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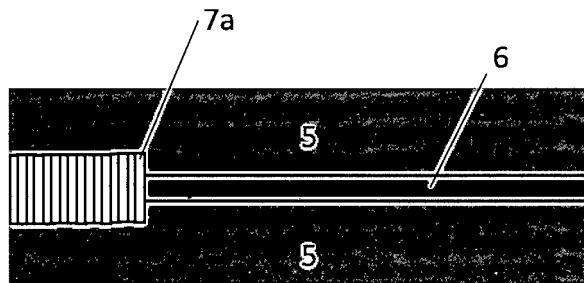
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## (54) POWER CABLE WITH LEAD-FREE METAL WATER BARRIER

(57) The present invention relates to a power cable comprising a cable core (1) comprising at least one conductor (2) with an insulation system (3), and a water barrier system (4) encapsulating said cable core (1) and/or said insulation system (3) of each of the at least one conductor (2), wherein said water barrier system (4) comprises a metal sheath (5) encapsulating the cable core (1) and/or the insulation system (3) of each of the at least one conductor (2), and wherein the metal sheath (5) is

made by wrapping a metal foil around the cable core (1) and/or the insulation system (3) of each of the at least one conductor (2) and then welding together opposing ends of the wrapped metal foil forming a longitudinal welding seam (6), characterised in that the water barrier system further comprises an additional metal layer (7) deposited onto an outer surface of the metal sheath (5) and covering at least said longitudinal welding seam (6).

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## Description

**[0001]** The present invention relates to a power cable having a non-leaded metallic water barrier.

## Background

**[0002]** Electrical high voltage cables contain one or more electrically insulated current carrying conductors at its core section. However, intrusion of humidity or water into the core section may cause electrical breakdown of the insulation system making it vital to keep the current carrying core of high voltage power cables dry. High voltage power cables are therefore typically equipped with a circumferentially arranged water-tight layer sealing off the current carrying parts of the power cable towards ambient moisture/water.

## Prior art

**[0003]** The water-barrier layer typically comprises a layer of a metal. Lead/lead-alloys are commonly applied. However, lead is a high-density material adding significant weight to the cable. The heavy weight induces extra costs in the entire value chain from production, under transport, storage, deployment, and when the cable is discarded after reaching its lifetime. Lead is also a neurotoxic material meeting increasing environmental regulation restrictions. Furthermore, lead has a relatively low fatigue resistance making leaden water barriers less suited for dynamical power cables.

**[0004]** A known alternative to water barriers of lead is the use of high resistance (non-lead) metallic screens laid around the core and/or the insulated conductors of the power cable and joining opposite ends of the wrapped screen by e.g. welding. However, these alternative water barriers still have an unacceptable risk of failure, especially when producing long cables of several kilometres of length, because it is difficult to identify eventual production failures due to the welding process- in the welding seam such as e.g. pinholes in the metal, welding defects, etc.

## Objective of the invention

**[0005]** The main objective of the invention is to provide a high-voltage power cable having a lead-free low weight water-barrier around the cable core and/or the conductor(s) of the power cable.

## Description of the invention

**[0006]** In the scope of the instant invention, the inventors have now shown that, when applying a high resistance (non-leaded) metallic screen covering the core and/or the insulated conductors of the power cable by being wrapped around and joined by welding, the problem with potential production defects along the welding

seam, such as e.g. pinholes in the metal, welding defects etc., may be repaired and/or sealed by utilizing additive manufacturing techniques to deposit a metal layer at least covering identified welding defects in said welding seam, or alternatively covering the entire welded seam of the metallic screen.

**[0007]** According to a first aspect, the invention relates to a power cable comprising:

10 a cable core comprising at least one conductor with an insulation system encapsulating said conductor, and  
15 a water barrier system that encapsulating said cable core and/or encapsulating said insulation system of each of the at least one conductor, wherein  
said water barrier system comprises a metal sheath encapsulating the cable core and/or encapsulating the insulation system of each of the at least one conductor,  
20 and wherein  
the metal sheath is made by wrapping a metal foil around the cable core and/or the insulation system of each of the at least one conductor and then welding together opposing ends of the wrapped metal foil forming a longitudinal welding seam,  
characterised in that  
25 the water barrier system further comprises an additional metal layer deposited onto an outer surface of the metal sheath and covering at least identified welding defects in said longitudinal welding seam.

**[0008]** In the power cable of the invention, the metal sheath preferably encapsulates:

35 - the whole cable core; and/or  
- the insulation system of the at least one conductor, when only one insulation system is present (around an unique conductor or around several conductors);  
40 or each of the insulation systems when several insulation systems are present around several conductors.

**[0009]** The following description is made with reference to the appended illustrative Figures, which refer to a specific example of a power cable as shown in Figure 1 that comprises:

50 a cable core 1 comprising several conductors 2 with an insulation system 3 encapsulating each of said conductor 2, and  
a water barrier system 4 encapsulating each of the conductors 2,

55 wherein :

said water barrier system 4 comprises metal sheaths 5 encapsulating each of the insulation system 3 of

each of the conductors 2;  
 each of the metal sheaths 5 is made by wrapping a metal foil around an insulation system 3 of a conductor 2 and then welding together opposing ends of the wrapped metal foil forming a longitudinal welding seam 6;  
 and  
 the water barrier system further comprises a metal layer 7 deposited onto an outer surface of each of the metal sheath 5 and covering at least identified welding defects in said longitudinal welding seams 6.

**[0010]** The term "longitudinal" as used herein refers to the main direction of the power cable. Namely, a longitudinal direction is parallel with or co-axial with the longitudinal centre axis of the power cable.

**[0011]** The term "metal sheath" as used herein, refers to the primary water-impenetrable layer of the water-barrier system of the invention. The metal sheath is typically formed by folding and welding together opposite ends of a metal foil such that the resulting metal sheath is laid around to encompass and encapsulate the core and/or the insulated conductors of the power cable. The invention is not tied to use of any specific metal foil to make the metal sheath, except that it should not be made of Pb or a Pb-alloy. The metal foil may be made of any non-lead metal/metal alloy having any thickness known to the skilled person to be suited for use as a metallic screen/water-barrier in power cables. In one example embodiment, the metal foil is either an Al/Al-alloy such as for example an AA1xxx series, an AA5xxx series or an AA6xxx series alloy according to the Aluminum Association Standard, or a Cu/Cu-alloy such as for example pure Cu, a CuNi-alloy or a CuNiSi-alloy, or a Fe/Fe-alloy, such for example stainless alloy SS316 or S32750. The thickness of the metal sheath may in an example embodiment be in one of the following ranges; from 10 to 1000  $\mu\text{m}$ , preferably from 20 to 750  $\mu\text{m}$ , more preferably from 30 to 500  $\mu\text{m}$ , more preferably from 40 to 100  $\mu\text{m}$ , and most preferably from 50 to 75  $\mu\text{m}$ .

**[0012]** The specific metal layer deposited according to the invention onto an outer surface of the metal sheath (herein-above referred as the layer 7) should at least cover identified defects in the welding seam 6. Namely, this metal layer may cover one or more local areas on the metal sheath 5 and/or the welding seam 6. Alternatively, in one embodiment, the metal foil constituting the metal sheath may be shaped into a substantially rectangular metallic layer having a longitudinal centre axis of length  $l_1$  and a width  $w_1$ . The length  $l_1$  is preferably equal to the length of the power cable, while the width  $w_1$  needs to be at least equal to the outer perimeter,  $p$ , of the cable core 1 or the electrically insulated conductor 2 at which the metal heath 5 is to be applied in order to enable encapsulate said cable core 1 or the electrically insulated 3 conductor 2. Alternatively, the width  $w_1$ , may be larger than the outer perimeter,  $p$ , of the cable core 1 or the electrically insulated 3 conductor 2, in which case the

wrapped/folded metal foil 5a will encapsulate the cable core 1 or the electrically insulated 3 conductor 2 with some overlap.

**[0013]** The term "opposing ends" as used herein, refers to the longitudinal sides of the metal foil (5a in figure 2) which will be facing each other with or without some overlap when the metal foil 5a it is folded/wrapped around the cable core 1 and/or the insulation system 3 of each of the at least one conductor 2 at which the metal sheath 5 is to be formed.

**[0014]** According to the invention, the water-barrier system includes an additional metal layer laid onto and covering at least the welding seam formed when joining the wrapped/foled metal foil to make the metallic screen encompassing and encapsulating the core and/or the insulated conductors of the power cable. In other words, the additional meta layer (e.g. the metal layer 7 described with reference to the Figures) acts as a reinforcing additional metal layer covering and sealing-off the welding seam which may contain pin holes or other welding defects due to unintentional manufacturing inaccuracies when forming the metal sheath.

**[0015]** The invention is not tied to use of any specific metal in the additional metal layer, except that it should not be made of Pb or a Pb-alloy. Any non-lead metal/metal alloy at any thickness known to the skilled person to be suited for use as metallic screen/water-barrier layer may be applied as the additional metal layer. In one example embodiment, the additional metal layer is either an Al/Al-alloy such as for example an AA1xxx series, an AA5xxx series or an AA6xxx series alloy according to the Aluminium Association Standard, or a Cu/Cu-alloy such as for example pure Cu, a CuNi-alloy or a CuNiSi-alloy, Ti, a Ti-alloy, or a Fe/Fe-alloy, such for example stainless alloy SS316 or S32750. The thickness of the additional metal layer may in an example embodiment be in one of the following ranges; from 2 to 500  $\mu\text{m}$ , preferably from 3 to 300  $\mu\text{m}$ , more preferably from 4 to 150  $\mu\text{m}$ , more preferably from 5 to 125  $\mu\text{m}$ , more preferably from 10 to 100  $\mu\text{m}$ , more preferably from 20 to 75  $\mu\text{m}$ , and most preferably from 30 to 50  $\mu\text{m}$ .

**[0016]** In one embodiment, the metal layer 7 may advantageously have a substantially rectangular shape with a longitudinal centre axis of length  $l_2$  and a width  $w_2$ . The length  $l_1$  is preferably equal to the length of the welding seam to be covered, while the width  $w_2$  is preferably in the range from 0.1 to 5 cm, preferably from 0.25 to 4 cm, more preferably from 0.5 to 3 cm, more preferably from 0.75 to 2.5 cm, more preferably from 1 to 2 cm, and most preferably from 1.25 to 1.5 cm. By depositing the additional metal layer such that its longitudinal centre axis becomes substantially co-centric with the longitudinal welding seam of the metallic sheath, the additional metal layer will cover both the welding seam and some of the adjacent outer surface area of the underlying metal sheath. Alternatively, the substantially rectangular additional metallic layer having a longitudinal centre axis of length  $l_2$  and a width  $w_2$ . In one embodiment, the sub-

stantially rectangularly shaped additional metal layer 7 may have a somewhat concave cross-section, i.e. being thickest at its longitudinal centre axis and gradually thinner towards its longitudinal side-edges to better conform with the curvature of the metal sheath 5. In the latter case, the above given ranges for thickness of the additional metal layer 7 refers to its thickness at its longitudinal centre axis.

**[0017]** The term "electric conductor" as used herein refers to the current carrying inner core of the power cable. The invention may apply any known or conceivable current carrying inner core known to the skilled person being suited to carry/transport electric current, including but not limited to a single strand of an electrically conductive material, a plurality of strands of an electrically conductive material arranged in a bunt, etc. In the latter case of applying an electric conductor comprising a bunt of strands, the space in-between the strands of electrically conductive material may be occupied by a semiconducting filler compound. The electric conductor may in further example embodiments also comprise a semiconducting conductor screen arranged radially around and encompassing the single strand or bunt of strands. Examples of materials being suited as the current carrying strand(s) of the electric conductor of power cables include, but are not limited to; Cu, Cu-alloy, Al, or an Al-alloy. In practice, the electrically conductive material being applied as conductor(s) in power cables may advantageously have an electric conductivity of at least  $4.8 \cdot 10^6$  S/m at 20 °C, preferably of at least  $1.0 \cdot 10^7$  S/m at 20 °C and most preferably of at least  $3.6 \cdot 10^7$  S/m at 20 °C.

**[0018]** Each conductor of power cables should be individually electrically insulated. This is typically obtained by covering the surface of the conductor by a layer of an electric insulating material, i.e. to make the conductor being sheathed in the electrically insulating material. The invention may apply any known or conceivable material, including dielectric materials, known to the skilled person as being suited as insulation of the current carrying conductor(s) of power cables. In practice the electric conductivity of the material being applied as insulation may advantageously have an electric conductivity of less than  $10^{-14}$  S/m at 20 °C, preferably less than  $10^{-16}$  S/m at 20 °C, preferably less than  $10^{-18}$  S/m at 20 °C, and most preferably less than  $10^{-20}$  S/m at 20 °C. Examples of materials suited for being applied to form the electric insulation of the conductor(s) include, but are not limited to; ethylene propylene rubber (EPR), ethylene propylene diene monomer (EDPM), rubber, polyethylene (EP), polypropylene (PP), polyurethane (PUR), cross-linked polyethylene (XLPE), and mass-impregnated (MI) paper. The insulation effect of the insulating material depends on the thickness of the layer of insulating material. In general, the higher voltage of the electric current in the conductor, the more insulation is needed. The determination of amount of insulating material required to electrically insulate a conductor is within the ordinary skills of the person skilled in the art.

**[0019]** The term "cable core" as used herein refers to the interior part of power cables containing the electrically insulated current carrying conductor(s) of the power cable. If more than one cable core is present, the cable core usually also contains one or more spacers arranged and adapted to provide the cable core with a circular cross-section. The cable core may also further comprise signal cables, optic fibres, and/or any other component known to the skilled person suited for being located in a cable core. Thus, the term "a water barrier system encapsulating said cable core" as used herein means that the water barrier system is laid onto and around the outer surface of the cable core to form a watertight enclosure of the interior of the cable core preventing water and/or moisture from penetrating into the cable core.

**[0020]** In a second aspect, the invention relates to a method of forming a water barrier system (identified by reference 4 in the Figures) on a cable core (1) and/or an electrically insulated conductor (2 with an insulation system 3) of a power cable, wherein the method comprises: forming a metal sheath (5) encapsulating the cable core (1) and/or the insulation system (3) of each of the at least one conductor (2) by:

25 folding/wrapping a metal foil around the cable core (1) and/or the insulation system (3) of each of the at least one conductor (2), and

30 welding together opposite ends of the folded/wrapped metal foil forming a longitudinal welding seam (6),

characterised in that the method further discloses: depositing a metal layer (7) onto an outer surface of the metal sheath 5 which at least covers the longitudinal welding seam (6).

**[0021]** The invention according to the first and/or second aspect is not tied to use of any specific method of forming/depositing the metal layer (referred as the layer 7 in the Figures) onto the metal sheath 5 as long as the additional metal layer 7 is made to at least covering the longitudinal welding seam 6 and to make a water impermeable reinforcement/seal of the longitudinal welding seam 6. A well suited and preferred method is making/depositing the additional metal layer 7 by additive manufacturing (AM), which also may be labelled as 3D-printing in the literature. AM works by a computer controlled process that builds the three-dimensional objects onto a substrate by successively depositing strips or layers of material until the object is formed. In this manner, a dense and compact (continuous) sheet or layer of the additional metal is laid onto and firmly attached to the underlying metal sheath 5 and welding seam 6 which effectively closes and seals-off eventual welding defects in the longitudinal welding seam 6.

**[0022]** A particularly suited and preferred additive manufacturing technology is cold spray additive manufacturing, which may build the additional metal layer by blowing a powder of the additional metal by a high-ve-

lacity compressed gas stream onto the deposition area of the outer surface of the metal sheath 5 and/or the welding seam 6 causing the powder upon impingement on the target surface to deform and bond together to a layer of the additional metal. An advantage of cold spraying is that the physical and chemical properties of the underlying substrate is mainly unaffected due to a relatively limited heating since no melting is involved. The formed additional metal layer 7 obtains also relatively strong mechanical properties by attaining a typical cold-worked microstructure.

**[0023]** Alternatively, another particularly suited and preferred additive manufacturing technology is direct energy deposition additive manufacturing in which an object is built by successive deposition of strips of a material being melted (and subsequently solidified) upon deposition by a thermal energy source. The invention may apply any known direct energy deposition, but an especially preferred method of forming the additional metal layer 7 is laser powder deposition in which deposition is achieved by combining a focused spray of a powder of the additional metal to the point or region of interest onto the outer surface of the metal sheath 5 and/or the welding seam 6 and melting the powder of the additional metal by a high power laser. This technique is a relatively common technique within additive manufacturing known and mastered by the person skilled in the. The technique is particularly suitable for forming the additional metal layer of the present invention as the powder can readily penetrate and cover potential holes in the underlying metal sheath. The powder may constitute an alloy or alloy constituents that mix when re-melted. Relevant powder materials include the same metals and alloys as listed above for the additional metal layer.

**[0024]** The principle of laser powder deposition is illustrated schematically in figure 3 (the figure is a facsimile figure 1 of [ref 1]). A nozzle directs a gas flow containing entrained particles of the material to be deposited onto a deposition area of a substrate or workpiece under construction where the particles are heated and melted by a laser beam to form a melt pool on the substrate/workpiece. By moving the nozzle and substrate/workpiece relative to each other, typically in a straight line, the deposition area/melt pool moves correspondingly on the substrate/workpiece and causes the particulate material to be continuously deposited and melted in a corresponding pattern. The part of the molten pool which is left behind by the moving nozzle and laser beam will rapidly solidify. If the nozzle moves in a straight, the deposited material will form a continuous stripe onto the substrate/- workpiece. A plate or layer of material may be formed by depositing a number of parallel stripes adjacent to each other. When applying laser powder deposition to form the additional metal layer according to the invention, the substrate may advantageously be the metal sheath 5 including the longitudinal welding seam 6.

**[0025]** In one embodiment the method according to the invention may further comprise depositing an adhesive

layer, e.g. a polyethylene, onto the sheath metal 5 and the deposited additional metal layer 7 and then depositing a polymeric sheath onto the adhesive layer.

**[0026]** The water barrier system according to the first and/or the additional aspect of the invention, may be applied to encapsulate the cable core, alternatively encapsulating the cable core and each of the at least one electrically insulated conductors, or alternatively (only) encapsulating each of the at least one electrically insulated conductors of the power cable. Figure 1 is a cut-view drawing schematically illustrating a typical construction of a three-phase power cable. As seen on the figure, each electric conductor 2 typically comprises a plurality of strands bundled together. Each bundle of strands is radially encapsulated by an electric insulation system 3. In this example embodiment, the water barrier system 4 (shown as a single layer for the sake of clarity in the figure) is laid onto the electric insulation system 3 of each conductor 2. The three electrically insulated and water intrusion protected conductors 2 are bundled together with three spacers 24 as shown on the figure to obtain a circular cross-section. I.e. the spacers 24 are adapted to fill the space between adjacent electrically insulated and water intrusion protected conductors 2 and provide an overall cylindrical geometry of the cable. Said arrangement of three conductors 2 (with insulation 3 and water protection 4) and three spacers 24 constitutes the cable core 1 as indicated by the stapled parenthesis. Typically, there will be a semiconductive layer 21 onto the cable core to conduct capacitive charges induced in the cable, an armoring 22 and an outer polymer sheathing 23. In the case of applying the water barrier system 4 according to the invention on the cable core 1, the water barrier system 4 would in this example embodiment typically be laid onto the semiconductive layer 21.

**[0027]** An example embodiment of the process for manufacturing a water system 4 according to the invention is illustrated schematically in figures 2a) to 2d).

**[0028]** Figure 2a) is a drawing, as seen from above, illustrating a metal 5a foil, having a width  $w_1$  and a length  $l_1$ , being prepared to be folded around the insulated conductor and form the metal sheath 5 encompassing an electrically insulated 3 conductor 2. The length  $l_1$  equals the longitudinal length of the electrically insulated 3 conductor 2, while the width  $w_1$  equals the outer perimeter (the circumference) of the insulated 3 conductor 2 to enable the opposite ends in the longitudinal direction to contact each other and be welded together when the metal foil 5a is folded around the insulated 3 core 2.

**[0029]** Figure 2b) is a cut-view drawing as seen from the side in and in the direction of the longitudinal centre axis of the conductor illustrated by the stapled line marked A-A' in figure 2a). The figure is a drawing schematically illustrating the process of forming the metal sheath 5 around an electrically insulated 3 conductor 2 just before the folding of the metal foil 5a is fully folded around the insulated 3 conductor 2 such that the opposing longitudinal ends 9, 10 contact each other and joining

by welding (not shown on the figures). The resulting longitudinal welding seam 6 is illustrated schematically in figure 2c). As seen from figure 2b), this embodiment of the electrically insulated conductor comprises a swelling tape 8 laid onto the insulation system 3 of the conductor 2.

**[0030]** Figure 2d) illustrates schematically an example embodiment of how the additional metal layer 7 may be formed by additive manufacturing by successively depositing stripes of metal material onto outer surface of the metal sheath 5 including the longitudinal welding seam 6.

**[0031]** In one embodiment the method according to the invention may further comprise a drawing, rolling or corrugation process that reduces the overall diameter of the sheath metal 5 with the deposited additional metal layer 7.

### List of figures

**[0032]**

Figure 1 is a cut view drawing illustrating the typical construction of a three-phase power cable.

Figures 2a) to 2d) are drawings schematically illustrating an example embodiment of forming a water-barrier system according to the invention on a conductor.

Figure 3 is a facsimile of figure 1 of [ref 1] illustrating a typical embodiment of laser powder deposition.

Figures 4a) to 4c) are photographs of a verification experiment on two CuNi plates joined by welding followed by deposition of Cu as an additional metal layer according to the invention.

Figures 5a) to 5c) are photographs of a verification experiment where two plates of a CuNi25 alloy were welded together and received a copper layer made by laser powder deposition.

### Example embodiment

**[0033]** The invention is described in further detail by way of example embodiments of forming a water-barrier system according to the invention using laser powder deposition of a Cu-layer onto a longitudinal welding seam joining two CuNi-plates welded together at opposite ends.

**[0034]** The first verification test is shown in the photograph in figure 4a), which shows a section of the front side of the joined CuNi-plates. The longitudinal welding seam 6 of the joint is clearly visible on the photograph. Two defects on the form of a drilled hole 12 of 1 mm diameter were deliberately introduced in the welding seam 6 and marked with the white arrows.

**[0035]** The photograph shown in figure 4b) shows the

front side of the joined CuNi-plates after deposition of the additional metal layer 7. The drilled holes are no longer visible. The defects have been completely covered by the deposited Cu-layer constituting the additional metal layer.

**[0036]** The photograph shown in figure 4c) shows the back-side of the joined CuNi-plates after deposition of the additional metal layer 7 and confirms the result shown in figure 4b).

**[0037]** A further verification of the invention is shown in figures 5a) to 5c) which present a photograph of an additional metal layer 7 according to the invention of copper deposited on top of a laser welded seam 6 joining two metal strips of a CuNi25 alloy.

**[0038]** Before the deposition of the additional metal layer 7, there was intentionally made holes in the welding seam 6 ranging from 0.5 to 5 mm in diameter. The holes were thereafter plugged by depositing a layer of Cu onto the welded seam including the holes by laser powder deposition using a precursor powder of metallic copper. The holes were covered both on a spot basis and the full length - i.e., also areas of the weld where no holes were present. The laser powder deposition applied a Trumpf trudisk machine with 1030 nm laser wavelength and 80-3000 W. The deposition speed was in the range of 3- 10 m/min.

**[0039]** As seen on the photographs of figures 5a) to 5c), the holes in the welded seams are effectively plugged. In this test, the additional metal layer 7 was only deposited on a section of the welded seam 6 since the test was aimed at proof of concept of the present invention.

**[0040]** Furthermore, it is assumed that a power material consisting of Cu-Ni alloy would improve the situation due to improved laser absorption.

### Reference

**[0041]**

1. Lim et al. (2021), "Selection of effective manufacturing conditions for directed energy deposition process using machine learning methods", Scientific Reports volume 11, Article number: 24169. Retrievable on: <https://www.nature.com/articles/s41598-021-03622-z>

### Claims

**50** 1. A power cable comprising:

**55** a cable core (1) comprising at least one conductor (2) with an insulation system (3) encapsulating said conductor (2), and  
a water barrier system (4) encapsulating said cable core (1) and/or encapsulating said insulation system (3) of each of the at least one con-

ductor (2), wherein  
said water barrier system (4) comprises a metal  
sheath (5) encapsulating the cable core (1)  
and/or encapsulating the insulation system (3)  
of each of the at least one conductor (2),  
5 and wherein

the metal sheath (5) is made by wrapping a metal  
foil around the cable core (1) and/or the insula-  
tion system (3) of each of the at least one con-  
ductor (2) and then welding together opposing  
10 ends of the wrapped metal foil forming a longi-  
tudinal welding seam (6),

**characterised in that**

the water barrier system further comprises an  
15 additional metal layer (7) deposited onto an outer  
surface of the metal sheath (5) and covering  
at least identified welding defects in said longi-  
tudinal welding seam (6).

2. The power cable according to claim 1, wherein the  
metal foil constituting the metal sheath (5) is made  
of either:

aluminium,  
25 an aluminium alloy of the AA1xxx series, AA5xxx  
series or the AA6xxx series according to the Alu-  
minium Association Standard,  
copper,  
a copper-alloy,  
a CuNi-alloy,  
a CuNiSi-alloy,  
iron,  
a Fe-alloy,  
stainless steel alloy SS316,  
30 or  
stainless steel alloy S32750.

3. The power cable according to claim 1 or 2, wherein  
the thickness of the metal foil constituting the metal  
sheath (5) is in one of the following ranges; from 10  
to 1000  $\mu\text{m}$ , preferably from 20 to 750  $\mu\text{m}$ , more  
preferably from 30 to 500  $\mu\text{m}$ , more preferably from  
40 to 100  $\mu\text{m}$ , and most preferably from 50 to 75  $\mu\text{m}$ .

4. The power cable according to any preceding claim,  
wherein the additional metal layer (7) is made of ei-  
ther:

aluminium,  
an aluminium alloy of the AA1xxx series, AA5xxx  
series or the AA6xxx series,  
copper,  
a copper-alloy,  
a CuNi-alloy,  
a CuNiSi-alloy,  
iron,  
a Fe-alloy,  
55 Ti,

a Ti-alloy,  
stainless steel alloy SS316,  
or  
stainless steel alloy S32750.

5. The power cable according to claim 4, wherein the  
thickness of the additional metal layer (7) is in one  
of the following ranges; from 2 to 500  $\mu\text{m}$ , preferably  
from 3 to 300  $\mu\text{m}$ , more preferably from 4 to 150  $\mu\text{m}$ ,  
more preferably from 5 to 125  $\mu\text{m}$ , more preferably  
from 10 to 100  $\mu\text{m}$ , more preferably from 20 to 75  
 $\mu\text{m}$ , and most preferably from 30 to 50  $\mu\text{m}$ .

6. The power cable according to any preceding claim,  
wherein the additional metal layer (7) is made to cov-  
er the entire welding seam (6) of the metal sheath  
(5) and is shaped into a substantially rectangular me-  
tallic layer having a longitudinal centre axis of length  
 $l_2$  and a width  $w_2$ , where the length  $l_2$  is equal to the  
length of the welding seam (6), and the width  $w_2$  is  
in the range from 0.1 to 5 cm, preferably from 0.25  
to 4 cm, more preferably from 0.5 to 3 cm, more  
preferably from 0.75 to 2.5 cm, more preferably from  
1 to 2 cm, and most preferably from 1.25 to 1.5 cm.

7. The power cable according to claim 6, wherein the  
additional metal layer (7) is laid onto the outer surface  
of the metal sheath (5) such that its longitudinal cen-  
tre axis is co-centric with the longitudinal welding  
seam (6) of the metallic sheath (5).

8. The power cable according to claim 7, wherein the  
additional metal layer (7) have a somewhat concave  
cross-section by being thickest at a longitudinal cen-  
tre axis and gradually thinner towards its longitudinal  
side-edges.

9. The power cable according to any preceding claim,  
wherein the additional metal layer (7) is deposited  
by additive manufacturing.

10. The power cable according to claim 9, wherein the  
additional metal layer (7) is deposited by cold spray  
additive manufacturing.

11. The power cable according to claim 9, wherein the  
additional metal layer (7) is deposited by direct en-  
ergy deposition additive manufacturing.

12. The power cable according to claim 11, wherein the  
direct energy deposition additive manufacturing is  
laser powder deposition.

13. A method of forming a water barrier system (4) on a  
cable core (1) and/or an electrically insulated (3) con-  
ductor (2) of a power cable, wherein the method com-  
prises:  
forming a metal sheath (5) encapsulating the cable

core (1) and/or the insulation system (3) of each of the at least one conductor (2) by:

folding/wrapping a metal foil around the cable core (1) and/or the insulation system (3) of each of the at least one conductor (2), and welding together opposite ends of the folded/wrapped metal foil forming a longitudinal welding seam (6),

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**characterised in that** the method further discloses: depositing an additional metal layer (7) onto an outer surface of the metal sheath (5) which at least covers the longitudinal welding seam (6).

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14. The method according to claim 13, wherein the additional metal layer (7) is deposited onto the metal sheath (5) and/or the longitudinal welding seam (6) by additive manufacturing.

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15. The method according to claim 13 or 14, wherein the additional metal layer (7) is deposited onto the metal sheath (5) and/or the longitudinal welding seam (6) by cold spray additive manufacturing.

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16. The method according to any of claims 13 to 15, wherein the additional metal layer (7) is deposited onto the metal sheath (5) and/or the longitudinal welding seam (6) by direct energy deposition additive manufacturing.

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17. The method according to claim 16, wherein the direct energy deposition additive manufacturing is laser powder deposition.

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18. The method according to any of claims 13 to 17, wherein the method further comprises a drawing, rolling or corrugation process that reduces the overall diameter of the sheath metal (5) with the deposited additional metal layer (7).

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19. The method according to any of claims 13 to 18, wherein the method further comprises depositing a polymeric sheath into the sheath metal (5) and the deposited additional metal layer (7).

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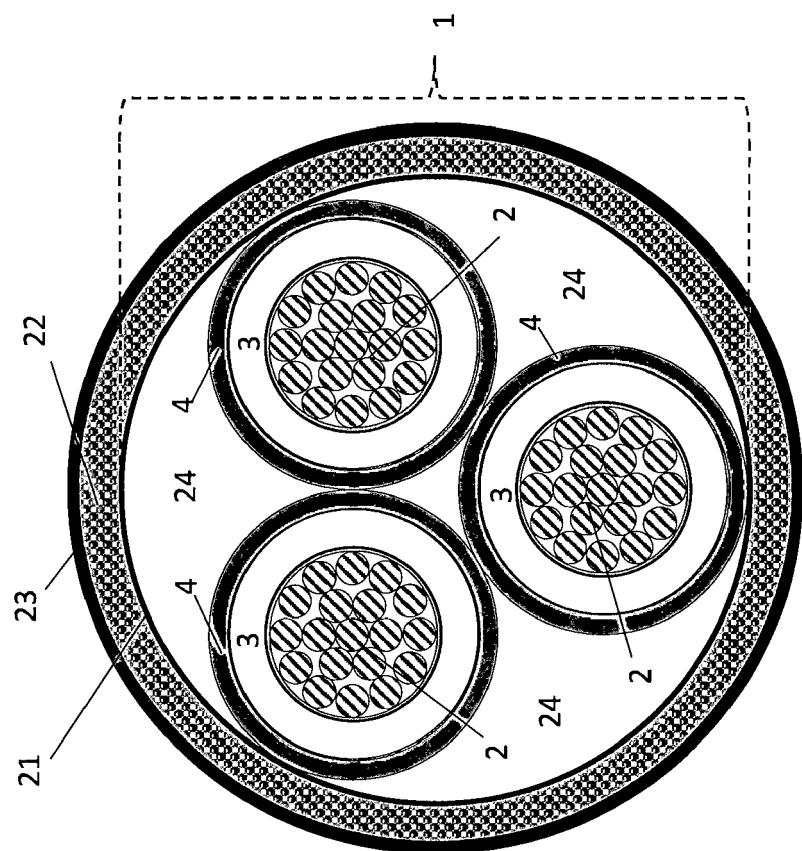


Figure 1

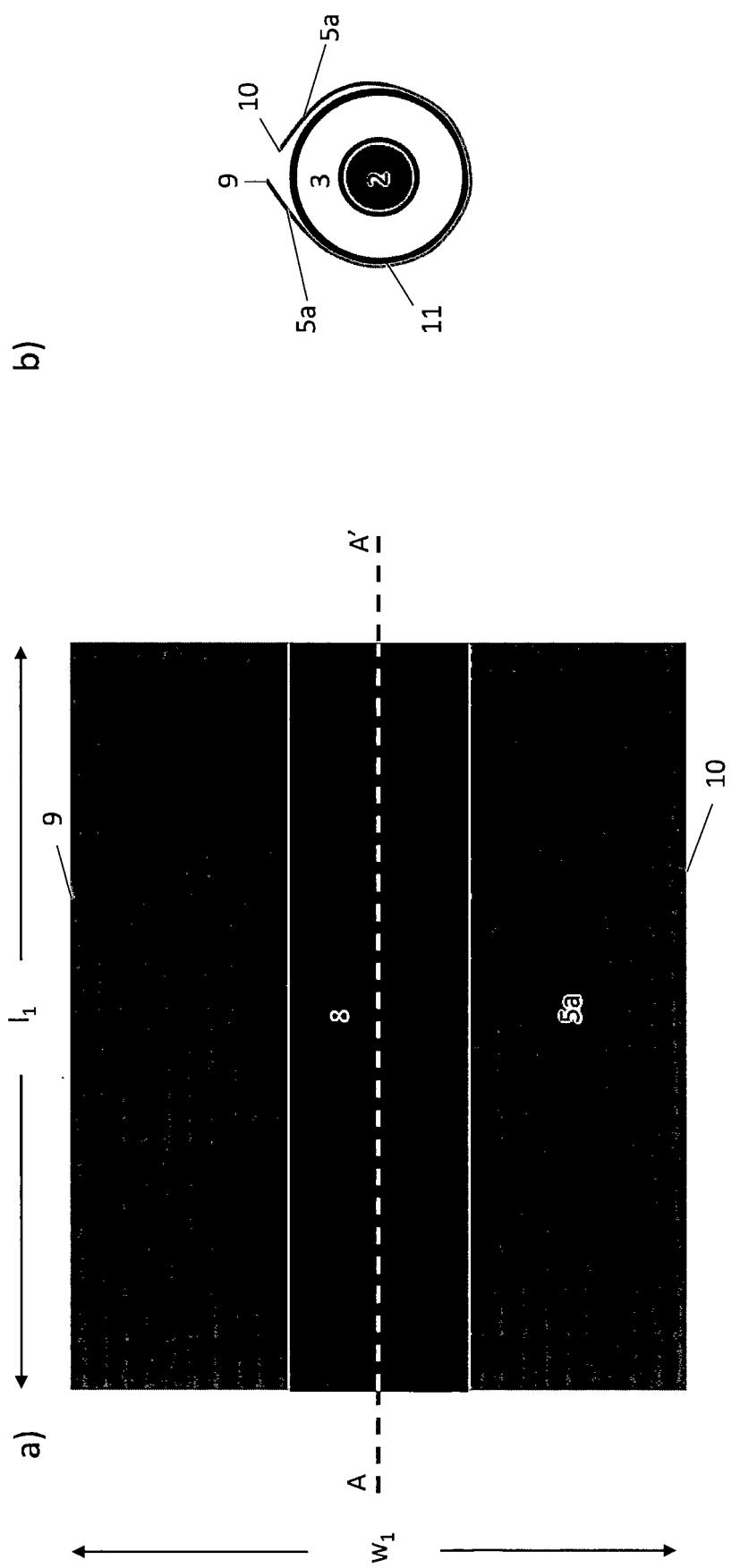


Figure 2

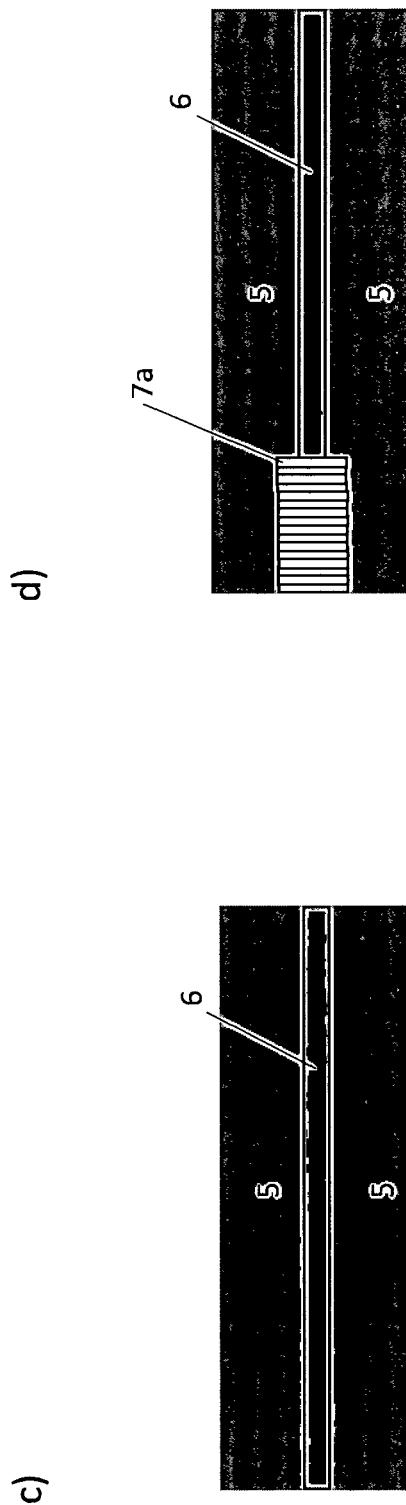


Figure 2

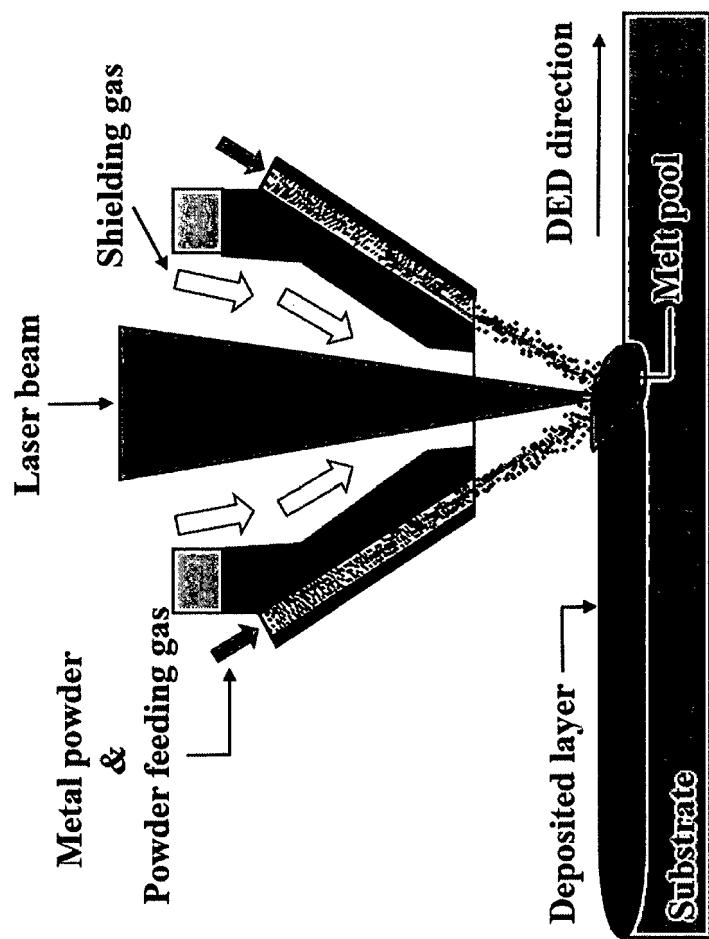


Figure 3 facsimile of fig. 1 of [ref 1]

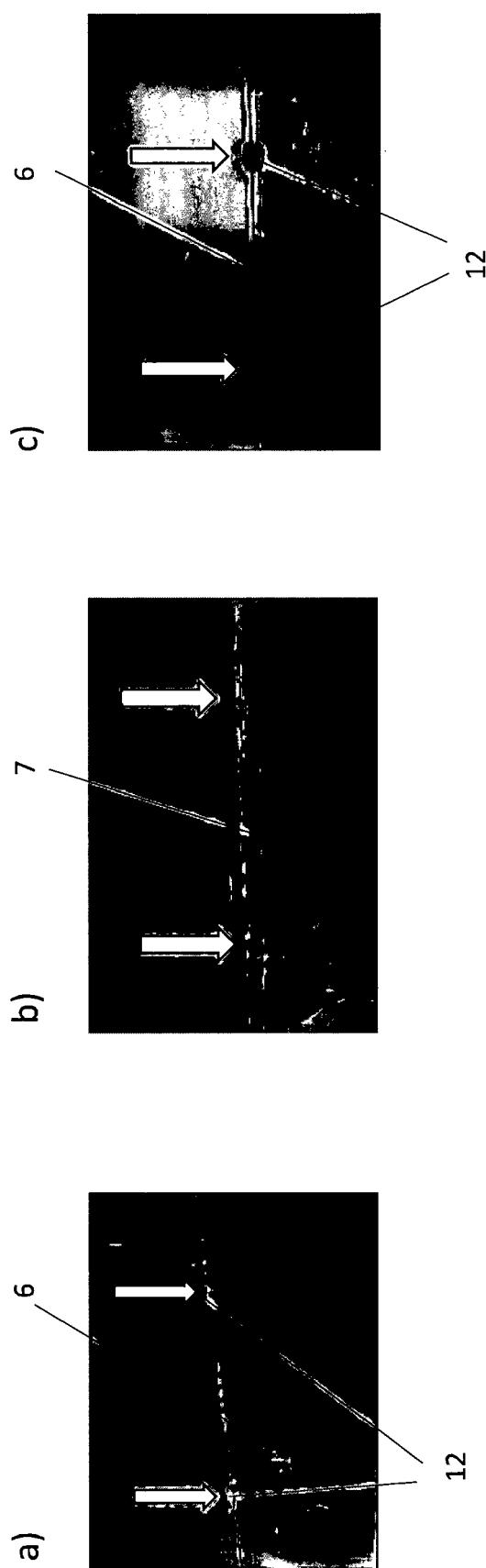


Figure 4

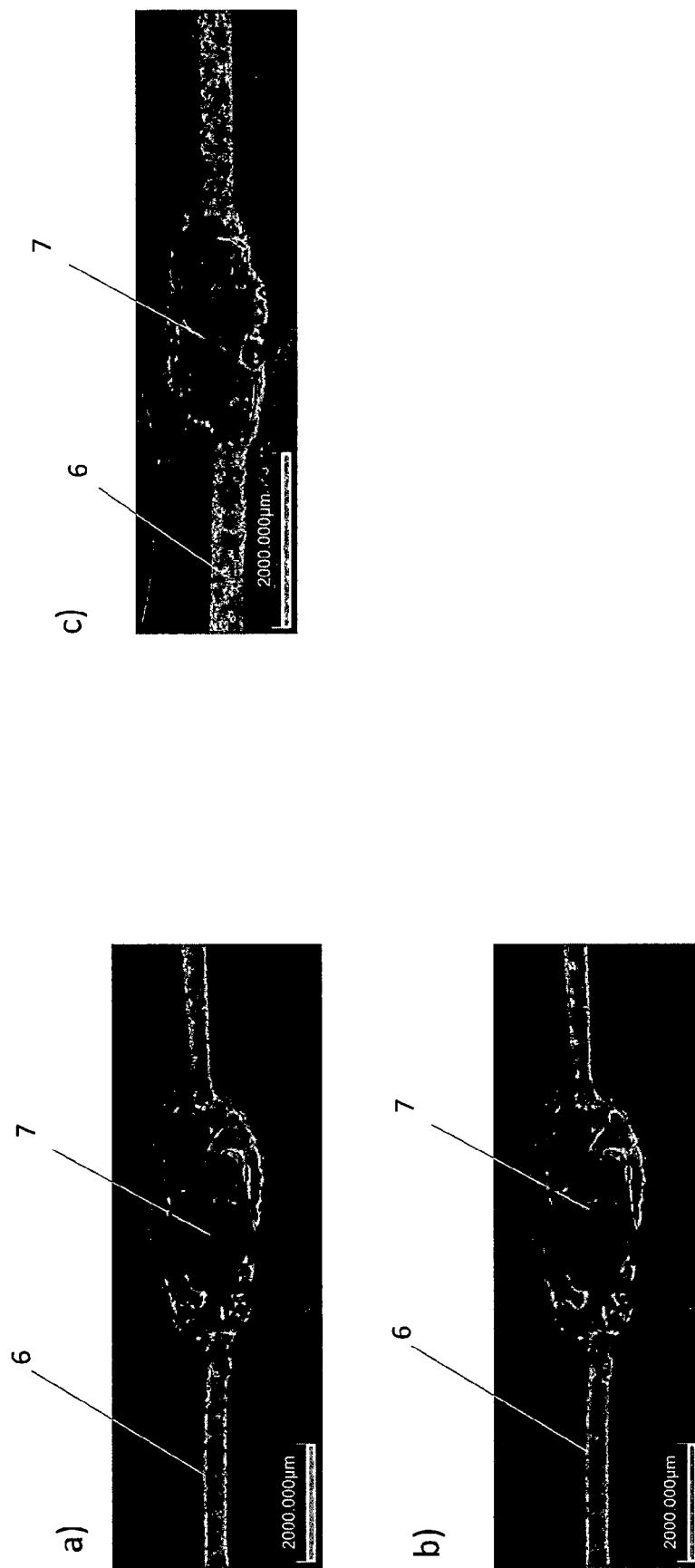


Figure 5



## EUROPEAN SEARCH REPORT

Application Number

EP 23 31 5176

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Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (IPC)
10	<p><b>X</b> EP 3 014 632 A1 (PRYSMIAN SPA [IT]) 4 May 2016 (2016-05-04) * paragraphs [0025], [0034], [0040], [0041], [0043], [0028]; figures 3d, 1a *</p> <p>-----</p> <p><b>X</b> DE 33 12 551 A1 (SIEMENS AG [DE]) 11 October 1984 (1984-10-11) * figure 1 *</p> <p>-----</p> <p><b>Y</b> US 2021/210253 A1 (CRISTOFANI FABRIZIO [IT] ET AL) 8 July 2021 (2021-07-08) * figures 1, 2 *</p> <p>-----</p> <p><b>A</b> US 2009/068495 A1 (DEMBOWSKI THADDEUS J [US] ET AL) 12 March 2009 (2009-03-12) * figure 4 *</p> <p>-----</p>	<p>1-17, 19</p> <p>18</p> <p>1, 2, 13</p> <p>18</p> <p>1-19</p>	<p>INV.</p> <p>H01B7/282</p> <p>H01B7/20</p> <p>H01B13/26</p>
15			
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30			<p>TECHNICAL FIELDS SEARCHED (IPC)</p> <p>H01B</p> <p>H05B</p>
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50	<p>1</p> <p>The present search report has been drawn up for all claims</p>		
55	<p>1</p> <p>Place of search</p> <p>The Hague</p> <p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone</p> <p>Y : particularly relevant if combined with another document of the same category</p> <p>A : technological background</p> <p>O : non-written disclosure</p> <p>P : intermediate document</p>	<p>Date of completion of the search</p> <p>10 October 2023</p> <p>T : theory or principle underlying the invention</p> <p>E : earlier patent document, but published on, or after the filing date</p> <p>D : document cited in the application</p> <p>L : document cited for other reasons</p> <p>&amp; : member of the same patent family, corresponding document</p>	<p>Examiner</p> <p>Alberti, Michele</p>

ANNEX TO THE EUROPEAN SEARCH REPORT  
ON EUROPEAN PATENT APPLICATION NO.

EP 23 31 5176

5 This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

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