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• YANAGISAWA, Takayuki

Tokyo 1008310 (JP)

• SHIGA, Akira

Tokyo 1008310 (JP)

• YOSHIKI, Wataru

Tokyo 1008310 (JP)

• HAMADA, Mamoru

Tokyo 1008310 (JP)

• SAKAI, Yu

Tokyo 1008310 (JP)

(71) Applicant: Mitsubishi Electric Corporation
Tokyo 100-8310 (JP)

(74) Representative: Pfenning, Meinig & Partner mbB

Patent- und Rechtsanwälte

Joachimsthaler Straße 10-12

10719 Berlin (DE)

(72) Inventors:

• KOTAKE, Nobuki

Tokyo 1008310 (JP)

• SUZUKI, Masataka

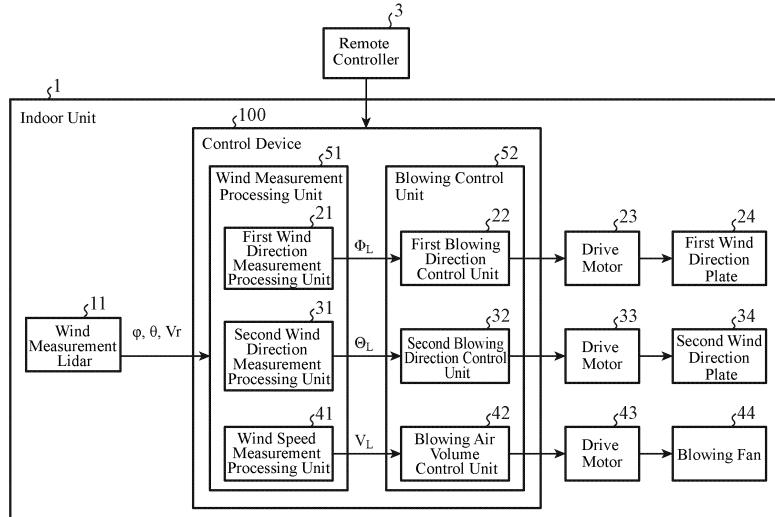
Tokyo 1008310 (JP)

(54) AIR CONDITIONER AND CONTROL METHOD

(57) An air conditioning device (200) includes: a wind measurement processing unit (51) calculating wind directions (Φ , Θ) using measured values by a wind measurement lidar (11); and a blowing control unit (52) con-

trolling blowing directions (Φ' , Θ') using measured wind direction values (Φ_L , Θ_L) calculated by the wind measurement processing unit (51).

FIG. 2



Description**TECHNICAL FIELD**

[0001] The present invention relates to an air conditioning device and a control method.

BACKGROUND ART

[0002] Various devices for air conditioning have been developed conventionally. More specifically, an air-conditioner, a fan, a blower, an air duct device, and the like have been developed. Hereinafter, these devices are generally referred to as the "air conditioning device".

[0003] A technique has conventionally been developed in which a wind speed in a space that is to be an air conditioning target of an air-conditioner is measured and the measured wind speed is used to control a blowing air volume by the air-conditioner (see, for example, Patent Literature 1).

CITATION LIST**PATENT LITERATURE**

[0004] Patent Literature 1: JP 2017-180940 A

SUMMARY OF INVENTION**TECHNICAL PROBLEM**

[0005] From a viewpoint of improving user comfort in the space described above, it is of course important to control a blowing air volume by an air-conditioner, and it is also important to control a blowing direction by the air-conditioner. In the conventional technique described in Patent Literature 1, a wind direction in the space is not included as a measurement target, and the blowing direction by the air-conditioner is not included as a control target. For this reason, there has been a problem that the user comfort in the space cannot be sufficiently improved.

[0006] Furthermore, the conventional technique described in Patent Literature 1 uses a sensor unit for measurement of the wind speed in the space. The sensor unit is provided in a remote controller for the air-conditioner. For this reason, when a position of a user in the space and a position of the remote controller in the space are separated from each other (that is, when the user does not hold the remote controller), the wind speed at the position of the remote controller is measured, and the blowing air volume is controlled on the basis of the measured wind speed. In this case, there is a problem that the wind speed at the position of the user may not become a suitable wind speed. As a result, there has been a problem that the user comfort in the space cannot be sufficiently improved.

[0007] The present invention has been made to solve

the problems as described above, and an object of the present invention is to provide an air conditioning device and a control method capable of improving user comfort.

5 **SOLUTION TO PROBLEM**

[0008] An air conditioning device of the present invention includes: a wind measurement processing unit calculating a wind direction value indicating a wind direction using a measured value by a lidar for measuring a wind; and a blowing control unit executing control of a blowing direction using the wind direction value calculated by the wind measurement processing unit.

10 **15 ADVANTAGEOUS EFFECTS OF INVENTION**

[0009] According to the present invention, since the blowing direction is controlled using the wind direction measured by the lidar for measuring the wind, appropriate blowing control is possible, and the user comfort can be improved.

BRIEF DESCRIPTION OF DRAWINGS

25 **[0010]**

FIG. 1 is a block diagram illustrating a main part of an air conditioning device according to a first embodiment.

30 FIG. 2 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the first embodiment.

FIG. 3 is an explanatory diagram illustrating an example of one measurement target area.

35 FIG. 4 is an explanatory diagram illustrating an example of a state in which one measurement target area moves in an air conditioning target space by scanning of a laser beam.

FIG. 5 is an explanatory diagram illustrating an example of a portion of a first calibration value table corresponding to a predetermined Z coordinate value.

40 FIG. 6A is an explanatory diagram illustrating a hardware configuration of a control device in the air conditioning device according to the first embodiment.

45 FIG. 6B is an explanatory diagram illustrating another hardware configuration of the control device in the air conditioning device according to the first embodiment.

50 FIG. 7A is a flowchart illustrating the operation of the control device in the air conditioning device according to the first embodiment.

FIG. 7B is a flowchart illustrating an operation of the control device in the air conditioning device according to the first embodiment.

55 FIG. 8 is a flowchart illustrating a detailed operation of the control device in the air conditioning device according to the first embodiment.

FIG. 9 is a flowchart illustrating another detailed operation of the control device in the air conditioning device according to the first embodiment.

FIG. 10 is an explanatory diagram illustrating an example of a plurality of measurement target areas.

FIG. 11 is a block diagram illustrating a main part of an air conditioning device according to a second embodiment.

FIG. 12 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the second embodiment.

FIG. 13A is a flowchart illustrating the operation of a control device in the air conditioning device according to the second embodiment.

FIG. 13B is a flowchart illustrating an operation of the control device in the air conditioning device according to the second embodiment.

FIG. 13C is a flowchart illustrating another operation of the control device in the air conditioning device according to the second embodiment.

FIG. 14 is a block diagram illustrating a main part of another indoor unit of the air conditioning device according to the second embodiment.

FIG. 15 is a block diagram illustrating the main part of the other indoor unit of the air conditioning device according to the second embodiment.

FIG. 16 is a block diagram illustrating a main part of an air conditioning device according to a third embodiment.

FIG. 17 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the third embodiment.

FIG. 18A is a flowchart illustrating the operation of a control device in the air conditioning device according to the third embodiment.

FIG. 18B is a flowchart illustrating an operation of the control device in the air conditioning device according to the third embodiment.

DESCRIPTION OF EMBODIMENTS

[0011] Hereinafter, to explain the present invention in more detail, embodiments for carrying out the present invention will be described with reference to the accompanying drawings.

First Embodiment.

[0012] FIG. 1 is a block diagram illustrating a main part of an air conditioning device according to a first embodiment. FIG. 2 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the first embodiment. An air conditioning device 200 of the first embodiment will be described with reference to FIGS. 1 and 2.

[0013] As illustrated in FIG. 1, the air conditioning device 200 includes an air-conditioner. That is, the air conditioning device 200 includes an indoor unit 1 and an

outdoor unit 2. The indoor unit 1 includes a heat exchanger (not illustrated), and the outdoor unit 2 includes another heat exchanger (not illustrated), and these heat exchangers are thermally connected to each other via a refrigerant pipe (not illustrated). The outdoor unit 2 includes a compressor (not illustrated) for refrigerant, and the like. Since structures, arrangements, operations, and the like of these members are known, detailed description thereof will be omitted. The air conditioning device 200 is operated with a remote controller 3.

[0014] Hereinafter, the left-right direction with respect to the indoor unit 1 is referred to as the "X direction". The front-back direction with respect to the indoor unit 1 is referred to as the "Y direction". The up-down direction with respect to the indoor unit 1 is referred to as the "Z direction". The azimuth direction with respect to the indoor unit 1, that is, the azimuth direction with respect to a virtual axis (hereinafter referred to as the "Y axis") along the Y direction is simply referred to as the "azimuth direction". The elevation or depression angle direction with respect to the indoor unit 1, that is, the elevation or depression angle direction with respect to the Y axis is simply referred to as the "elevation or depression angle direction".

[0015] A space S that is to be an air conditioning target of the air conditioning device 200 is referred to as the "air conditioning target space". One or more areas A1 that are to be measurement targets for wind directions Φ and Θ and a wind speed V in the air conditioning target space S are referred to as the "measurement target areas". Usually, each measurement target area A1 is set to a small area in which it can be assumed that the wind directions Φ and Θ and wind speed V in the area are constant.

[0016] The wind direction Φ with respect to the azimuth direction in the air conditioning target space S may be referred to as the "first wind direction". The wind direction Θ with respect to the elevation or depression angle direction in the air conditioning target space S may be referred to as the "second wind direction". The blowing direction Φ' by the indoor unit 1 with respect to the azimuth direction may be referred to as the "first blowing direction". The blowing direction Θ' by the indoor unit 1 with respect to the elevation or depression angle direction may be referred to as the "second blowing direction".

[0017] As illustrated in FIG. 2, the indoor unit 1 includes a wind measurement lidar 11. The wind measurement lidar 11 includes, for example, a pulse modulation type lidar, a continuous wave (CW) type lidar, or a lidar of a type using intensity correlation. Since the configuration and operation principle of the lidar of each type are known, detailed description thereof will be omitted.

[0018] An emission port O for a laser beam of the wind measurement lidar 11 is provided, for example, on the front surface portion of the indoor unit 1. In the wind measurement lidar 11, an emission direction D, that is, a line-of-sight direction, of the laser beam is variable. The wind measurement lidar 11 emits the laser beam to the air conditioning target space S, thereby measuring a wind

speed (hereinafter, referred to as the "line-of-sight direction wind speed") V_r with respect to the line-of-sight direction, at a point (hereinafter referred to as the "measurement target point") P at any distance with respect to the emission direction D . Since the method of measuring the line-of-sight direction wind speed V_r by the wind measurement lidar 11 is known, detailed description thereof will be omitted.

[0019] An output signal of the wind measurement lidar 11 includes angle values φ and θ corresponding to the emission direction D . That is, φ is an angle value with respect to the azimuth direction, and θ is an angle value with respect to the elevation or depression angle direction. Furthermore, the output signal of the wind measurement lidar 11 includes a value of the line-of-sight direction wind speed V_r at the measurement target point P .

[0020] A first wind direction measurement processing unit 21 calculates a measured value Φ_L of the first wind direction Φ in the measurement target area A1 by using the output signal of the wind measurement lidar 11. A second wind direction measurement processing unit 31 calculates a measured value Θ_L of the second wind direction Θ in the measurement target area A1 by using the output signal of the wind measurement lidar 11. A wind speed measurement processing unit 41 calculates a measured value V_L of the wind speed V in the measurement target area A1 by using the output signal of the wind measurement lidar 11.

[0021] Hereinafter, the measured value Φ_L may be referred to as the "first measured wind direction value". The measured value Θ_L may be referred to as the "second measured wind direction value". The first measured wind direction value Φ_L and the second measured wind direction value Θ_L may be collectively referred to as the "measured wind direction values". The measured value V_L may be referred to as the "measured wind speed value".

[0022] The first wind direction measurement processing unit 21, the second wind direction measurement processing unit 31, and the wind speed measurement processing unit 41 constitute a main part of a wind measurement processing unit 51. That is, the wind measurement processing unit 51 calculates the measured wind direction values Φ_L and Θ_L and the measured wind speed value V_L by using the output signal of the wind measurement lidar 11. Hereinafter, pieces of processing in which the wind measurement processing unit 51 calculates the measured wind direction values Φ_L and Θ_L and the measured wind speed value V_L are collectively referred to as the "wind measurement processing".

[0023] Here, a specific example of the wind measurement processing will be described with reference to FIG. 3.

[0024] The line-of-sight direction wind speed V_r at the measurement target point P is expressed by the following expression (1) using the angle values φ and θ corresponding to the emission direction D . V_u in the expression (1) is a wind speed value in the X direction at the measurement target point P . V_v in the expression (1) is

a wind speed value in the Y direction at the measurement target point P . V_w in the expression (1) is a wind speed value in the Z direction at the measurement target point P .

$$\begin{aligned} V_r = & V_u \times \sin\varphi \times \cos\theta \\ & + V_v \times \cos\varphi \times \cos\theta \\ & + V_w \times \sin\theta \end{aligned} \quad (1)$$

[0025] The wind measurement lidar 11 emits the laser beam in N directions D_1 to D_N , thereby measuring the line-of-sight direction wind speed V_r at each of N measurement target points P_1 to P_N in the inside (more specifically, an edge portion) of the measurement target area A1. Here, N is an integer greater than or equal to 3, and $N = 3$ in the example illustrated in FIG. 3. As a result, the output signal is obtained including N angle values φ_1 to φ_N , N angle values θ_1 to θ_N , and N line-of-sight direction wind speeds V_{r1} to V_{rN} . That is, the N emission directions D_1 to D_N , the N measurement target points P_1 to P_N , the N angle values φ_1 to φ_N , the N angle values θ_1 to θ_N , and the N line-of-sight direction wind speeds V_{r1} to V_{rN} have a one-to-one correspondence with each other.

[0026] Note that, the difference value between each two angle values φ among the N angle values φ_1 to φ_N is set to a predetermined value (for example, 2 degrees). Furthermore, the difference value between each two angle values θ among the N angle values θ_1 to θ_N is set to a predetermined value (for example, 2 degrees).

[0027] These values φ_1 to φ_N , θ_1 to θ_N , and V_{r1} to V_{rN} are substituted to the expression (1), whereby simultaneous equations with three unknowns including the three variables V_u , V_v , and V_w are obtained. The wind measurement processing unit 51 calculates the wind speed values V_u , V_v , and V_w by solving the simultaneous equations with three unknowns.

[0028] The first wind direction measurement processing unit 21 calculates the first measured wind direction value Φ_L by the following expression (2) by using the calculated wind speed values V_u , V_v , and V_w . The second wind direction measurement processing unit 31 calculates the second measured wind direction value Θ_L by the following expression (3) by using the calculated wind speed values V_u , V_v , and V_w . The wind speed measurement processing unit 41 calculates the measured wind speed value V_L by the following expression (4) by using the calculated wind speed values V_u , V_v , and V_w .

$$\Phi_L = \tan(V_u/V_v) \quad (2)$$

$$\Theta_L = \tan\{V_w/\sqrt{(V_u^2 + V_v^2)}\} \quad (3)$$

$$V_L = \sqrt{(V_u^2 + V_v^2 + V_w^2)} \quad (4)$$

[0029] That is, the wind measurement processing unit 51 calculates the measured wind direction values Φ_L and Θ_L and the measured wind speed value V_L on the assumption that the wind directions Φ and Θ and the wind speed V in the measurement target area A1 are constant.

[0030] As illustrated in FIG. 4, the wind measurement lidar 11 performs scanning of the laser beam, whereby the measurement target area A1 moves in the air conditioning target space S. The wind measurement processing unit 51 calculates the measured values Φ_L , Θ_L , and V_L multiple times during the scanning, whereby measurement of the wind directions Φ and Θ and the wind speed V can be implemented over a wide range in the air conditioning target space S. More specifically, the measurement of the wind directions Φ and Θ and the wind speed V can be implemented in substantially the entire air conditioning target space S.

[0031] The indoor unit 1 includes a wind direction plate (hereinafter, may be referred to as the "first wind direction plate") 24 whose mounting angle with respect to the azimuth direction is variable. The indoor unit 1 includes a drive motor 23 for the first wind direction plate 24. A first blowing direction control unit 22 controls the first blowing direction Φ' by controlling a rotation position of a rotor in the drive motor 23, that is, by controlling the mounting angle of the first wind direction plate 24.

[0032] The indoor unit 1 includes a wind direction plate (hereinafter, may be referred to as the "second wind direction plate") 34 whose mounting angle with respect to the elevation or depression angle direction is variable. The indoor unit 1 includes a drive motor 33 for the second wind direction plate 34. A second blowing direction control unit 32 controls the second blowing direction Θ' by controlling a rotation position of a rotor in the drive motor 33, that is, by controlling the mounting angle of the second wind direction plate 34.

[0033] The indoor unit 1 includes a blowing fan 44. The indoor unit 1 includes a drive motor 43 for the blowing fan 44. A blowing air volume control unit 42 controls a blowing air volume V' by the indoor unit 1 by controlling a rotation speed of a rotor in the drive motor 43, that is, by controlling a rotation speed of the blowing fan 44.

[0034] The first blowing direction control unit 22, the second blowing direction control unit 32, and the blowing air volume control unit 42 constitute a main part of a blowing control unit 52. That is, the blowing control unit 52 controls the blowing directions Φ' and Θ' and the blowing air volume V' by the indoor unit 1.

[0035] Here, the first blowing direction control unit 22 has a function of calibrating the first blowing direction Φ' by using the first measured wind direction value Φ_L calculated by the first wind direction measurement processing unit 21. The second blowing direction control unit 32 has a function of calibrating the second air direction Φ' by using the second measured wind direction value Θ_L calculated by the second wind direction measurement processing unit 31. The blowing air volume control unit 42 has a function of calibrating the blowing air volume V'

by using the measured wind speed value V_L calculated by the wind speed measurement processing unit 41. Hereinafter, controls in which the blowing control unit 52 calibrates the blowing directions Φ' and Θ' and the blowing air volume V' using the measured values Φ_L , Θ_L , and V_L are collectively referred to as the "calibration control". Hereinafter, a specific example of the calibration control will be described.

[0036] First, the first blowing direction control unit 22 sets the first blowing direction Φ' to an initial value (for example, a predetermined value). The second blowing direction control unit 32 sets the second blowing direction Θ' to an initial value (for example, a predetermined value). The blowing air volume control unit 42 sets the blowing air volume V' to an initial value (for example, a predetermined value). Hereinafter, each of the set values may be referred to as the "set value".

[0037] Here, in the blowing control unit 52, a plurality of three-dimensional tables (hereinafter referred to as the "wind direction and wind speed table") is stored in advance indicating a correspondence between the values of Φ' , Θ' , and V' with respect to the indoor unit 1 and the values of Φ , Θ , and V in each of a plurality of areas (hereinafter referred to as the "unit area") A2 obtained by dividing the air conditioning target space S in the X direction, the Y direction, and the Z direction. The blowing control unit 52 selects a wind direction and wind speed table corresponding to the set values of Φ' , Θ' , and V' from among the plurality of wind direction and wind speed tables stored in advance.

[0038] When the first measured wind direction value Φ_L is calculated by the first wind direction measurement processing unit 21, the first blowing direction control unit 22 sets a target value Φ_A of the first wind direction Φ in the measurement target area A1 by using the selected wind direction and wind speed table. That is, the target value Φ_A is set depending on the value of Φ in the unit area A2 corresponding to the measurement target area A1 among the values of Φ included in the selected wind direction and wind speed table. Hereinafter, the target value Φ_A may be referred to as the "first target wind direction value".

[0039] The first blowing direction control unit 22 calculates a difference value Φ_E between the first target wind direction value Φ_A and the first measured wind direction value Φ_L . The first blowing direction control unit 22 compares the absolute value of the difference value Φ_E with a predetermined threshold value Φ_{th} . When the absolute value of the difference value Φ_E is larger than the threshold value Φ_{th} , the first blowing direction control unit 22 calculates a calibration value Φ_C depending on the difference value Φ_E . The first blowing direction control unit 22 corrects the first blowing direction Φ' on the basis of the calculated calibration value Φ_C . As a result, the first blowing direction Φ' is calibrated.

[0040] When the second measured wind direction value Θ_L is calculated by the second wind direction measurement processing unit 31, the second blowing direction

control unit 32 sets a target value Θ_A of the second wind direction Θ in the measurement target area A1 by using the selected wind direction and wind speed table. That is, the target value Θ_A is set depending on the value of Θ in the unit area A2 corresponding to the measurement target area A1 among the values of Θ included in the selected wind direction and wind speed table. Hereinafter, the target value Θ_A may be referred to as the "second target wind direction value". The first target wind direction value Φ_A and the second target wind direction value Θ_A may be collectively referred to as the "target wind direction values".

[0041] The second blowing direction control unit 32 calculates a difference value Θ_E between the second target wind direction value Θ_A and the second measured wind direction value Θ_L . The second blowing direction control unit 32 compares the absolute value of the difference value Θ_E with a predetermined threshold value Θ_{th} . When the absolute value of the difference value Θ_E is larger than the threshold value Θ_{th} , the second blowing direction control unit 32 calculates a calibration value Oc depending on the difference value Θ_E . The first blowing direction control unit 22 corrects the second blowing direction Θ' on the basis of the calculated calibration value Oc . As a result, the second blowing direction Θ' is calibrated.

[0042] When the measured wind speed value V_L is calculated by the wind speed measurement processing unit 41, the blowing air volume control unit 42 sets a target value V_A of the wind speed V in the measurement target area A1 by using the selected wind direction and wind speed table. That is, the target value V_A is set depending on the value of V in the unit area A2 corresponding to the measurement target area A1 among the values of V included in the selected wind direction and wind speed table. Hereinafter, the target value V_A may be referred to as the "target wind speed value".

[0043] The blowing air volume control unit 42 calculates a difference value V_E between the target wind speed value V_A and the measured wind speed value V_L . The blowing air volume control unit 42 compares the absolute value of the difference value V_E with a predetermined threshold value V_{th} . When the absolute value of the difference value V_E is larger than the threshold value V_{th} , the blowing air volume control unit 42 calculates a calibration value Vc depending on the difference value V_E . The blowing air volume control unit 42 corrects the blowing air volume V' on the basis of the calculated calibration value Vc . As a result, the blowing air volume V' is calibrated.

[0044] Note that, the wind measurement lidar 11 can measure the line-of-sight direction wind speed V_r continuously in time (so-called in "real time"). Thus, the first wind direction measurement processing unit 21 can calculate the first measured wind direction value Φ_L continuously in time. The second wind direction measurement processing unit 31 can calculate the second measured wind direction value Θ_L continuously in time. The wind

speed measurement processing unit 41 can calculate the measured wind speed value V_L continuously in time.

[0045] Thus, the first blowing direction control unit 22 may repeatedly execute correction of the first blowing direction Φ' so that the absolute value of the difference value Φ_E is gradually reduced, by using the continuously calculated first measured wind direction value Φ_L . The second blowing direction control unit 32 may repeatedly execute correction of the second blowing direction Θ' so that the absolute value of the difference value Θ_E is gradually reduced, by using the continuously calculated second measured wind direction value Θ_L . The blowing air volume control unit 42 may repeatedly execute correction of the blowing air volume V' so that the absolute value of the difference value V_E is gradually reduced, by using the continuously calculated measured wind speed value V_L . That is, the calibration control may be performed by so-called "feedback control".

[0046] Furthermore, the first blowing direction control unit 22 may manage the calibration value Φ_C calculated in the calibration control by using a dedicated three-dimensional table (hereinafter referred to as the "first calibration value table"). That is, the first calibration value table indicates the calibration value Φ_C in each of the plurality of unit areas A2. FIG. 5 illustrates an example of a portion of the first calibration value table corresponding to a predetermined Z coordinate value. In the example illustrated in FIG. 5, the calibration value Φ_C in each of the 99 unit areas A2 corresponding to the predetermined Z coordinate value is set to a value within a range of -5 degrees to +5 degrees.

[0047] Furthermore, the second blowing direction control unit 32 may manage the calibration value Oc calculated in the calibration control by using a dedicated three-dimensional table (hereinafter referred to as the "second calibration value table"). That is, the second calibration value table indicates the calibration value Oc in each of the plurality of unit areas A2. Since a specific example of the second calibration value table is similar to the specific example of the first calibration value table illustrated in FIG. 5, illustration and description will be omitted.

[0048] Furthermore, the blowing air volume control unit 42 may manage the calibration value Vc calculated in the calibration control by using a dedicated three-dimensional table (hereinafter referred to as the "third calibration value table"). That is, the third calibration value table indicates the calibration value Vc in each of the plurality of unit areas A2. Since a specific example of the third calibration value table is similar to the specific example of the first calibration value table illustrated in FIG. 5, illustration and description will be omitted. Hereinafter, the first calibration value table, the second calibration value table, and the third calibration value table may be collectively referred to as the "calibration value table".

[0049] The wind measurement processing unit 51 and the blowing control unit 52 constitute a main part of a control device 100. The wind measurement lidar 11, the drive motor 23, the first wind direction plate 24, the drive

motor 33, the second wind direction plate 34, the drive motor 43, the blowing fan 44, and the control device 100 constitute a main part of the indoor unit 1. The indoor unit 1 and the outdoor unit 2 constitute a main part of the air conditioning device 200.

[0050] Next, a hardware configuration of the main part of the control device 100 will be described with reference to FIG. 6.

[0051] As illustrated in FIG. 6A, the control device 100 includes a processor 61 and a memory 62. A nonvolatile memory of the memory 62 stores a program corresponding to functions of the wind measurement processing unit 51 and the blowing control unit 52. The processor 61 loads the stored program into a volatile memory of the memory 62 and executes the loaded program. As a result, the functions of the wind measurement processing unit 51 and the blowing control unit 52 are implemented.

[0052] Alternatively, as illustrated in FIG. 6B, the control device 100 includes a processing circuit 63. In this case, the functions of the wind measurement processing unit 51 and the blowing control unit 52 are implemented by the dedicated processing circuit 63.

[0053] Alternatively, the control device 100 includes the processor 61, the memory 62, and the processing circuit 63 (not illustrated). In this case, some of the functions of the wind measurement processing unit 51 and the blowing control unit 52 are implemented by the processor 61 and the memory 62, and the remaining functions are implemented by the dedicated processing circuit 63.

[0054] The processor 61 includes, for example, at least one of a central processing unit (CPU), a graphics processing unit (GPU), a microprocessor, a microcontroller, or a digital signal processor (DSP).

[0055] The volatile memory of the memory 62 includes, for example, a random access memory (RAM). The non-volatile memory of the memory 62 includes, for example, at least one of a read only memory (ROM), a flash memory, an erasable programmable read only memory (EPROM), an electrically erasable programmable read only memory (EEPROM), a solid state drive (SSD), or a hard disk drive (HDD).

[0056] The processing circuit 63 is formed by using, for example, an application specific integrated circuit (ASIC), a programmable logic device (PLD), a field-programmable gate array (FPGA), a system-on-a-chip (SoC), a system large-scale integration (LSI), or the like.

[0057] Next, the operation of the control device 100 will be described with reference to a flowchart of FIG. 7. The blowing control unit 52 starts processing of step ST1 when, for example, an operation for instructing the start of air conditioning (cooling, heating, or the like) is input to the remote controller 3.

[0058] First, in step ST1, the blowing control unit 52 executes initial setting of the blowing directions Φ' and Θ' and the blowing air volume V' . That is, the first blowing direction control unit 22 sets the first blowing direction Φ' to the initial value. The second blowing direction control unit 32 sets the second blowing direction Θ' to the initial

value. The blowing air volume control unit 42 sets the blowing air volume V' to the initial value.

[0059] Next, in step ST2, the blowing control unit 52 executes control to start blowing by the indoor unit 1. That is, the first blowing direction control unit 22 controls the rotation position of the rotor in the drive motor 23 so that the mounting angle of the first wind direction plate 24 becomes an angle corresponding to the set value of the first blowing direction Φ' in step ST1. The second blowing direction control unit 32 controls the rotation position of the rotor in the drive motor 33 so that the mounting angle of the second wind direction plate 34 becomes an angle corresponding to the set value of the second blowing direction Θ' in step ST1. The blowing air volume control unit 42 causes rotation of the drive motor 43 (that is, rotation of the blowing fan 44) to be started at a rotation speed corresponding to the set value of the blowing air volume V' in step ST1.

[0060] When an operation for instructing the end of the air conditioning is input to the remote controller 3, for example, the blowing control unit 52 executes control to end the blowing by the indoor unit 1. That is, the blowing air volume control unit 42 causes the rotation of the drive motor 43 (that is, the rotation of the blowing fan 44) to be stopped.

[0061] Here, while the blowing by the indoor unit 1 is executed, the wind measurement lidar 11 repeatedly executes processing of measuring the line-of-sight direction wind speed V_r (more specifically, N line-of-sight direction wind speeds V_{r1} to V_{rN}) while performing scanning of the laser beam (that is, while moving the measurement target area A1) (see FIG. 4). Furthermore, the wind measurement lidar 11 repeatedly executes processing of outputting the signal including the angle values φ (more specifically, the N angle values φ_1 to φ_{N_r}), the angle values θ (more specifically, the N angle values θ_1 to θ_{N_r}), and the values of the line-of-sight direction wind speeds V_r (more specifically, the N line-of-sight direction wind speeds V_{r1} to V_{rN}). As a result, the wind measurement processing by the wind measurement processing unit 51 (step ST3) and the calibration control by the blowing control unit 52 (step ST4) are repeatedly executed.

[0062] Next, details of the processing of steps ST3 and ST4 of each time will be described with reference to a flowchart of FIG. 8. That is, processing of steps ST11, ST21, and ST31 in FIG. 8 is included in the processing of step ST3 (that is, the wind measurement processing) of each time. Furthermore, processing of steps ST12 to ST15, ST22 to ST25, and ST32 to ST35 in FIG. 8 is included in the processing of step ST4 (that is, calibration control) of each time.

[0063] First, the first wind direction measurement processing unit 21 calculates the first measured wind direction value Φ_L in the measurement target area A1 by using the output signal of the wind measurement lidar 11 (step ST11). Next, the first blowing direction control unit 22 calculates the difference value Φ_E between the first target wind direction value Φ_A and the first measured

wind direction value Φ_L calculated in step ST11 (step ST12). The first target wind direction value Φ_A is set using the wind direction and wind speed table corresponding to the set values of Φ' , Θ' , and V' in step ST1. More specifically, the first target wind direction value Φ_A is set depending on the value of Φ in the unit area A2 corresponding to the measurement target area A1 among the values of Φ included in the wind direction and wind speed table.

[0064] Next, the first blowing direction control unit 22 compares the absolute value of the difference value Φ_L calculated in step ST12 with the threshold value Φ_{th} (step ST13). When the absolute value of the difference value Φ_E is larger than the threshold value Φ_{th} (step ST13 "NO"), the first blowing direction control unit 22 calculates the calibration value Φ_C depending on the difference value Φ_E (step ST14). Next, the first blowing direction control unit 22 corrects the first blowing direction Φ' on the basis of the calibration value Φ_C calculated in step ST14 (step ST15). That is, the first blowing direction control unit 22 corrects the mounting angle of the first wind direction plate 24 by correcting the rotation position of the rotor in the drive motor 23.

[0065] The second wind direction measurement processing unit 31 calculates the second measured wind direction value Θ_L in the measurement target area A1 by using the output signal of the wind measurement lidar 11 (step ST21). Next, the second blowing direction control unit 32 calculates the difference value Θ_E between the second target wind direction value Θ_A and the second measured wind direction value Θ_L calculated in step ST21 (step ST22). The second target wind direction value Θ_A is set using the wind direction and wind speed table corresponding to the set values of Φ' , Θ' , and V' in step ST1. More specifically, the second target wind direction value Θ_A is set depending on the value of Θ in the unit area A2 corresponding to the measurement target area A1 among the values of Θ included in the wind direction and wind speed table.

[0066] Next, the second blowing direction control unit 32 compares the absolute value of the difference value Θ_E calculated in step ST22 with the threshold value Θ_{th} (step ST23). When the absolute value of the difference value Θ_E is larger than the threshold value Θ_{th} (step ST23 "NO"), the second blowing direction control unit 32 calculates the calibration value Θ_C depending on the difference value Θ_E (step ST24). Next, the second blowing direction control unit 32 corrects the second blowing direction Θ' on the basis of the calibration value Θ_C calculated in step ST24 (step ST25). That is, the second blowing direction control unit 32 corrects the mounting angle of the second wind direction plate 34 by correcting the rotation position of the rotor in the drive motor 33.

[0067] The wind speed measurement processing unit 41 calculates the measured wind speed value V_L in the measurement target area A1 by using the output signal of the wind measurement lidar 11 (step ST31). Next, the blowing air volume control unit 42 calculates the difference value V_E between the target wind speed value V_A

and the measured wind speed value V_L calculated in step ST31 (step ST32). The target wind speed value V_A is set using the wind direction and wind speed table corresponding to the set values of Φ' , Θ' , and V' in step ST1.

5 More specifically, the target wind speed value V_A is set depending on the value of V in the unit area A2 corresponding to the measurement target area A1 among the values of V included in the wind direction and wind speed table.

10 **[0068]** Next, the blowing air volume control unit 42 compares the absolute value of the difference value V_E calculated in step ST32 with the threshold value V_{th} (step ST33). When the absolute value of the difference value V_E is larger than the threshold value V_{th} (step ST33 "NO"), the blowing air volume control unit 42 calculates the calibration value V_C depending on the difference value V_E (step ST34). Next, the blowing air volume control unit 42 corrects the blowing air volume V' on the basis of the calibration value V_C calculated in step ST34 (step

15 ST35). That is, the blowing air volume control unit 42 corrects the rotation speed of the blowing fan 44 by correcting the rotation speed of the rotor in the drive motor 43.

[0069] Next, effects of the air conditioning device 200 **25** will be described.

[0070] As described above, the control device 100 measures the wind directions Φ and Θ in the air conditioning target space S, and uses the measured wind direction values Φ_L and Θ_L for the control (more specifically, the calibration control) of the blowing directions Φ' and Θ' .

[0071] Usually, the correspondence between the blowing directions Φ' and Θ' by the indoor unit 1 and the wind directions Φ and Θ at each point in the air conditioning **35** target space S may change depending on an installation situation of furniture and the like in the air conditioning target space S. Furthermore, such a correspondence may change due to aging degradation of constituent members (for example, the drive motors 23 and 33, and the wind direction plates 24 and 34) of the indoor unit 1 and the like. If the blowing control unit 52 controls the blowing directions Φ' and Θ' on the basis of a predetermined table (for example, the wind direction and wind speed table) without executing the wind measurement

40 processing and the calibration control, there has been a problem that it is not possible to cope with such a change. As a result, there has been a problem that the difference values of the wind directions Φ and Θ with respect to the target wind direction values Φ_A and Θ_A are increased, and the user comfort in the air conditioning target space S is decreased.

[0072] On the other hand, the wind measurement processing unit 51 executes the wind measurement processing, and the blowing control unit 52 executes the **45** calibration control, whereby it becomes possible to cope with such a change. That is, the difference values of the wind direction Φ and Θ with respect to the target wind direction values Φ_A , Θ_A can be decreased regardless of

55

the installation situation of the furniture and the like in the air conditioning target space S, and regardless of the aging degradation of the constituent members of the indoor unit 1 and the like. As a result, it is possible to suppress the decrease in user comfort in the air conditioning target space S. In other words, the user comfort in the air conditioning target space S can be improved.

[0073] Furthermore, the control device 100 measures the wind speed V in the air conditioning target space S, and uses the measured wind speed value V_L for the control of the blowing air volume V' (more specifically, the calibration control). As a result, the user comfort in the air conditioning target space S can be improved similarly to the above.

[0074] Furthermore, in the control device 100, the wind measurement lidar 11 integrated with the indoor unit 1 is used for the measurement of the wind directions Φ and Θ and the wind speed V. As a result, it is possible to eliminate the need for a dedicated measuring device that is a separate member from the indoor unit 1. Furthermore, the measurement of the wind directions Φ and Θ and the wind speed V can be implemented over a wide range in the air conditioning target space S.

[0075] Next, another specific example of the wind measurement processing and the calibration control will be described with reference to a flowchart of FIG. 9.

[0076] In the example illustrated in FIG. 8, the wind measurement processing is executed every time the wind measurement lidar 11 outputs the signal including the values of φ_1 to cp_N , θ_1 to θ_M , and Vr_1 to Vr_N once during the scanning of the laser beam. As a result, one each of the measured values Φ_L , Θ_L , and V_L is calculated in the wind measurement processing (step ST3) of each time.

[0077] On the other hand, in the example illustrated in FIG. 9, the wind measurement processing is executed every time the wind measurement lidar 11 outputs the signal including the values of φ_1 to cp_N , θ_1 to θ_M , and Vr_1 to Vr_N M times during the scanning of the laser beam. As a result, M each of the measured values Φ_L , Θ_L , and V_L are calculated in the wind measurement processing (step ST3) of each time. Here, M is an integer greater than or equal to 2. That is, the M measured values Φ_L , Θ_L , and V_L are different from each other in coordinate values of the corresponding measurement target areas A1.

[0078] That is, in step ST11a, the first wind direction measurement processing unit 21 calculates M first measured wind direction values Φ_{L1} to Φ_{LM} .

[0079] Next, the first blowing direction control unit 22 calculates difference values Φ_{E1} to Φ_{EM} between first target wind direction values Φ_{A1} to Φ_{AM} and the first measured wind direction values Φ_{L1} to Φ_{EM} , individually (step ST12a). Here, the M first target wind direction values Φ_{A1} to Φ_{AM} have a one-to-one correspondence with the M first measured wind direction values Φ_{L1} to Φ_{EM} . The method of setting each of the M first target wind direction values Φ_{A1} to Φ_{AM} is as described above. Next,

the first blowing direction control unit 22 calculates a root mean square (RMS) error Φ_{RMSE} based on the M difference values Φ_{E1} to Φ_{EM} (step ST12a).

[0080] Next, the first blowing direction control unit 22 compares the RMS error Φ_{RMSE} with the predetermined threshold value Φ_{th} (step ST13a). When the RMS error Φ_{RMSE} is larger than the threshold value Φ_{th} (step ST13a "NO"), the first blowing direction control unit 22 calculates the calibration value Φ_C depending on any one difference value Φ_E among the M difference values Φ_{E1} to Φ_{EM} (for example, the largest difference value Φ_E among the M difference values Φ_{E1} to Φ_{EM}) (step ST14a). Next, the first blowing direction control unit 22 corrects the first blowing direction Φ' on the basis of the calculated calibration value Φ_C (step ST15).

[0081] In step ST21a, the second wind direction measurement processing unit 31 calculates M second measured wind direction values Θ_{L1} to Θ_{LM} .

[0082] Next, the second blowing direction control unit 32 calculates difference values Θ_{E1} to Θ_{EM} between second target wind direction values Θ_{A1} to Θ_{AM} and the second measured wind direction values Θ_{L1} to Θ_{LM} (step ST22a). Here, the M second target wind direction values Θ_{A1} to Θ_{AM} have a one-to-one correspondence with the M second measured wind direction values Θ_{L1} to Θ_{LM} . The method of setting each of the M second target wind direction values Θ_{A1} to Θ_{AM} is as described above. Next, the second blowing direction control unit 32 calculates an RMS error Θ_{RMSE} based on the M difference values Θ_{E1} to Θ_{EM} (step ST22a).

[0083] Next, the second blowing direction control unit 32 compares the RMS error Θ_{RMSE} with the predetermined threshold Θ_{th} (step ST23a). When the RMS error Θ_{RMSE} is larger than the threshold value Θ_{th} (step ST23a "NO"), the second blowing direction control unit 32 calculates the calibration value Θ_C depending on any one difference value Θ_E among the M difference values Θ_{E1} to Θ_{EM} (for example, the largest difference value Θ_E among the M difference values Θ_{E1} to Θ_{EM}) (step ST24a).

[0084] Next, the second blowing direction control unit 32 corrects the second blowing direction Θ' on the basis of the calculated calibration value Θ_C (step ST25).

[0085] Next, the blowing air volume control unit 42 calculates difference values V_{E1} to V_{EM} between target wind speed values V_{A1} to V_{AM} and the measured wind speed values V_{L1} to V_{LM} (step ST32a). Here, the M target wind speed values V_{A1} to V_{AM} have a one-to-one correspondence with the M measured wind speed values V_{L1} to V_{LM} . The method of setting each of the M target wind speed values V_{A1} to V_{AM} is as described above. Next, the blowing air volume control unit 42 calculates an RMS error V_{RMSE} based on the M difference values V_{E1} to V_{EM} (step ST32a).

[0086] Next, the blowing air volume control unit 42 compares the RMS error V_{RMSE} with the predetermined

threshold value V_{th} (step ST33a). When the RMS error V_{RMSE} is larger than the threshold value V_{th} (step ST33a "NO"), the blowing air volume control unit 42 calculates the calibration value V_c depending on any one difference value V_E among the M difference values V_{E1} to V_{EM} (for example, the largest difference value V_E among the M difference values V_{E1} to V_{EM}) (step ST34a). Next, the blowing air volume control unit 42 corrects the blowing air volume V' on the basis of the calculated calibration value V_c (step ST35).

[0087] Note that, the first blowing direction control unit 22 may use an average value of the M difference values Φ_{E1} to Φ_{EM} instead of the RMS error Φ_{RMSE} . The second blowing direction control unit 32 may use an average value of the M difference values Θ_{E1} to Θ_{EM} instead of the RMS error Θ_{RMSE} . The blowing air volume control unit 42 may use an average value of the M difference values V_{E1} to V_{EM} instead of the RMS error V_{RMSE} .

[0088] Usually, the accuracy of the calibration control can be improved by increasing the value of M. However, as the value of M increases, the time required for the wind measurement processing and calibration control of each time increases. That is, responsiveness of the calibration control is reduced. Thus, the value of M may be freely settable by the user using the remote controller 3.

[0089] For example, the air conditioning device 200 may have an operation mode with $M = 1$ (hereinafter referred to as the "high-speed calibration mode"), an operation mode with $M = 3$ (hereinafter referred to as the "medium-speed calibration mode"), and an operation with $M = 10$ (hereinafter referred to as the "low-speed calibration mode"). Any operation mode may be freely selectable by the user using the remote controller 3, among the high-speed calibration mode, the medium-speed calibration mode, and the low-speed calibration mode.

[0090] Furthermore, in a case where the wind measurement lidar 11 includes a pulse modulation type lidar, when the wind measurement lidar 11 emits the laser beam in one direction D, the line-of-sight direction wind speed V_r at each of the M measurement target points P arranged along the emission direction D is measured at once. Thus, as illustrated in FIG. 10, M measurement target areas Al_1 to Al_M can be set at once. In the example illustrated in FIG. 10, $M = 5$.

[0091] In this case, the M first measured wind direction values Φ_{L1} to Φ_{LM} calculated in step ST11a may have a one-to-one correspondence with the M measurement target areas Al_1 to Al_M . The M second measured wind direction values Θ_{L1} to Θ_{LM} calculated in step ST21a may have a one-to-one correspondence with the M measurement target areas Al_1 to Al_M . The M measured wind speed values V_{L1} to V_{LM} calculated in step ST31a may have a one-to-one correspondence with the M measurement target areas Al_1 to Al_M .

[0092] However, the value of M in this case is a different value depending on a maximum measurable distance by the wind measurement lidar 11, and a distance resolution

by the wind measurement lidar 11. Furthermore, the value of M in this case is a different value depending on presence or absence of a hard target in the emission direction D, a distance between the wind measurement lidar 11 and the hard target when the hard target is present, and the like.

[0093] Next, other modifications of the air conditioning device 200 will be described.

[0094] First, a control method for the blowing air volume V' by the blowing air volume control unit 42 is not limited to the method of controlling the rotation speed of the rotor in the drive motor 43. For example, the indoor unit 1 may include a damper (not illustrated) for air volume adjustment. The blowing air volume control unit 42 may control the blowing air volume V' by controlling the damper, that is, by changing a duct resistance curve.

[0095] Furthermore, a measurement target by the wind measurement processing does not have to include the wind speed V (that is, may include only the wind directions Φ and Θ), and a calibration target by the calibration control does not have to include the blowing air volume V' (that is, may include only the blowing directions Φ' and Θ'). However, from a viewpoint of further improving the user comfort in the air conditioning target space S, it is more preferable to include the wind speed V in the measurement target and include the blowing air volume V' in the calibration target.

[0096] Furthermore, from a viewpoint of speeding up the calibration control, only the wind direction with respect to the horizontal direction may be a target of calibration. In this case, the value of N mentioned above may be 2. Furthermore, in this case, the term of $V_w \times \sin\theta$ in the expression (1) mentioned above is unnecessary.

[0097] Furthermore, the air conditioning device 200 is only required to be a device for air conditioning, and is not limited to the air-conditioner. For example, the air conditioning device 200 may include a fan, a blower, or an air duct device.

[0098] As described above, the air conditioning device 200 of the first embodiment includes the wind measurement processing unit 51 for calculating the wind directions Φ and Θ using the measured values by the wind measurement lidar 11, and the blowing control unit 52 for controlling the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L calculated by the wind measurement processing unit 51. As a result, the wind directions Φ and Θ in the air conditioning target space S can be measured by using the wind measurement lidar 11 integrated with the air conditioning device 200. Furthermore, the measured wind direction values Φ_L and Θ_L can be used for the control of the blowing directions Φ' and Θ' . As a result, the user comfort in the air conditioning target space S can be improved.

[0099] Furthermore, the wind measurement processing unit 51 calculates the wind directions Φ and Θ continuously in time, and the blowing control unit 52 controls the blowing directions Φ' and Θ' by feedback control for bringing the wind direction values Φ_L and Θ_L closer to

the target wind direction values Φ_A and Θ_A . As a result, calibration of the blowing directions Φ' and Θ' can be implemented by the feedback control.

[0100] Furthermore, the wind measurement processing unit 51 calculates the wind speed V using the measured value by the wind measurement lidar 11, and the blowing control unit 52 controls the blowing air volume V' using the wind speed value V_L calculated by the wind measurement processing unit 51. As a result, the wind speed V in the air conditioning target space S can be measured by using the wind measurement lidar 11 integrated with the air conditioning device 200. Furthermore, the measured wind speed value V_L can be used for the control of the blowing air volume V'. As a result, the user comfort in the air conditioning target space S can be further improved.

[0101] Furthermore, the wind measurement processing unit 51 calculates the wind directions Φ and Θ and the wind speed V continuously in time, and the blowing control unit 52 controls the blowing directions Φ' and Θ' by feedback control for bringing the wind direction values Φ_L and Θ_L closer to the target wind direction values Φ_A and Θ_A , and controls the blowing air volume V' by feedback control for bringing the wind speed value V_L closer to the target wind speed value V_A . As a result, calibration can be implemented of the blowing directions Φ' and Θ' and the blowing air volume V' by the feedback control.

[0102] Furthermore, the control method of the first embodiment is a control method for the air conditioning device 200, and the wind measurement processing unit 51 calculates the wind directions Φ and Θ by using the wind measurement lidar 11, and the blowing control unit 52 controls the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L calculated by the wind measurement processing unit 51. As a result, as described above, the user comfort in the air conditioning target space S can be further improved.

Second Embodiment.

[0103] FIG. 11 is a block diagram illustrating a main part of an air conditioning device according to a second embodiment. FIG. 12 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the second embodiment. An air conditioning device 200a of the second embodiment will be described with reference to FIGS. 11 and 12. In FIG. 11, blocks similar to the blocks illustrated in FIG. 1 are designated by the same reference numerals, and the description thereof will be omitted. In FIG. 12, blocks similar to the blocks illustrated in FIG. 2 are designated by the same reference numerals, and the description thereof will be omitted.

[0104] As described in the first embodiment, the wind measurement lidar 11 includes, for example, a pulse modulation type lidar, a CW type lidar, or a lidar of a type using intensity correlation. These lidars can of course be used for measurement of the line-of-sight direction wind

speed V_r (that is, measurement of the wind directions Φ and Θ and wind speed V), and can also be used for detection of an object such as a person (that is, a hard target) in the air conditioning target space S.

[0105] That is, the wind measurement lidar 11 emits a laser beam in any direction D, whereby a distance-intensity characteristic in the direction D is obtained. Furthermore, an amount of movement of the object in the direction D (more specifically, Doppler quantity corresponding to a moving velocity of the object in the direction D) is obtained. Thus, the wind measurement lidar 11 generates a so-called "intensity image" and "distance image" by performing scanning of the laser beam in the air conditioning target space S. Each pixel in the intensity image indicates an intensity value of a received signal obtained by emitting the laser beam in the direction D corresponding to the pixel. Each pixel in the distance image indicates a distance value obtained by emitting the laser beam in the direction D corresponding to the pixel. The wind measurement lidar 11 outputs intensity image information indicating the generated intensity image, distance image information indicating the generated distance image, and the like. Hereinafter, these images may be collectively referred to as the "lidar image".

[0106] A human detection processing unit 71 executes processing of detecting an object such as a person in the air conditioning target space S (hereinafter referred to as the "human detection processing") using output information by the wind measurement lidar 11. The human detection processing unit 71 outputs information indicating a result of the human detection processing (hereinafter referred to as the "detection result information"). Hereinafter, a specific example of the human detection processing will be described.

[0107] First, the human detection processing includes processing of determining presence or absence of a person in the air conditioning target space S (hereinafter referred to as the "human presence/absence determination processing"). That is, the human presence/absence determination processing determines whether it is a state in which there is a person in the air conditioning target space S (hereinafter referred to as the "present state") or it is a state in which there is no person in the air conditioning target space S (hereinafter referred to as the "absent state").

[0108] Specifically, for example, the human detection processing unit 71 executes threshold processing for the intensity image, and pattern matching processing for the intensity image or the distance image, thereby determining whether or not a pixel group corresponding to a person is included in the lidar image. When the pixel group corresponding to a person is included in the lidar image, the human detection processing unit 71 determines that the air conditioning target space S is in the present state. On the other hand, when the pixel group corresponding to a person is not included in the lidar image, the human detection processing unit 71 determines that the air conditioning target space S is in the absent state.

[0109] Secondly, the human detection processing may include processing of determining presence or absence of a moving object in the air conditioning target space S (hereinafter referred to as the "moving object presence/absence determination processing").

[0110] Specifically, for example, the human detection processing unit 71 compares an intensity value I of each pixel in the lidar image with a predetermined threshold value I_{th} . Furthermore, the human detection processing unit 71 compares the absolute value $|\rho|$ of Doppler quantity ρ of each pixel in the lidar image with a predetermined threshold value ρ_{th} . When the number of pixels satisfying the condition indicated in the following expression (5) and the condition indicated in the following expression (6) is greater than or equal to a predetermined number, the human detection processing unit 71 determines that a moving object is present in the air conditioning target space S.

$$I > I_{th} \quad (5)$$

$$|\rho| > \rho_{th} \quad (6)$$

[0111] Here, in a case where the air conditioning target space S is in the present state, the pixel group corresponding to the person is included in the lidar image. The determination using the expressions (5) and (6) for the pixel group corresponding to the person is also a determination of whether it is a state in which the person is moving or it is a state in which the person is not moving (hereinafter referred to as the "stationary state"). That is, the moving object presence/absence determination processing in the case where the air conditioning target space S is in the present state includes processing of determining whether or not a person in the air conditioning target space S is in the stationary state.

[0112] Each of the wind measurement processing unit 51 and the blowing control unit 52 acquires the detection result information output by the human detection processing unit 71. The wind measurement processing unit 51 determines whether or not to execute the wind measurement processing, by using the acquired detection result information. The blowing control unit 52 determines whether or not to execute the calibration control, by using the acquired detection result information.

[0113] Specifically, for example, in a case where the detection result information indicates that the air conditioning target space S is in the absent state, the wind measurement processing and the calibration control are executed. On the other hand, in a case where the detection result information indicates that the air conditioning target space S is in the present state, the wind measurement processing and the calibration control are skipped.

[0114] Alternatively, for example, in the case where the detection result information indicates that the air conditioning target space S is in the absent state, the wind

measurement processing and the calibration control are executed. Furthermore, in the case where the detection result information indicates that the air conditioning target space S is in the present state, when the detection result information indicates that a moving object is not present in the air conditioning target space S (that is, when the detection result information indicates that a person in the air conditioning target space S is in the stationary state), the wind measurement processing and the calibration control are executed. On the other hand, in the case where the detection result information indicates that the air conditioning target space S is in the present state, when the detection result information indicates that a moving object is present in the air conditioning target

space S, the wind measurement processing and the calibration control are skipped.

[0115] That is, in the air conditioning device 200a, the wind measurement processing and the calibration control are executed when these conditions are satisfied.

[0116] The wind measurement processing unit 51, the blowing control unit 52, and the human detection processing unit 71 constitute a main part of a control device 100a. The wind measurement lidar 11, the drive motor 23, the first wind direction plate 24, the drive motor 33, the second wind direction plate 34, the drive motor 43, the blowing fan 44, and the control device 100a constitute a main part of an indoor unit 1a. The indoor unit 1a and the outdoor unit 2 constitute a main part of the air conditioning device 200a.

[0117] Since a hardware configuration of the main part of the control device 100a is similar to that described with reference to FIG. 6 in the first embodiment, illustration and description will be omitted. That is, a function of each of the wind measurement processing unit 51, the blowing control unit 52, and the human detection processing unit 71 may be implemented by the processor 61 and the memory 62, or may be implemented by the dedicated processing circuit 63.

[0118] Next, the operation of the control device 100a will be described with reference to a flowchart of FIG. 13. In FIG. 13, steps similar to the steps illustrated in FIG. 7 are designated by the same reference numerals and the description thereof will be omitted.

[0119] As illustrated in FIG. 13A, first, the blowing control unit 52 executes initial setting of the blowing directions Φ' and Θ' and the blowing air volume V' (step ST1). Next, the blowing control unit 52 executes control to start blowing by the indoor unit 1a (step ST2).

[0120] After that, while the blowing by the indoor unit 1a is executed, processing illustrated in FIG. 13B or processing illustrated in FIG. 13C is repeatedly executed. That is, when the first calibration mode is set to be turned on by the remote controller 3 (step ST41 "YES"), the fol-

lowing processing is repeatedly executed.

[0121] In the example illustrated in FIG. 13B, in step ST42, the human detection processing unit 71 executes the human detection processing. More specifically, the human detection processing unit 71 executes the human presence/absence determination processing.

[0122] In a case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the absent state (step ST43 "YES"), the wind measurement processing (step ST3) and the calibration control (step ST4) are executed. Since the detailed processing contents of steps ST3 and ST4 are similar to those described with reference to FIG. 8 or 9 in the first embodiment, the repeated description thereof will be omitted.

[0123] On the other hand, in a case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the present state (step ST43 "NO"), the wind measurement processing (step ST3) and the calibration control (step ST4) are skipped.

[0124] In the example illustrated in FIG. 13C, in step ST42, the human detection processing unit 71 executes the human detection processing. More specifically, the human detection processing unit 71 executes the human presence/absence determination processing and the moving object presence/absence determination processing.

[0125] In a case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the absent state (step ST43 "YES"), the wind measurement processing (step ST3) and the calibration control (step ST4) are executed. Furthermore, in a case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the present state (step ST43 "NO"), when it is determined by the moving object presence/absence determination processing that a moving object is not present in the air conditioning target space S (step ST44 "NO"), that is, when it is determined that a person in the air conditioning target space S is in the stationary state, the wind measurement processing (step ST3) and the calibration control (step ST4) are executed. Since the detailed processing contents of steps ST3 and ST4 are similar to those described with reference to FIG. 8 or 10 in the first embodiment, the repeated description thereof will be omitted.

[0126] On the other hand, in a case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the present state (step ST43 "NO"), when it is determined by the moving object presence/absence determination processing that a moving object is present in the air conditioning target space S (step ST44 "YES"), the wind measurement processing (step ST3) and the calibration control (step ST4) are skipped.

[0127] Note that, when the first calibration mode is set to be turned on (step ST41 "YES"), the control device

100a may execute control of causing a display unit (not illustrated) to display an image indicating that the wind measurement processing and the calibration control in the first calibration mode will be started. The display unit 5 may be provided on the indoor unit 1a, or may be provided on the remote controller 3.

[0128] Next, effects of the air conditioning device 200a will be described.

[0129] If a user is in the air conditioning target space 10 S and the wind measurement processing is executed in a state in which the user is moving, the measurement accuracy of the wind direction Φ and Θ and the wind speed V may decrease due to an air flow generated depending on the user's movement. Furthermore, if the calibration control is executed in a state in which a user is in the air conditioning target space S, due to the change in the blowing directions Φ' and Θ' and the blowing air volume V' depending on the calibration values Φ_C , Θ_C , and V_C , the user may feel uncomfortable.

[0130] On the other hand, occurrence of these problems can be avoided by executing the wind measurement processing and the calibration control in a case where the air conditioning target space S is in the absent state. That is, it is possible to avoid a decrease in the measurement accuracy of the wind directions Φ and Θ and the wind speed V. Furthermore, it is possible to avoid that the user feels uncomfortable with changes in the blowing direction Φ' and Θ' and the blowing air volume V'.

[0131] Furthermore, in the case where the air conditioning target space S is in the present state, when a moving object is not present in the air conditioning target space S (that is, when a person in the air conditioning target space S is in the stationary state), the wind measurement processing and the calibration control are executed, whereby occurrence of the former problem can be avoided. That is, it is possible to avoid a decrease in the measurement accuracy of the wind directions Φ and Θ and the wind speed V.

[0132] Next, a modification of the air conditioning device 200a will be described.

[0133] The indoor unit 1a may include an infrared camera 12 in addition to the wind measurement lidar 11 (see FIG. 14 or 15). The infrared camera 12 generates a so-called "infrared image" by imaging an area in of the air conditioning target space S. The infrared camera 12 outputs infrared image information indicating the generated infrared image, and the like.

[0134] When the indoor unit 1a is provided with the infrared camera 12, the human detection processing unit 71 may use output information (infrared image information and the like) by the infrared camera 12 for the human detection processing, instead of the output information (intensity image information, distance image information, and the like) by the wind measurement lidar 11 (see FIG. 14). As a result, it is possible to eliminate the need for scanning of the laser beam for the human detection processing, so that a time required for the human detection processing can be shortened.

[0135] However, the infrared image in the infrared camera 12 corresponds to the intensity image in the wind measurement lidar 11. Thus, when the output information by the infrared camera 12 is used instead of the output information by the wind measurement lidar 11, the intensity value of each pixel can be acquired, but the distance value, Doppler quantity, and the like of each pixel cannot be acquired.

[0136] Thus, when the indoor unit 1a is provided with the infrared camera 12, it is more preferable that the human detection processing unit 71 uses the output information by the infrared camera 12 in addition to the output information by the wind measurement lidar 11 for the human detection processing (see FIG. 15). As a result, types of the information used for the human detection processing increase, so that the accuracy of the human detection processing can be improved.

[0137] In addition, the air conditioning device 200a can adopt various modifications similar to those described in the first embodiment.

[0138] As described above, the air conditioning device 200a of the second embodiment includes the human detection processing unit 71 for executing the human detection processing in the air conditioning target space S, and the blowing control unit 52 determines whether or not to execute the control of the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L , on the basis of the result of the human detection processing. The calibration accuracy of the blowing directions Φ' and Θ' can be improved by improving the measurement accuracy of the wind directions Φ and Θ .

[0139] Furthermore, in a case where the result of the human detection processing indicates that the air conditioning target space S is in the absent state, the blowing control unit 52 executes the control of the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L . As a result, the calibration accuracy of the blowing directions Φ' and Θ' can of course be improved, and it is possible to avoid that a user in the air conditioning target space S feels uncomfortable with the changes in the blowing directions Φ' and Θ' due to the calibration control.

[0140] Furthermore, in a case where the result of the human detection processing indicates that the air conditioning target space S is in the present state, when the result of the human detection processing indicates that a person in the air conditioning target space S is in the stationary state, the blowing control unit 52 executes the control of the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L . The calibration accuracy of the blowing directions Φ' and Θ' can be improved by improvement of the measurement accuracy of the wind directions Φ and Θ .

[0141] Furthermore, the air conditioning device 200a includes the human detection processing unit 71 for executing the human detection processing in the air conditioning target space S, and the blowing control unit 52 determines whether or not to execute the control of the blowing directions Φ' and Θ' using the wind direction val-

ues Φ_L and Θ_L and the control of the blowing air volume V' using the wind speed value V_L , on the basis of the result of the human detection processing. The calibration accuracy of the blowing directions Φ' and Θ' and the blowing air volume V' can be improved by improvement of the measurement accuracy of the wind directions Φ and Θ and the wind speed V .

[0142] Furthermore, in a case where the result of the human detection processing indicates that the air conditioning target space S is in the absent state, the blowing control unit 52 executes the control of the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L and the control of the blowing air volume V' using the wind speed value V_L . As a result, the calibration accuracy of the blowing directions Φ' and Θ' and the blowing air volume V' can of course be improved, and it is possible to avoid that a user in the air conditioning target space S feels uncomfortable with the changes in the blowing directions Φ' and Θ' and the blowing air volume V' due to the calibration control.

[0143] Furthermore, in a case where the result of the human detection processing indicates that the air conditioning target space S is in the present state, when the result of the human detection processing indicates that a person in the air conditioning target space S is in the stationary state, the blowing control unit 52 executes the control of the blowing directions Φ' and Θ' using the wind direction values Φ_L and Θ_L and the control of the blowing air volume V' using the wind speed value V_L . The calibration accuracy of the blowing directions Φ' and Θ' and the blowing air volume V' can be improved by improvement of the measurement accuracy of the wind directions Φ and Θ and the wind speed V .

[0144] Furthermore, the human detection processing unit 71 uses the wind measurement lidar 11 for the human detection processing. As a result, it is possible to eliminate the need for a dedicated detection device (for example, the infrared camera 12) for the human detection processing. Furthermore, by using the distance image information in addition to the intensity image information, the accuracy of the human detection processing can be improved.

Third Embodiment.

[0145] FIG. 16 is a block diagram illustrating a main part of an air conditioning device according to a third embodiment. FIG. 17 is a block diagram illustrating a main part of an indoor unit of the air conditioning device according to the third embodiment. An air conditioning device 200b of the third embodiment will be described with reference to FIGS. 16 and 17. In FIG. 16, blocks similar to the blocks illustrated in FIG. 1 are designated by the same reference numerals, and the description thereof will be omitted. In FIG. 17, blocks similar to the blocks illustrated in FIG. 2 are designated by the same reference numerals, and the description thereof will be omitted.

[0146] A human detection processing unit 81 executes

processing of detecting an object such as a person in the air conditioning target space S, that is, the human detection processing, by using the output information by the wind measurement lidar 11. The human detection processing unit 81 outputs information indicating the result of the human detection processing, that is, the detection result information.

[0147] Here, the human detection processing by the human detection processing unit 81 includes the processing of determining presence or absence of a person in the air conditioning target space S, that is, the human presence/absence determination processing. Furthermore, in the case where the air conditioning target space S is in the present state, the human detection processing by the human detection processing unit 81 includes processing of measuring a position of the person in the air conditioning target space S (hereinafter referred to as the "human position measurement processing").

[0148] The blowing control unit 52 has a function of implementing so-called "human-targeted" blowing, by using the detection result information output by the human detection processing unit 81.

[0149] That is, first, the first blowing direction control unit 22 sets the first blowing direction Φ' to the initial value. Furthermore, the second blowing direction control unit 32 sets the second blowing direction Θ' to the initial value. Furthermore, the blowing air volume control unit 42 sets the blowing air volume V' to the initial value.

[0150] After that, in the case where the air conditioning target space S is in the present state, the blowing control unit 52 sets an area corresponding to the position of the person in the air conditioning target space S as an area (hereinafter, referred to as the "blowing target area".) A3 to be a target of blowing by an indoor unit 1b. The blowing control unit 52 selects a wind direction and wind speed table with which blowing for the blowing target area A3 can be implemented from among the plurality of wind direction and wind speed tables stored in advance.

[0151] The first blowing direction control unit 22 resets the first blowing direction Φ' depending on the value of Φ' in the unit area A2 corresponding to the blowing target area A3 in the selected wind direction and wind speed table. The second blowing direction control unit 32 resets the second blowing direction Θ' depending on the value of Θ' in the unit area A2 corresponding to the blowing target area A3 in the selected wind direction and wind speed table. The blowing air volume control unit 42 resets the blowing air volume V' depending on the value of V' in the unit area A2 corresponding to the blowing target area A3 in the selected wind direction and wind speed table. As a result, the human-targeted blowing is implemented.

[0152] The wind measurement processing unit 51 sets the area corresponding to the position of the person in the air conditioning target space S as the measurement target area A1, by using the detection result information output by the human detection processing unit 81. That is, in the air conditioning device 200b, at least a part of

the blowing target area A3 is set as the measurement target area A1.

[0153] The wind measurement processing unit 51 executes the wind measurement processing in the set measurement target area A1. The blowing control unit 52 executes the calibration control in the set measurement target area A1 in a state in which the human-targeted blowing is implemented.

[0154] That is, in the air conditioning device 200b, the wind measurement processing and the calibration control are executed in the case where the air conditioning target space S is in the present state. Hereinafter, such an operation mode in which the wind measurement processing and the calibration control are executed is referred to as the "second calibration mode". Turning on and off of the second calibration mode is freely switchable by the remote controller 3.

[0155] The wind measurement processing unit 51, the blowing control unit 52, and the human detection processing unit 81 constitute a main part of a control device 100b. The wind measurement lidar 11, the drive motor 23, the first wind direction plate 24, the drive motor 33, the second wind direction plate 34, the drive motor 43, the blowing fan 44, and the control device 100b constitute a main part of the indoor unit 1b. The indoor unit 1b and the outdoor unit 2 constitute a main part of the air conditioning device 200b.

[0156] Since a hardware configuration of the main part of the control device 100b is similar to that described with reference to FIG. 6 in the first embodiment, illustration and description will be omitted. That is, a function of each of the wind measurement processing unit 51, the blowing control unit 52, and the human detection processing unit 81 may be implemented by the processor 61 and the memory 62, or may be implemented by the dedicated processing circuit 63.

[0157] Next, the operation of the control device 100b will be described with reference to a flowchart of FIG. 18. In FIG. 18, steps similar to the steps illustrated in FIG. 7 are designated by the same reference numerals and the description thereof will be omitted.

[0158] As illustrated in FIG. 18A, first, the blowing control unit 52 executes initial setting of the blowing directions Φ' and Θ' and the blowing air volume V' (step ST1). Next, the blowing control unit 52 executes control to start blowing by the indoor unit 1b (step ST2).

[0159] After that, while the blowing by the indoor unit 1b is executed, processing illustrated in FIG. 18B is repeatedly executed. That is, when the second calibration mode is set to be turned on by the remote controller 3 (step ST51 "YES"), the following processing is repeatedly executed.

[0160] As illustrated in FIG. 18B, in step ST52, the human detection processing unit 81 executes the human detection processing. More specifically, the human detection processing unit 81 executes the human presence/absence determination processing. Furthermore, in the case where it is determined by the human pres-

ence/absence determination processing that the air conditioning target space S is in the present state, the human detection processing unit 81 executes the human position measurement processing.

[0161] In the case where it is determined by the human presence/absence determination processing that the air conditioning target space S is in the present state (step ST53 "YES"), the blowing control unit 52 sets the blowing target area A3 by using the detection result information. More specifically, the blowing control unit 52 sets the area corresponding to the position of the person in the air conditioning target space S as the blowing target area A3 on the basis of a result of the human position measurement processing (step ST54).

[0162] Next, the blowing control unit 52 resets the blowing directions Φ' and Θ' and the blowing air volume V' so that the blowing for the blowing target area A3 set in step ST54 is implemented (step ST55). Due to the resetting while the blowing by the indoor unit 1b is executed, the human-targeted blowing is started.

[0163] Next, the wind measurement processing unit 51 sets the measurement target area A1 by using the detection result information. More specifically, the wind measurement processing unit 51 sets the area corresponding to the position of the person in the air conditioning target space S as the measurement target area A1 on the basis of the result of the human position measurement processing (step ST56).

[0164] Next, the wind measurement processing (step ST3) and the calibration control (step ST4) are executed for the measurement target area A1 set in step ST56. Since the detailed processing contents of steps ST3 and ST4 are similar to those described with reference to FIG. 8 or 10 in the first embodiment, the repeated description thereof will be omitted. However, the target values Φ_A , Θ_A , and V_A in the calibration control are set depending on the set values of Φ' , Θ' , and V' in step ST55 instead of the set values of Φ' , Θ' , and V' in step ST1.

[0165] The blowing target area A3 is set depending on the result of the human position measurement processing in this way, whereby the human-targeted blowing can be implemented. Furthermore, the measurement target area A1 is set depending on the result of the human position measurement processing, whereby the wind directions Φ and Θ and the wind speed V in an area corresponding to a position of the user in the air conditioning target space S can be brought into suitable states. As a result, the user comfort in the air conditioning target space S can be further improved.

[0166] Note that, the air conditioning device 200b may operate in the following operation mode after the second calibration mode is turned off (step ST51 "NO"). That is, it is an operation mode in which the blowing directions Φ' and Θ' and the blowing air volume V' are controlled using the wind direction and wind speed table stored in advance and the calibration value table at a time when the second calibration mode is turned off (that is, the latest calibration value table), without executing the wind

measurement processing, the calibration control, the human detection processing, and the human-targeted blowing in a state in which the power of the wind measurement lidar 11 is turned off. This operation mode may

5 be, for example, referred to by the name of the "energy saving mode". Turning on and off of the energy saving mode may be freely switchable by the remote controller 3.

[0167] Alternatively, the air conditioning device 200b may operate in the following operation mode after the second calibration mode is turned off (step ST51 "NO"). That is, it is an operation mode in which the wind measurement processing and the calibration control are not executed, but the human detection processing and the human-targeted blowing are executed, in a state in which

10 the power of the wind measurement lidar 11 is turned on. This operation mode may be, for example, referred to by the name of the "high-precision human-targeted mode". Turning on and off of the high-precision human-targeted mode may be freely switchable by the remote controller 3.

[0168] Furthermore, the human detection processing unit 81 may use the infrared camera 12 for the human detection processing instead of or in addition to the wind measurement lidar 11, similarly to the human detection processing unit 71.

[0169] In addition, the air conditioning device 200b can adopt various modifications similar to those described in the first embodiment.

[0170] As described above, the air conditioning device 200b of the third embodiment includes the human detection processing unit 81 for executing the human detection processing in the air conditioning target space S, and the wind measurement processing unit 51 sets the measurement target area A1 for the wind directions Φ and Θ in the air conditioning target space S on the basis of the result of the human detection processing. As a result, for example, it is possible to measure the wind directions Φ and Θ in the area corresponding to the position of the user in the air conditioning target space S.

[0171] Furthermore, the air conditioning device 200b includes the human detection processing unit 81 for executing the human detection processing in the air conditioning target space S, and the wind measurement processing unit 51 sets the measurement target area A1 for the wind directions Φ and Θ and the wind speed V in the air conditioning target space S on the basis of the result of the human detection processing. As a result, for example, it is possible to measure the wind directions Φ and Θ and the wind speed V in the area corresponding to the position of the user in the air conditioning target space S.

[0172] Furthermore, the wind measurement processing unit 51 sets the area corresponding to the position of the person in the air conditioning target space S as the measurement target area A1. As a result, an appropriate area can be set as the measurement target area A1 depending on the position of the user in the air conditioning target space S.

[0173] Furthermore, the human detection processing

unit 81 uses the wind measurement lidar 11 for the human detection processing. As a result, it is possible to eliminate the need for a dedicated detection device (for example, the infrared camera 12) for the human detection processing. Furthermore, by using the distance image information in addition to the intensity image information, the accuracy of the human detection processing can be improved.

[0174] Note that, in the invention of the present application, within the scope of the invention, free combination of embodiments, a modification of an any component of each embodiment, or omission of any component in each embodiment is possible.

INDUSTRIAL APPLICABILITY

[0175] The air conditioning device and control method of the present invention can be used, for example, in an air-conditioner for home use or for business use.

REFERENCE SIGNS LIST

[0176] 1, 1a, 1b: indoor unit, 2: outdoor unit, 3: remote controller (remote controller), 11: wind measurement lidar, 12: infrared camera, 21: first wind direction measurement processing unit, 22: first blowing direction control unit, 23: drive motor, 24: wind direction plate (first wind direction plate), 31: second wind direction measurement processing unit, 32: second blowing direction control unit, 33: drive motor, 34: wind direction plate (second wind direction plate), 41: wind speed measurement processing unit, 42: blowing air volume control unit, 43: drive motor, 44: blowing fan, 51: wind measurement processing unit, 52: blowing control unit, 61: processor, 62: memory, 63: processing circuit, 71: human detection processing unit, 81: human detection processing unit, 100, 100a, 100b: control device, 200, 200a, 200b: air conditioning device

Claims

1. An air conditioning device comprising:

a wind measurement processing unit calculating a wind direction value indicating a wind direction using a measured value by a lidar for measuring a wind; and
a blowing control unit executing control of a blowing direction using the wind direction value calculated by the wind measurement processing unit.

2. The air conditioning device according to claim 1, wherein

the wind measurement processing unit calculates the wind direction value continuously in

time, and

the blowing control unit controls the blowing direction by feedback control for bringing the wind direction value closer to a target wind direction value.

3. The air conditioning device according to claim 1, wherein

the wind measurement processing unit calculates a wind speed value indicating a wind speed using a measured value by the lidar, and the blowing control unit executes control of a blowing air volume using a wind speed value calculated by the wind measurement processing unit.

4. The air conditioning device according to claim 3, wherein

the wind measurement processing unit calculates the wind direction value and the wind speed value continuously in time, and the blowing control unit controls the blowing direction by feedback control for bringing the wind direction value closer to a target wind direction value, and executes the control of the blowing air volume by feedback control for bringing the wind speed value closer to a target wind speed value.

5. The air conditioning device according to claim 1, further comprising

a human detection processing unit executing human detection processing in an air conditioning target space, wherein the blowing control unit determines whether or not to execute the control of the blowing direction using the wind direction value, on a basis of a result of the human detection processing.

6. The air conditioning device according to claim 5, wherein in a case where the result of the human detection processing indicates that the air conditioning target space is in an absent state indicating that there is no person, the blowing control unit executes the control of the blowing direction using the wind direction value.

7. The air conditioning device according to claim 5 or 6, wherein in a case where the result of the human detection processing indicates that the air conditioning target space is in a present state indicating that there is a person, when the result of the human detection processing indicates that a person in the air conditioning target space is in a stationary state, the blowing control unit executes the control of the blow-

ing direction using the wind direction value.

8. The air conditioning device according to claim 3, further comprising

a human detection processing unit executing human detection processing in an air conditioning target space, wherein the blowing control unit determines whether or not to execute the control of the blowing direction using the wind direction value and the control of the blowing air volume using the wind speed value, on a basis of a result of the human detection processing.

9. The air conditioning device according to claim 8, wherein in a case where the result of the human detection processing indicates that the air conditioning target space is in an absent state indicating that there is no person, the blowing control unit executes the control of the blowing direction using the wind direction value and the control of the blowing air volume using the wind speed value.

10. The air conditioning device according to claim 8 or 9, wherein in a case where the result of the human detection processing indicates that the air conditioning target space is in a present state indicating that there is a person, when the result of the human detection processing indicates that a person in the air conditioning target space is in a stationary state, the blowing control unit executes the control of the blowing direction using the wind direction value and the control of the blowing air volume using the wind speed value.

11. The air conditioning device according to claim 1, further comprising

a human detection processing unit executing human detection processing in an air conditioning target space, wherein the wind measurement processing unit sets a measurement target area for the wind direction in the air conditioning target space on a basis of a result of the human detection processing.

12. The air conditioning device according to claim 3, further comprising

a human detection processing unit executing human detection processing in an air conditioning target space, wherein the wind measurement processing unit sets a measurement target area for the wind direction and the wind speed in the air conditioning target space on a basis of a result of the human detection processing.

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13. The air conditioning device according to claim 11 or 12, wherein the wind measurement processing unit sets an area corresponding to a position of a person in the air conditioning target space as the measurement target area.

14. The air conditioning device according to any one of claims 5 to 13, wherein the human detection processing unit uses the lidar for the human detection processing.

15. A control method for an air conditioning device, the control method comprising:

calculating, by a wind measurement processing unit, a wind direction value indicating a wind direction using a measured value by a lidar for measuring a wind; and executing, by a blowing control unit, control of a blowing direction using a wind direction value calculated by the wind measurement processing unit.

FIG. 1

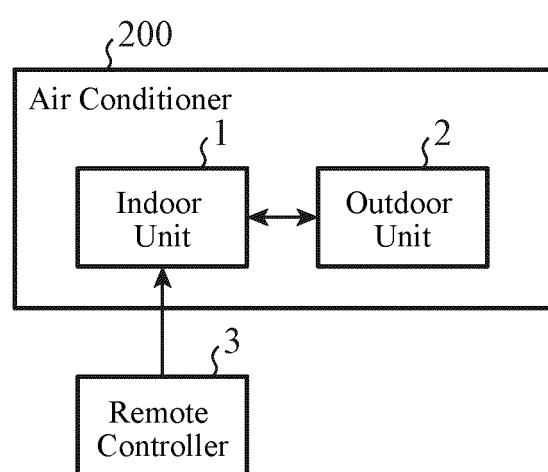


FIG. 2

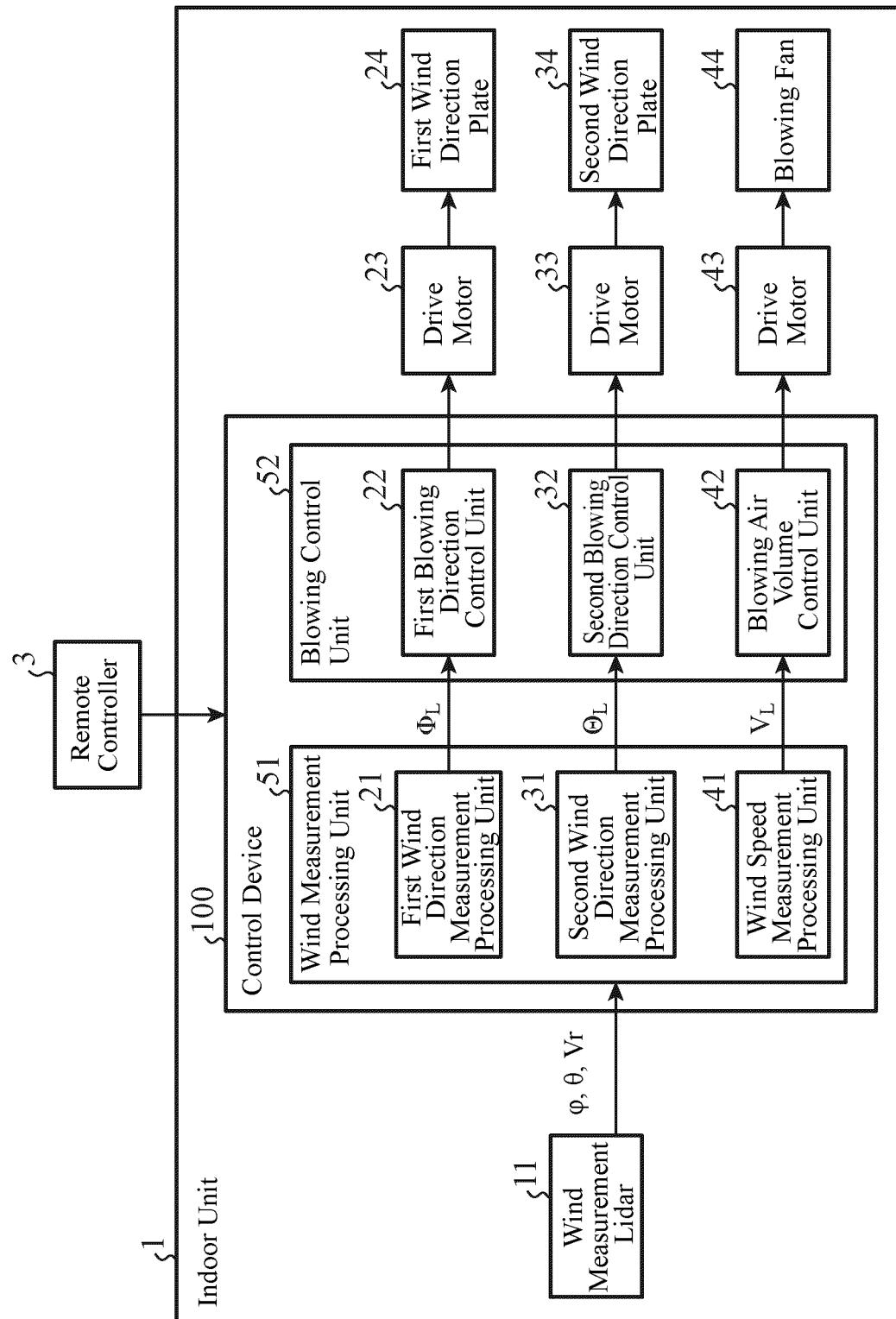


FIG. 3

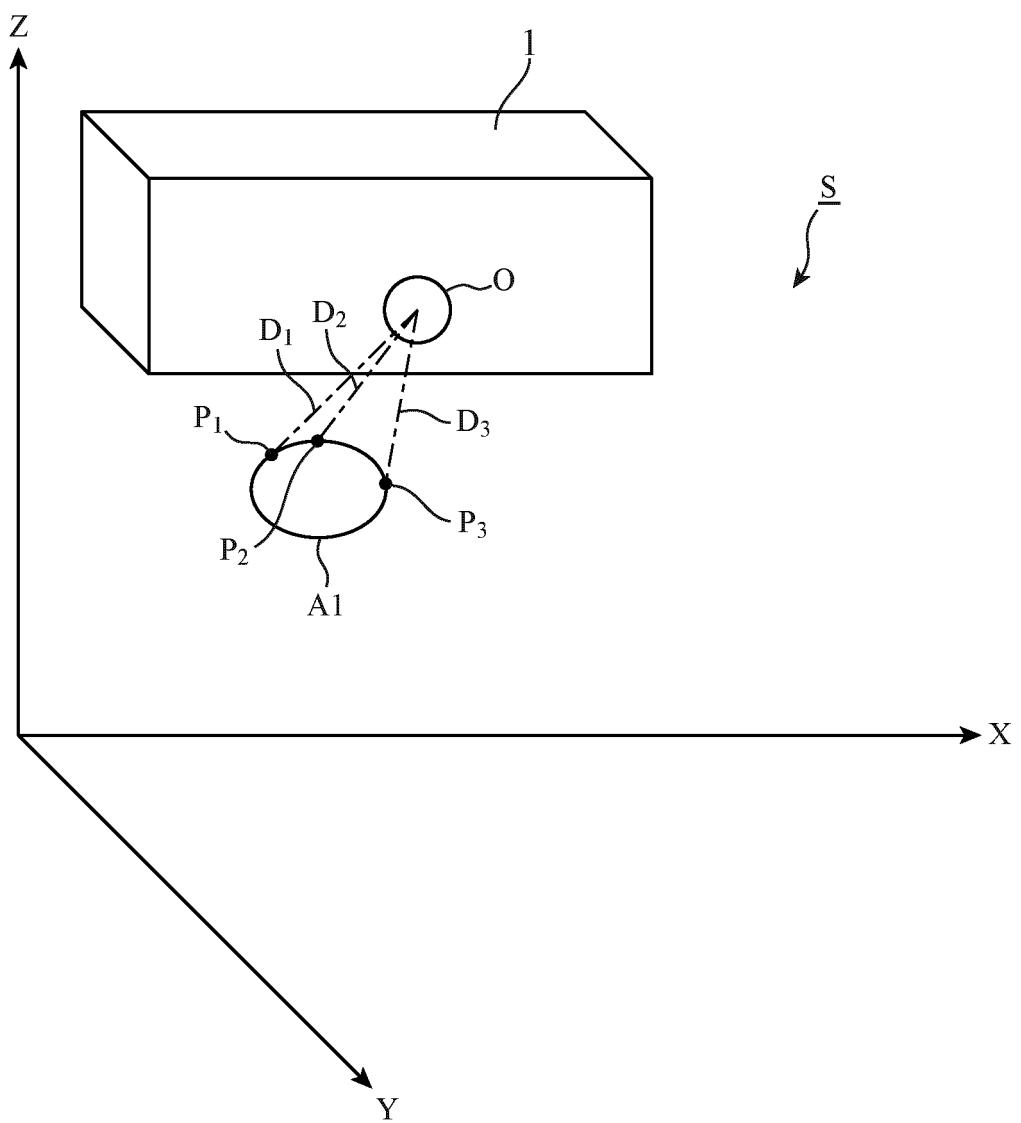


FIG. 4

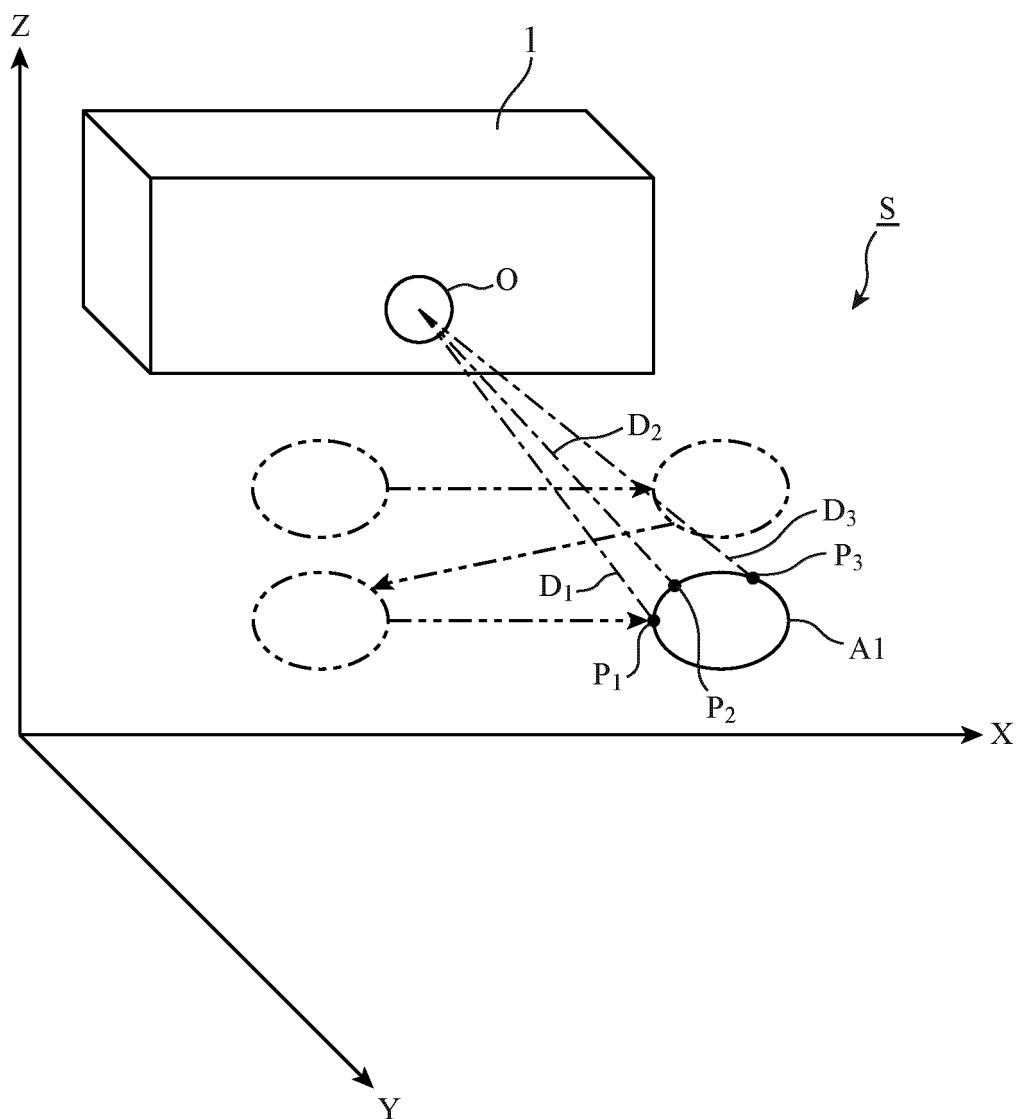


FIG. 5

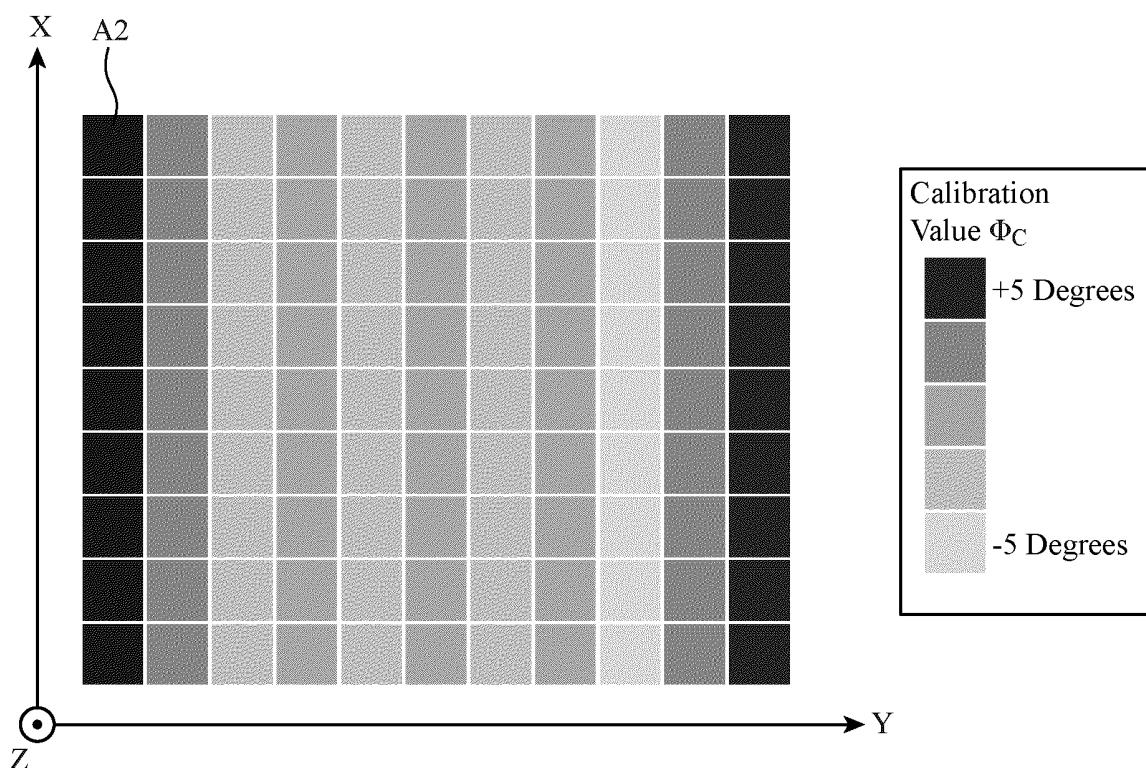


FIG. 6A

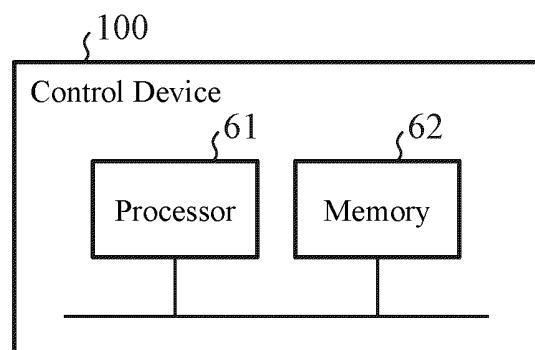


FIG. 6B

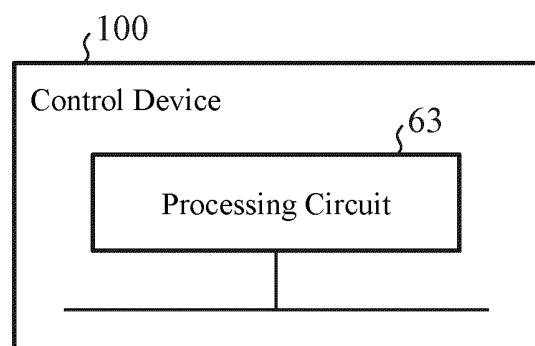


FIG. 7A

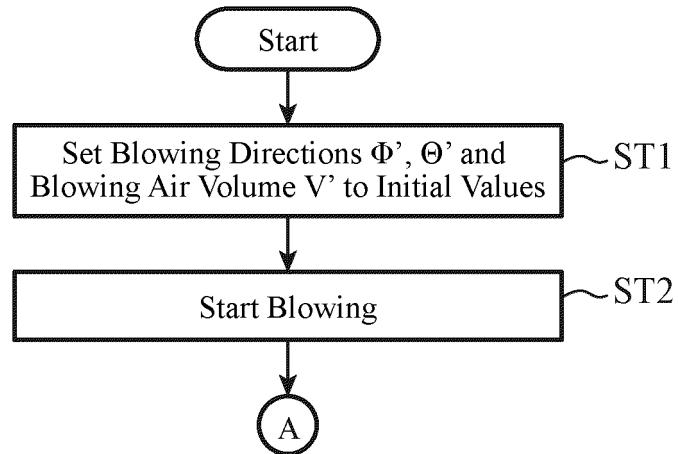


FIG. 7B

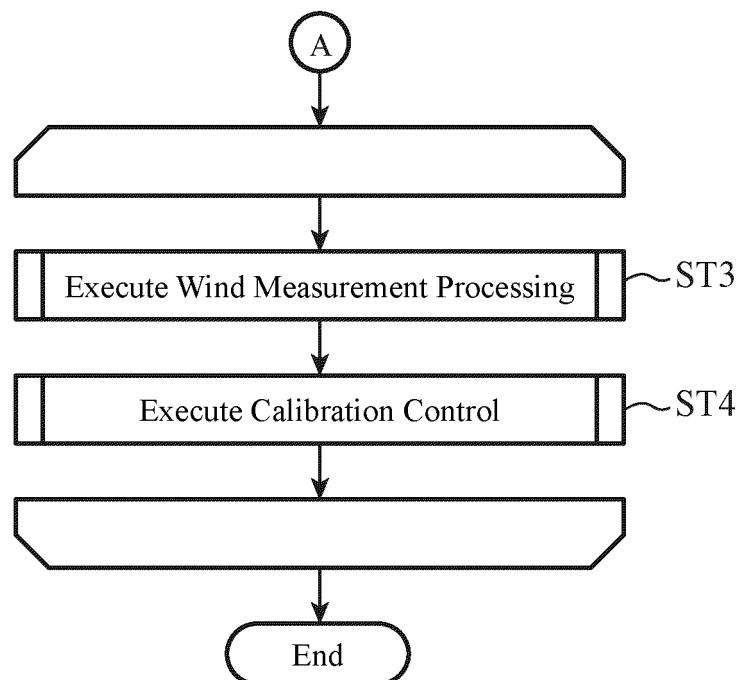


FIG. 8

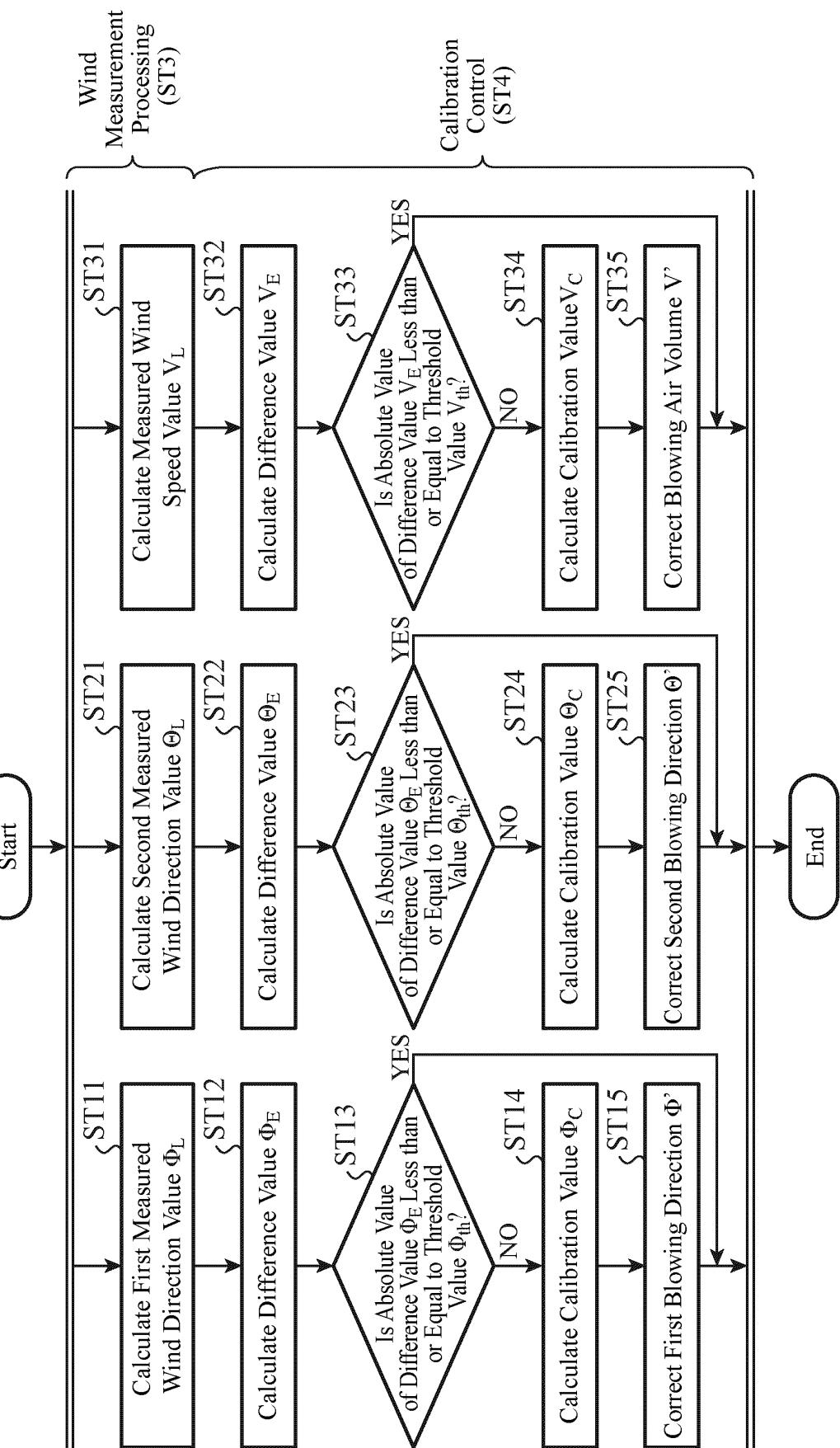


FIG. 9

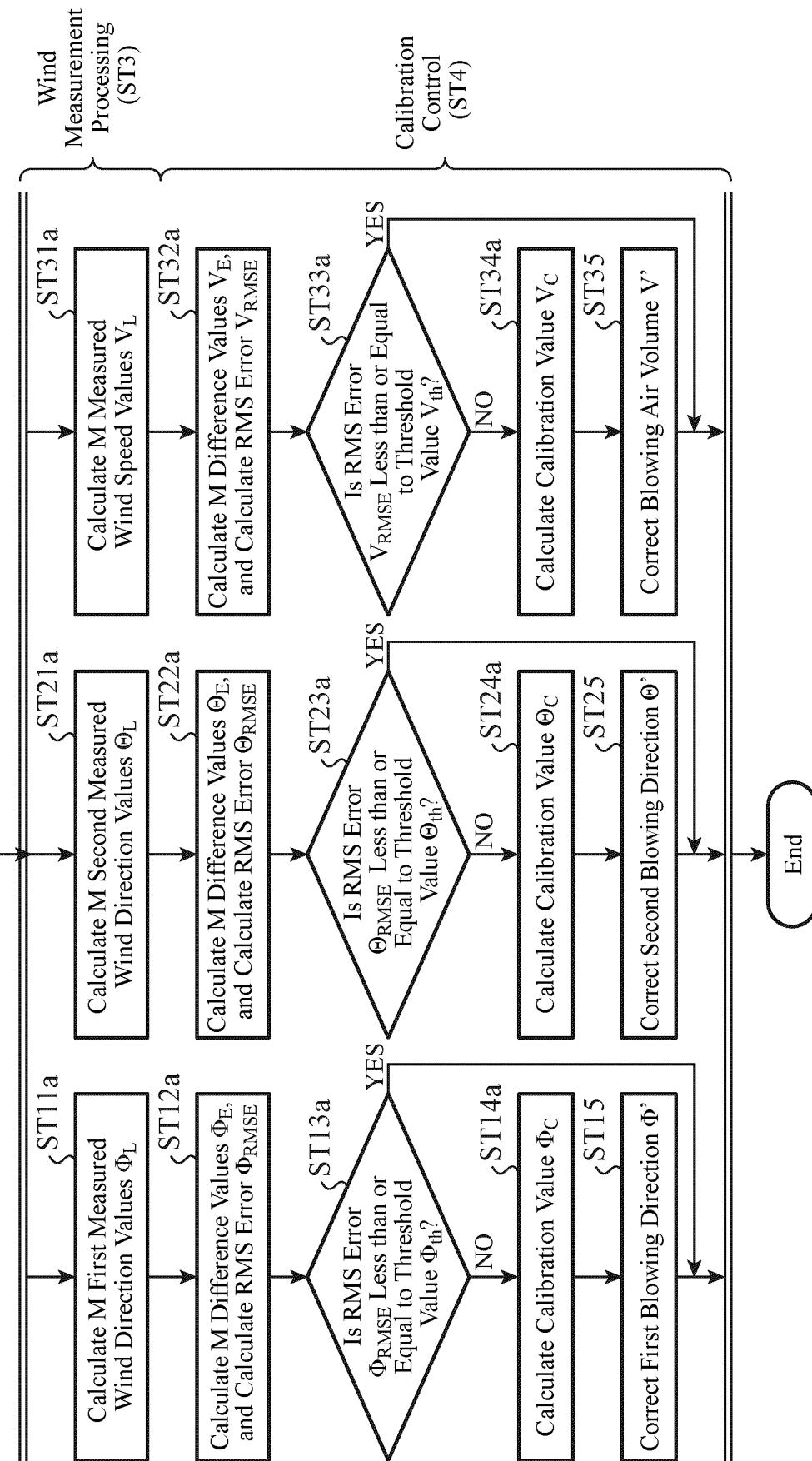


FIG. 10

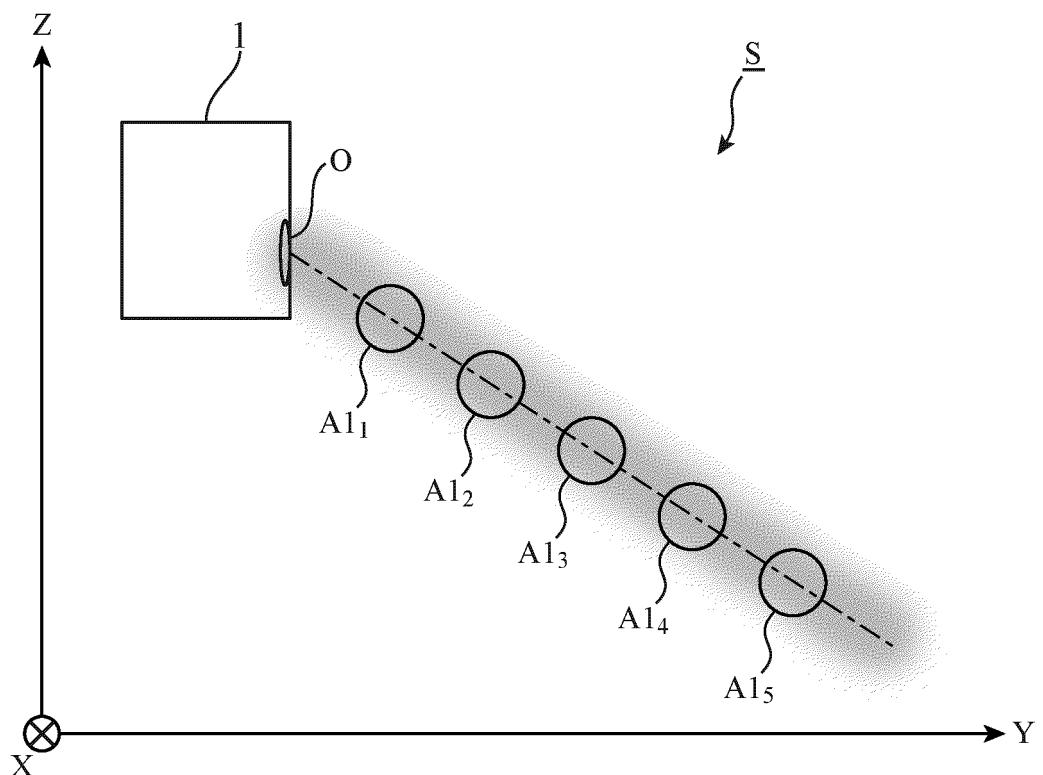


FIG. 11

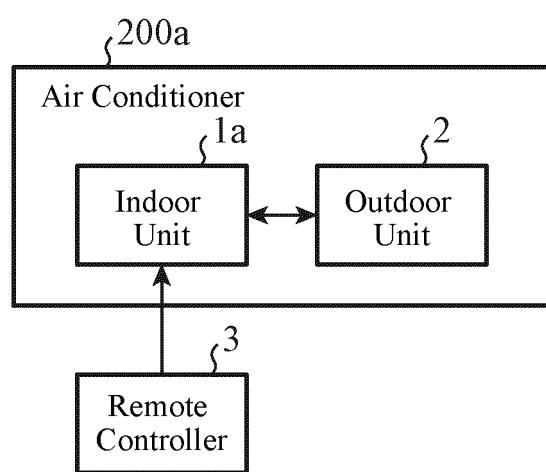


FIG. 12

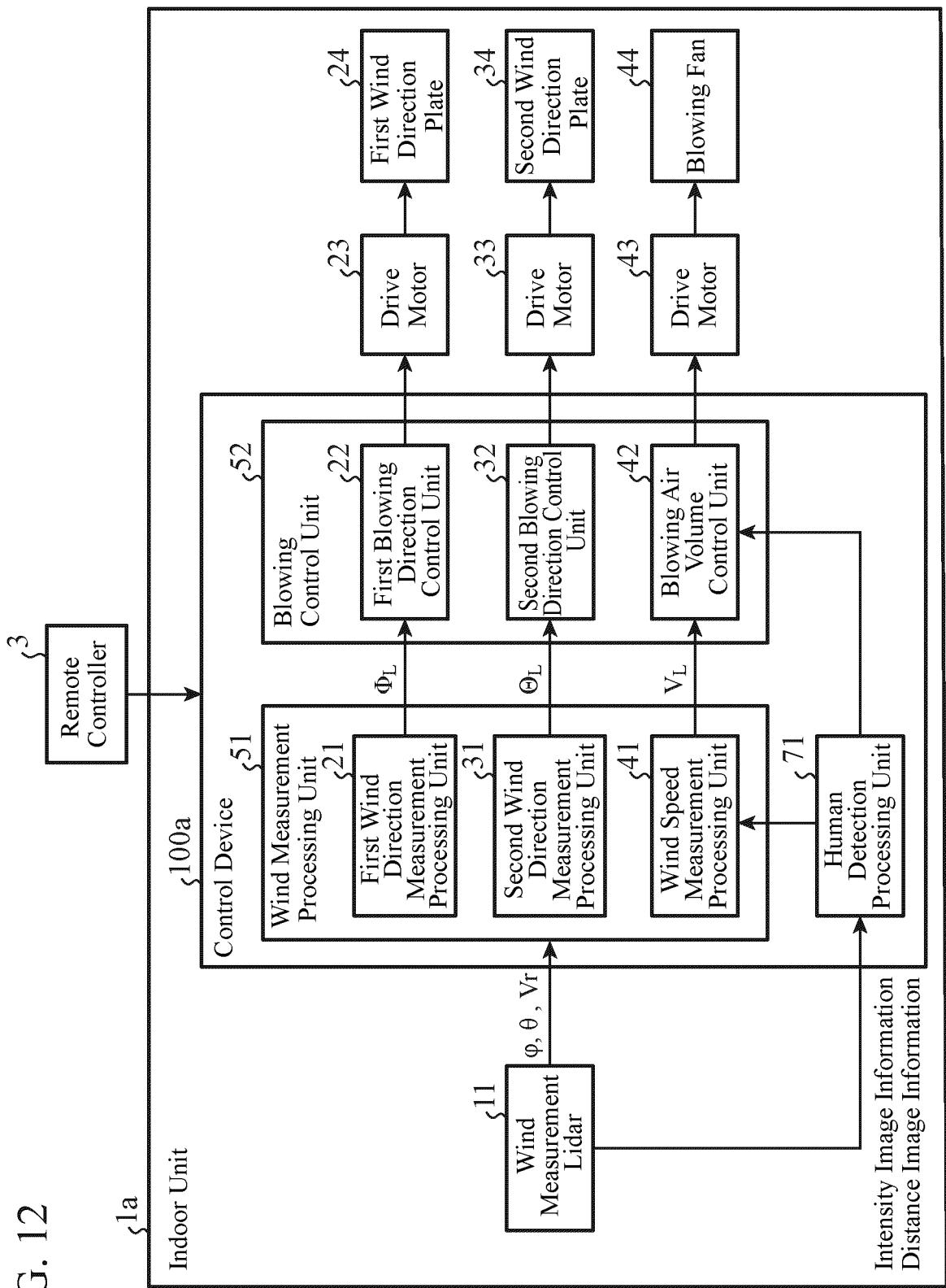


FIG. 13A

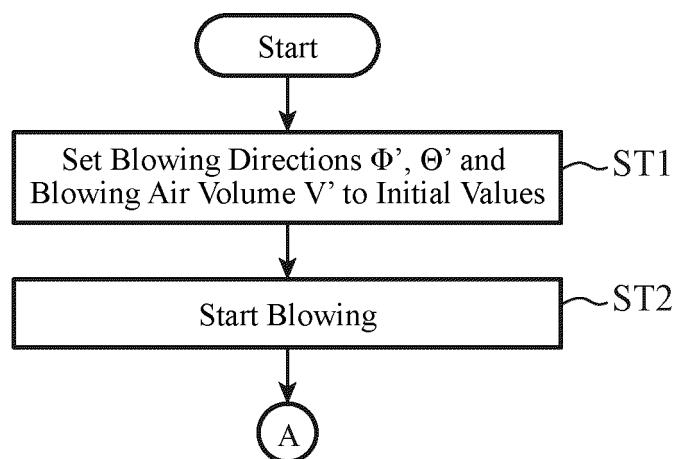


FIG. 13B

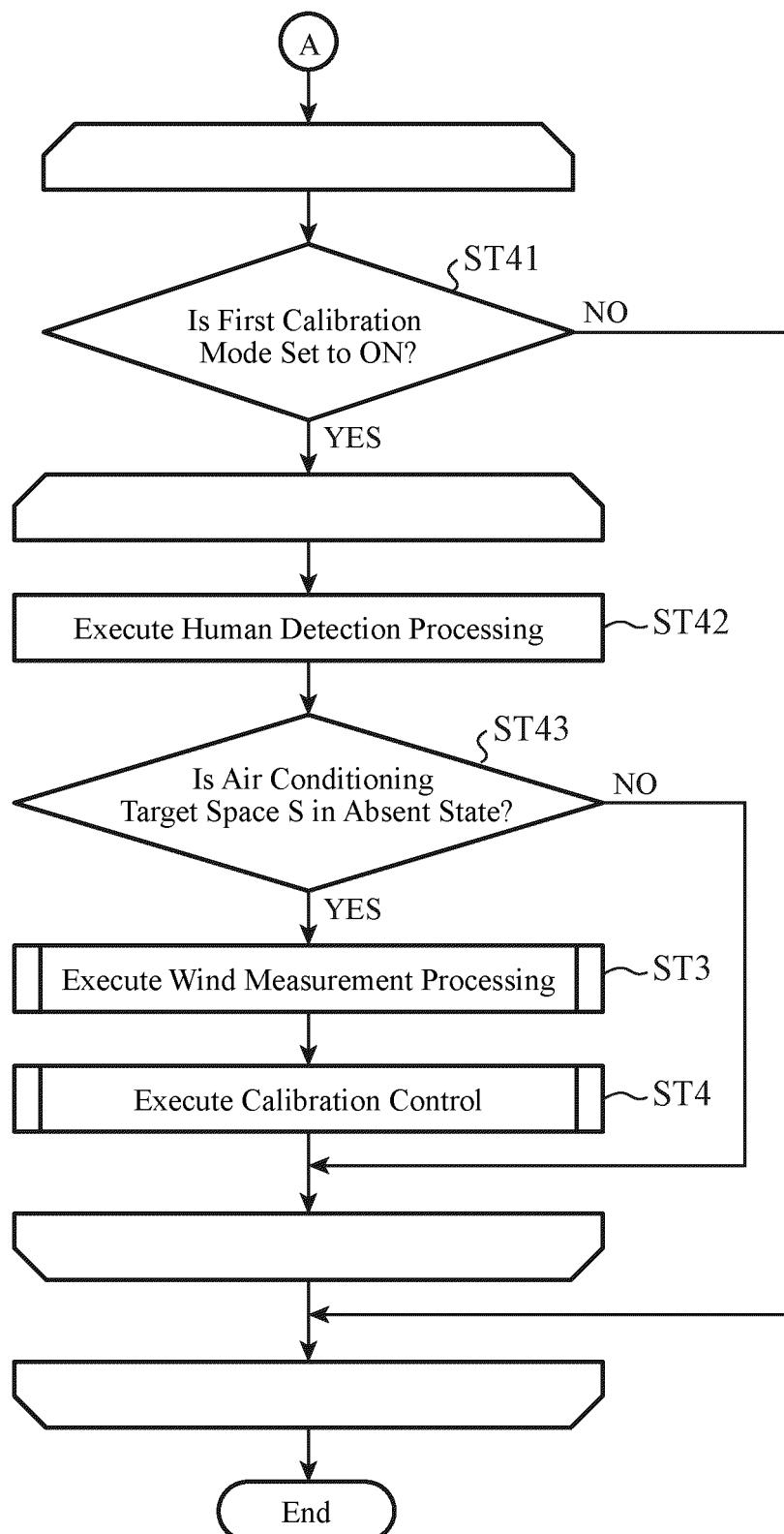


FIG. 13C

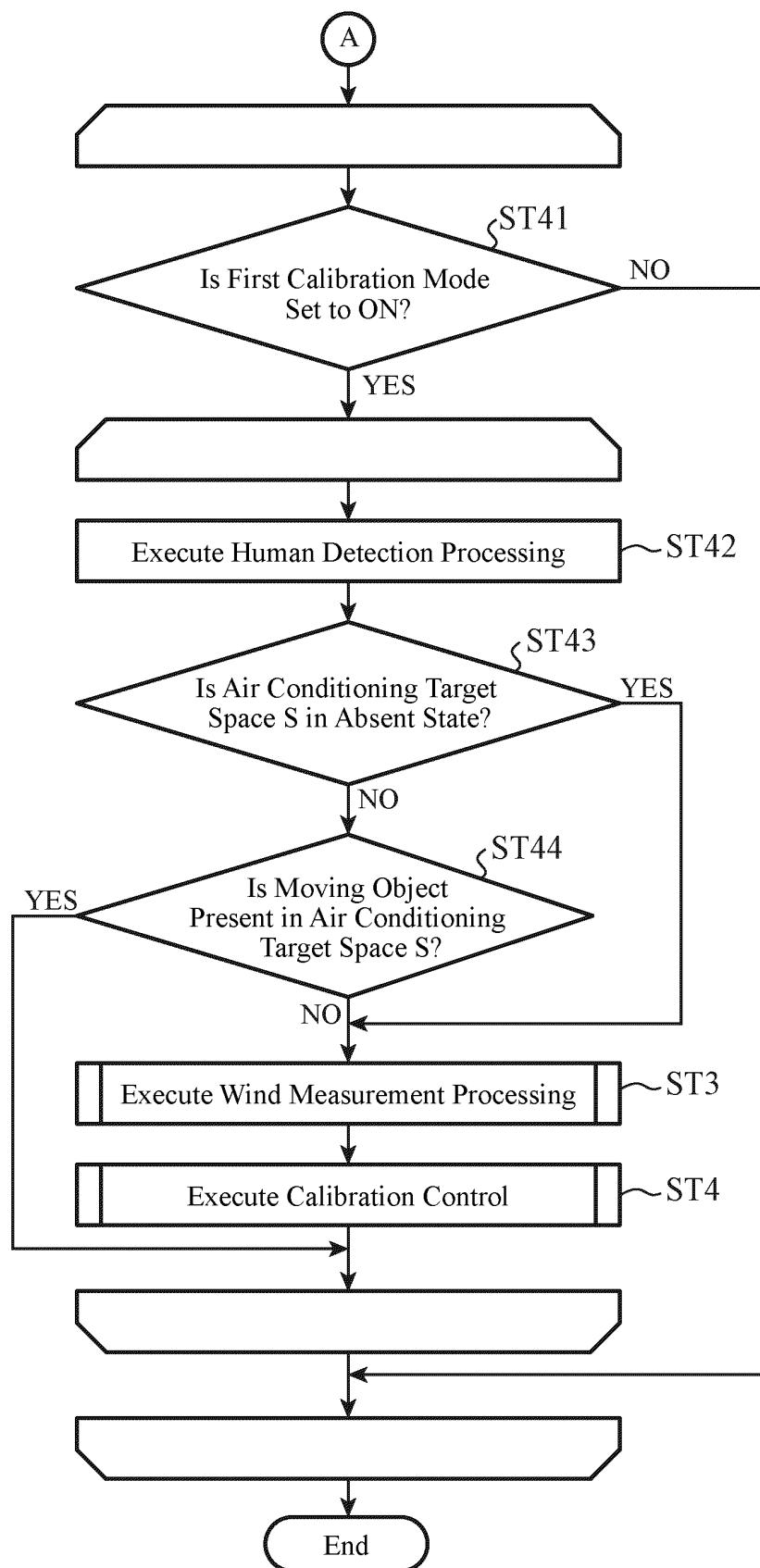


FIG. 14

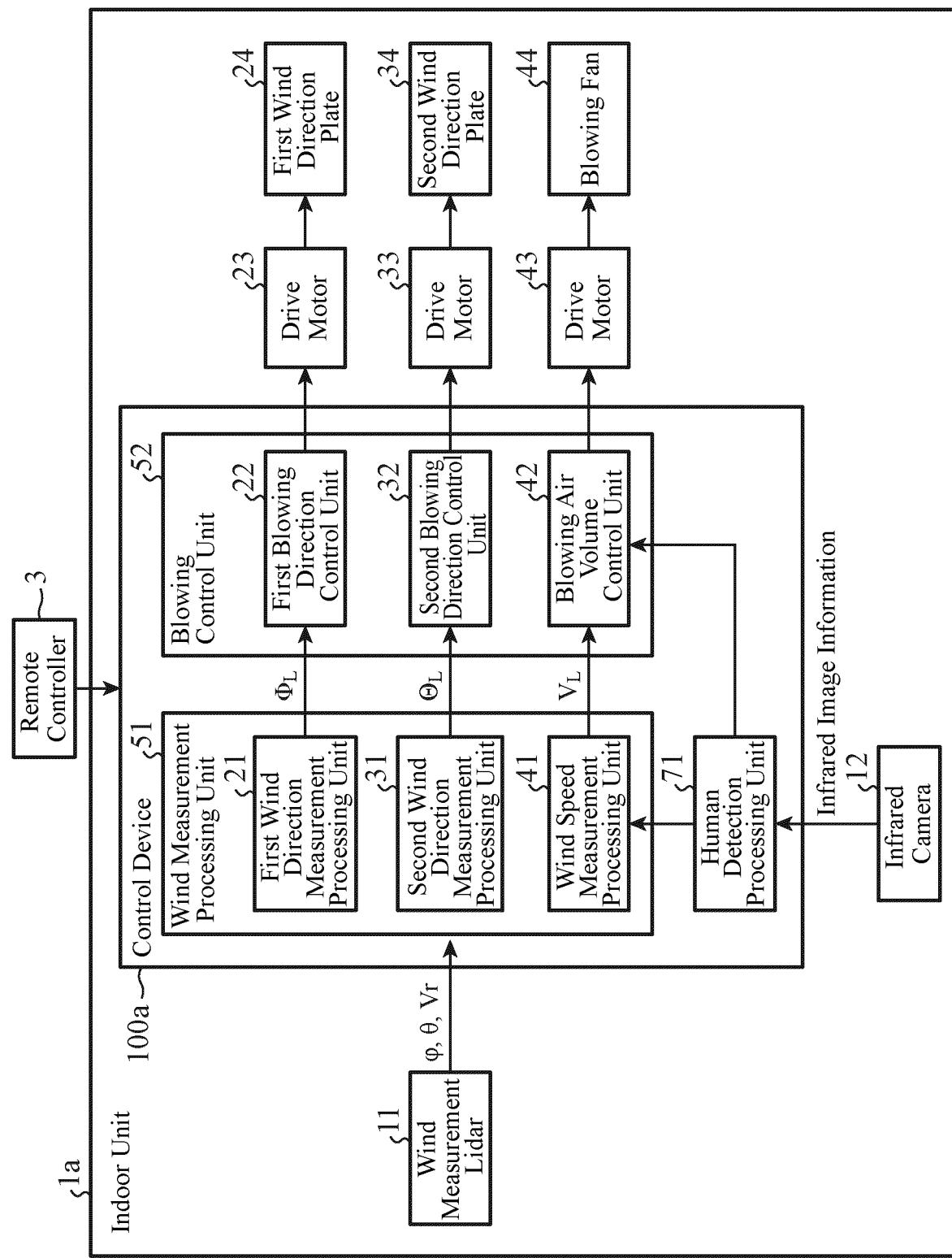


FIG. 15

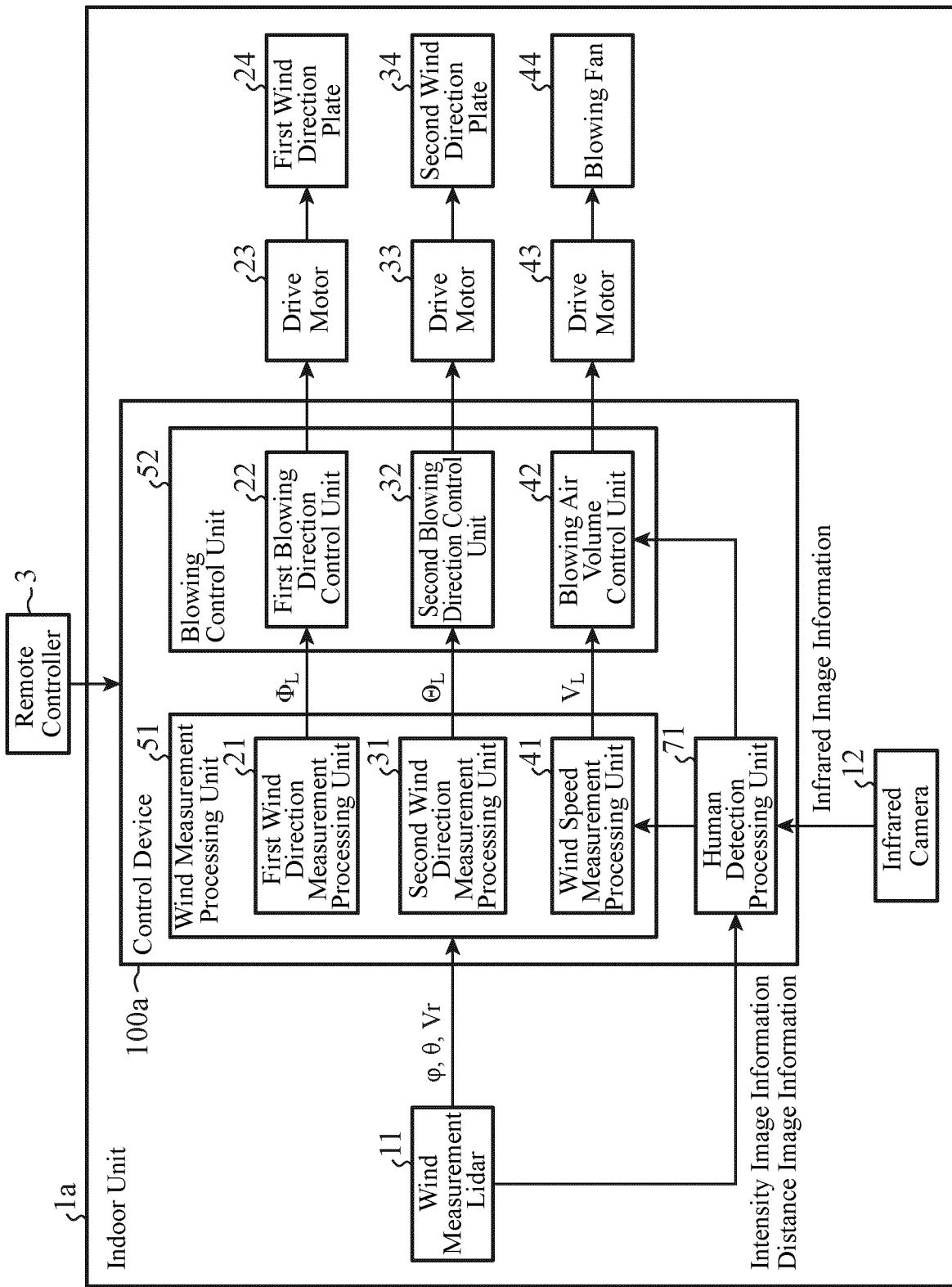


FIG. 16

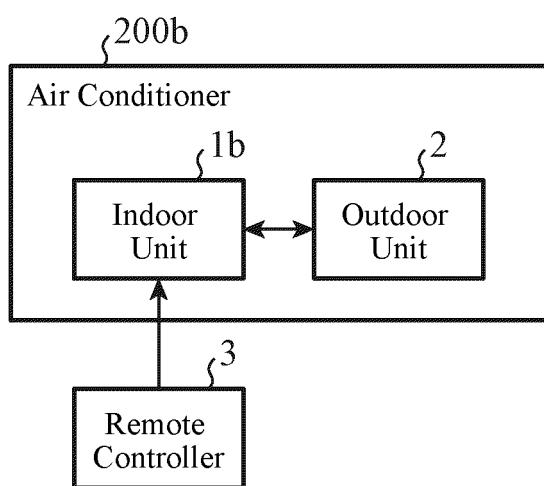


FIG. 17

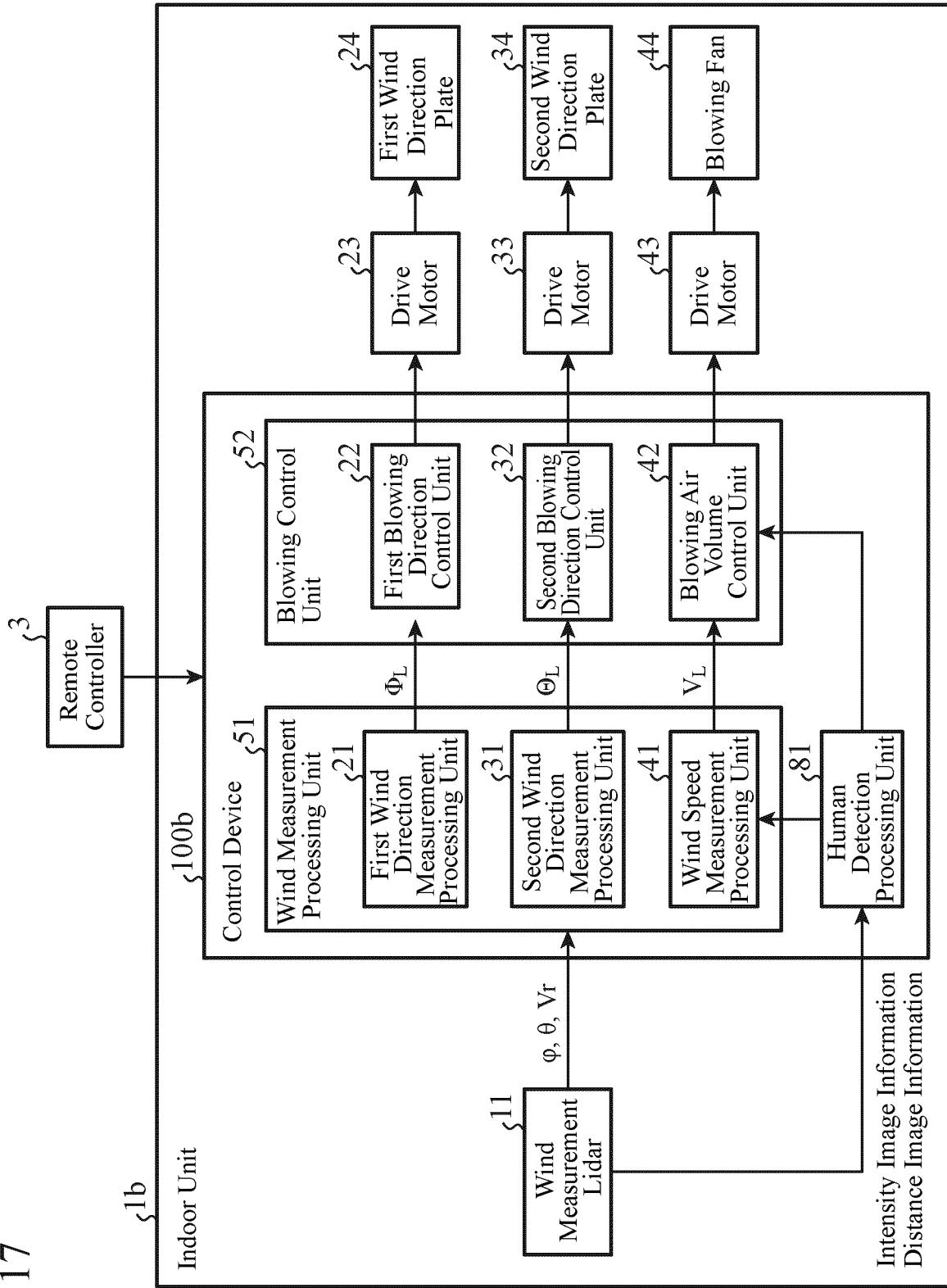


FIG. 18A

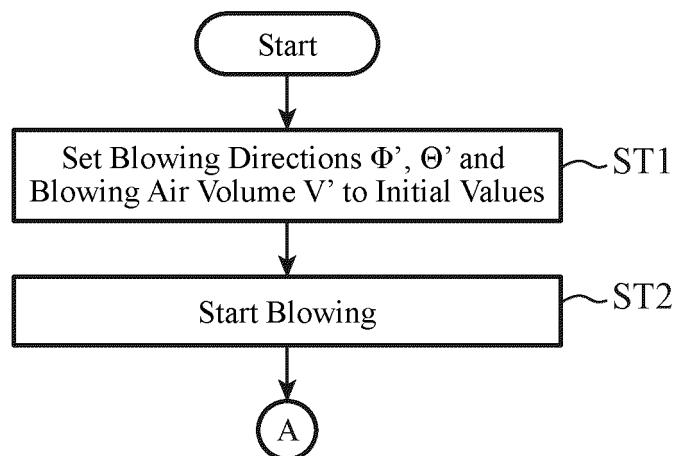
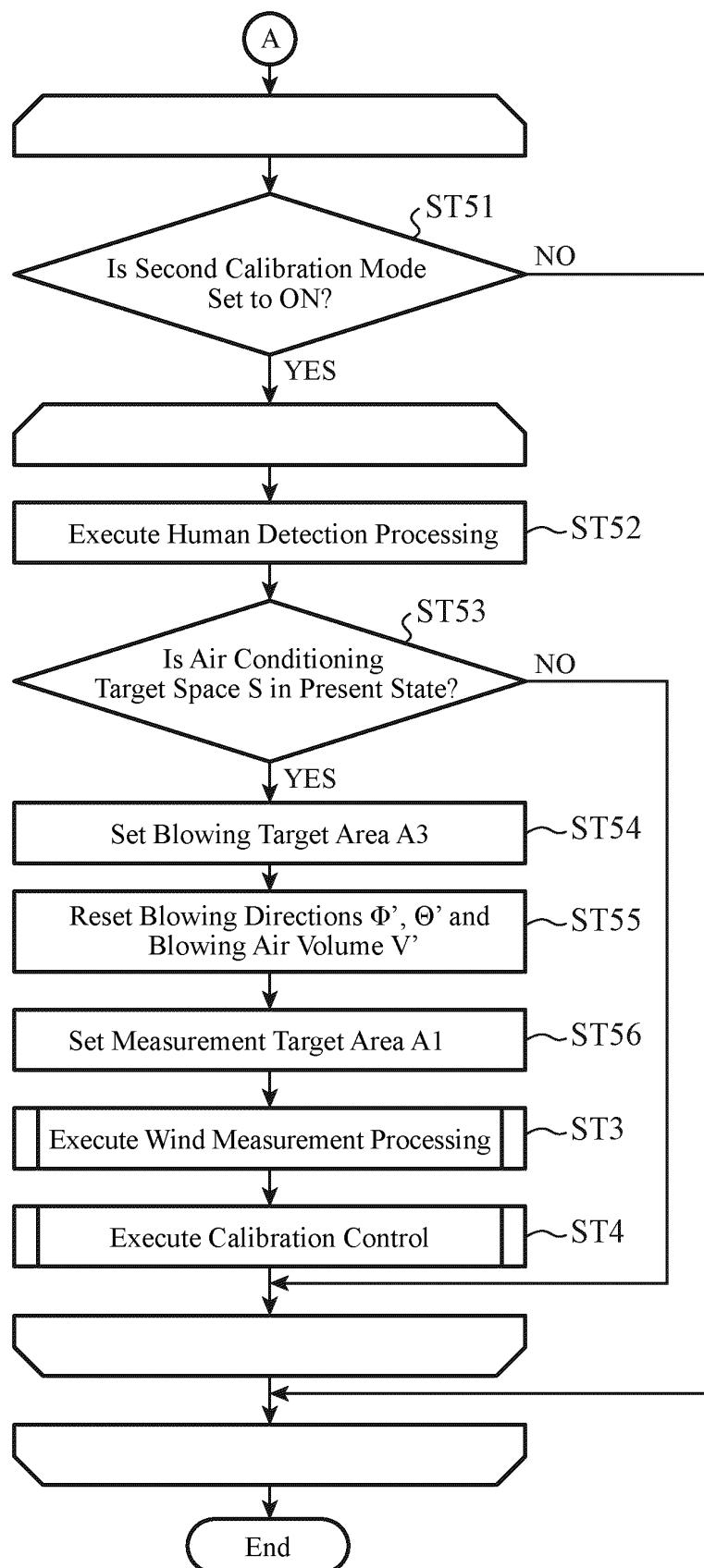


FIG. 18B



INTERNATIONAL SEARCH REPORT		International application No. PCT/JP2018/045494																		
5	A. CLASSIFICATION OF SUBJECT MATTER Int. Cl. F24F11/79(2018.01)i, F24F110/30(2018.01)n, F24F120/10(2018.01)n																			
10	According to International Patent Classification (IPC) or to both national classification and IPC																			
15	B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) Int. Cl. F24F11/00-11/89																			
20	Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Published examined utility model applications of Japan 1922-1996 Published unexamined utility model applications of Japan 1971-2018 Registered utility model specifications of Japan 1996-2018 Published registered utility model applications of Japan 1994-2018																			
25	Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)																			
30	C. DOCUMENTS CONSIDERED TO BE RELEVANT																			
35	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left; padding-right: 10px;">Category*</th> <th style="text-align: left; padding-right: 10px;">Citation of document, with indication, where appropriate, of the relevant passages</th> <th style="text-align: left;">Relevant to claim No.</th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">A</td> <td>JP 2017-180941 A (FUJITSU GENERAL LTD.) 05 October 2017, entire text, all drawings</td> <td style="text-align: center;">1-15</td> </tr> <tr> <td style="text-align: center;">A</td> <td>JP 2012-63077 A (PANASONIC CORP.) 29 March 2012, entire text, all drawings</td> <td style="text-align: center;">1-15</td> </tr> <tr> <td style="text-align: center;">A</td> <td>US 2017/0097169 A1 (PLUG AND PLAY ROBOTICS, LLC) 06 April 2017, paragraph [0047]</td> <td style="text-align: center;">1-15</td> </tr> <tr> <td style="text-align: center;">A</td> <td>JP 2012-63055 A (TAISEI CORP.) 29 March 2012, entire text, all drawings</td> <td style="text-align: center;">1-15</td> </tr> <tr> <td style="text-align: center;">A</td> <td>JP 2012-32038 A (FUJITSU GENERAL LTD.) 16 February 2012, entire text, all drawings</td> <td style="text-align: center;">1-15</td> </tr> </tbody> </table>		Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.	A	JP 2017-180941 A (FUJITSU GENERAL LTD.) 05 October 2017, entire text, all drawings	1-15	A	JP 2012-63077 A (PANASONIC CORP.) 29 March 2012, entire text, all drawings	1-15	A	US 2017/0097169 A1 (PLUG AND PLAY ROBOTICS, LLC) 06 April 2017, paragraph [0047]	1-15	A	JP 2012-63055 A (TAISEI CORP.) 29 March 2012, entire text, all drawings	1-15	A	JP 2012-32038 A (FUJITSU GENERAL LTD.) 16 February 2012, entire text, all drawings	1-15
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40	<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.																			
45	<p>* Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p>																			
50	Date of the actual completion of the international search 28.12.2018	Date of mailing of the international search report 15.01.2019																		
55	Name and mailing address of the ISA/ Japan Patent Office 3-4-3, Kasumigaseki, Chiyoda-ku, Tokyo 100-8915, Japan	Authorized officer Telephone No.																		

INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP2018/045494

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 2017/149657 A1 (MITSUBISHI ELECTRIC CORP.) 08 September 2017, entire text, all drawings	1-15
A	CN 105890740 A (FOSHAN UNIVERSITY) 24 August 2016, paragraph [0016]	1-15

INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.
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Patent Documents referred to in the Report	Publication Date	Patent Family	Publication Date
JP 2017-180941 A	2017.10.05	Family: none	
JP 2012-63077 A	2012.03.29	CN 102434938 A	
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JP 2012-63055 A	2012.03.29	Family: none	
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REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- JP 2017180940 A [0004]