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(54) **APPLIANCE FOR THE MOIRÉ MEASUREMENT OF AN OPTICAL TEST OBJECT**

VORRICHTUNG ZUR MOIRÉ-VERMESSUNG EINES OPTISCHEN PRÜFKÖRPERS

APPAREIL DESTINÉ À LA MESURE DU MOIRÉ D'UN OBJET DE TEST OPTIQUE

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**Description**

## BACKGROUND OF THE INVENTION

5 Field of the invention

**[0001]** The invention relates to an appliance for the moiré measurement of an optical test object.

10 Prior art

**[0002]** Microlithography is used for producing microstructured components such as, for example, integrated circuits or LCDs. The microlithography process is carried out in a so-called projection exposure apparatus comprising an illumination device and a projection lens. The image of a mask (reticle) illuminated by means of the illumination device is in this case projected by means of the projection lens onto a substrate (for example a silicon wafer) coated with a light-sensitive layer (photoresist) and arranged in the image plane of the projection lens, in order to transfer the mask structure to the light-sensitive coating of the substrate.

**[0003]** In practice, there is a need to determine optical aberrations, such as e.g. the distortion of the projection lens, as exactly as possible. In particular, the technique of a moiré measurement is known in this respect, said technique comprising the projection of a first grating arranged in an object plane of the projection lens onto a second grating (also referred to as "moiré mask") arranged in the image plane of the projection lens and the measurement of the light intensity respectively transmitted through this arrangement using an (e.g. camera-based) detector arrangement.

**[0004]** Fig. 8 and 9 show merely schematic illustrations for explaining this principle. Here, the first grating situated in the object plane of the test object in the form of a projection lens 6 is denoted by "5", the produced image of the test structures contained in the first grating 5 is denoted by "7" and the second grating or the moiré mask is denoted by "8".

As a rule, the planes of the test structure image on the one hand and of the second grating 8 or of the moiré mask on the other hand coincide and are depicted with spatial separation in Fig. 8 and 9 only for the purposes of a better illustration. The light distribution 10 (which in accordance with Fig. 9 typically has a characteristic stripe pattern) obtained downstream of the second grating 8 or of the moiré mask in the light propagation direction is determined by way of a detector arrangement 9. Here, in the case of an appropriate design of the grating arrangement made of the first grating and the second grating, the transmitted light intensity in the case of aberration-free imaging is at a maximum and it is reduced in the case where optical aberrations of the projection lens 6 are present since the light from bright regions of the test structures contained in the first grating 5 are increasingly incident on dark regions of the second grating 8 or of the moiré mask in the case of aberration-afflicted imaging.

**[0005]** Different measurement and evaluation methods based on the moiré measurement are known for ascertaining the respectively relevant optical aberrations of the test object or projection lens.

**[0006]** However, what needs to be taken into account here in practice is that the respective measurement signals obtained with the detector arrangement 9 during the aforementioned moiré measurement are not only determined by optical aberrations of the test object or projection lens 6 to be measured, but may possibly also be influenced by manufacturing faults of the first grating 5 containing the test structures and/or of the second grating 8 forming the moiré mask. This is because a consequence of such manufacturing faults is that the respective gratings 5, 8 no longer "fit to one another" in respect of the caused superposition, even in the case of aberration-free imaging by the projection lens 6, and hence fabricate the presence of an optical aberration of the test object in the respectively obtained measurement results.

**[0007]** In order to overcome this problem, it is known to carry out a so-called calibration method, in which - as indicated in Fig. 10 - the test object or projection lens 6 is measured in a plurality of different measurement positions, wherein these measurement positions differ from one another in respect of the positioning of the test object relative to the measurement system or the aforementioned grating arrangement made of first grating 5 and second grating 8. In principle, this facilitates a separation of the respective components of the test object from the components of the measurement system in the obtained measurement signals or in the evaluation result obtained in the detection plane. Sometimes, the method is also referred to as a self-calibration method.

**[0008]** In practice, further, there is also the need for a moiré measurement of so-called anamorphic imaging systems. Here, anamorphic imaging is understood to mean imaging which produces a distorted image of the object and which is not an instance of similarity imaging (i.e. which is not representable by a combination of displacement, rotation, mirroring and scaling). In a special case, such an anamorphic imaging system may be e.g. a projection lens which has different imaging scales along two mutually different axes.

**[0009]** A problem occurring when measuring such anamorphic imaging systems in conjunction with the above-described calibration method is that - as indicated in Fig. 11 (in which components which are analogous or have substantially the same function to those in Fig. 8 and Fig. 10 are denoted by corresponding reference signs which, however, have

been appended by an apostrophe) - in the different measurement positions brought about during the calibration, there is no longer an originally present fit or correspondence between the moiré mask and these test structures in specific measurement positions (which e.g. are brought about by rotations) as a consequence of the distorted imaging of the test structures, with the consequence that a correct evaluation of the measurement signals becomes difficult or even impossible and the aforementioned calibration method is no longer applicable.

**[0010]** WO 2016/097048 A1 discloses inter alia a wavefront measuring device for measuring a wavefront in a projection lens of a projection exposure apparatus, the wavefront measuring device comprising a Moiré grating arrangement having an object grating and an image grating which are coordinated with one another in a manner true to scale in such a way as to generate a Moiré superimposition pattern from an imaging of the object grating onto the image plane and the image grating.

**[0011]** US 2011/0063592 A1 discloses inter alia an optical property measuring apparatus which makes it possible to measure distortion in an optical system under examination based on a detected moiré fringe, wherein a first periodic pattern is positioned in the optical path upstream of the optical system under examination and a second periodic pattern is positioned in the optical path downstream of the optical system under examination.

**[0012]** WO 2015/124372 A2 discloses inter alia a lithographic system comprising an anamorphic projection system.

**[0013]** DE 10 2005 041 373 A1 discloses inter alia a method and device for a calibrating wavefront measurement of an optical system.

**[0014]** With regard to the further prior art, reference is made purely by way of example to US 6,816,247 B1.

## SUMMARY OF THE INVENTION

**[0015]** Against the aforementioned background, it is an object of the present invention to provide an appliance for the moiré measurement of an optical test object, which facilitates a correct moiré measurement which takes into account possible manufacturing faults of the measurement system, in particular including the above-described calibration method, even in the case of anamorphic imaging systems.

**[0016]** This object is achieved by the arrangement according to the features of independent claim 1.

**[0017]** An appliance for the moiré measurement of an optical test object comprises:

- a test object, which is an anamorphic imaging system;
- a grating arrangement made of a first grating which is positioned in the optical beam path upstream of the test object and which comprises test structures to be imaged and a second grating which is positioned in the optical beam path downstream of the test object; and
- an evaluation unit comprising at least one detector, for evaluating moiré structures produced by superposition of the two gratings in a detection plane situated downstream of the second grating in the optical beam path;
- wherein the respective grating periods of the first grating and of the second grating are selected in such a way that the grating period of the second grating corresponds to a common multiple or a common divisor of the respective periods of two test structure images of the test structures of the first grating produced by the imaging system in two different measurement positions, wherein the two measurement positions differ in respect of the relative position of grating arrangement and test object.

**[0018]** Here it is possible, for example (without, however, the invention being restricted thereto), to obtain respectively one measurement result in the at least two measurement positions, in which the light intensity transmitted through the grating arrangement is at a maximum in the case of aberration-free imaging by the test object and reduced in the case where optical aberrations of the test object are present. In other embodiments (where use is made of so-called "inverse" structures which lead to the greatest possible shadowing in the case of aberration-free imaging), a signal minimum may conversely also be obtained for the aberration-free imaging.

**[0019]** Here, in line with conventional terminology, "anamorphic" imaging is understood to mean imaging which produces a distorted image of an object and which does not represent similarity imaging (such that the imaging is not representable by a combination of displacement, rotation, mirroring and scaling). An example of an anamorphic imaging system is a projection lens which has different imaging scales along two different axes.

**[0020]** In particular, the invention is based on the concept of providing such a design of the moiré mask in the grating arrangement made of a first grating having the respective test structures and a second grating forming the moiré mask within an appliance for the moiré measurement that, in the case of aberration-free imaging by the test object, there is correspondence for at least some lines (preferably as many lines as possible) of the image of the test structures produced during the anamorphic imaging with the structures present on the moiré mask in each of the at least two individual

measurement positions.

**[0021]** By way of example, in one exemplary embodiment, it is possible for instance to select a design of the moiré mask in which, in a second measurement position which is rotated in relation to the first initial measurement position, only every second line on the moiré mask still "sees light" whereas the lines situated therebetween "remain dark"; i.e., expressed differently, the period of the moiré mask is twice the size of the period of the images of the respective test structures.

**[0022]** In this case, a correct evaluation is possible, wherein use is made of the fact that, even in the scenario described above, the brightness occurring in the detection plane still is at a maximum in the case of a perfect fit of the images of the test structures to the structures on the moiré mask but said brightness is at a minimum in the case of the offset thereof by half a period, wherein, further, a decrease in the entire luminous energy in the detection plane, occurring overall, is not important here.

**[0023]** Expressed differently, the invention contains the concept of designing the grating arrangement made of the first grating positioned upstream of the test object in the optical beam path and the second grating positioned downstream of the test object in the optical beam path within an appliance for the moiré measurement such that the calibration method described at the outset is facilitated in each case in combination with the test object to be measured, even in the case of anamorphic imaging by the test object; i.e., a correct moiré measurement or evaluation of the signals obtained here in the plurality of rotational and/or displacement positions between the measurement arrangement comprising said grating arrangement on the one hand and the test object on the other hand is possible.

**[0024]** Here, the invention further also contains the concept of selecting the relevant rotational positions in a suitable manner to the extent that a light loss which is too great is avoided in the respective specific application situation, i.e. not leaving large regions of the respective gratings of the grating arrangement unused where possible.

**[0025]** Further, the invention also contains the concept of suitably selecting the respective line widths of the structures on the moiré mask on the one hand and of the grating positioned upstream of the test object on the other hand. By way of example, what is possible to be avoided here - as will still be explained in more detail below - is that one and the same line on the moiré mask is simultaneously exposed by two lines or test structures of the first grating in specific measurement positions. In particular, it is possible to avoid an unwanted overlap of lines that do not fit to one another arising.

**[0026]** In accordance with one embodiment, the respective grating periods of the first grating and of the second grating are selected in such a way that, for the two measurement positions, the light intensity transmitted through the grating arrangement is either at a maximum or at a minimum in the case of aberration-free imaging by the test object.

**[0027]** In accordance with one embodiment, the at least two measurement positions differ by a relative rotation of the test object and the grating arrangement in relation to one another and/or by a relative translation of the test object and the grating arrangement in relation to one another.

**[0028]** In accordance with one embodiment, the at least two measurement positions are selected in such a way that the imaging scales, in each case effective for these measurement positions, have a rational relationship with respect to one another.

**[0029]** In accordance with one embodiment, line widths of test structures on the first grating and line widths of structures on the second grating are selected in such a way that, for the at least two measurement positions, no line on the second grating is exposed simultaneously by two lines of the test structures of the first grating.

**[0030]** In accordance with one embodiment, line widths of test structures on the first grating and line widths of structures on the second grating are selected in such a way that, for the at least two measurement positions, respectively all pairs of test structure lines, contributing to the imaging, on the first grating and lines on the second grating have the same dependence on optical aberrations of the test object in respect of the luminous energy transmitted through the respective line pair. Expressed differently, all exposed lines on the second grating or the moiré mask which contribute to the imaging are in phase to the extent that when a line on the second grating just has a maximum brightness or maximum shadowing, every other line on the second grating contributing to the measurement signal likewise has a maximum brightness or maximum shadowing. What this avoids is that a line on the second grating is completely illuminated at a specific instant while another line on the second grating is only partly illuminated at the same instant.

**[0031]** In accordance with one embodiment, the optical test object is a projection lens of a microlithographic projection exposure apparatus.

**[0032]** In accordance with one embodiment, the optical test object is designed for operation at an operating wavelength of less than 30 nm, in particular less than 15 nm.

**[0033]** The invention further relates to a method for the moiré measurement of an optical test object, wherein the test object is an anamorphic imaging system and wherein the method comprises the following steps:

- positioning a first grating having test structures to be imaged in the optical beam path upstream of the test object and positioning a second grating in the optical beam path downstream of the test object; and
- evaluating moiré structures produced by superposition of the two gratings in a detection plane situated in the optical

beam path downstream of the second grating, in at least two measurement positions which differ from one another in respect of the relative position of grating arrangement and test object;

- wherein the respective grating periods of the first grating and of the second grating are selected in such a way that the grating period of the second grating corresponds to a common multiple or a common divisor of the respective periods of two test structure images of the test structures of the first grating produced by the imaging system in the two different measurement positions.

**[0034]** In accordance with one embodiment, the first grating and the second grating are rotated by mutually different angles of rotation in a second measurement position relative to a first measurement position.

$$\theta_{img} = \arctan\left(\frac{\beta_y}{\beta_x} \cdot \tan \theta_{obj}\right)$$

**[0035]** In accordance with one embodiment, the relationship applies for these angles of rotation, wherein  $\theta_{obj}$  denotes the angle of rotation of the first grating,  $\theta_{img}$  denotes the angle of rotation of the second grating and  $\beta_x$ ,  $\beta_y$  denote the imaging scales of the test object in two mutually perpendicular directions.

**[0036]** Further configurations of the invention can be gathered from the description and the dependent claims.

**[0037]** The invention is explained in greater detail below on the basis of exemplary embodiments illustrated in the accompanying figures.

## BRIEF DESCRIPTION OF THE DRAWINGS

**[0038]** In the figures:

Figures 1-7 show schematic illustrations for explaining different embodiments of the present invention;

Figures 8-9 show schematic illustrations for explaining structure and functional principle of a conventional appliance for the moiré measurement of an optical test object; and

Figures 10-11 show schematic illustrations for explaining a problem occurring in accordance with the prior art.

## DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

**[0039]** Below, different embodiments of the invention are described with reference to Fig. 1 to 6, in each case proceeding from the basic structure for the moiré measurement described on the basis of Fig. 8 to 10.

**[0040]** In accordance with Fig. 1, an appliance for the moiré measurement of an optical test object 12 comprises a grating arrangement made of a first grating 11 which is positionable in the optical beam path upstream of the test object 12 and which comprises test structures to be imaged and a second grating 14 which is positionable in the optical beam path downstream of the test object 12, and an evaluation unit comprising at least one detector 15, for evaluating moiré structures produced by superposition of the two gratings in a detection plane situated downstream of the second grating 14 in the optical beam path. The produced image of the test structures contained in the first grating 11 is denoted by "13". As a rule, the planes of the test structure image 13 on the one hand and of the second grating 14 or of the moiré mask on the other hand also coincide here and are depicted with spatial separation only for the purposes of a better illustration. Furthermore, the detector 15 should also follow as closely as possible in the optical beam path downstream of the image plane in which the test structure image 13 is produced.

**[0041]** What is common to the exemplary embodiments described below is that, proceeding from the basic structure for the moiré measurement described on the basis of Fig. 8 to 10, the grating arrangement made of the first grating 11 and the second grating 14 (i.e. the moiré mask) is designed in such a way that, in each case in combination with the anamorphic test object or projection lens to be measured, the calibration method described at the outset on the basis of Fig. 10 is facilitated; i.e., a correct moiré measurement or evaluation of the signals obtained here is possible in a plurality of rotational and/or displacement positions between the measurement arrangement comprising said grating arrangement on the one hand and the test object 12 on the other hand.

**[0042]** In each case, this is achieved by virtue of the first grating 11 and the second grating 14 being fitted to one another in such a way that an evaluation result is obtained in the detection plane, the light intensity transmitted through the grating arrangement being at a maximum in the case of aberration-free imaging by the test object 12 and being reduced in the case of present optical aberrations of the test object 12 in said evaluation result for at least two measurement positions (which are selectable for calibration purposes) which differ in respect of the relative position of grating arrange-

ment and test object 12.

**[0043]** Below, the assumption is initially made that the ratio of the periods of the test structure images of the first grating 11 in two different measurement positions, which differ in respect of the relative position of grating arrangement and test object 12, is rational and hence representable as

$$\frac{p_{img,1}}{p_{img,2}} = \frac{P}{Q} \quad (1),$$

where  $P$  and  $Q$  are integers and where  $p_{img,1}$  and  $p_{img,2}$  denote the periods of the test structure images in the first measurement position and a second measurement position, respectively. Then, the period  $p_{mask}$  of the structures or of the line grating on the second grating 14 (i.e. the moiré mask) may be selected to be an integer multiple of the periods  $p_{img,1}$  and  $p_{img,2}$  such that, for example, the following applies:

$$p_{mask} = Q \cdot p_{img,1} = P \cdot p_{img,2} \quad (2).$$

**[0044]** Then, each  $Q$ -th line of the test structures contained on the first grating 11 in the first measurement position and each  $P$ -th line in the second measurement position makes a meaningful contribution to the moiré signal.

**[0045]** interference signals from line combinations not fitting to one another can be reduced by the selection of the line widths on the basis of the following consideration: All lines of the test structures contained on the first grating 11, which are not mapped perfectly onto a line on the second grating 14 or the moiré mask in the case of aberration-free imaging are considered. From the position of these line images, the smallest distance  $d$  to one of the lines on the second grating 14 or the moiré mask is considered in each case. Now, if  $d_{min,1}$  and  $d_{min,2}$  are used to denote the minima of all of these smallest distances in the two measurement positions (i.e. the smallest distances of "non-fitting line combinations"), it is possible, by selecting the line widths  $a_{mask}$  (the lines on the moiré mask) and  $a_{obj}$  (the lines on the first grating 11) in accordance with

$$a_{mask} + a_{img}(a_{obj}, \theta_{obj,1}, M) < d_{min,1} \quad (3)$$

and

$$a_{mask} + a_{img}(a_{obj}, \theta_{obj,2}, M) < d_{min,2} \quad (4),$$

to ensure that there are no overlaps of lines "that do not fit to one another". Here,  $a_{img}$  denotes the line width of the test structure images,  $\theta_{obj,1}$  and  $\theta_{obj,2}$  denote the rotational angle in the two measurement positions and  $M$  denotes the transformation during the mapping from object to image. This method is restricted by the imaging of the test structures by the test object 12 and the width of a line image is bounded below by the resolution capacity of the projection optical unit (e.g. the diameter of the Airy disk).

**[0046]** Fig. 2 shows an example for designing the second grating 14 or the moiré mask if the ratio of the periods of the test structure images in the aforementioned two measurement positions is 3:5, where "21" shows the period of the test structure image for "measurement position 1", "22" shows the period of the test structure image for "measurement position 2" and "23" shows the period of the lines on the second grating 14 or the moiré mask. The period of the second grating 14 or of the moiré mask in this case corresponds to a common multiple of the periods of the test structure images in the two aforementioned measurement positions.

**[0047]** A likewise advantageous embodiment, schematically indicated in Fig. 3, corresponds to the selection of the period of the second grating 14 or of the moiré mask as a common divisor of the periods of the test structure images in the two measurement positions. If the ratio of the periods of the test structure images of the first grating 11 is rational in both measurement positions and hence representable in accordance with the aforementioned Equation (1), it is also possible to carry out a moiré measurement in a meaningful way if the period of the line grating on the second grating 14 or the moiré mask is selected as

$$p_{mask} = \frac{p_{img,1}}{P} = \frac{p_{img,2}}{Q} \quad (5).$$

**[0048]** Then, in the first measurement position, each  $P$ -th line  $n$  contributes to the moiré signal in a meaningful manner and, in the second measurement position, each  $Q$ -th line of the structures present on the second grating 14 contributes to the moiré signal in a meaningful manner. Fig. 3 shows a corresponding example for designing the second grating 14 or the moiré mask if the ratio of the periods of the test structure images in the two measurement positions is 3:5, where "31" shows the period of the test structure image for "measurement position 1", "32" shows the period of the test structure image for "measurement position 2" and "33" shows the period of the lines on the second grating 14 or the moiré mask. As already described in conjunction with Fig. 2, the occurrence of interference signals may also be suppressed here by a suitable selection of the line widths in accordance with Equations (3) and (4).

**[0049]** A special case of the general affine transformation is a map of the form

$$\begin{pmatrix} x_{img} \\ y_{img} \end{pmatrix} = \begin{pmatrix} \beta_x & 0 \\ 0 & \beta_y \end{pmatrix} \cdot \begin{pmatrix} x_{obj} \\ y_{obj} \end{pmatrix} + \begin{pmatrix} x_0 \\ y_0 \end{pmatrix} \quad (6),$$

with the transformation matrix  $M = \begin{pmatrix} \beta_x & 0 \\ 0 & \beta_y \end{pmatrix}$ . Such imaging has the imaging scales  $\beta_x$  and  $\beta_y$  along the x-direction and the y-direction. Without loss of generality, the assumption is made here that the imaging contains no rotation (otherwise, it is possible to compensate the rotation of the imaging by a rotation of the coordinate system in the image plane).

**[0050]** In the case assumed above, there are two measurement positions or rotational positions of the test structures contained on the first grating 11, in which the orientation of the test structures and the orientation of the test structure images are identical, namely if the lines of the test structures extend parallel to the x-axis or to the y-axis. Then, for the period  $p_{img}$  and the line width  $a_{img}$  of the test structure images,  $p_{img} = \beta_x \cdot p_{obj}$  and  $a_{img} = \beta_x \cdot a_{obj}$  apply to lines extending parallel to the y-axis and  $p_{img} = \beta_y \cdot p_{obj}$  and  $a_{img} = \beta_y \cdot a_{obj}$  apply to lines extending parallel to the x-axis. Therefore, the

$$k = \frac{\beta_x}{\beta_y}$$

ratio of the periods of the test structure images respectively contained in the measurement positions is  $k = \frac{\beta_x}{\beta_y}$ . These rotational positions lend themselves for a calibration measurement, wherein the moiré mask may be suitably designed using the methods described above such that it fits to this ratio of the periods.

**[0051]** In Fig. 4a-f, the associated test structure images (Fig. 4b, 4d and 4f) are respectively schematically illustrated for three different orientations of the first grating 11 or the test structures (Fig. 4a, 4c and 4e) contained therein, wherein an imaging scale of 1:1 is assumed along the x-axis and an imaging scale of 1:2 is assumed along the y-axis. Here, "41" denotes the test structure with lines parallel to the y-axis, "42" denotes the associated test structure image, "43" denotes the test structure with lines parallel to the x-axis, "44" denotes the associated test structure image, "45" denotes the test structure with diagonal lines and "46" denotes the associated test structure image. The test structures and the images thereof only have the same orientation if the lines lie parallel to a coordinate axis, in accordance with Fig. 4a or Fig. 4b.

**[0052]** If two measurement or rotational positions, in which the lines of the test structures with period  $p_{obj}$  include the angle  $\theta_{obj,1}$  and include the angle  $\theta_{obj,2}$  in alternation, are considered, the imaging described above with the asymmetric imaging scale causes the periods of the test structure images in the two measurement positions to be

$$p_{img,1} = p_{obj} \cdot \frac{\beta_x \cdot \beta_y}{\sqrt{\beta_x^2 \cdot \cos^2 \theta_{obj,1} + \beta_y^2 \cdot \sin^2 \theta_{obj,1}}} \quad (7)$$

$$p_{img,2} = p_{obj} \cdot \frac{\beta_x \cdot \beta_y}{\sqrt{\beta_x^2 \cdot \cos^2 \theta_{obj,2} + \beta_y^2 \cdot \sin^2 \theta_{obj,2}}} \quad (8).$$

**[0053]** By way of a suitable selection of the rotational positions  $\theta_{obj,1}$  and  $\theta_{obj,2}$ , it is thus possible to set the ratio of the periods

$$\frac{p_{img,2}}{p_{img,1}} = \frac{\sqrt{\beta_x^2 \cdot \cos^2 \theta_{obj,1} + \beta_y^2 \cdot \sin^2 \theta_{obj,1}}}{\sqrt{\beta_x^2 \cdot \cos^2 \theta_{obj,2} + \beta_y^2 \cdot \sin^2 \theta_{obj,2}}} \quad (9)$$

to any value between  $\frac{\beta_x}{\beta_y}$  and  $\frac{\beta_y}{\beta_x}$  and correspondingly maximize the number of evaluable lines. To this end, the

$$k = \frac{p_{img,2}}{p_{img,1}} = \frac{P}{Q}$$

ratio of the periods is set in such a way that the numbers  $P$  and  $Q$  (which are respectively integers) become as small as possible.

**[0054]** Then, in general, the orientation  $\theta_{img}$  of the images of the test structure lines no longer corresponds to the orientation  $\theta_{obj}$  of the lines of the test structures in the object plane. The following relationship applies:

$$\theta_{img} = \arctan \left( \frac{\beta_y}{\beta_x} \cdot \tan \theta_{obj} \right) \quad (10).$$

**[0055]** If the orientation of the test structures in the object plane  $\theta_{obj}$  is given, the orientation of the moiré mask in the image plane  $\theta_{mask} = \theta_{img}$  is selected.

**[0056]** For a simple example of an anamorphic scale of  $\beta_x=1/4$  and  $\beta_y=1/8$ , the measurement positions in which the lines are oriented parallel to the coordinate axes are well suited to a moiré measurement. The ratio of the two imaging

scales is  $\frac{\beta_x}{\beta_y} = 2:1$ . In the example, the period of the test structures contained on the first grating 11 is  $p_{obj}=8 \mu\text{m}$  and the period of the lines on the second grating 14 or the moiré mask is  $p_{mask}=1 \mu\text{m}$ . Then, for  $\theta_{obj,1}=0^\circ$  (lines parallel to the x-axis), the period of the image of the test structures is  $p_{img,1}=1 \mu\text{m}$  and, for  $\theta_{obj,1}=90^\circ$  (lines parallel to the y-axis), the period of the image of the test structures is  $p_{img,1}=2 \mu\text{m}$ . Each line on the moiré mask contributes to the measurement signal in the first case and each second line on the moiré mask contributes to the measurement signal in the second case.

**[0057]** In this simple case, the associated orientations of the moiré mask in the image plane are  $\theta_{mask,1}=0^\circ$  and  $\theta_{mask,2}=90^\circ$ .

**[0058]** The aforementioned situation is illustrated in Fig. 5, where "51" shows the period of the test structure image for the  $90^\circ$  position, "52" shows the period of the test structure image for the  $0^\circ$  position and "53" shows the period of the lines on the second grating 14 or the moiré mask. If the line width of the structures on the moiré mask is selected to be  $a_{mask}=0.5 \mu\text{m}$  and the line width of the test structures on the first grating 11 is selected to be  $a_{obj}=2 \mu\text{m}$ , interference signals by line combinations that do not fit to one another are suppressed. This result may be transferred to all test

objects in which the ratio of the imaging scales  $\frac{\beta_x}{\beta_y}$  has the value of 2:1 or 1:2.

**[0059]** Fig. 6 shows an exemplary embodiment for two mask structures, fitting to one another, in the object plane (denoted by "61") and in the image plane (denoted by "62"), which can be used for anamorphic imaging, in which the



imaging scale along the horizontal or x-axis is twice as large as the imaging scale along the vertical or y-axis. Each partial structure (a line grating) corresponds to a measurement point for a moiré measurement. The line width of the test structures is a quarter of the grating period and the line width on the moiré mask in the image plane is half the grating period. On the object mask, the distance between two adjacent partial structures is twice as large in the vertical direction as in the horizontal direction. The orientation of the lines respectively alternates between one measurement point and the adjacent measurement point. In the 0° rotational position, there is, for each partial structure in the object plane, precisely one structure fitting thereto on the moiré mask in the image plane. In the 90° rotational position, there are, albeit not for all partial structures but at least for some partial structures in the object plane, structures respectively fitting thereto in the image plane.

**[0060]** Preferably, in accordance with the invention, the respective measurement positions (which are then respectively selected in the calibration method) are also selected in a suitable manner depending on the specific application situation or the specific configuration of the test object. By way of example, if the anamorphic test object has imaging scales of  $\beta_x=25$  and  $\beta_y=16$ , the ratio of the periods for lines with an orientation parallel to the coordinate axes is significantly less

expedient than in the scenarios described above. The ratio of the two imaging scales is  $\frac{\beta_x}{\beta_y}=25:16$ . If the period of the test structures is  $p_{obj}=1\text{ }\mu\text{m}$ , the periods of the test structure images in the 0° position and in the 90° position respectively are  $p_{img,1}=25\text{ }\mu\text{m}$  and  $p_{img,2}=16\text{ }\mu\text{m}$ . The greatest common divisor of these two periods, which may therefore be selected as period of the lines on the moiré mask, is  $p_{mask}=1\text{ }\mu\text{m}$ . Hence, only every 25th line would contribute to the measurement signal for the 0° position and only every 16th line would contribute to the measurement signal for the 90° position.

**[0061]** If, instead, use is made of the rotational positions  $\theta_{obj,1}=0^\circ$  and  $\theta_{obj,2}=68.629^\circ$ , the periods of the test structure images are  $p_{img,1}=25\text{ }\mu\text{m}$  and  $p_{img,2}=16.667\text{ }\mu\text{m}$  and therefore have a ratio of 3:2. If  $p_{mask}=8.333\text{ }\mu\text{m}$  is selected as grating period on the moiré mask, then every second line contributes to the measurement signal in the first measurement position (0° position) and still every third line contributes to the measurement signal in the second measurement position (68.629° position).

**[0062]** In this case, the associated orientations of the moiré mask in the image plane are  $\theta_{mask,1}=0^\circ$  and  $\theta_{mask,2}=58.5570^\circ$ .

**[0063]** The aforementioned result may be transferred to all test objects in which the ratio of the imaging scales  $\frac{\beta_x}{\beta_y}$  has the value of 16:25 or 25:16.

**[0064]** For illustrative purposes, Fig. 7a and 7b show schematic illustrations of overall views of a possible measurement structure in different positions when a calibration method is carried out. Here, Fig. 7a shows the structure for an anamorphic projection lens (test object 72) with an imaging scale of 1:1 in one direction and 2:1 in another direction, where "71" denotes the grating having the test structures and "73" denotes the second grating (moiré mask) positioned downstream of the test object in the optical beam path. Fig. 7b shows an analogous illustration for an anamorphic projection lens (test object 82) with imaging scales of 16:1 and 25:1 in the respective different directions, where "81" denotes the grating having the test structures and "83" denotes the second grating (moiré mask) positioned downstream of the test object in the optical beam path.

**[0065]** Even though the invention has been described on the basis of specific embodiments, numerous variations and alternative embodiments are apparent to the person skilled in the art, e.g. by combination and/or exchange of features of individual embodiments. Accordingly, it goes without saying for the person skilled in the art that such variations and alternative embodiments are concomitantly encompassed by the present invention, and the scope of the invention is restricted only within the meaning of the accompanying patent claims.

## Claims

1. Appliance for the moiré measurement of an optical test object, comprising

- a test object (12), which is an anamorphic imaging system;
- a grating arrangement made of a first grating (11) which is positioned in the optical beam path upstream of the test object (12) and which comprises test structures to be imaged and a second grating (14) which is positioned in the optical beam path downstream of the test object (12); and

- an evaluation unit comprising at least one detector, for evaluating moiré structures produced by superposition of the two gratings in a detection plane situated downstream of the second grating (14) in the optical beam path;
- wherein the respective grating periods of the first grating (11) and of the second grating (14) are selected in such a way that the grating period of the second grating (14) corresponds to a common multiple or a common divisor of the respective periods of two test structure images of the test structures of the first grating (11) produced by the imaging system in two different measurement positions, wherein the two measurement positions differ in respect of the relative position of grating arrangement and test object (12).

2. Appliance according to Claim 1, **characterized in that** the respective grating periods of the first grating (11) and of the second grating (14) are selected in such a way that, for the two measurement positions, the light intensity transmitted through the grating arrangement is either at a maximum or at a minimum in the case of aberration-free imaging by the test object (12).

3. Appliance according to Claim 1 or 2, **characterized in that** the at least two measurement positions differ by a relative rotation of the test object (12) and the grating arrangement in relation to one another and/or by a relative translation of the test object (12) and the grating arrangement in relation to one another.

4. Appliance according to any one of Claims 1 to 3, **characterized in that** the at least two measurement positions are selected in such a way that the imaging scales of the test object (12), in each case effective for these measurement positions, have a rational relationship with respect to one another.

5. Appliance according to any one of the preceding claims, **characterized in that** line widths of test structures on the first grating (11) and line widths of structures on the second grating (14) are selected in such a way that, for the at least two measurement positions, no line on the second grating (14) is exposed simultaneously by two lines of the test structures of the first grating (11).

6. Appliance according to any one of the preceding claims, **characterized in that** the test object (12) is a projection lens of a microlithographic projection exposure apparatus.

7. Appliance according to any one of the preceding claims, **characterized in that** the test object (12) is designed for operation at an operating wavelength of less than 30 nm, in particular less than 15 nm.

8. Method for the moiré measurement of an optical test object, wherein the test object (12) is an anamorphic imaging system and wherein the method comprises the following steps:

- positioning a first grating (11) having test structures to be imaged in the optical beam path upstream of the test object (12) and positioning a second grating (14) in the optical beam path downstream of the test object (12); and
- evaluating moiré structures produced by superposition of the two gratings in a detection plane situated in the optical beam path downstream of the second grating (14), in at least two measurement positions which differ from one another in respect of the relative position of grating arrangement and test object (12);
- wherein the respective grating periods of the first grating (11) and of the second grating (14) are selected in such a way that the grating period of the second grating (14) corresponds to a common multiple or a common divisor of the respective periods of two test structure images of the test structures of the first grating (11) produced by the imaging system in the two different measurement positions.

9. Method according to Claim 8, **characterized in that** the first grating (11) and the second grating (14) are rotated by mutually different angles of rotation in a second measurement position relative to a first measurement position.

$$\theta_{img} = \arctan\left(\frac{\beta_y}{\beta_x} \cdot \tan \theta_{obj}\right)$$

10. Method according to Claim 9, **characterized in that** the relationship applies for these angles of rotation, wherein  $\theta_{obj}$  denotes the angle of rotation of the first grating (11),  $\theta_{img}$  denotes the angle of rotation of the second grating (14) and  $\beta_x, \beta_y$  denote the imaging scales of the test object (12) in two mutually perpendicular directions.

## Patentansprüche

### 1. Einrichtung zur Moiré-Vermessung eines optischen Prüfobjekts, umfassend

- ein Prüfobjekt (12), das ein anamorphotisches Abbildungssystem ist;
- eine Gitteranordnung, die aus einem ersten Gitter (11), das im optischen Strahlengang dem Prüfobjekt (12) vorgelagert positioniert ist und das abzubildende Prüfstrukturen umfasst, und einem zweiten Gitter (14), das im optischen Strahlengang dem Prüfobjekt (12) nachgelagert positioniert ist, besteht; und
- eine Auswertungseinheit, die mindestens einen Detektor umfasst, zum Auswerten von Moiré-Strukturen, die durch Überlagerung der zwei Gitter in einer Detektionsebene erzeugt werden, die sich im optischen Strahlengang nachgelagert zu dem zweiten Gitter (14) befindet;
- wobei die jeweiligen Gitterperioden des ersten Gitters (11) und des zweiten Gitters (14) derart ausgewählt sind, dass die Gitterperiode des zweiten Gitters (14) einem gemeinsamen Vielfachen oder einem gemeinsamen Teiler der jeweiligen Perioden von zwei Prüfstrukturbildern der Prüfstrukturen des ersten Gitters (11) entspricht, die durch das Abbildungssystem in zwei unterschiedlichen Messpositionen erzeugt wurden, wobei sich die zwei Messpositionen in Bezug auf die relative Position der Gitteranordnung und des Prüfobjekts (12) unterscheiden.

### 2. Einrichtung nach Anspruch 1, **dadurch gekennzeichnet, dass** die jeweiligen Gitterperioden des ersten Gitters (11) und des zweiten Gitters (14) derart ausgewählt sind, dass für die zwei Messpositionen die durch die Gitteranordnung transmittierte Lichtintensität im Fall einer aberrationsfreien Abbildung durch das Prüfobjekt (12) entweder maximal oder minimal ist.

### 3. Einrichtung nach Anspruch 1 oder 2, **dadurch gekennzeichnet, dass** sich die mindestens zwei Messpositionen um eine relative Drehung des Prüfobjekts (12) und der Gitteranordnung in Relation zueinander und/oder um eine relative Translation des Prüfobjekts (12) und der Gitteranordnung in Relation zueinander unterscheiden.

### 4. Einrichtung nach einem der Ansprüche 1 bis 3, **dadurch gekennzeichnet, dass** die mindestens zwei Messpositionen derart ausgewählt sind, dass die Abbildungsmaßstäbe des Prüfobjekts (12), die jeweils für diese Messpositionen wirksam sind, eine rationale Beziehung zueinander aufweisen.

### 5. Einrichtung nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet, dass** Linienbreiten von Prüfstrukturen auf dem ersten Gitter (11) und Linienbreiten von Strukturen auf dem zweiten Gitter (14) derart ausgewählt sind, dass für die mindestens zwei Messpositionen keine Linie auf dem zweiten Gitter (14) gleichzeitig durch zwei Linien der Prüfstrukturen des ersten Gitters (11) belichtet wird.

### 6. Einrichtung nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet, dass** das Prüfobjekt (12) eine Projektionslinse einer mikrolithographischen Projektionsbelichtungseinrichtung ist.

### 7. Einrichtung nach einem der vorhergehenden Ansprüche, **dadurch gekennzeichnet, dass** das Prüfobjekt (12) für einen Betrieb bei einer Betriebswellenlänge von weniger als 30 nm, insbesondere weniger als 15 nm, ausgelegt ist.

### 8. Verfahren zur Moiré-Vermessung eines optischen Prüfobjekts, wobei das Prüfobjekt (12) ein anamorphotisches Abbildungssystem ist, und wobei das Verfahren die folgenden Schritte umfasst:

- Positionieren eines ersten Gitters (11), das abzubildende Prüfstrukturen umfasst, im optischen Strahlengang dem Prüfobjekt (12) vorgelagert und Positionieren eines zweiten Gitters (14) im optischen Strahlengang dem Prüfobjekt (12) nachgelagert; und
- Auswerten von Moiré-Strukturen, die durch Überlagerung der zwei Gitter in einer Detektionsebene erzeugt werden, die sich im optischen Strahlengang nachgelagert zu dem zweiten Gitter (14) befindet, in mindestens zwei Messpositionen, die sich in Bezug auf die relative Position der Gitteranordnung und des Prüfobjekts (12) voneinander unterscheiden;
- wobei die jeweiligen Gitterperioden des ersten Gitters (11) und des zweiten Gitters (14) derart ausgewählt werden, dass die Gitterperiode des zweiten Gitters (14) einem gemeinsamen Vielfachen oder einem gemeinsamen Teiler der jeweiligen Perioden von zwei Prüfstrukturbildern der Prüfstrukturen des ersten Gitters (11) entspricht, die durch das Abbildungssystem in den zwei unterschiedlichen Messpositionen erzeugt wurden.

### 9. Verfahren nach Anspruch 8, **dadurch gekennzeichnet, dass** das erste Gitter (11) und das zweite Gitter (14) in einer zweiten Messposition relativ zu einer ersten Messposition um voneinander unterschiedliche Drehwinkel gedreht

werden.

$$\theta_{img} = \arctan \left( \frac{\beta_y}{\beta_x} \cdot \tan \theta_{obj} \right)$$

10. Verfahren nach Anspruch 9, **dadurch gekennzeichnet, dass** die Beziehung für diesen Drehwinkel gilt, wobei  $\theta_{obj}$  den Drehwinkel des ersten Gitters (11) bezeichnet,  $\theta_{img}$  den Drehwinkel des zweiten Gitters (14) bezeichnet und  $\beta_x$ ,  $\beta_y$  die Abbildungsmaßstäbe des Prüfobjekts (12) in zwei zueinander senkrechten Richtungen bezeichnen.

## Revendications

1. Appareil pour la mesure de moiré d'un objet d'essai optique, comprenant :

- un objet d'essai (12), qui est un système d'imagerie anamorphique ;
- un agencement de réseaux, fait d'un premier réseau (11), qui est positionné dans le trajet de faisceau optique en amont de l'objet d'essai (12) et qui comprend des structures d'essai destinées à être imagées, et d'un second réseau (14), qui est positionné dans le trajet de faisceau optique en aval de l'objet d'essai (12) ; et
- une unité d'évaluation comprenant au moins un détecteur, pour évaluer des structures de moiré produites par superposition des deux réseaux dans un plan de détection situé en aval du second réseau (14) dans le trajet de faisceau optique ;
- dans lequel les périodes de réseau respectives du premier réseau (11) et du second réseau (14) sont sélectionnées de manière telle que la période de réseau du second réseau (14) corresponde à un multiple commun ou un diviseur commun des périodes respectives de deux images de structure d'essai des structures d'essai du premier réseau (11) produites par le système d'imagerie dans deux positions de mesure différentes, dans lequel les deux positions de mesure diffèrent en ce qui concerne la position relative de l'agencement de réseaux et de l'objet d'essai (12).

2. Appareil selon la revendication 1, **caractérisé en ce que** les périodes de réseau respectives du premier réseau (11) et du second réseau (14) sont sélectionnées de manière telle que, pour les deux positions de mesure, l'intensité de lumière transmise à travers l'agencement de réseaux soit à un maximum ou à un minimum dans le cas d'imagerie sans aberration par l'objet d'essai (12).

3. Appareil selon la revendication 1 ou 2, **caractérisé en ce que** les au moins deux positions de mesure diffèrent à raison d'une rotation relative de l'objet d'essai (12) et de l'agencement de réseaux l'un par rapport à l'autre et/ou d'une translation relative de l'objet d'essai (12) et de l'agencement de réseaux l'un par rapport à l'autre.

4. Appareil selon l'une quelconque des revendications 1 à 3, **caractérisé en ce que** les au moins deux positions de mesure sont sélectionnées de manière telle que les échelles d'imagerie de l'objet d'essai (12), dans chaque cas efficaces pour ces positions de mesure, aient une relation rationnelle les unes par rapport aux autres.

5. Appareil selon l'une quelconque des revendications précédentes, **caractérisé en ce que** des largeurs de ligne de structures d'essai sur le premier réseau (11) et des largeurs de ligne de structures sur le second réseau (14) sont sélectionnées de manière telle que, pour les au moins deux positions de mesure, aucune ligne sur le second réseau (14) ne soit exposée simultanément par deux lignes des structures d'essai du premier réseau (11).

6. Appareil selon l'une quelconque des revendications précédentes, **caractérisé en ce que** l'objet d'essai (12) est une lentille de projection d'un appareil d'exposition par projection microlithographique.

7. Appareil selon l'une quelconque des revendications précédentes, **caractérisé en ce que** l'objet d'essai (12) est conçu pour le fonctionnement à une longueur d'onde de fonctionnement inférieure à 30 nm, en particulier inférieure à 15 nm.

8. Procédé pour la mesure de moiré d'un objet d'essai optique, dans lequel l'objet d'essai (12) est un système d'imagerie anamorphique et dans lequel le procédé comprend les étapes suivantes :

- le positionnement d'un premier réseau (11) ayant des structures d'essai, destinées à être imagées, dans le trajet de faisceau optique en amont de l'objet d'essai (12) et le positionnement d'un second réseau (14) dans le trajet de faisceau optique en aval de l'objet d'essai (12) ; et

• l'évaluation de structures de moiré produites par superposition des deux réseaux dans un plan de détection situé dans le trajet de faisceau optique en aval du second réseau (14), dans au moins deux positions de mesure qui diffèrent l'une de l'autre en ce qui concerne la position relative de l'agencement de réseaux et de l'objet d'essai (12) ;

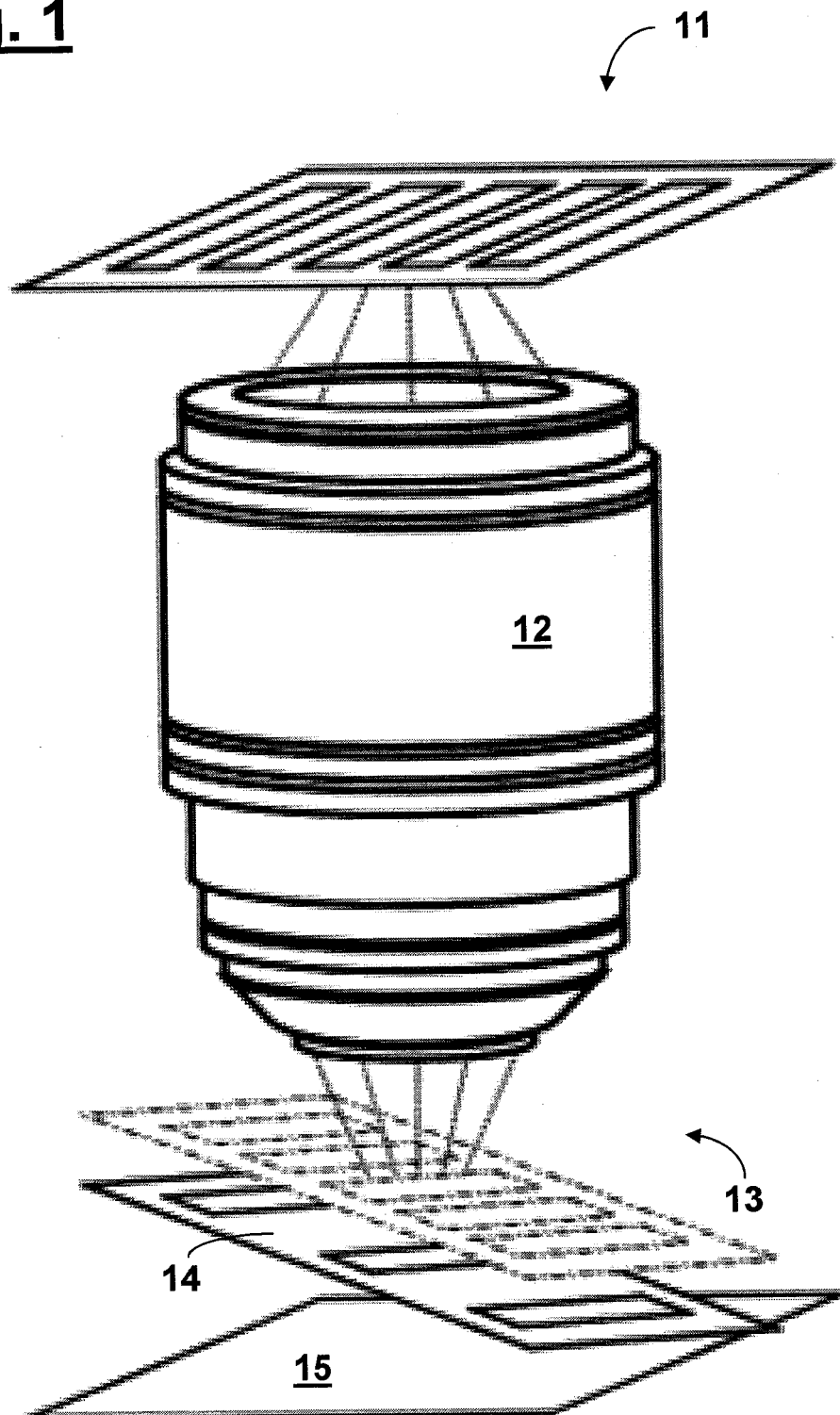
• dans lequel les périodes de réseau respectives du premier réseau (11) et du second réseau (14) sont sélectionnées de manière telle que la période de réseau du second réseau (14) corresponde à un multiple commun ou un diviseur commun des périodes respectives de deux images de structure d'essai des structures d'essai du premier réseau (11) produites par le système d'imagerie dans les deux positions de mesure différentes.

9. Procédé selon la revendication 8, **caractérisé en ce que** la rotation du premier réseau (11) et du second réseau (14) est effectuée selon des angles de rotation mutuellement différents dans une seconde position de mesure relativement à une première position de mesure.

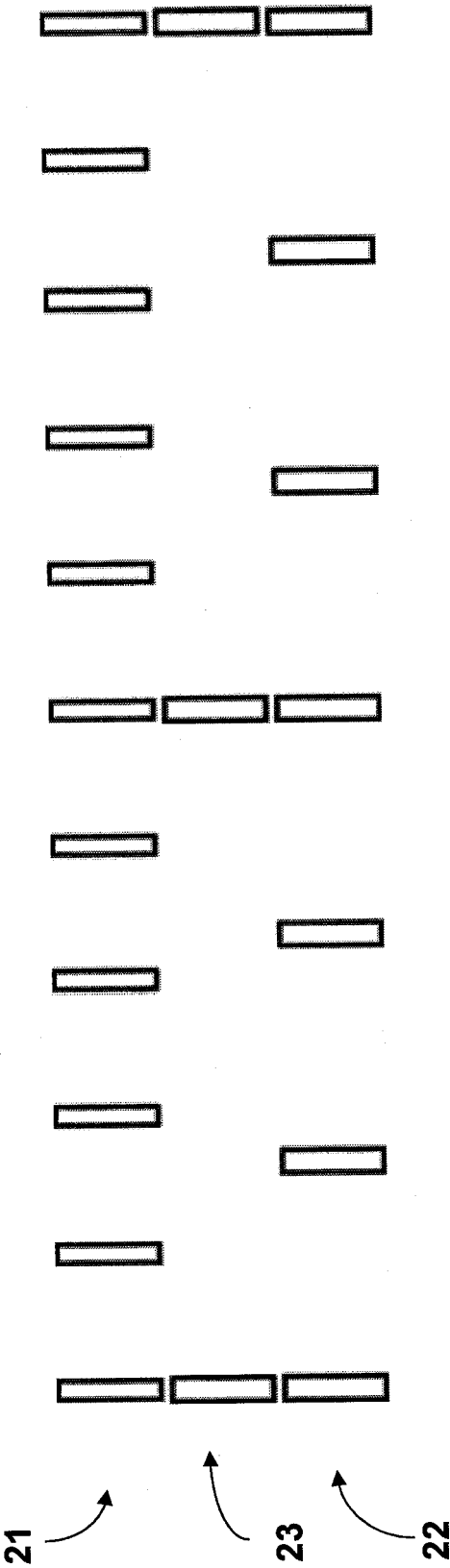
$$\theta_{img} = \arctan \left( \frac{\beta_y}{\beta_x} \cdot \tan \theta_{obj} \right)$$

10. Procédé selon la revendication 9, **caractérisé en ce que** la relation est vraie pour ces angles de rotation, dans lequel  $\theta_{obj}$  dénote l'angle de rotation du premier réseau (11),  $\theta_{img}$  dénotes l'angle de rotation du second réseau (14) et  $\beta_x, \beta_y$  dénotent les échelles d'imagerie de l'objet d'essai (12) dans deux directions mutuellement perpendiculaires.

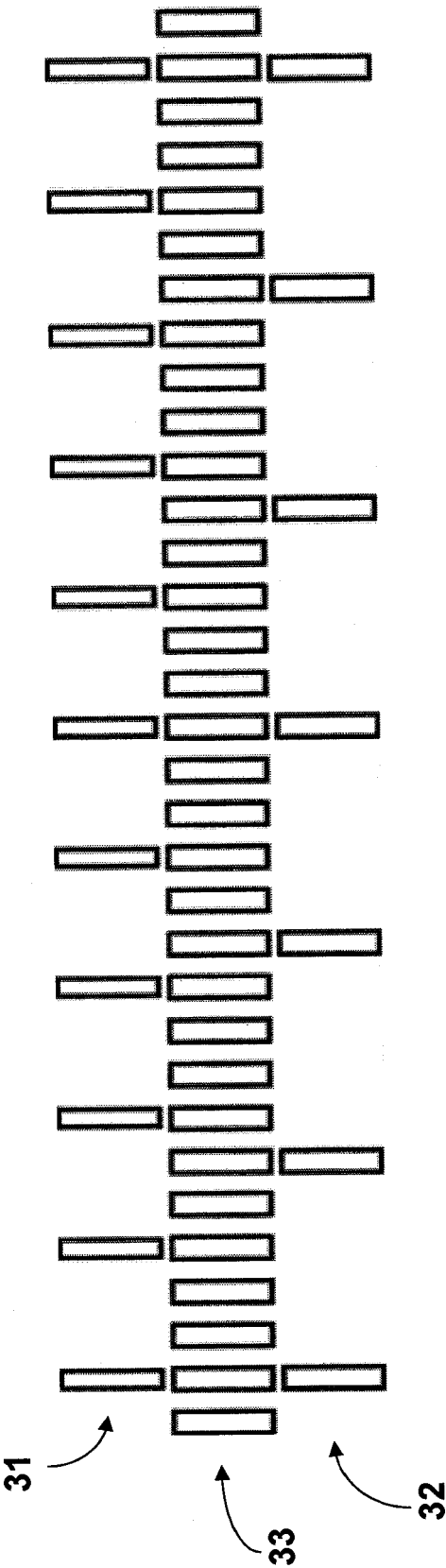
**Fig. 1**



**Fig. 2**

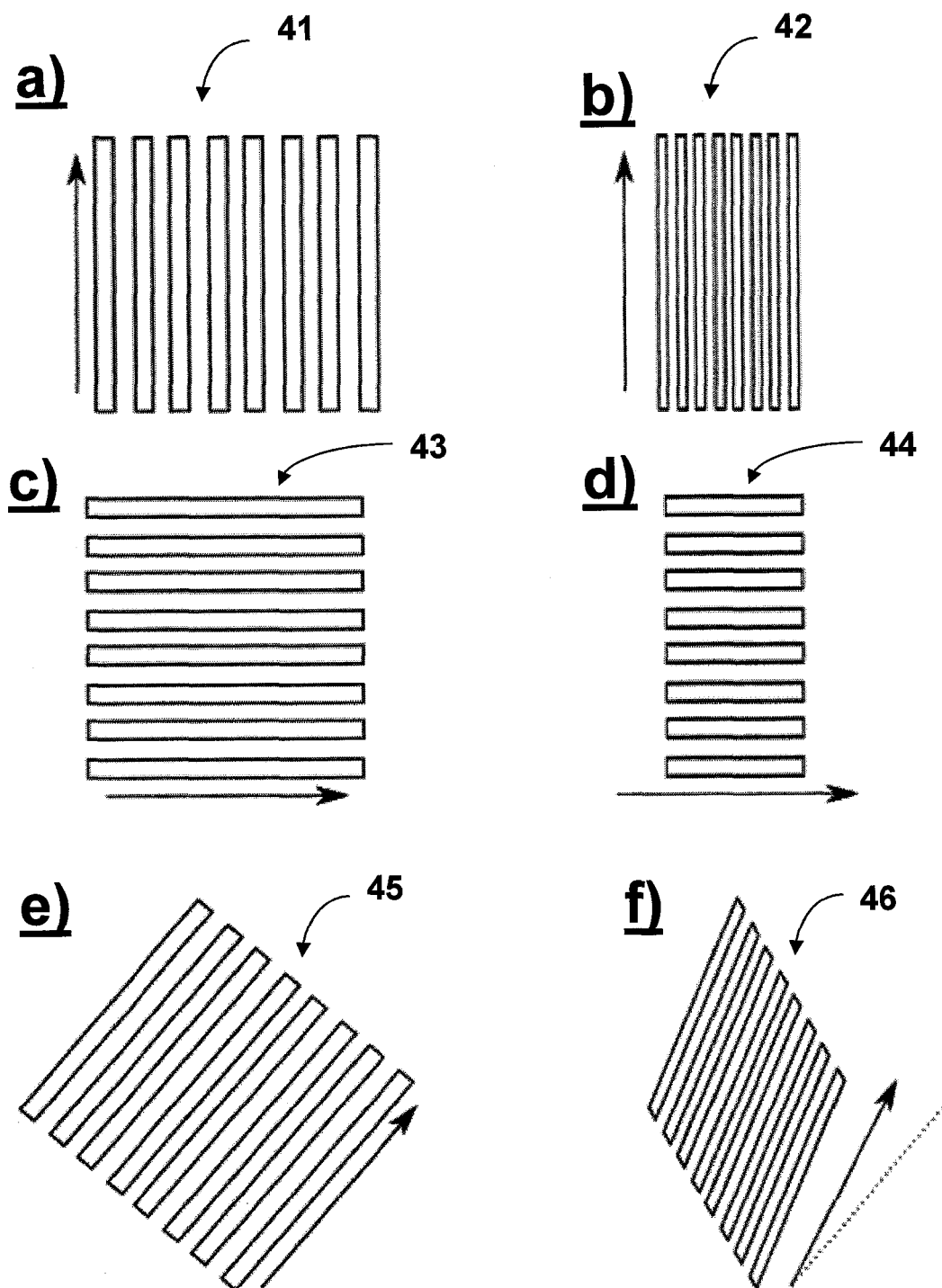


**Fig. 3**

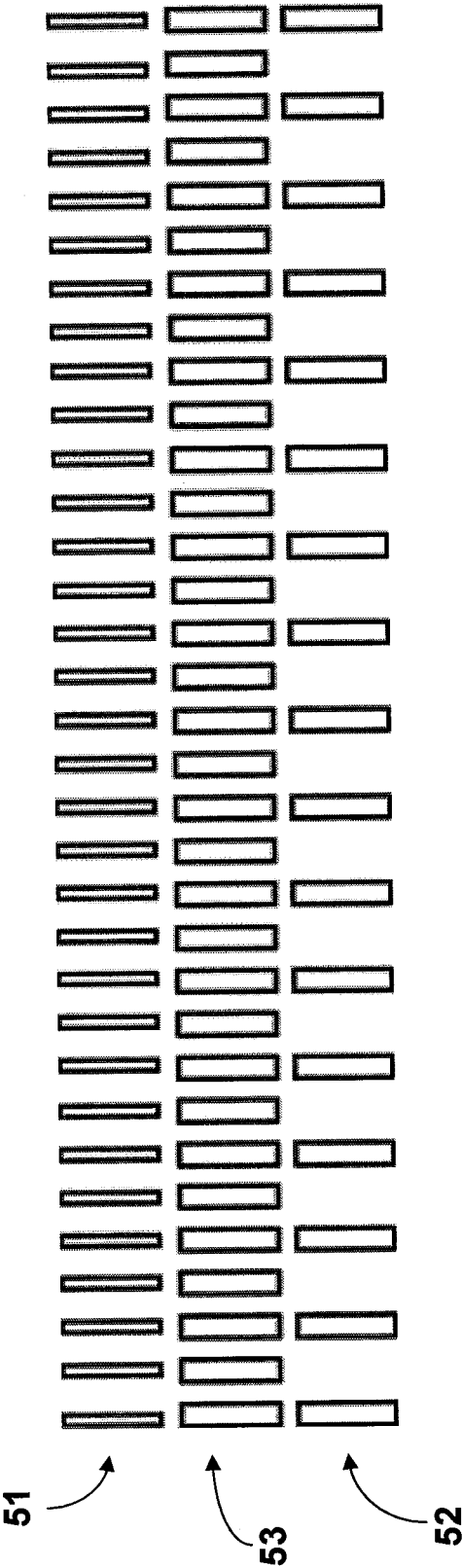


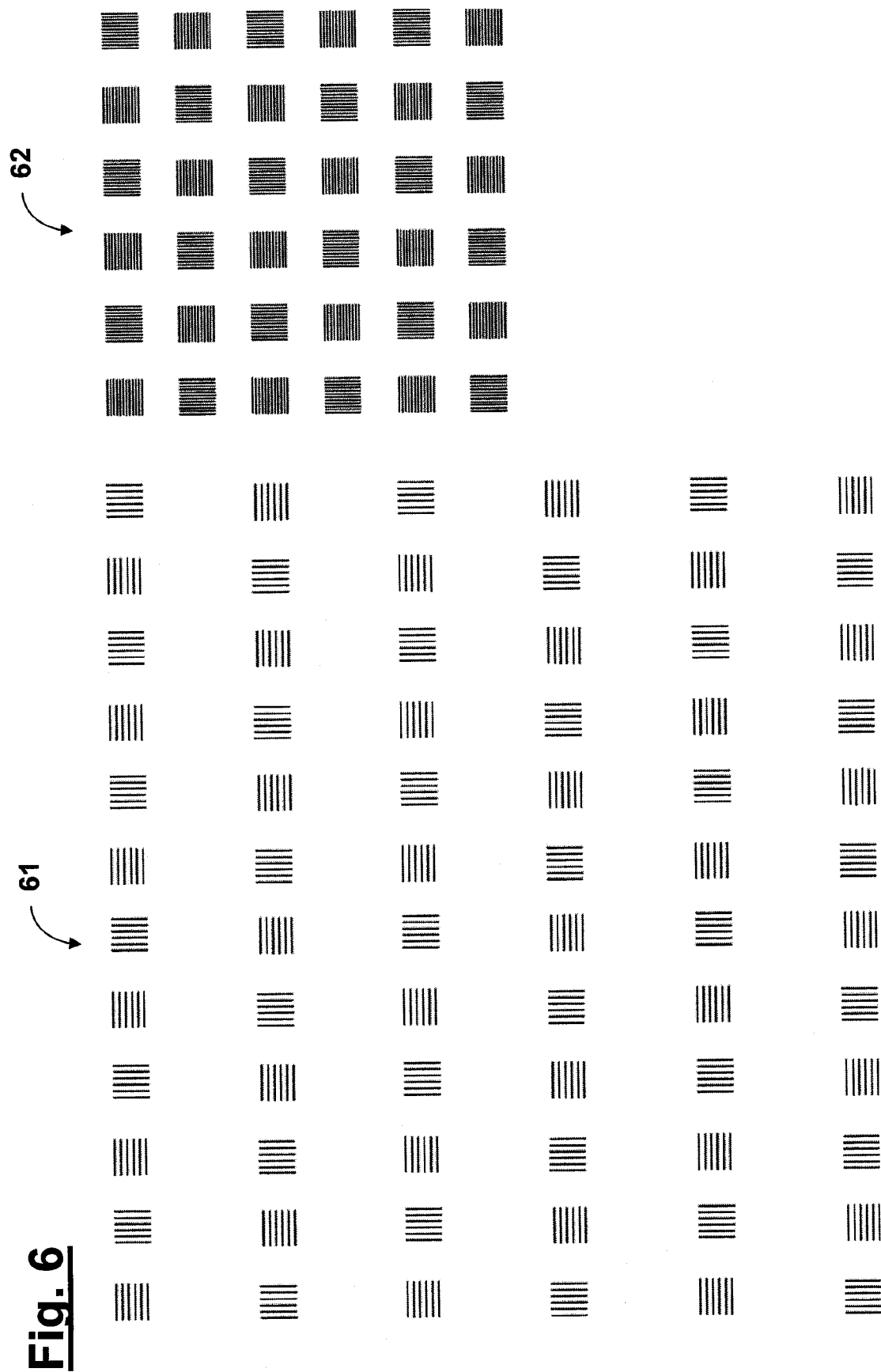


**Fig. 4**

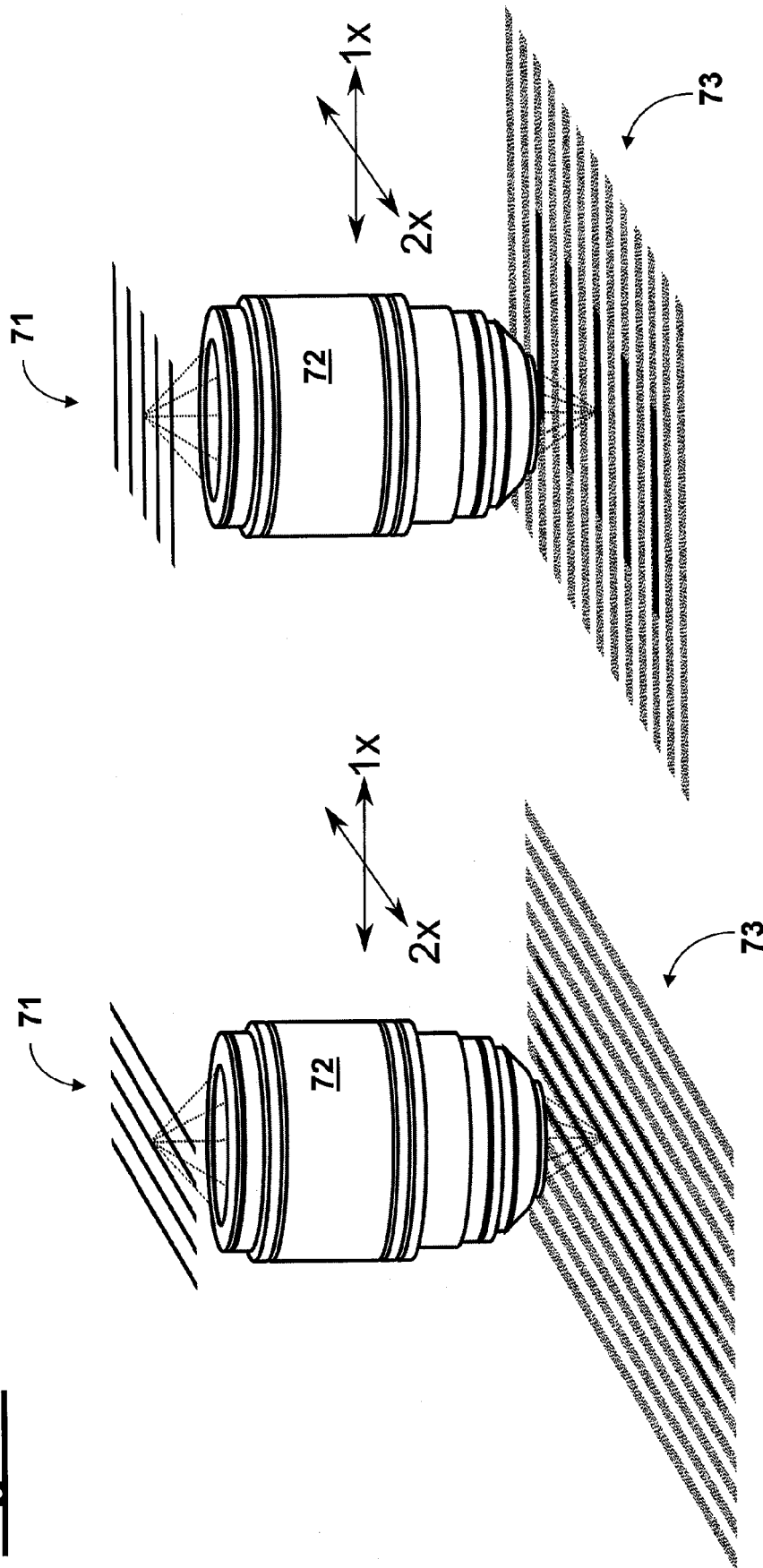


**Fig. 5**

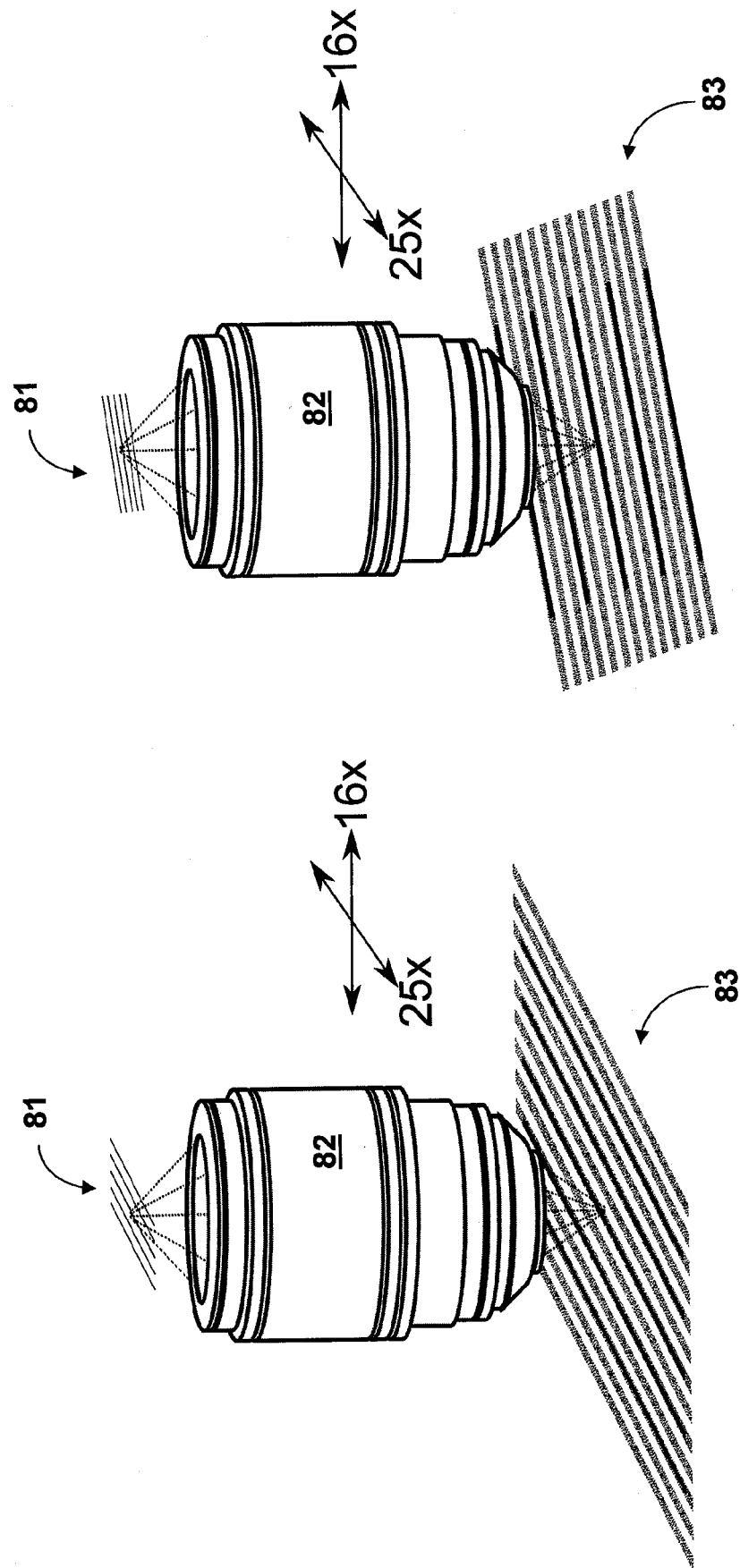




**Fig. 7a**

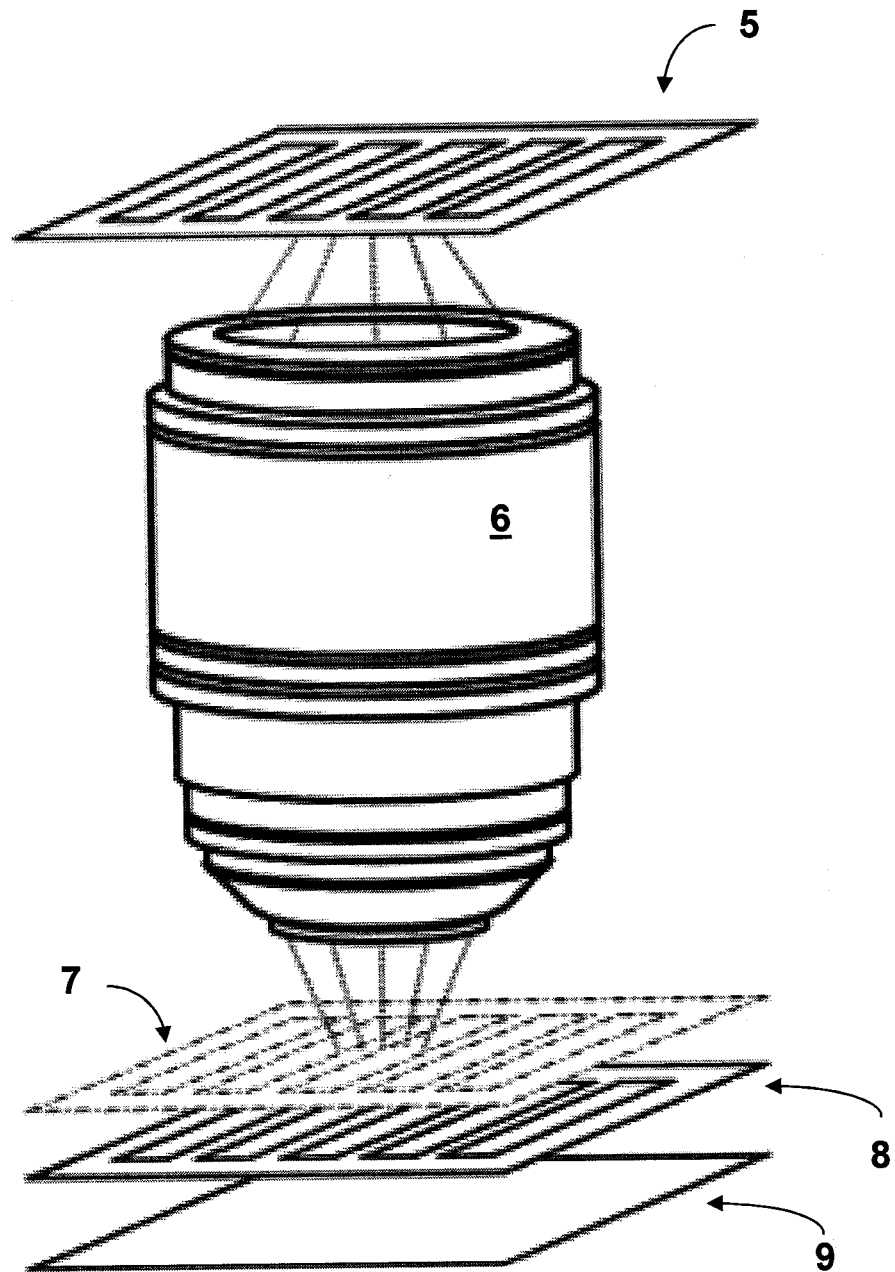


**Fig. 7b**



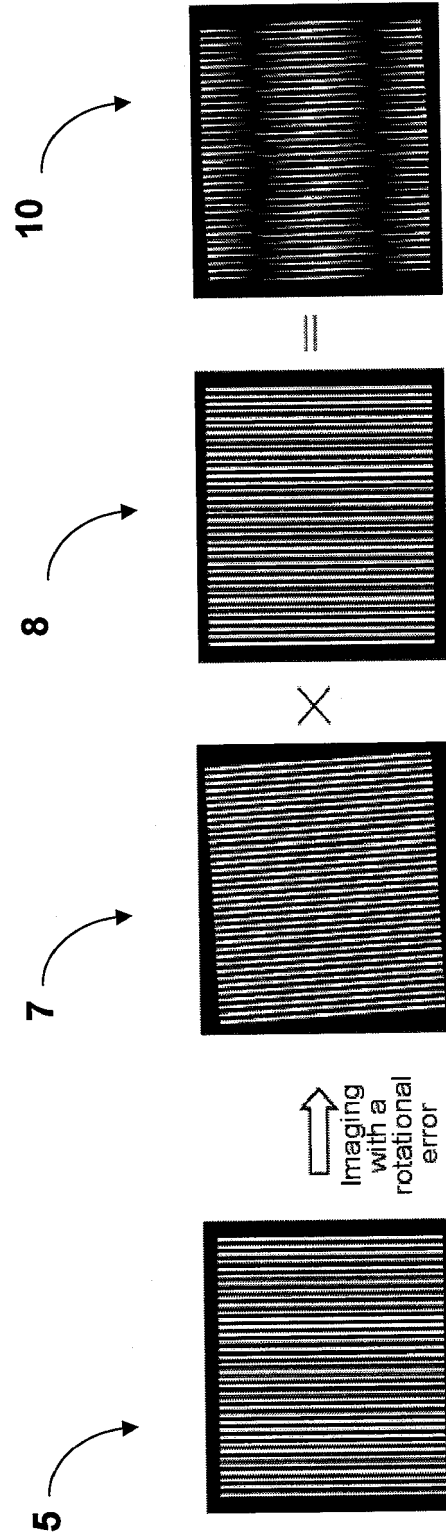
**Fig. 8**

**Prior art**



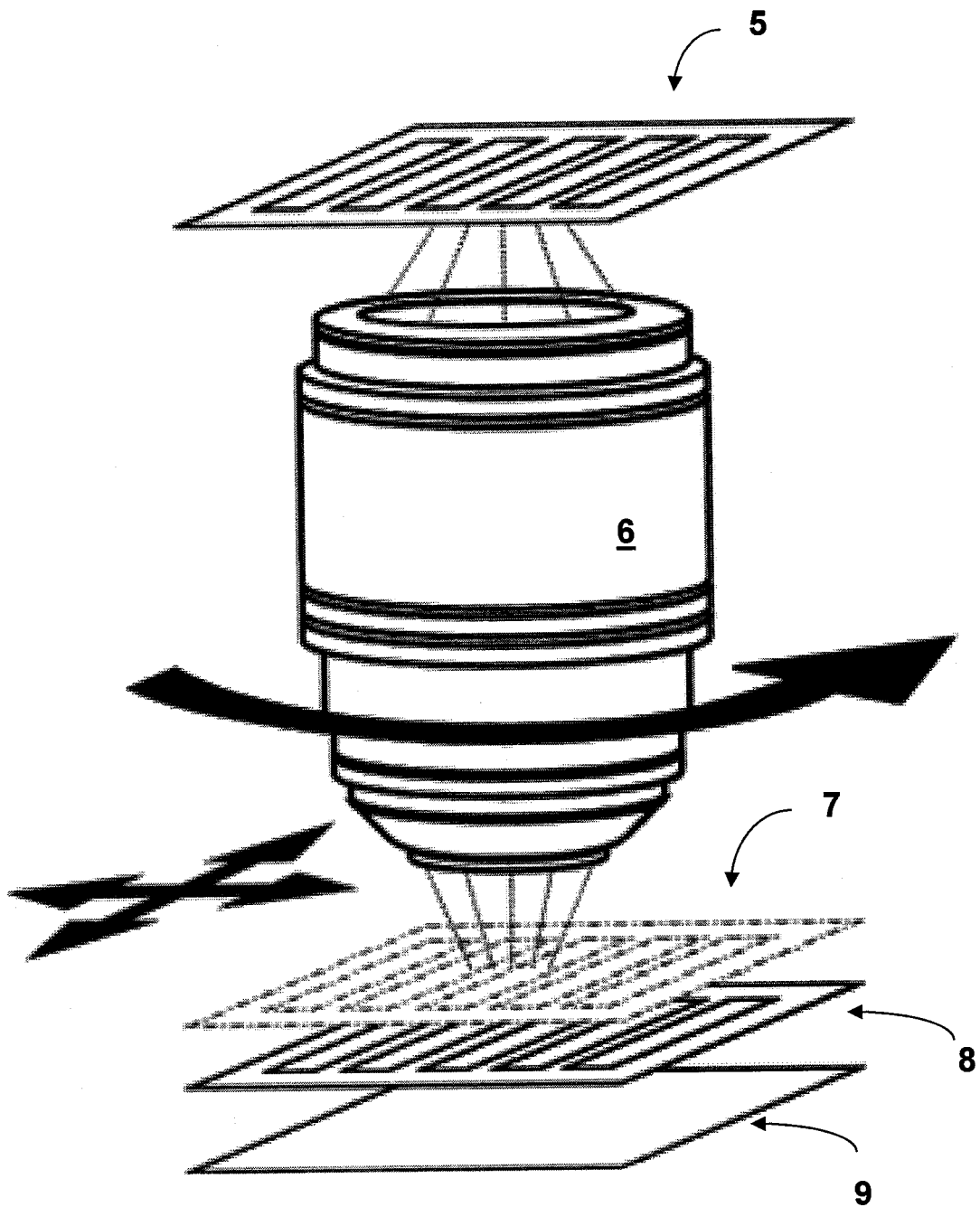
**Fig. 9**

**Prior art**



**Fig. 10**

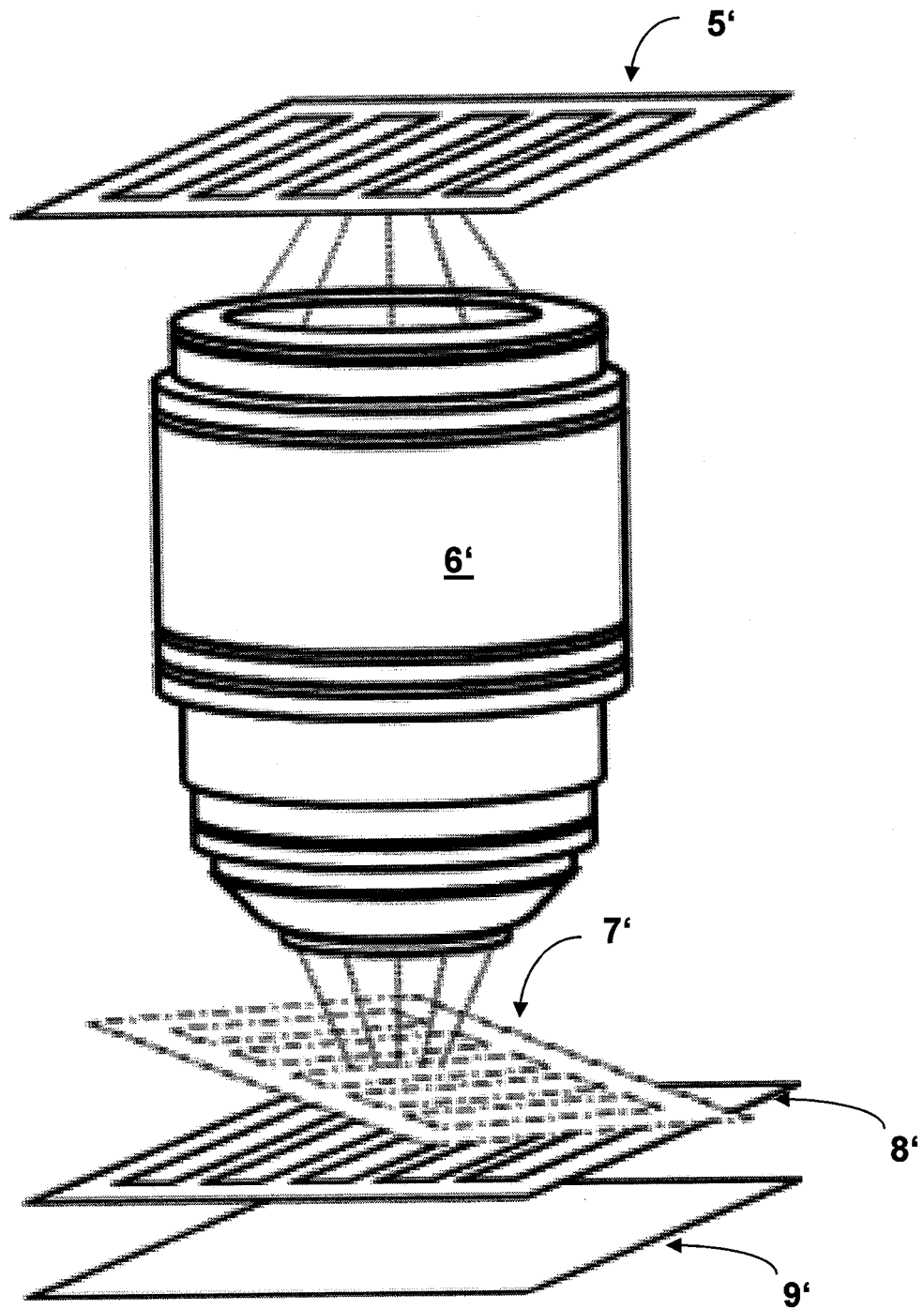
**Prior art**





**Fig. 11**

**Prior art**



**REFERENCES CITED IN THE DESCRIPTION**

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