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(54) **GRAIN-ORIENTED ELECTRICAL STEEL SHEET AND METHOD FOR MANUFACTURING SAME**

KORNORIENTIERTES ELEKTRISCHES STAHLBLECH UND VERFAHREN ZUR HERSTELLUNG DAVON

TÔLE D'ACIER ÉLECTRIQUE À GRAINS ORIENTÉS ET SON PROCÉDÉ DE FABRICATION

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Description**[Technical Field]**

5 **[0001]** The present disclosure relates to a grain-oriented electrical steel sheet and a method for manufacturing the same.

[Background Art]

10 **[0002]** The grain-oriented electrical steel sheet is used as a core material for energy conversion of electronic equipment such as a transformer, by developing <001> magnetization easy axis texture in rolling direction. For applications in the transformer, a steel sheet with a relatively low core loss and excellent flux density properties is required, which will result in reduced power loss and higher energy conversion efficiency.

15 **[0003]** For the purpose of improving the magnetic properties of grain-oriented electrical steel sheet, a method of magnetic domain refinement may be used, which modifies the solidification characteristics and the specific resistivity properties and decreases the width of magnetic domains by way of component designing. The magnetic domain refinement may be divided into temporary magnetic domain refinement and permanent magnetic domain refinement depending on presence/absence of the lasting enhancement effect of the magnetic domain refinement after the stress relief annealing.

20 **[0004]** The grooving method, which is one of the permanent magnetic domain refinement methods, involves surface melting by laser emission to form a groove on the sheet surface. Accordingly, the method has a disadvantage of having transfer and scattering melts around the groove and occurrence of unavoidable surface spatter and hill-up. In addition, the method for suppressing increased groove depth and generation of defects around the groove area by way of applying or coating organic or inorganic material on the sheet surface has a disadvantage in that the process is complicated because it requires additional application and coating of organic or inorganic materials before the formation of the groove.

25 In addition, the spatter removal method, which is more aggressive removal method that uses the brush, can leave damages on the surface due to the increased frictional force at a contact area between the brush and the steel sheet surface, when the frictional force is increased to deal with the increasing hill-up and spatter. WO 2015/170755 discloses a method of using laser impingement on the tension coating of a grain oriented electrical steel sheet to control the magnetic domains.

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[DISCLOSURE]**[Technical Problem]**

35 **[0005]** The present invention has been made in an effort to provide a grain-oriented electrical steel sheet and a method for manufacturing the same, which are capable of removing the hill-up and spatter formed on a sheet surface that has underwent hot annealing when the linear groove is formed on the sheet surface.

[Technical Solution]

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[0006] A grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes: a forsterite layer formed on the surface of an electrical steel sheet; a groove which is formed on the forsterite layer in a direction perpendicular to a rolling direction; and a forsterite calcination layer which is formed in the direction of both ends of the electrical steel sheet on the basis of an upper end of the groove and has a width of 1.1 to 1.3 times the width of the groove.

45 **[0007]** A 'hill-up', which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove on an upper portion of the forsterite calcination layer, or the spatter, which is generated by scattering melt, may be formed to 1.5 μm or less from the surface of the forsterite calcination layer.

[0008] The groove may be formed to a depth of 2.5 to 10 % with respect to a thickness of the electrical steel sheet.

50 **[0009]** The groove may be formed at an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet and may be formed in a linear shape.

[0010] The hill-up, which is an elevation of the melt generated during formation of the groove and accumulated on both sides of the groove on the upper portion of the forsterite calcination layer, or the spatter, which is generated by scattering melt, may be removed by brushing or pickling.

55 **[0011]** A method for manufacturing a grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes steps of: heating a slab including 1.5 to 7 wt% of Si and other unavoidable impurities, with the remainder being Fe, and hot rolling the slab to prepare a hot rolled steel sheet; cold rolling the hot rolled steel sheet to prepare a cold rolled steel sheet, and then subjecting the cold rolled steel sheet to decarburization annealing and/or nitriding annealing to form an oxide layer on the surface of steel sheet; applying an annealing separator including MgO

on the surface of the steel sheet on which the oxide layer is formed and performing hot annealing to form a forsterite layer (forsterite; Mg_2SiO_4) on the surface of the steel sheet; and emitting a continuous-wave laser of Gaussian mode onto the steel sheet formed with the forsterite layer to form a groove on the surface of a steel sheet, in which, in the step of forming the groove, the beam shape of the continuous-wave laser satisfies the range of Formula 1 below, and the retention time T_d of the continuous wave laser satisfies the range of Formula 2 below.

$$1.3 \leq L_b/L_a \leq 7.0 \text{-----1)}$$

$$0.5 \leq T_d \leq 10.0 \text{-----2)}$$

wherein L_a is the length of the laser beam in the rolling direction and L_b is the widthwise length of the laser beam and T_d is a ratio (W/V_s) of the scanning rate (V_s) of the laser beam scanned in the width direction to the widthwise emission width (W) emitted to the steel sheet width.

[0012] The step of forming the groove may include a step of emitting a continuous-wave laser of Gaussian mode to form a forsterite calcination layer in the direction of both ends of the electric steel sheet on the basis of the upper end of the groove, by a width of 1.1 to 1.3 times the width of the groove.

[0013] The step of forming the groove may include a step of forming the groove to a depth of 2.5 to 10 % with respect to the thickness of the electrical steel sheet.

[0014] The step of forming the groove may include a step of forming the groove at an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet, and in a linear shape.

[0015] The step of forming the groove may further include steps of forming a hill-up, which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove, or the spatter, which is generated by scattering melt, may be formed on an upper portion of the forsterite calcination layer, and removing the hill-up or the spatter to 1.5 μm or less from the surface of the forsterite calcination layer.

[0016] The step of removing the hill-up or the spatter may include a step of dry-removing using brush.

[0017] The brush may be a metal-based material or an abrasive material.

[0018] The step of removing the hill-up or the spatter may include a step of wet-removing through pickling.

[0019] The pickling may be carried out using an aqueous solution including hydrochloric acid, nitric acid or sulfuric acid.

[0020] The concentration of aqueous solution may be 1 to 30 wt%.

[Advantageous Effects]

[0021] According to an embodiment of the present disclosure, the hill-up or spatter defects around the groove appearing during the formation of the groove by laser emission can be effectively removed, thereby it is possible to manufacture a low core-loss grain-oriented electric steel sheet having excellent insulation and space factor as well as a core loss reduction effect provided by the groove.

[Description of the Drawings]

[0022]

FIG. 1 is a view schematically showing the laser emission in the direction perpendicular to the rolling direction on the surface of the grain-oriented electrical steel sheet according to an embodiment of the present disclosure.

FIG. 2 is a schematic view showing a hill-up or spatter formed on an upper portion of a forsterite calcination layer when a laser is emitted onto a surface of a grain-oriented electrical steel sheet according to an embodiment of the present disclosure.

FIG. 3 is a process diagram of a method for manufacturing a grain-oriented electrical steel sheet according to the present disclosure.

FIG. 4 is a view showing a shape of a laser on an XY plane when the laser is emitted onto the surface of a grain-oriented electrical steel sheet according to an embodiment of the present disclosure.

[Mode for Invention]

[0023] The terms "first", "second" and "third" as used herein are intended to describe various parts, components, regions, layers and/or sections, but not construed as limiting. These terms are merely used to distinguish any parts,

components, regions, layers and/or sections from another parts, components, regions, layers and/or sections. Accordingly, a first part, component, region, layer or section to be described below may be referred to as a second part, component, region, layer or section without departing from the scope of the present disclosure.

[0024] The terminology used herein is for the purpose of describing particular embodiments only and is not intended to limit the present disclosure. The singular forms used herein include plural forms as long as the phrases do not expressly mean to the contrary. As used herein, the meaning of "comprising" specifies specific features, regions, integers, steps, operations, elements and/or components, and does not exclude the presence or the addition of other features, regions, integers, steps, operations, elements and/or components.

[0025] When a portion is referred to as being "above" or "on" another portion, it may be directly on another portion or may be accompanied by yet another portion disposed in between. In contrast, when a portion is referred to as being "directly above" another portion, no other portion is interposed in between.

[0026] Unless otherwise defined, all terms including technical and scientific terms used herein have the same meaning as commonly understood by those with ordinary knowledge in the art to which this invention belongs. Hereinafter, preferred embodiments of the present disclosure will be described in detail to help those with ordinary knowledge in the art easily achieve the present disclosure.

[0027] FIG. 1 is a view showing a groove 30 formed by emission of a continuous-wave laser of Gaussian mode, after a forsterite layer 20 is formed on a surface of the grain-oriented electrical steel sheet 10.

[0028] As shown in FIG. 1, forming the groove 30 inevitably suffers a disadvantage that the surface spatter or hill-up occurs due to transferring and scattering of the melt around the groove. The grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes a forsterite calcination layer 40 in the direction of both ends of the electric steel sheet 10 on the basis of the upper end of the groove 30, by a width (W_s) of 1.1 to 1.3 times the width (W_0) of the groove 30. Since the forsterite calcination layer 40 does not react with spatter or hill-up, spatter or hill-up can be easily removed.

[0029] FIG. 2 is a schematic view showing a hill-up or spatter 25 formed on an upper portion of the forsterite calcination layer 40 when a laser is emitted onto a surface of a grain-oriented electrical steel sheet 10 according to an embodiment of the present disclosure.

[0030] In an embodiment of the present invention, the forsterite calcination layer 40 may be formed in the direction of both ends of the electrical steel sheet 10 on the basis of the upper end of the groove 30, by a width W_s of 1.1 to 1.3 times the width W_0 of the groove 30. Accordingly, 85% or more of the spatter or hill-up 25 that occurs during emission of the laser is formed on the forsterite calcination layer 40, and the spatter or hill-up 25 can be easily removed.

[0031] As shown in FIGS. 1 and 2, a grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes: a forsterite layer 20 formed on the surface of the electrical steel sheet 10; a groove 30 which is formed on the forsterite layer 20 in a direction perpendicular to a rolling direction; and a forsterite calcination layer which is formed in the direction of both ends of the electrical steel sheet on the basis of an upper end of the groove and has a width (W_s) of 1.1 to 1.3 times the width (W_0) of the groove.

[0032] First, the grain-oriented electrical steel sheet 10 will be described below. The grain-oriented electrical steel sheet is used as a core material of electrical device such as transformer and is a steel sheet with magnetic properties of low core loss and high flux density in order to reduce the power loss of electrical device and increase efficiency. The grain-oriented electrical steel sheet used in one embodiment of the present disclosure is not limited to a grain-oriented electrical steel sheet having a specific composition or crystalline structure, but is applicable to all grain-oriented electrical steel sheets. More specifically, the grain-oriented electrical steel sheet including 1.5 to 7 wt% of Si, with the remainder of Fe and unavoidable impurities may be used. In addition to Si, the grain-oriented electrical steel sheet may further include C, Al, N, P, Mn, Sn, Sb, or the like.

[0033] A forsterite (Mg_2SiO_4) layer 20 is formed on the surface of the grain-oriented electrical steel sheet 10. The forsterite layer 20 may be formed to a thickness of 1 to 5 μm on the surface of the grain-oriented electrical steel sheet 10. The forsterite layer 20 may be generated by a reaction of the oxide layer (SiO_2 or $FeSiO_4$) of the steel sheet surface produced by decarburization annealing in the hot annealing step of the grain-oriented electrical steel sheet 10 with MgO which is the main component of the annealing separator.

[0034] The groove 30 is formed on the forsterite layer 20 in a direction perpendicular to the rolling direction. The groove 30 is formed to reduce the width of magnetic domains for the purpose of improving the magnetic properties of the grain-oriented electrical steel sheet.

[0035] The groove 30 may be formed to a depth of 2.5 to 10 % with respect to the thickness of the electrical steel sheet 10. It is possible to efficiently achieve the effect of magnetic domain refinement within the range described above.

[0036] FIGS. 1 and 2 show the groove 30 being formed in a direction perpendicular to the rolling direction of the electrical steel sheet 10 by way of example, but the present disclosure is not limited thereto. Specifically, the groove 30 may be formed at an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet and may be formed in a linear shape. The noise reduction effect of the grain-oriented electrical steel sheet 10 may be achieved in the range of angles described above.

[0037] The forsterite calcination layer 40 may be formed in the direction of both ends of the electrical steel sheet 10 on the basis of the upper end of the groove 30, by a width (W_s) of 1.1 to 1.3 times the width (W_0) of the groove 30.

[0038] The forsterite calcination layer 40 is calcined by the heat generated during the laser emission of the forsterite layer 20, and has a reduced surface roughness due to sintering of the surface MgO-based forsterite and some unreacted MgO layers. The sheet surface roughness before insulation coating is 0.3 to 5 μm , and the sheet surface roughness is reduced during sintering to 0.1 to 3 μm .

[0039] Since the forsterite calcination layer 40 does not react with spatter or hill-up, compared to when there is no forsterite calcination layer formed, the spatter or the hill-up can be removed more easily. The width (W_s) of the forsterite calcination layer 40 is formed to be 1.1 to 1.3 times the width of the groove (W_0). The spatter or the hill-up 25 can be formed on the forsterite calcination layer 40 only when the width (W_s) of the forsterite calcination layer 40 is formed in the range described above, allowing easy removal thereof. The method for adjusting the width (W_s) of the forsterite calcination layer 40 to the range described above is not particularly limited, although according to an embodiment of the present disclosure, the method may appropriately limit the shape of the laser beam and the laser retention time. This will be described in greater detail below with reference to a method for manufacturing the grain-oriented electrical steel sheet according to an embodiment of the present disclosure.

[0040] The hill-up, which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove 30, or the spatter, which is generated by scattering melt, adversely affects the core loss and the insulation of the electrical steel sheet. Accordingly, it is preferable to remove the hill-up or spatter 25 as much as possible. The grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes the forsterite calcination layer 40 suitably formed therewith, and allows easy removal of the spatter or hill-up 25 formed on the forsterite calcination layer 40. Accordingly, a grain-oriented electrical steel sheet according to an embodiment of the present disclosure may have the hill-up or spatter 25 formed from the surface of the forsterite calcination layer 40 to 1.5 μm or less.

[0041] Brushing or pickling may be implemented to more reliably remove the hill-up or spatter 25. When both brushing and pickling are performed, the hill-up or spatter may remain at a much smaller size.

[0042] FIG. 3 schematically shows a flow diagram of a method for manufacturing a grain-oriented electrical steel sheet according to an embodiment of the present disclosure. The flowchart of the method for manufacturing a grain-oriented electrical steel sheet of FIG. 3 is intended to merely illustrate the present disclosure, while the present disclosure is not limited thereto. Accordingly, various modifications of the method for manufacturing a grain-oriented electrical steel sheet may be contemplated.

[0043] A method for manufacturing a grain-oriented electrical steel sheet according to an embodiment of the present disclosure includes steps of: heating a slab including 1.5 to 7 wt% of Si and other unavoidable impurities, with the remainder being Fe, and hot rolling the slab to prepare a hot rolled steel sheet (S10); cold rolling the hot rolled steel sheet to prepare a cold rolled steel sheet, and then subjecting the cold rolled steel sheet to decarburization annealing and/or nitriding annealing to form an oxide layer on the surface of steel sheet (S20); applying an annealing separator including MgO on the surface of the steel sheet on which the oxide layer is formed and performing hot annealing to form a forsterite layer (forsterite; Mg_2SiO_4) on the surface of the steel sheet (S30); and emitting a continuous-wave laser of Gaussian mode onto the steel sheet formed with the forsterite layer to form a groove on the surface of a steel sheet (S40).

[0044] At this time, in order to form the forsterite calcination layer 40 on the electrical steel sheet, the step of forming a groove (S40) may include a step of appropriately limiting the type, shape, laser retention time, and so on of the laser beam.

[0045] Specifically, the type of the laser beam may be a continuous-wave laser of Gaussian mode. The continuous-wave laser may be used, because pulsed wave oscillation induces evaporation rather than accompanying melting.

[0046] In addition, the shape of the laser beam may be the one that satisfies the range of Formula 1 below.

$$1.3 \leq L_b/L_a \leq 7.0 \text{-----} 1)$$

[0047] FIG. 4 schematically shows the shape of the laser beam according to an embodiment of the present disclosure. As shown in FIG. 4, the ratio (L_b/L_a) of the rolling direction beam length (L_a) to the width direction beam length (L_b) may be in the range of 1.3 to 7.0. When the final beam length ratio is less than 1.3, that is, when the beam shape is close to the circular shape, the width (W_s) of the forsterite calcination layer 40 formed around the groove 30 may be narrowed, and the partial trap of the melt of the groove may occur. When the final beam length ratio exceeds 7.0, that is, when the beam shape is close to the line shape, there may arise a problem in that the formation of the groove 30 becomes difficult, and it is difficult to secure the effect of the magnetic domain refinement. Accordingly, the shape of the laser beam described above may be used.

[0048] The laser retention time (T_d) is defined as a ratio (W/V_s) of the scanning rate (V_s) of the laser beam scanned in the width direction to the widthwise emission width (W) emitted to the steel sheet width and it may be adjusted so as

to satisfy Formula 2 below.

$$0.5 \leq T_d \leq 10.0 \text{ -----2)}$$

[0049] When the retention time is too short, i.e., 0.5 ms or less, problem may occur, in which case the width (W_s) of the forsterite calcination layer is overly narrowed during groove formation. If the retention time is too long, i.e., greater than 10 ms, problem may also occur, in which case the width (W_s) of the forsterite calcination layer is increased, with the scattering length of the hill-up or spatter also being relatively lengthened. Accordingly, the retention time may be adjusted to the range described above. More specifically, the retention time may be 1.0 to 9.6 ms.

[0050] Hereinafter, each step will be described in detail.

[0051] First, in S10, a slab including 1.5 to 7 wt% of Si and other unavoidable impurities, with the remainder being Fe, is heated and hot rolled to prepare a hot rolled steel sheet. The slab used in an embodiment of the present disclosure is not limited to a slab of a particular composition, but is applicable to general slabs used in the manufacture of a grain-oriented electrical steel sheet. More specifically, a slab including 1.5 to 7 wt% of Si, with the remainder of Fe and impurities may be used. In addition to Si, the grain-oriented electrical steel sheet may further include C, Al, N, P, Mn, Sn, Sb, or the like

[0052] Next, in S20, the hot rolled steel sheet is cold rolled to prepare a cold rolled steel sheet, and then subjected to decarburization annealing and/or nitriding annealing to form an oxide layer on the surface of steel sheet. Either the decarburization annealing or the nitriding annealing may be performed, or both the decarburization annealing and the nitriding annealing may be performed. When both the decarburization annealing and the nitriding annealing are performed, the order in which the annealing is performed is not limited, and may also be performed simultaneously. The oxide layer of the steel sheet surface may be formed from SiO_2 or FeSiO_4 .

[0053] Next, in S30, an annealing separator including MgO is applied to the surface of the steel sheet on which the oxide layer is formed, and hot annealing is performed to form a forsterite layer (forsterite; Mg_2SiO_4) on the surface of the steel sheet. At this time, the forsterite layer 20 may be formed to a thickness of 1 to 5 μm on the surface of the grain-oriented electrical steel sheet 10 and may include unreacted MgO as well as forsterite (Mg_2SiO_4).

[0054] Next, in S40, a continuous-wave laser of Gaussian mode is emitted onto the steel sheet formed with the forsterite layer to form a groove on the surface of a steel sheet. At this time, the forsterite layer is sintered by the heat generated from the laser, to thus form the forsterite calcination layer 40. In S40, the width (W_s) of the forsterite calcination layer 40 may be adjusted by limiting the type, shape, and retention time of the emitted laser. The width (W_s) of the forsterite calcination layer 40 may be formed to be 1.1 to 1.3 times the width of the groove (W_0).

[0055] In S40, the groove 30 may be formed to a depth of 2.5 to 10 % with respect to the thickness of the electrical steel sheet 10. It is possible to efficiently achieve the effect of magnetic domain refinement within the range described above. In addition, in S40, the groove 30 may be formed at an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet, and may be formed in a linear shape. The noise reduction effect of the grain-oriented electrical steel sheet 10 may be achieved in the range of angles described above.

[0056] During the process of forming the groove 30 through the laser emission in S40, the hill-up, which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove, or the spatter, which is generated by scattering melt, is formed on the forsterite calcination layer 40. At this time, since the forsterite calcination layer 40 does not react with the spatter or hill-up, spatter or hill-up may be easily removed.

[0057] Although not shown in FIG. 3, after step S40, the method may further include a step of removing the hill-up or spatter on the surface of the forsterite calcination layer to 1.5 μm or less (S50).

[0058] The step (S50) may include dry-removing using brush (S50-1), or wet-removing through pickling (S50-2). The method may include either or both of the two steps mentioned above. When both of the two steps are included, the surface roughness characteristic of 1.0 μm or less may be secured.

[0059] The step (S50-1) is about dry-removing using brush. In this case, brush is not particularly limited as long as it is a material capable of removing hill-up or spatter, and may be specifically metal-based material or abrasive material, for example. As described above, since the forsterite calcination layer 40 does not react with the spatter or hill-up 25, it may be easily removed with a less frictional force.

[0060] The step (S50-2) is about wet-removing by pickling. For pickling, a solution that can dissolve away the hill-up or spatter may be used, such as an aqueous solution including hydrochloric acid, nitric acid or sulfuric acid, for example. In this example, the concentration of aqueous solution may be 1 to 30 wt%.

[0061] After step (S50), a step of stress relief annealing may be further included.

[0062] Hereinafter, the present disclosure is explained in more detail with reference to Examples. However, the Examples are described merely to illustrate the present disclosure, and the present disclosure is not limited thereto.

Example 1

[0063] A grain-oriented electrical steel sheet with a thickness of 0.23 mm was prepared, having a forsterite layer formed on the surface thereof by applying a MgO annealing separator and performing hot annealing. The continuous wave laser of Gaussian mode was emitted, with the emission linewidth of 6 distinct lines at the interval of 200 mm, and the laser retention time being maintained for 3.0 ms. The beam shape (L_a/L_b) of the laser was controlled to be 1.3 and the groove depth was controlled to be 13 μm . The width (W_0) of the upper portion of the groove was 45 μm , and the maximum height of the hill-up and spatter appearing around the groove was 5 μm . The width (W_s) of the forsterite calcination layer was 55 μm .

[0064] The hill-up and spatter were polished with brush (200 μm diameter, stainless steel material, 50 % areal density). The maximum height of the hill-up and spatter after polishing was 0.95 μm . Then, the grain-oriented electrical steel sheet was prepared using 10 wt% sulfuric acid aqueous solution. The maximum height of hill-up and spatter after pickling was 0.3 μm .

[0065] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

Example 2

[0066] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1 below and that pickling was not performed.

[0067] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

Example 3

[0068] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1.

[0069] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

Example 4

[0070] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1, and that brushing was not performed.

[0071] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

Example 5

[0072] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1 below and that pickling was not performed.

[0073] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

Comparative Example 1

[0074] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1 below and that neither brushing, nor pickling was performed.

[0075] The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

5 **Comparative Example 2**

[0076] The sample was prepared in the same manner as in Example 1 described above except that the beam shape (L_a/L_b) of the laser, the depth of the groove and the laser retention time were changed to the values summarized in the Table 1 below and that neither brushing, nor pickling was performed.

10 **[0077]** The core loss ($W_{17/50}$) of the electric steel sheet before laser emission and the core loss after laser emission and stress relief annealing (SRA) were measured and are summarized in Table 1 below. The electrical insulating value and space factor were measured and are summarized in Table 1 below.

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(Table 1)

Items	Groove depth (μm)	Laser beam shape (L_a/L_b)	Retention time (ms)	Ratio of calcination layer width to groove width	Use of brush	Use of pickling	Before laser emission	After SRA	Core loss enhance	Electrical insulating value	Space factor
							$W_{17/50}$		%		mA
Ex. 1	13	1.3	0.5	1.1	Yes	Yes	0.83	0.71	14.5	5	97.0
Ex. 2	18	1.3	10.0	1.3	Yes	No	0.83	0.72	13.3	30	96.5
Ex. 3	13	6.7	6.5	1.2	Yes	Yes	0.84	0.70	16.7	0	96.9
Ex. 4	12	7.0	0.5	1.1	No	Yes	0.83	0.71	14.5	10	96.9
Ex. 5	17	7.0	10.0	1.3	Yes	No	0.84	0.73	13.1	35	96.6
Comp. Ex. 1	21	7.0	11.0	1.4	No	No	0.83	0.77	7.2	650	93.5
Comp. Ex. 2	8	7.0	0.3	0.9	No	No	0.84	0.78	7.1	350	94.5

[0078] As shown in Table 1, the grain-oriented electrical steel sheet prepared according to Examples 1 to 5 was prevented from experiencing deterioration of the electrical insulating value and space factor, and the core loss improvement rate of 13% or more could be achieved after heat treatment.

<Description of symbols>

[0079]

10: grain-oriented electrical steel sheet, 20: forsterite layer

25: hill-up, spatter 30: groove

40: forsterite calcination layer

Claims

1. A grain-oriented electrical steel sheet, comprising:
a forsterite layer formed on the surface of an electrical steel sheet;

a groove which is formed on the forsterite layer in a direction perpendicular to a rolling direction; and
a forsterite calcination layer which is formed in the direction of both ends of the electrical steel sheet on the basis of an upper end of the groove and has a width of 1.1 to 1.3 times the width of the groove.
2. The grain-oriented electrical steel sheet of claim 1, wherein
a hill-up, which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove on an upper portion of the forsterite calcination layer, or the spatter, which is generated by scattering melt, is formed to $1.5\ \mu\text{m}$ or less from a surface of the forsterite calcination layer.
3. The grain-oriented electrical steel sheet of claim 1, wherein
the groove is formed to a depth of 2.5 to 10 % with respect to a thickness of the electrical steel sheet.
4. The grain-oriented electrical steel sheet of claim 1, wherein
the groove is formed at an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet and formed in a linear shape.
5. The grain-oriented electrical steel sheet of any of claims 1 to 4, wherein
the hill-up, which is an elevation of melt generated during formation of the groove and accumulated on both sides of the groove on the upper portion of the forsterite calcination layer, or the spatter, which is generated by scattering melt, is removed by brushing or pickling.
6. A method for manufacturing a grain-oriented electrical steel sheet, comprising steps of:

heating a slab including 1.5 to 7 wt% of Si and other unavoidable impurities, with the remainder being Fe, and hot rolling the slab to prepare a hot rolled steel sheet;
cold rolling the hot rolled steel sheet to prepare a cold rolled steel sheet, and then subjecting the cold rolled steel sheet to decarburization annealing and/or nitriding annealing to form an oxide layer on the surface of steel sheet;
applying an annealing separator including MgO on the surface of the steel sheet on which the oxide layer is formed and performing hot annealing to form a forsterite layer (forsterite; Mg_2SiO_4) on the surface of the steel sheet; and
emitting a continuous-wave laser of Gaussian mode onto the steel sheet formed with the forsterite layer to form a groove on the surface of a steel sheet,
wherein, in the step of forming the groove, the beam shape of the continuous-wave laser satisfies the range of Formula 1 below, and the retention time T_d of the continuous wave laser satisfies the range of Formula 2 below.

$$1.3 \leq L_b/L_a \leq 7.0 \text{-----} 1)$$

$$0.5 \leq T_d \leq 10.0 \text{ -----2)}$$

wherein L_a is the length of the laser beam in the rolling direction and L_b is the widthwise length of the laser beam and T_d is a ratio (W/V_s) of the scanning rate (V_s) of the laser beam scanned in the width direction to the widthwise emission width (W) emitted to the steel sheet width.

7. The method of claim 6, wherein the step of forming the groove comprises a step of emitting a continuous-wave laser of Gaussian mode to form a forsterite calcination layer in the direction of both ends of the electric steel sheet on the basis of the upper end of the groove, by a width of 1.1 to 1.3 times the width of the groove.
8. The method of claim 6, wherein the step of forming the groove comprises a step of forming the groove to a depth of 2.5 to 10 % with respect to the thickness of the electrical steel sheet.
9. The method of claim 6, wherein the step of forming the groove comprises a step of forming the groove to an angle of ± 90 to $\pm 85^\circ$ with respect to the rolling direction of the electrical steel sheet, and in a linear shape.
10. The method of any of claims 6 to 9, wherein the step of forming the groove further comprises steps of: forming a hill-up, which is an elevation of melt generated during a formation of the groove and accumulated on both sides of the groove, or the spatter, which is generated by scattering melt, on an upper portion of the forsterite calcination layer; and removing the hill-up or the spatter on the surface of the forsterite calcination layer to 1.5 μm or less.
11. The method of claim 10, wherein the step of removing the hill-up or the spatter comprises a step of dry-removing using brush.
12. The method of claim 11, wherein the brush is a metal-based material or abrasive material.
13. The method of claim 10, wherein the step of removing the hill-up or the spatter further comprises a step of wet-removing using pickling.
14. The method of claim 13, wherein the pickling is carried out using an aqueous solution including hydrochloric acid, nitric acid or sulfuric acid.
15. The method of claim 14, wherein a concentration of the aqueous solution is 1 to 30 wt%.

Patentansprüche

1. Kornorientiertes Elektrostahlblech, umfassend:

eine Forsteritschicht, die auf der Oberfläche eines Elektrostahlblechs ausgebildet ist;
eine Nut, die auf der Forsteritschicht in einer Richtung senkrecht zu einer Walzrichtung ausgebildet ist; und
eine Forsteritkalzinierungsschicht, die in der Richtung beider Enden des Elektrostahlblechs auf Grundlage eines oberen Endes der Nut ausgebildet ist und eine Breite vom 1,1- bis 1,3-Fachen der Breite der Nut aufweist.

2. Kornorientiertes Elektrostahlblech nach Anspruch 1, wobei

eine Erhebung, bei der es sich um eine Erhöhung aus Schmelze handelt, die während einer Ausbildung der Nut erzeugt wird und sich auf beiden Seiten der Nut an einem oberen Abschnitt der Forsteritkalzinierungsschicht ansammelt, oder die Spritzer, die durch Streuung von Schmelze erzeugt werden, auf 1,5 μm oder weniger von einer

Oberfläche der Forsteritkalzinierungsschicht aus ausgebildet werden.

3. Kornorientiertes Elektrostahlblech nach Anspruch 1, wobei die Nut auf eine Tiefe von 2,5 bis 10 % in Bezug auf eine Dicke des Elektrostahlblechs ausgebildet wird.
4. Kornorientiertes Elektrostahlblech nach Anspruch 1, wobei die Nut in einem Winkel von ± 90 bis $\pm 85^\circ$ in Bezug auf die Walzrichtung des Elektrostahlblechs ausgebildet ist und in einer linearen Form ausgebildet ist.
5. Kornorientiertes Elektrostahlblech nach einem der Ansprüche 1 bis 4, wobei die Erhebung, bei der es sich um eine Erhöhung aus Schmelze handelt, die während einer Ausbildung der Nut erzeugt wird und sich auf beiden Seiten der Nut an einem oberen Abschnitt der Forsteritkalzinierungsschicht ansammelt, oder die Spritzer, die durch Streuung von Schmelze erzeugt werden, durch Bürsten oder Beizen entfernt werden.

6. Verfahren zum Herstellen eines kornorientierten Elektrostahlblechs, umfassend die Schritte:

Erwärmen einer Bramme, die 1,5 bis 7 Gew.-% Si und andere unvermeidbare Verunreinigungen enthält, wobei der Rest aus Fe besteht, und Warmwalzen der Bramme, um ein warmgewalztes Stahlblech herzustellen;
 Kaltwalzen des warmgewalzten Stahlblechs, um ein kaltgewalztes Stahlblech herzustellen, und dann Unterziehen des kaltgewalzten Stahlblechs einem Entkohlungsglühen und/oder Nitrierungsglühen, um eine Oxidschicht auf der Oberfläche des Stahlblechs auszubilden;
 Auftragen eines MgO enthaltenden Glühseparators auf die Oberfläche des Stahlblechs, auf der die Oxidschicht ausgebildet ist, und Durchführen von Warmglühen, um eine Forsteritschicht (Forsterit; Mg_2SiO_4) auf der Oberfläche des Stahlblechs auszubilden; und
 Bestrahlen des mit der Forsteritschicht ausgebildeten Stahlblechs mit einem Dauerstrichlaser im Gauß-Modus, um eine Nut an der Oberfläche eines Stahlblechs auszubilden;
 wobei beim Schritt zum Ausbilden der Nut die Strahlform des Dauerstrichlasers den Bereich der unten stehenden Formel 1 erfüllt und die Verweildauer T_d des Dauerstrichlasers den Bereich der unten stehenden Formel 2 erfüllt,

$$1,3 \leq L_b/L_a \leq 7,0 \text{ -----1)}$$

$$0,5 \leq T_d \leq 10,0 \text{ -----2)}$$

wobei L_a die Länge des Laserstrahls in der Walzrichtung ist und L_b die Quirlänge des Laserstrahls ist und T_d ein Verhältnis (W/V_s) der Abtastrate (V_s) des Laserstrahls ist, mit dem in der Breitenrichtung abgetastet wird, zur auf die Stahlblechbreite abgegebenen Emissionsbreite (W) in Querrichtung ist.

7. Verfahren nach Anspruch 6, wobei der Schritt zum Ausbilden der Nut einen Schritt zum Bestrahlen mit einem Dauerlichtlaser im Gauß-Modus umfasst, um eine Forsteritkalzinierungsschicht in der Richtung beider Enden des Elektrostahlblechs auf Grundlage des oberen Endes der Nut mit einer Breite vom 1,1- bis 1,3-Fachen der Breite der Nut auszubilden.
8. Verfahren nach Anspruch 6, wobei der Schritt zum Ausbilden der Nut einen Schritt zum Ausbilden der Nut auf eine Tiefe von 2,5 bis 10 % in Bezug auf die Dicke des Elektrostahlblechs umfasst.
9. Verfahren nach Anspruch 6, wobei der Schritt zum Ausbilden der Nut einen Schritt zum Ausbilden der Nut in einem Winkel von ± 90 bis $\pm 85^\circ$ in Bezug auf die Walzrichtung des Elektrostahlblechs und in einer linearen Form umfasst.
10. Verfahren nach einem der Ansprüche 6 bis 9, wobei der Schritt zum Ausbilden der Nut ferner die folgenden Schritte umfasst:

Ausbilden einer Erhebung, bei der es sich um eine Erhöhung aus Schmelze handelt, die während einer Aus-

bildung der Nut erzeugt wird und sich auf beiden Seiten der Nut ansammelt, oder der Spritzer, die durch Streuung von Schmelze erzeugt werden, an einem oberen Abschnitt der Forsteritkalzinierungsschicht; und Entfernen der Erhebung oder der Spritzer an der Oberfläche der Forsteritkalzinierungsschicht auf 1,5 µm oder weniger.

11. Verfahren nach Anspruch 10, wobei der Schritt zum Entfernen der Erhebung oder der Spritzer einen Schritt zum trockenen Entfernen mittels einer Bürste umfasst.
12. Verfahren nach Anspruch 11, wobei es sich bei der Bürste um ein metallhaltiges Material oder ein Schleifmaterial handelt.
13. Verfahren nach Anspruch 10, wobei der Schritt zum Entfernen der Erhebung oder der Spritzer ferner einen Schritt zum nassen Entfernen mittels Beizen umfasst.
14. Verfahren nach Anspruch 13, wobei das Beizen unter Verwendung einer wässrigen Lösung, einschließlich Salzsäure, Salpetersäure oder Schwefelsäure, ausgeführt wird.
15. Verfahren nach Anspruch 14, wobei eine Konzentration der wässrigen Lösung 1 bis 30 Gew.-% beträgt.

Revendications

1. Tôle d'acier magnétique à grains orientés, comprenant :

une couche de forstérite formée sur la surface d'une tôle d'acier magnétique ;
une rainure qui est formée sur la couche de forstérite dans une direction perpendiculaire à une direction de laminage ; et
une couche de calcination de forstérite qui est formée dans la direction des deux extrémités de la tôle d'acier magnétique sur la base d'une extrémité supérieure de la rainure et a une largeur de 1,1 à 1,3 fois la largeur de la rainure.

2. Tôle d'acier magnétique à grains orientés selon la revendication 1, dans laquelle un monticule, qui est une élévation de bain fondu généré pendant une formation de la rainure et accumulé sur les deux côtés de la rainure sur une portion supérieure de la couche de calcination de forstérite, ou l'éclaboussure, qui est générée par diffusion de bain fondu, est formé à 1,5 µm ou moins d'une surface de la couche de calcination de forstérite.
3. Tôle d'acier magnétique à grains orientés selon la revendication 1, dans laquelle la rainure est formée à une profondeur de 2,5 à 10 % par rapport à une épaisseur de la tôle d'acier magnétique.
4. Tôle d'acier magnétique à grains orientés selon la revendication 1, dans laquelle la rainure est formée à un angle de ± 90 à $\pm 85^\circ$ par rapport à la direction de laminage de la tôle d'acier magnétique et formée selon une forme linéaire.
5. Tôle d'acier magnétique à grains orientés selon l'une quelconque des revendications 1 à 4, dans laquelle le monticule, qui est une élévation de bain fondu généré pendant une formation de la rainure et accumulé sur les deux côtés de la rainure sur la portion supérieure de la couche de calcination de forstérite, ou l'éclaboussure, qui est générée par diffusion de bain fondu, est éliminé par brossage ou décapage.
6. Procédé de fabrication d'une tôle d'acier magnétique à grains orientés, comprenant des étapes de :

chauffage d'une brame incluant de 1,5 à 7 % en poids de Si et autres impuretés inévitables, le reste étant du Fe, et laminage à chaud de la brame pour préparer une tôle d'acier laminée à chaud ;
laminage à froid de la tôle d'acier laminée à chaud pour préparer une tôle d'acier laminée à froid, puis présentation

de la tôle d'acier laminée à froid à un recuit de décarburation et/ou un recuit de nitruration pour former une couche d'oxyde sur la surface de tôle d'acier ;
 application d'un séparateur de recuit incluant du MgO sur la surface de la tôle d'acier sur laquelle la couche d'oxyde est formée et réalisation d'un recuit à chaud pour former une couche de forstérite (forstérite ; Mg_2SiO_4) sur la surface de la tôle d'acier ; et
 émission d'un laser à onde continue de mode gaussien sur la tôle d'acier formée avec la couche de forstérite pour former une rainure sur la surface d'une tôle d'acier,
 dans lequel, à l'étape de formation de la rainure, la forme de faisceau du laser à onde continue satisfait la plage de formule 1 ci-dessous, et le temps de séjour T_d du laser à onde continue satisfait la plage de formule 2 ci-dessous,

$$1,3 \leq L_b/L_a \leq 7,0 \text{-----1)}$$

$$0,5 \leq T_d \leq 10,0 \text{-----2)}$$

dans lequel L_a est la longueur du faisceau laser dans la direction de laminage et L_b est la longueur dans le sens de la largeur du faisceau laser et T_d est un rapport (W/V_s) entre le taux de balayage (V_s) du faisceau laser balayé dans la direction de largeur et la largeur d'émission dans le sens de la largeur (W) émise sur la largeur de tôle d'acier.

7. Procédé selon la revendication 6, dans lequel l'étape de formation de la rainure comprend une étape d'émission d'un laser à onde continue de mode gaussien pour former une couche de calcination de forstérite dans la direction des deux extrémités de la tôle d'acier magnétique sur la base de l'extrémité supérieure de la rainure, d'une largeur de 1,1 à 1,3 fois la largeur de la rainure.
8. Procédé selon la revendication 6, dans lequel l'étape de formation de la rainure comprend une étape de formation de la rainure à une profondeur de 2,5 à 10 % par rapport à l'épaisseur de la tôle d'acier magnétique.
9. Procédé selon la revendication 6, dans lequel l'étape de formation de la rainure comprend une étape de formation de la rainure à un angle de ± 90 à $\pm 85^\circ$ par rapport à la direction de laminage de la tôle d'acier magnétique, et selon une forme linéaire.
10. Procédé selon l'une quelconque des revendications 6 à 9, dans lequel l'étape de formation de la rainure comprend en outre des étapes de :
 formation d'un monticule, qui est une élévation de bain fondu généré pendant une formation de la rainure et accumulé sur les deux côtés de la rainure, ou l'éclaboussure, qui est générée par diffusion de bain fondu, sur une portion supérieure de la couche de calcination de forstérite ; et
 élimination du monticule et/ou de l'éclaboussure sur la surface de la couche de calcination de forstérite jusqu'à $1,5 \mu\text{m}$ ou moins.
11. Procédé selon la revendication 10, dans lequel l'étape d'élimination du monticule ou de l'éclaboussure comprend une étape d'élimination à sec à l'aide d'une brosse.
12. Procédé selon la revendication 11, dans lequel la brosse est un matériau à base de métal ou un matériau abrasif.
13. Procédé selon la revendication 10, dans lequel l'étape d'élimination du monticule ou de l'éclaboussure comprend en outre une étape d'élimination humide à l'aide d'un décapage.
14. Procédé selon la revendication 13, dans lequel le décapage est réalisé à l'aide d'une solution aqueuse incluant de l'acide chlorhydrique, de l'acide nitrique ou de l'acide sulfurique.

- 15.** Procédé selon la revendication 14, dans lequel
une concentration de la solution aqueuse est de 1 à 30 % en poids.

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FIG. 1

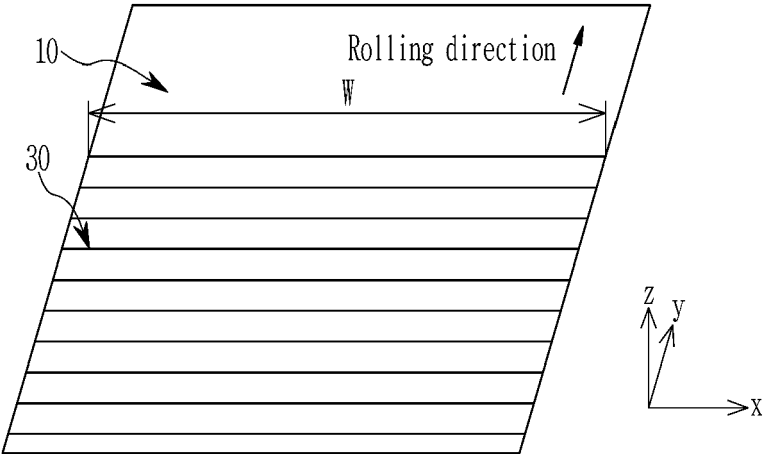


FIG. 2

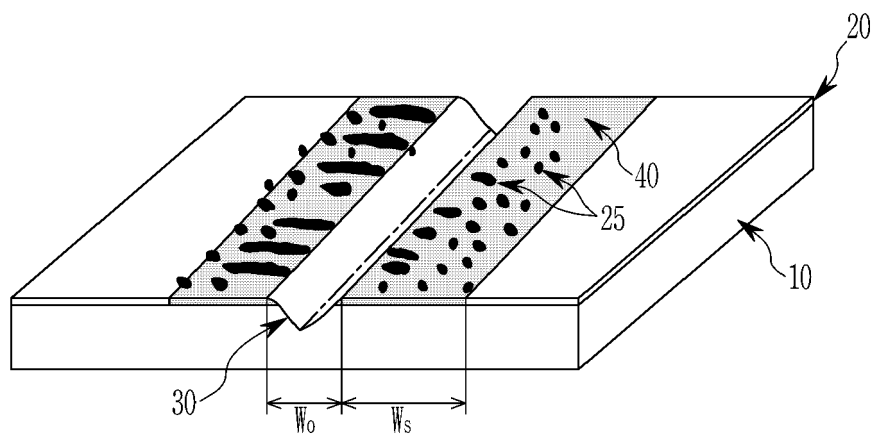


FIG. 3

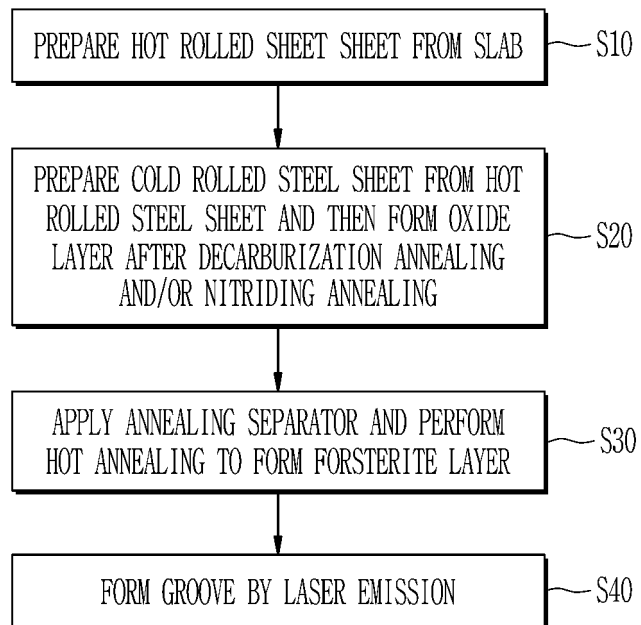
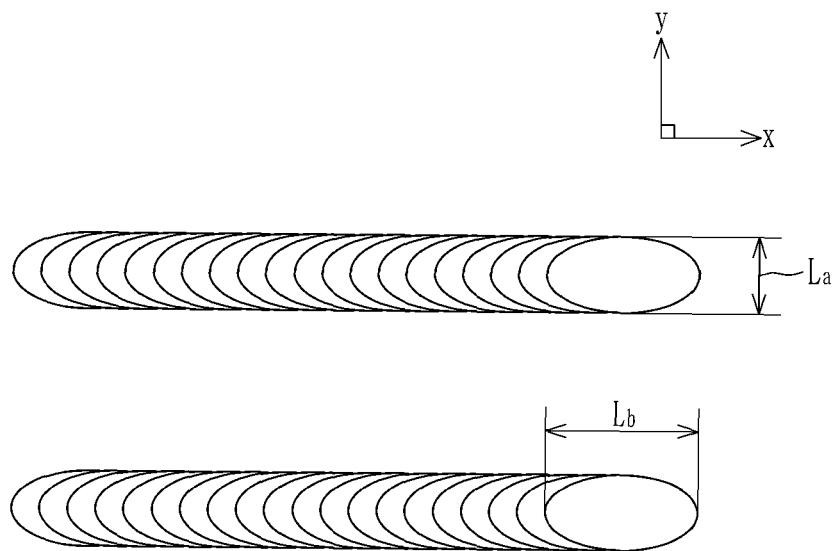


FIG. 4



REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

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