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**(54) HIGH-PLASTICITY THERMOFORMED STEEL HAVING OXIDATION RESISTANCE FOR  
AUTOMOBILE, AND THERMOFORMING PROCESS**

(57) Provided are a high-plasticity hot-forming steel with oxidation resistance for automobiles and a hot-forming process thereof, and the hot-forming steel has chemical compositions in mass percentages as follows: C: 0.18%-0.28%, Si: <0.20%, Mn: 1.20%-2.0%, P: 0.030%-0.080%, S≤0.004%, Als: 0.02%-0.06%, Nb: 0.02%-0.06%, Ti: 0.025%-0.045%, V: 0.05%-0.15%, Cr:

0.5%-2.50%, Mo: 0.10%-0.30%, B: 0.0015%-0.0035%, N≤0.005%, the balance Fe and inevitable impurities. The hot-forming steel provided in the present invention has high oxidation resistance, high plasticity. The steel does not need atmosphere protection during hot forming, and does not need shot blasting treatment after hot forming.

**Description****TECHNICAL FIELD**

5 [0001] The present invention relates to the technical field of automobile steel, in particular to a high-plasticity hot-forming steel with oxidation resistance for automobiles and a hot-forming process thereof.

**BACKGROUND ART**

10 [0002] In recent years, new materials for car body have been continuously developed and applied to car bodies. However, ultra-high strength steel plates for cold stamping at strength levels above 1000 MPa are often used for manufacturing components with simple shapes due to the constraints of easy cracking and large springback. However, the hot-forming steel is formed in an austenite zone by using hot-forming process, and has small springback, which can meet the requirements of assembly accuracy. Through pressure-holding and quenching, the ultra-high strength components of 1500 MPa level and above can be obtained, which effectively simplifies the design of body structure and parts, and greatly reduces the weight of the vehicle.

15 [0003] At present, hot-forming steels on the market can be classified as coated hot-forming steels and uncoated hot-forming steels according to their surface conditions. The uncoated steel is easy to form scale on its surface and suffers from decarburization when being heated in a heating furnace, which affects the performance of the steel; therefore, it is necessary to use protective atmosphere during heating of the hot-forming steel, and to make the shot peening treatment after hot forming, which increases the cost and working procedures. While the coated steel has an aluminum-silicon coating or zinc-based coating on the surface of the steel plate, which can effectively prevent the steel from surface decarburization and oxidation during heating, and the steel after hot forming can be exempted from the shot peening process, but the cost of the coated hot-forming steel is higher than the uncoated steel. At present, the strengthen level used for mass production and use of the hot-forming steel in the prior art is 1500 MPa; however, the elongation of the hot-forming steel after hot forming is only about 6-9%, which cannot meet the development requirements of the automotive field, and no better technology is available to keep a lower cost of the hot-forming steel, to solve the problem of surface oxidation and decarburization of the steel after hot forming, and to avoid the shot peening process, moreover, the hot-forming steel also has higher plasticity after hot forming.

20 [0004] The patent with the Publication No. being CN107354385B proposes a method for preparing an ultra-high strength hot-forming steel for automobiles. Chemical compositions of the steel include C: 0.5-0.6%, Mn: 0.5%-2.0%, Si: 1.5%-2.5%, Cr: 1.0%-3.0%, Al: 1.0%-2.0%, Nb: 0.01%-0.03%, and B: 0.001%-0.005%. The strength of the steel plate after hot forming reaches 1500-2000MPa, and the elongation is 10%-20%. The steel plate proposed in the patent has good strength-plasticity compatibility, but Cr and Al elements are higher in its compositions, which increases the cost and smelting difficulty. At the same time, the production process is complex, the existing tooling and equipment do not meet the production requirements, and the production also requires atmosphere protection and shot peening.

25 [0005] The patent with Publication No. being CN103255340B proposes a hot-forming steel plate with high strength and toughness for automobiles and a preparation method thereof. Chemical compositions of the steel sheet include C: 0.1-0.5%, Si: 0.5-1.5%, Mn: 1.2-2.4%, Ti: 0.01-0.05%, B: 0.001-0.005%, S:  $\geq 0.01\%$ , and P:  $\geq 0.01\%$ . After hot forming, the tensile strength of the steel plate reaches 1600MPa and the elongation reaches 16%, proving good comprehensive performance and relatively low alloy cost. However, the steel plate needs to be deformed during heating process, and then quenched twice to obtain the final microstructure and mechanical properties, which involves a complicated hot-forming process and is unable to be implemented through the existing equipment, moreover, it also needs gas protection during heating, and needs shot peening after hot forming.

30 [0006] To sum up, the development of high-plasticity hot-forming process with good oxidation resistance and the hot-forming technology for automobiles has good application prospects.

**SUMMARY**

35 [0007] According to the above technical problems, the present invention provides a high-plasticity hot-forming steel with oxidation resistance for automobiles and a hot-forming process thereof.

[0008] A technical solution adopted by the present invention is as follows:

40 A high-plasticity hot-forming steel with oxidation resistance for automobiles, where the hot-forming steel has chemical compositions in mass percentages as follows:

45 C: 0.18%-0.28%, Si:  $\geq 0.20\%$ , Mn: 1.20%-2.0%, P: 0.030%-0.080%, S:  $\geq 0.004\%$ , Al: 0.02%-0.06%, Nb: 0.02%-0.06%, Ti: 0.025%-0.045%, V: 0.05%-0.15%, Cr: 0.5%-2.50%, Mo: 0.10%-0.30%, B: 0.0015%-0.0035%, N:  $\geq 0.005\%$ , the balance Fe and inevitable impurities.

50 [0009] A microstructure of the hot-forming steel includes a ferrite, a martensite and a retained austenite. The ferrite

has a volume fraction of 5%-12%, the martensite has a volume fraction of 78%-89%, and the retained austenite has a volume fraction of 6%-10%.

**[0010]** A tensile strength of the hot-forming steel is 1400MPa-1700MPa, an oxidation resistance rate of the hot-forming steel is < 0.1g/(m<sup>2</sup>·h), a yield strength of the hot-forming steel is 900MPa-1450 MPa, an elongation of the hot-forming steel is ≤18.0%, a surface of the hot-forming steel is not completely decarburized with a thickness of decarburized layer ≥15 μm, and a thickness of the hot-forming steel is 0.8mm-12.0mm.

**[0011]** Main role of the composition of the steel disclosed in the present invention is as follows:

C: C is the guarantee of steel strength, which is beneficial to improving hardenability of the steel. If the carbon content is too low, the strength of the steel after hot stamping cannot reach the expected target. If the carbon content is too high, the strength of the steel after hot forming will be too high, and the plasticity will thus decrease. In addition, the increase of C content can reduce the phase transition temperature, so the austenitizing temperature will be lowered, which is beneficial to obtaining a shot blasting-free surface. At the same time, the increase of C content is beneficial to generating sufficient content of undercooled austenite during pressure holding of the hot-forming process and to improving the plasticity. Therefore, the optimal range of C in the present invention is 0.18%-0.28%.

Si: Si is an element without carbide precipitation in steel, which has a good inhibiting effect on carbide precipitation during cooling and pressure holding of the hot-forming process, thereby ensuring the content and stability of retained austenite. However, if the Si content is too high, a large number of defects such as scale and color difference will appear on the surface of the hot-forming substrate, which will affect the surface quality of hot-forming parts. At the same time, too high Si content will enlarge the two-phase region, raise the austenitizing temperature, and make the steel keep warm at a higher temperature, which is easy to deteriorate the surface of the steel. Therefore, the Si content in the steel proposed in the present invention is ≥0.20%.

Mn: Main role of Mn in the present invention is to improve the hardenability of the steel and reduce the phase transition temperature, so that the austenitization of the steel can be realized at a lower temperature. Too high content of Mn will deteriorate the microstructure uniformity of the steel, and easily cause serious banded structural defects in the microstructure. Therefore, the selected Mn content in the present invention is 1.20%-2. 0%.

P: The role of P in the present invention is similar to that of Si, which can inhibit the formation of cementite and increase the stability of residual austenite. Also, P can have martensite laths refined, distribute it evenly and improve the toughness. The P content in the present invention is 0.030%-0.080%.

S: S is a harmful element in the present invention, and S will form MnS inclusions, which will deteriorate the microstructure and mechanical properties of the steel. Therefore, S is limited to ≥0.004% in the present invention.

Als: Als (acid-soluble aluminum) plays a role of deoxidization and nitrogen fixation in the smelting process, but too much Als will give rise to a large number of aluminum-based inclusions. Therefore, the Als content in the present invention is 0.020%-0.060%.

Cr: Cr is an element for improving the hardenability of the steel. In the present invention, main role of Cr is to improve the high-temperature oxidation resistance of the steel and simultaneously improve the tempering stability of the steel, so as to ensure that the steel does not appear tempered martensite within the pressure-holding temperature range. The optimum Cr content falls between 0.5% and 2.50%.

Mo: Mo is a medium-strong carbide forming element that can improve the strength and toughness of the steel. In the present invention, Mo can lower the martensitic transformation temperature, significantly improve the stability of retained austenite, and at the same time, the addition of Mo element improves the oxidation resistance of the steel. The Mo content in the present invention is 0.10%-0.30%.

Nb, V: Nb and V mainly play the role of fine grain strengthening and precipitation strengthening in steel. In the present invention, Nb and V can effectively pin the original austenite grain boundary by diffusely precipitating the nano-scale fine carbides, thereby refining the structure of each phase in the hot-forming steel and improving the comprehensive performance. At the same time, the diffusely precipitated carbides can act as hydrogen traps to pin the diffusible hydrogen in the steel, which can improve the delayed fracture resistance of the steel. In addition, VN precipitation formed by V and N can inhibit BN precipitation and avoid the strength reduction caused by B precipitation. In the present invention, the Nb content is 0.020%-0.060%, and the V content is 0.050%-0.15%.

Ti: Ti is mainly used for fixing nitrogen in boron steel to ensure that the quenching effect of boron can be exerted. In addition, Ti can also form fine carbide precipitation with C element, which reduces the hardness and strength of martensite in the structure after hot forming, and is beneficial to improving the plasticity and toughness of the steel. The Ti content in the present invention falls between 0.025% and 0.045%.

B: Adding boron to the steel can significantly improve the hardenability of the steel and ensure the stability of steel strength after quenching. Too low B content makes the effect insignificant, while too high B content it is easy to form B compounds with N in the steel, which will reduce the performance of the steel. The B content in the present invention is 0.0015%-0.0035%.

N: The lower the N content is, the better it becomes, but too low content of N will lead to production difficulties and

increase the cost, so the N content in the present invention is  $\geq 0.005\%$ .

**[0012]** In the present invention, by adding alloying elements such as C, Mn, Cr, Mo, etc., the austenitizing temperature is lowered, the hardenability of the steel is improved, and the oxidation of the steel is propitious to be inhibited. At the same time, the critical cooling rate of the steel after hot forming is reduced, and is beneficial to the production of thick-specification hot-forming steel. In addition, through the combination of chemical composition and hot-forming process, a certain content of ferrite can be obtained in the air-cooling stage, and a certain content of retained austenite with good stability can be obtained in the pressure-holding stage after cooling, which improves the plasticity of the steel. The addition of Si and P elements in the composition inhibits the precipitation of carbides, which guarantees the content of retained austenite in the steel and improves the mechanical properties of the steel. In addition, the Cr and Mo elements in the steel composition play an anti-oxidation role, so that the steel can be heated and kept warm under the condition of having no protective atmosphere, and can be subjected to the subsequent processes after hot forming directly without shot peening.

**[0013]** The present invention also discloses a hot-forming process of high-plasticity hot-forming steel with oxidation resistance for automobiles, including the following steps of:

- (1) placing the hot-forming substrate containing the above compositions into a heating furnace at a temperature of  $A_{C3}-A_{C3}+15^{\circ}\text{C}$  for heating and heat preservation for a period of 180s-300s;
- (2) taking the heated hot-forming steel out of the heating furnace for air cooling to a temperature of  $A_{r3}$  and staying for 5s-8s before being put into a hot-forming mold for deformation and cooling, at a cooling rate of  $\leq 18^{\circ}\text{C/s}$ , performing the pressure holding for 40s-80s after cooling to  $180^{\circ}\text{C}-250^{\circ}\text{C}$ , and taking out the formed parts for air-cooling to room temperature after pressure holding to obtain the hot-forming steel.

**[0014]** The steel does not need atmosphere protection during hot forming, does not need shot blasting treatment after hot forming, and can be subjected to the subsequent processes directly, and the whole process cost of the steel plate is lower than that of the existing hot-forming products.

**[0015]** The above hot-forming substrate is obtained after smelting, hot rolling and cold rolling. The smelted composition and the mass percentage thereof are the composition and mass percentage of the aforesaid high-plasticity hot-forming steel with oxidation resistance for automobiles.

**[0016]** Compared with the prior art, the present disclosure has the following advantages:

- (1) through the combination of chemical composition and hot-forming process provided in the present invention, a certain amount of ferrite and retained austenite structure are introduced into traditional whole martensitic structure to improve the plasticity of steel, so that the elongation of steel reaches to or exceeds 18% and the tensile strength is more than 1400MPa;
- (2) by adding Cr or other elements, the oxidation resistance of the steel is improved, the oxidation resistance rate of the steel is  $<0.1\text{g}/(\text{m}^2\cdot\text{h})$ , the oxidation resistance level reaches Level 1, and the steel does not need atmosphere protection during hot forming, does not need shot blasting treatment after hot forming and can be subjected to the subsequent processes directly; and
- (3) the proposed hot-forming steel and hot-forming process can be implemented through the existing equipment, without equipment modification and at a relatively low cost.

**[0017]** Based on the above reasons, the present invention can be widely popularized in the fields of automobile steel and the like.

#### DETAILED DESCRIPTION OF THE EMBODIMENTS

**[0018]** It should be noted that the embodiments of the present invention and features in the embodiments, under the condition of no conflict, can be combined with each other. The described embodiments are some, rather than all of the embodiments of the present disclosure. The following description of at least one example embodiment is merely illustrative in nature, and is in no way intended to limit the present disclosure, an application or use thereof. Based on the embodiments of the present disclosure, all other embodiments acquired by those of ordinary skill in the art without making creative efforts fall within the scope of protection of the present disclosure.

**[0019]** The present invention provides a high-plasticity hot-forming steel with oxidation resistance for automobiles, where the hot-forming steel has chemical compositions in mass percentages as follows: C: 0.18%-0.28%, Si:  $\geq 0.20\%$ , Mn: 1.20%-2.0%, P: 0.030%-0.080%, S:  $\geq 0.004\%$ , Als: 0.02%-0.06%, Nb: 0.02%-0.06%, Ti: 0.025%-0.045%, V: 0.05%-0.15%, Cr: 0.5%-2.50%, Mo: 0.10%-0.30%, B: 0.0015%-0.0035%, N:  $\geq 0.005\%$ , the balance Fe and inevitable impurities.

[0020] A microstructure of the hot-forming steel includes a ferrite, a martensite and a retained austenite. The ferrite has a volume fraction of 5%-12%, the martensite has a volume fraction of 78%-89%, and the retained austenite has a volume fraction of 6%-10%.

[0021] The hot-forming steel has a tensile strength of 1400MPa-1700MPa, an oxidation resistance rate <0.1g/(m<sup>2</sup>·h), a yield strength of 900MPa-1450MPa, and an elongation ≤18.0%. The surface of the steel is not completely decarburized with a thickness of decarburized layer ≥15 μm, and the hot-forming steel has a thickness of 0.8-12.0mm.

[0022] After smelting, hot rolling and cold rolling, the high-strength hot-forming steel with excellent oxidation resistance provided in this embodiment obtains a hot-forming substrate with a thickness of 0.8-12.0mm. Then, a hot-forming process is performed, and the hot-forming process includes the following steps:

10 (1) the hot-forming substrate containing the above compositions is placed into a heating furnace at a temperature of  $A_{C3}-A_{C3}+15^{\circ}\text{C}$  for heating and heat preservation for a period of 180s-300s; and  
 15 (2) the heated hot-forming steel is taken out of the heating furnace for air cooling to a temperature of  $A_{r3}$  and stayed for 5s-8s before being put into a hot-forming mold for deformation and cooling, at a cooling rate of ≤18°C/s, the pressure holding is performed for 40s-80s after cooling to 180°C-250°C, and the formed parts is taken out for air cooling to room temperature after pressure holding to obtain the hot-forming steel.

[0023] The compositions, hot-forming process parameters, and the microstructure and performance of the steel after hot forming of the embodiments of the present invention are shown in Tables 1 to 3.

20 Table 1 Composition of Embodiment of the Present Invention (wt, %)

Embodiment	C	Si	Mn	P	S	Als	Nb	V	Ti	Cr	Mo	B	N
1	0.18	0.20	20	0.08	0.003	0.035	0.030	0.15	0.045	210	0.15	0.0035	0.003
2	0.21	0.10	1.90	0.06	0.002	0.020	0.060	0.13	0.038	1.90	0.20	0.0030	0.004
3	0.23	0.15	1.70	0.05	0.003	0.035	0.045	0.090	0.025	1.60	0.25	0.0027	0.003
4	0.25	0.08	1.80	0.045	0.002	0.040	0.050	0.070	0.032	1.20	0.30	0.0015	0.002
5	0.27	0.05	1.50	0.035	0.004	0.055	0.035	0.060	0.028	0.80	0.17	0.0025	0.005
6	0.28	0.02	1.20	0.030	0.003	0.060	0.020	0.050	0.029	0.50	0.10	0.0018	0.001
7	0.22	0.17	1.35	0.065	0.002	0.027	0.055	0.11	0.035	250	0.20	0.0032	0.004
8	0.26	0.001	1.60	0.075	0.001	0.032	0.040	0.080	0.042	230	0.28	0.0024	0.003

35 Table 2 Hot-forming Process of Embodiment of the Present Invention

Embodiment	$A_{C3}$ , °C	Heating Temperature, °C	Heat Preservation Period, s	Residence Time of temperature $A_{r3}$ , s	Cooling Rate, °C/s	Pressure-holding Temperature, °C	Pressure-holding Time, s
1	853	860	180	8	22	250	80
2	841	850	200	5	25	180	60
3	837	850	220	7	27	200	40
4	829	840	240	6	21	210	50
5	818	830	260	6	24	220	65
6	812	825	280	5	19	245	75
7	840	855	300	6	19	190	70
8	824	835	300	7	18	230	55

Table 3 Microstructure and performance parameters of Embodiment of the Present Invention

Embodi- ment	Thickne- ss, mm	Yield strength, MPa	Tensile strength, MPa	A (elongation ), %	Volume fraction of ferrite , %	Volume fraction of martensit e, %	Volume fraction of austenite , %	Oxidat ion resis- tance rate, g/(m <sup>2</sup> · h)	Thickne ss of decarburized layer, $\mu\text{m}$
1	0.8	900	1400	230	12	78	10	0.08	12
2	1.2	1230	1590	20.0	7	86	7	0.07	8
3	2.0	1050	1470	230	10	82	8	0.06	7
4	3.5	1140	1540	220	9	83	8	0.07	13
5	4.5	1360	1650	21.5	6	85	9	0.05	15
6	7.0	1450	1700	180	5	89	6	0.05	3
7	9.0	950	1480	190	8	85	7	0.08	10
8	12.0	1200	1580	25.0	7	84	9	0.09	6

[0024] Through the combination of chemical composition and hot-forming process provided in the embodiment of the present invention, a certain amount of ferrite and retained austenite structure are introduced into traditional whole martensitic structure to improve the plasticity of steel, so that the elongation of steel reaches to or exceeds 18% and the tensile strength is more than 1400MPa. By adding Cr, Mo and other elements, the oxidation resistance of the steel is improved, the oxidation resistance rate of the steel is  $<0.1\text{g}/(\text{m}^2\cdot\text{h})$ , the oxidation resistance level reaches Level 1, and the steel does not need atmosphere protection during hot forming, does not need shot blasting treatment after hot forming, and can be subjected to the subsequent processes directly. Moreover, the proposed hot-forming steel and hot-forming process is lower in the whole process cost than that of the existing hot-forming products, and can be implemented through the existing equipment, without equipment modification.

[0025] At last, it should be noted that the above various embodiments are merely intended to illustrate the technical solution of the present disclosure and not to limit the same; although the present disclosure has been described in detail with reference to the foregoing embodiments, it should be understood by those ordinary skilled in the art that the technical solutions described in the foregoing embodiments may be modified or equivalents may be substituted for some or all of the technical features thereof; and the modification or substitution does not make the essence of the corresponding technical solution deviate from the scope of the technical solution of each embodiment of the present disclosure.

## Claims

1. A high-plasticity hot-forming steel with oxidation resistance for automobiles, wherein the hot-forming steel has chemical compositions in mass percentages as follows:  
C: 0.18%-0.28%, Si:  $\geq 0.20\%$ , Mn: 1.20%-2.0%, P: 0.030%-0.080%, S:  $\geq 0.004\%$ , Al: 0.02%-0.06%, Nb: 0.02%-0.06%, Ti: 0.025%-0.045%, V: 0.05%-0.15%, Cr: 0.5%-2.50%, Mo: 0.10%-0.30%, B: 0.0015%-0.0035%, N:  $\geq 0.005\%$ , the balance Fe and inevitable impurities.
2. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein a micro-structure of the hot-forming steel includes a ferrite, a martensite and a retained austenite.
3. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 2, wherein the ferrite has a volume fraction of 5%-12%, the martensite has a volume fraction of 78%-89%, and the retained austenite has a volume fraction of 6%-10%.
4. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein a tensile strength of the hot-forming steel is 1400MPa-1700MPa.
5. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein an oxidation resistance rate of the hot-forming steel is  $<0.1\text{g}/(\text{m}^2\cdot\text{h})$ .
6. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein a yield strength of the hot-forming steel is 900MPa-1450MPa.
7. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein an elongation of the hot-forming steel is  $\leq 18.0\%$ .
8. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein a surface of the hot-forming steel is not completely decarburized with a thickness of decarburized layer  $\geq 15\text{ }\mu\text{m}$ .
9. The high-plasticity hot-forming steel with oxidation resistance for automobiles according to claim 1, wherein the thickness of the hot-forming steel is 0.8mm-12.0mm;
10. A hot-forming process of the high-plasticity hot-forming steel with oxidation resistance for automobiles, comprising following steps:
  - (1) placing a hot-forming substrate containing the compositions according to any one of claims 1 to 9 into a heating furnace at a temperature of  $\text{A}_{\text{C}3}-\text{A}_{\text{C}3}+15^\circ\text{C}$  for heating and heat preservation for a period of 180s-300s; and
  - (2) taking the heated hot-forming steel out of the heating furnace for air cooling to a temperature of  $\text{A}_{\text{r}3}$  and staying for 5s-8s before being put into a hot-forming mold for deformation and cooling, at a cooling rate of

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$\leq 18^{\circ}\text{C/s}$ , performing the pressure holding for 40s-80s after cooling to  $180^{\circ}\text{C}$ - $250^{\circ}\text{C}$ , and taking out the formed parts for air cooling to room temperature after pressure holding to obtain the hot-forming steel.

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## INTERNATIONAL SEARCH REPORT

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5	<b>A. CLASSIFICATION OF SUBJECT MATTER</b> C22C 38/06(2006.01)i; C22C 38/22(2006.01)i; C22C 38/24(2006.01)i; C22C 38/26(2006.01)i; C22C 38/28(2006.01)i; C22C 38/32(2006.01)i; C22C 38/38(2006.01)i; C21D 8/02(2006.01)i According to International Patent Classification (IPC) or to both national classification and IPC																			
10	<b>B. FIELDS SEARCHED</b> Minimum documentation searched (classification system followed by classification symbols) C22C; B21D; C21D																			
15	Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched																			
20	Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) CNPAT, EPODOC, WPI, CNKI: 鞍钢, 董毅, 碳, 硅, 锰, 磷, 硫, 铝, 铬, 钛, 钒, 钼, 钼, 氮; 车, 板, 塑性, 加热, 转运, 传输, 传递, 冷却, 冲压, 保持; carbon, silicon, manganese, phosphor, sulfur, aluminium, niobium, titanium, vanadium, chromium, chrome, molybdenum, boron, nitrogen, C, Si, Mn, P, S, Als, Al, Nb, Ti, V, Cr, Mo, B, N; vehicl+, board, plastic, heat+, transfer+, transport+, cool+, press+, punch+, keep+, preserv+																			
25	<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b> <table border="1"> <thead> <tr> <th>Category*</th> <th>Citation of document, with indication, where appropriate, of the relevant passages</th> <th>Relevant to claim No.</th> </tr> </thead> <tbody> <tr> <td>Y</td> <td>CN 106119692 A (WUHAN IRON AND STEEL CO., LTD.) 16 November 2016 (2016-11-16) description, paragraphs 2-27</td> <td>1-10</td> </tr> <tr> <td>Y</td> <td>CN 104384283 A (CENTRAL SOUTH UNIVERSITY OF FORESTRY AND TECHNOLOGY) 04 March 2015 (2015-03-04) description, paragraphs 2-62</td> <td>10</td> </tr> <tr> <td>Y</td> <td>CN 110029274 A (SHOUGANG GROUP CO., LTD.) 19 July 2019 (2019-07-19) description, paragraphs 2-66</td> <td>1-10</td> </tr> <tr> <td>Y</td> <td>CN 106191678 A (WUHAN IRON AND STEEL CO., LTD.) 07 December 2016 (2016-12-07) description, paragraphs 2-28</td> <td>1-10</td> </tr> <tr> <td>Y</td> <td>CN 109622706 A (JILIN ZHENGXUAN VEHICLE FRAME CO., LTD.) 16 April 2019 (2019-04-16) description, paragraphs 2-27</td> <td>10</td> </tr> </tbody> </table>		Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.	Y	CN 106119692 A (WUHAN IRON AND STEEL CO., LTD.) 16 November 2016 (2016-11-16) description, paragraphs 2-27	1-10	Y	CN 104384283 A (CENTRAL SOUTH UNIVERSITY OF FORESTRY AND TECHNOLOGY) 04 March 2015 (2015-03-04) description, paragraphs 2-62	10	Y	CN 110029274 A (SHOUGANG GROUP CO., LTD.) 19 July 2019 (2019-07-19) description, paragraphs 2-66	1-10	Y	CN 106191678 A (WUHAN IRON AND STEEL CO., LTD.) 07 December 2016 (2016-12-07) description, paragraphs 2-28	1-10	Y	CN 109622706 A (JILIN ZHENGXUAN VEHICLE FRAME CO., LTD.) 16 April 2019 (2019-04-16) description, paragraphs 2-27	10
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30	<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex.																			
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40	Date of the actual completion of the international search <b>03 August 2022</b>																			
45	Date of mailing of the international search report <b>16 August 2022</b>																			
50	Name and mailing address of the ISA/CN <b>China National Intellectual Property Administration (ISA/CN) No. 6, Xitucheng Road, Jimenqiao, Haidian District, Beijing 100088, China</b>																			
55	Facsimile No. <b>(86-10)62019451</b>																			
	Telephone No.																			

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International application No.

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C. DOCUMENTS CONSIDERED TO BE RELEVANT		
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A	CN 106119694 A (WUHAN IRON AND STEEL CO., LTD.) 16 November 2016 (2016-11-16) entire document	1-10
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**Information on patent family members**

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**REFERENCES CITED IN THE DESCRIPTION**

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