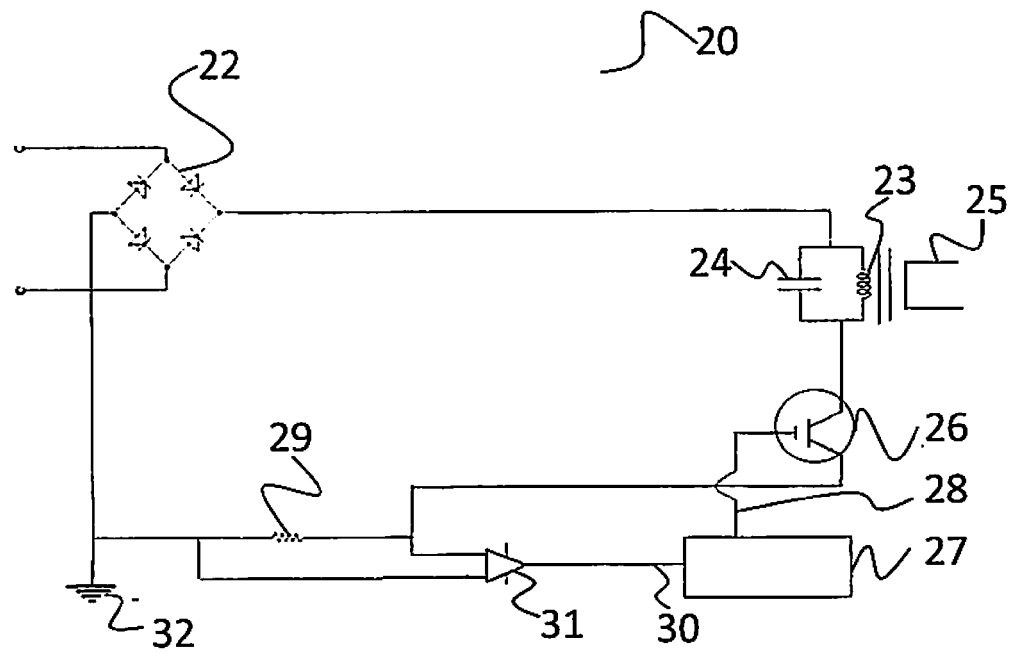


Fig. 2

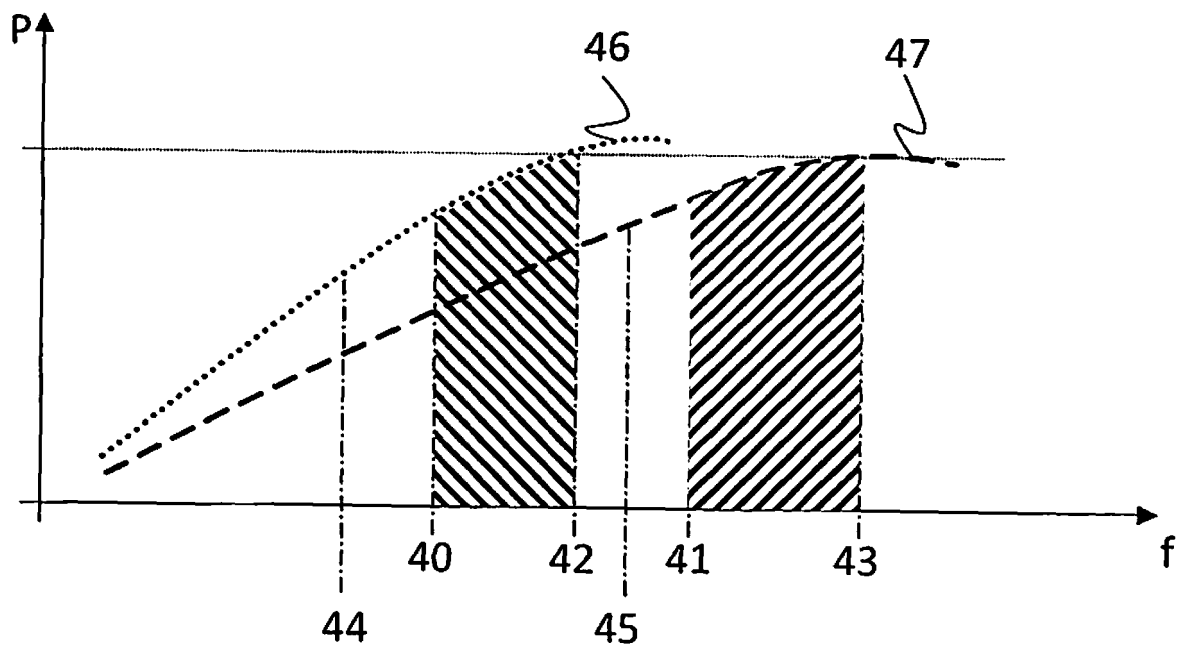


Fig. 3

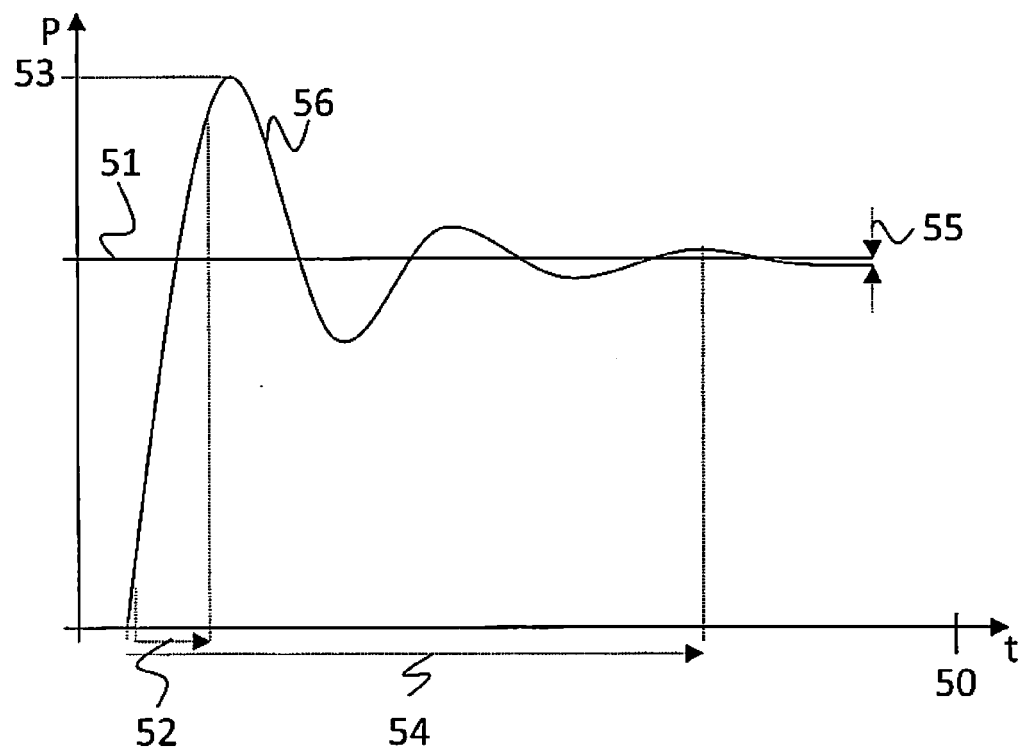


Fig. 4

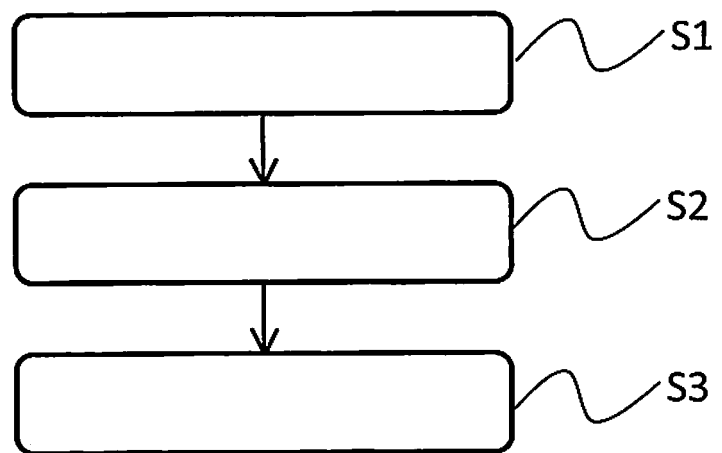


Fig. 5

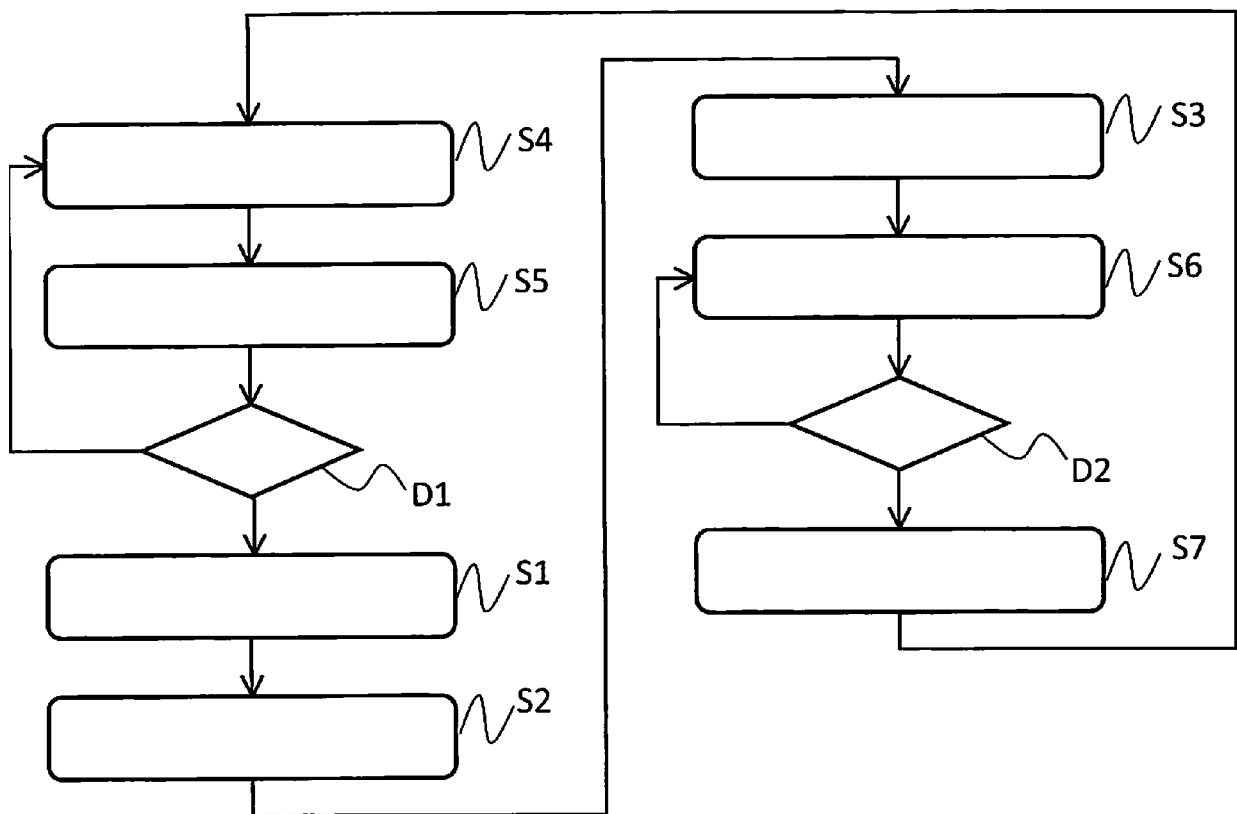


Fig. 6



EUROPEAN SEARCH REPORT

Application Number
EP 16 18 7048

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			H05B
The present search report has been drawn up for all claims			
Place of search Munich		Date of completion of the search 1 March 2017	Examiner Pierron, Christophe
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document</p>			

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